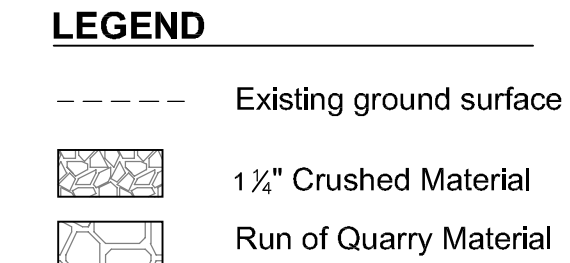


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Scale in Metres (Horizontal) Scale in Metres (Vertical)

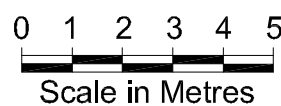
4X VERTICAL EXAGGERATION



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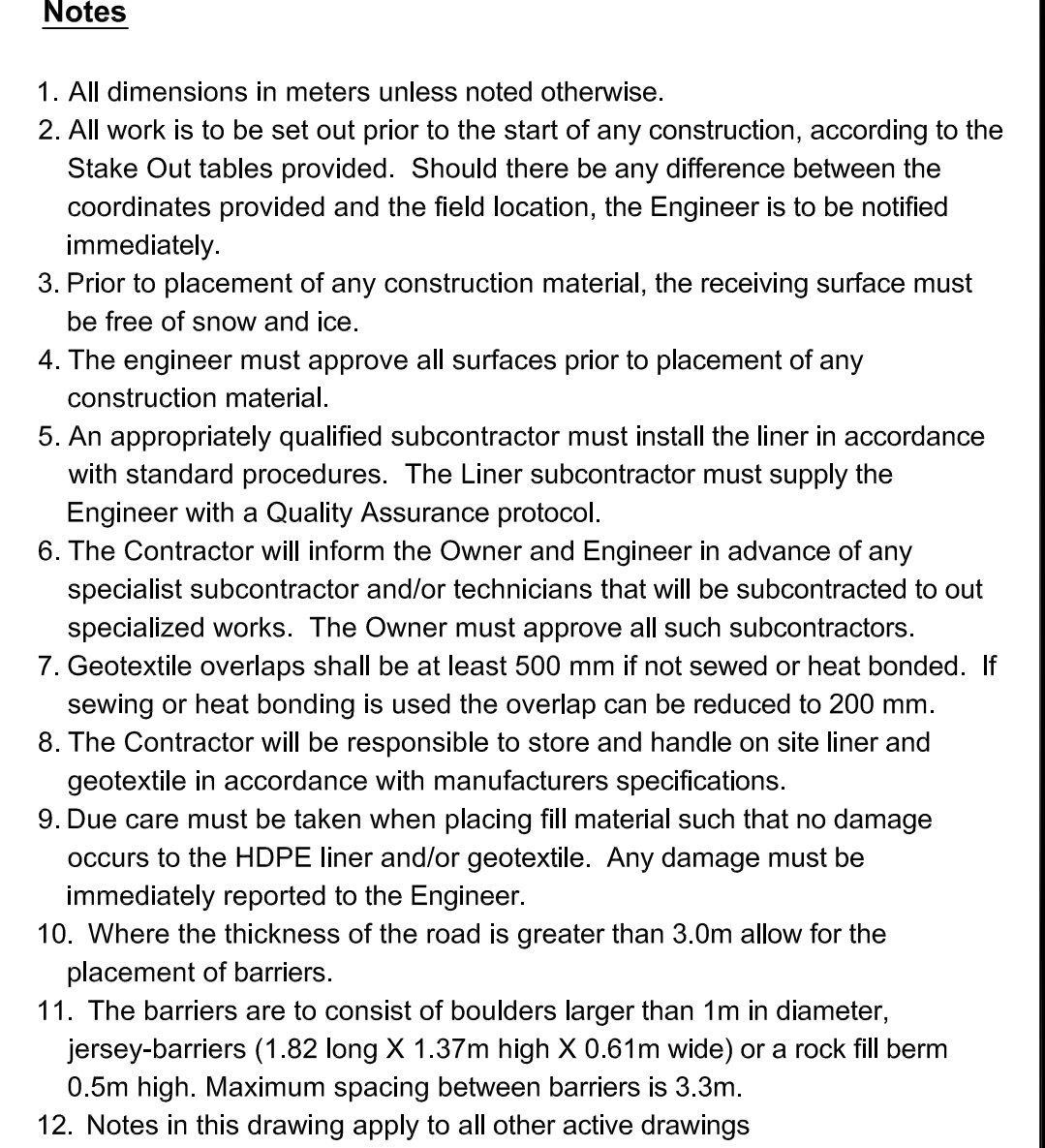
Scale in Metres (Horizontal) Scale in Metres (Vertical)

4X VERTICAL EXAGGERATION



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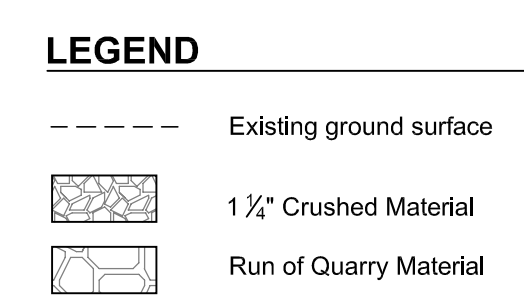
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Scale in Metres (Horizontal) Scale in Metres (Vertical)

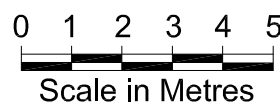
4X VERTICAL EXAGGERATION





0 4 8 12 16 20 0 1 2 3 4 5

Scale in Metres (Horizontal) Scale in Metres (Vertical)

4X VERTICAL EXAGGERATION



																DORIS NORTH PROJECT																					
													DRAWING TITLE:			Float Plan Access Road and Dyke Profiles																					
													HOPE BAY MINING LIMITED																								
										DESIGN: MK			DRAWN: MDDS		REVIEWED: EMR		NEWMONT DRAWING NO.			SHEET		REVISION NO.															
										CHECKED: LW		APPROVED: EMR		DATE: JULY 28, 2010																							
DMC-010 Sedimentation and Pollution Ponds Grading Plan										A		ISSUED FOR REVIEW		LW		EMR		28JUL10		PROFESSIONAL ENGINEERS STAMP			FILE NAME: DN-DMC-010.dwg			SRK JOB NO.: 1CH008 027		SRK DWG NO.: DN-DMC-012		HB+D-CIV-CIV-OND-0072		13 OF 15		A			
DRAWING NO. DRAWING TITLE DRAWING NO. DRAWING TITLE										NO.		DESCRIPTION		CHK'D		APP'D		DATE																			
REFERENCE DRAWINGS										REVISIONS																											

NOTES

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6. Liner shall be 60 mil textured HDPE liner.
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Materials List and Quantities



Item	Quantity/Area/Volume		Description
3/4" Finishing Material	Liner Subgrade (0.3 m)	1,100 m ³	Volumes Derived by Eagle Point V7.2 - Side slope 1.5H:1V for fill less than 2m - Side slope 2H:1V for fill greater than 2m -Fills are a min. 1.0m - Volume derived by merging Topography/As-built to Pad Design surfaces
	Overliner (0.3 m)	1,100 m ³	
	Culvert	60 m ³	
	Total	2,260 m ³	
Surfacing Material (1-1/4" Crush)	Berm Surfacing	100 m ³	
	Road surfacing	1,200 m ³	
	Total	1,300 m ³	
Run of Quarry Material	Berm	6,600 m ³	
	Road	14,000 m ³	
	Total	26,600 m ³	
Geotextile	Pollution Control Pond	8,200 m ²	12 oz. Non-Woven
	Total	8,200 m ²	
Liner	Pollution Control Pond	2,000 m ²	Textured HDPE 60 or equivalent
	Total	2,000 m ²	
Rip Rap		100 m ³	Spillway Aprons
	Total	100 m ²	
Culverts 4 in total		95 m	250mm Diameter Corrugated Steel Culvert
	Total	95 m	

SEDIMENTATION POND STAKE-OUT TABLE			
ID	Northing	Easting	Elevation (m)
SP-01	7,558,915.40	433,164.14	37.43
SP-02	7,558,965.46	433,119.21	40.26
SP-03	7,558,963.30	433,119.29	39.50
SP-04	7,558,930.28	433,088.97	39.50
SP-05	7,558,913.78	433,070.97	39.49
SP-06	7,558,906.68	433,072.64	39.38
SP-07	7,558,902.40	433,082.52	39.21
SP-08	7,558,919.76	433,151.32	34.24
SP-09	7,558,950.99	433,119.36	35.32
SP-10	7,558,924.38	433,094.87	35.33
SP-11	7,558,911.32	433,079.92	35.42
SP-12	7,558,910.20	433,083.15	35.34

POLLUTION CONTROL POND STAKE-OUT TABLE			
ID	Northing	Easting	Elevation (m)
PP-01	7,558,916.02	433,174.34	37.17
PP-02	7,558,971.42	433,124.60	40.27
PP-03	7,558,956.47	433,146.60	36.00
PP-04	7,558,980.84	433,189.66	36.00
PP-05	7,558,983.10	433,198.43	36.00
PP-06	7,558,982.91	433,234.79	36.00
PP-07	7,558,975.09	433,240.71	36.00
PP-08	7,558,921.36	433,241.22	36.00
PP-09	7,558,916.20	433,234.56	36.00
PP-10	7,558,923.81	433,178.43	33.28
PP-11	7,558,955.84	433,149.30	35.07
PP-12	7,558,979.05	433,191.02	34.88
PP-13	7,558,980.76	433,198.49	34.82
PP-14	7,558,980.92	433,233.79	35.00
PP-15	7,558,974.63	433,239.49	35.39
PP-16	7,558,961.93	433,238.83	35.00
PP-17	7,558,947.61	433,236.97	34.00
PP-18	7,558,923.98	433,235.81	33.31
PP-19	7,558,921.73	433,232.66	33.24

ROAD RAISE STAKE-OUT TABLE			
ID	Northing	Easting	Elevation (m)
RD-01	7,558,935.99	432,929.51	39.80
RD-02	7,558,923.63	432,921.02	39.80
RD-03	7,558,923.18	432,948.38	39.75
RD-04	7,558,910.31	432,940.63	39.75
RD-05	7,558,906.18	432,997.35	39.50
RD-06	7,558,887.56	432,989.00	39.50
RD-07	7,558,902.40	433,035.62	39.50
RD-08	7,558,879.29	433,035.66	39.50
RD-09	7,558,902.93	433,059.98	38.50
RD-10	7,558,883.06	433,061.75	39.17
RD-11	7,558,903.45	433,091.83	39.00
RD-12	7,558,888.55	433,093.64	39.00
RD-13	7,558,899.97	433,162.77	37.50
RD-14	7,558,901.05	433,183.38	37.00
RD-15	7,558,901.20	433,233.97	36.00
RD-16	7,558,917.58	433,260.20	35.50
RD-17	7,558,900.48	433,256.70	35.50
RD-18	7,558,912.91	433,279.21	35.00
RD-19	7,558,898.29	433,275.98	35.00
RD-20	7,558,890.48	433,345.81	33.50
RD-21	7,558,877.55	433,338.66	33.50
RD-22	7,558,878.02	433,365.99	33.00
RD-23	7,558,867.59	433,358.54	33.00
RD-24	7,558,857.68	433,390.74	33.00
RD-25	7,558,850.86	433,385.22	33.00
RD-26	7,558,849.04	433,399.29	32.22
RD-27	7,558,844.88	433,393.00	33.50

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								Original Drawings Stamped and Signed by Engineer	<div> DESIGN: MK DRAWN: MDDS REVIEWED: EMR CHECKED: LW APPROVED: EMR DATE: Sept. 29, 2010 FILE NAME: DN-DMC-010.dwg</div>	<div> HOPE BAY MINING LIMITED</div>				Doris North Project			
										DRAWING TITLE:							
										Material Specifications (Sedimentation and Pollution Control Ponds)							
										NEMONT DRAWING NO.							
										SHEET							
DRAWING NO.	DRAWING TITLE		DRAWING NO.	DRAWING TITLE		NO.	DESCRIPTION	CHK'D	APP'D	DATE	PROFESSIONAL ENGINEER'S STAMP						
REFERENCE DRAWINGS						REVISIONS						SRK JOB NO.: 1CH008-027 SRK DWG NO.: DN-DMC-013					
												HB+D-CIV-CIV-OND-0073 14 OF 18 0					

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Materials List and Quantities

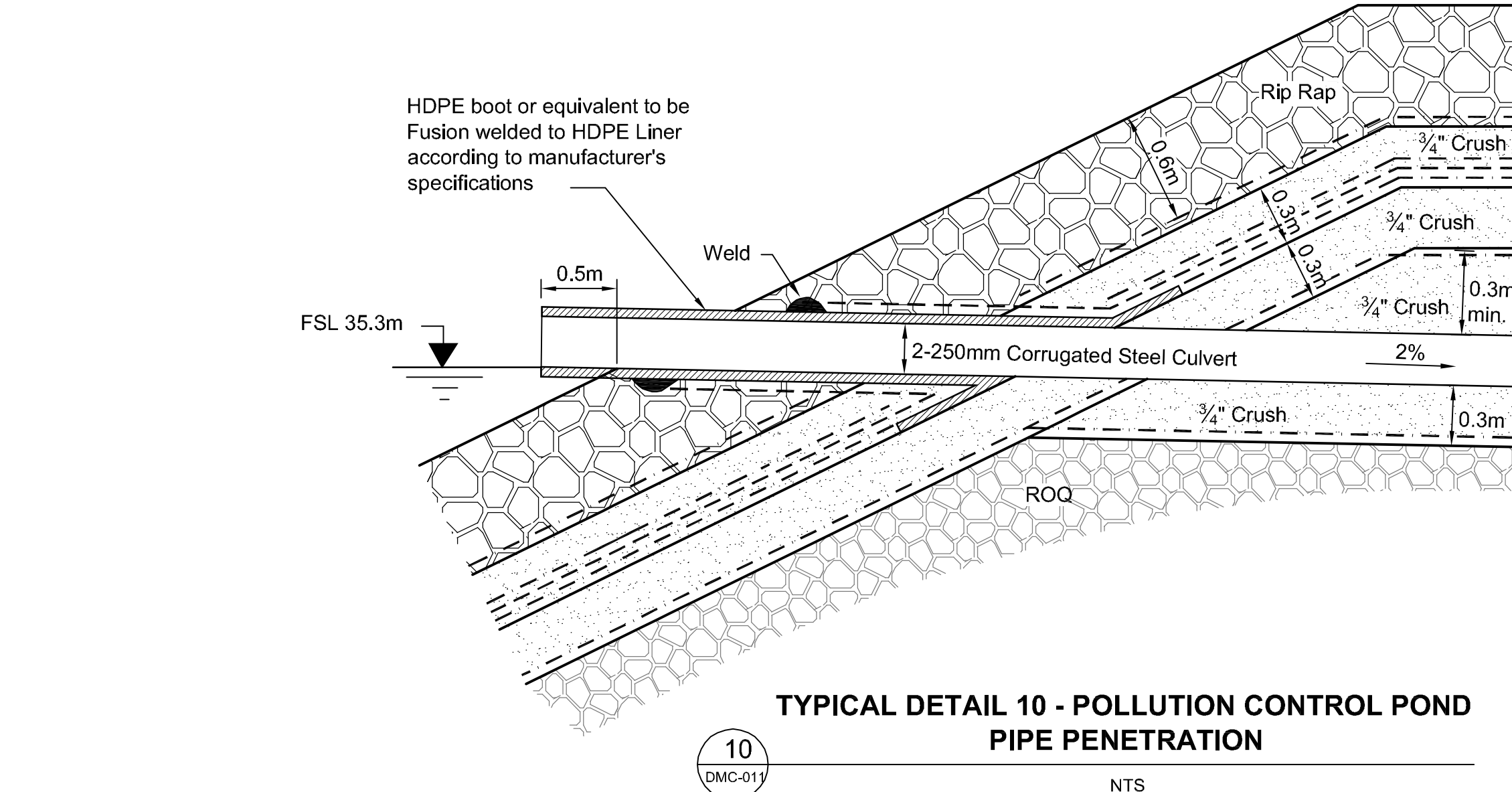
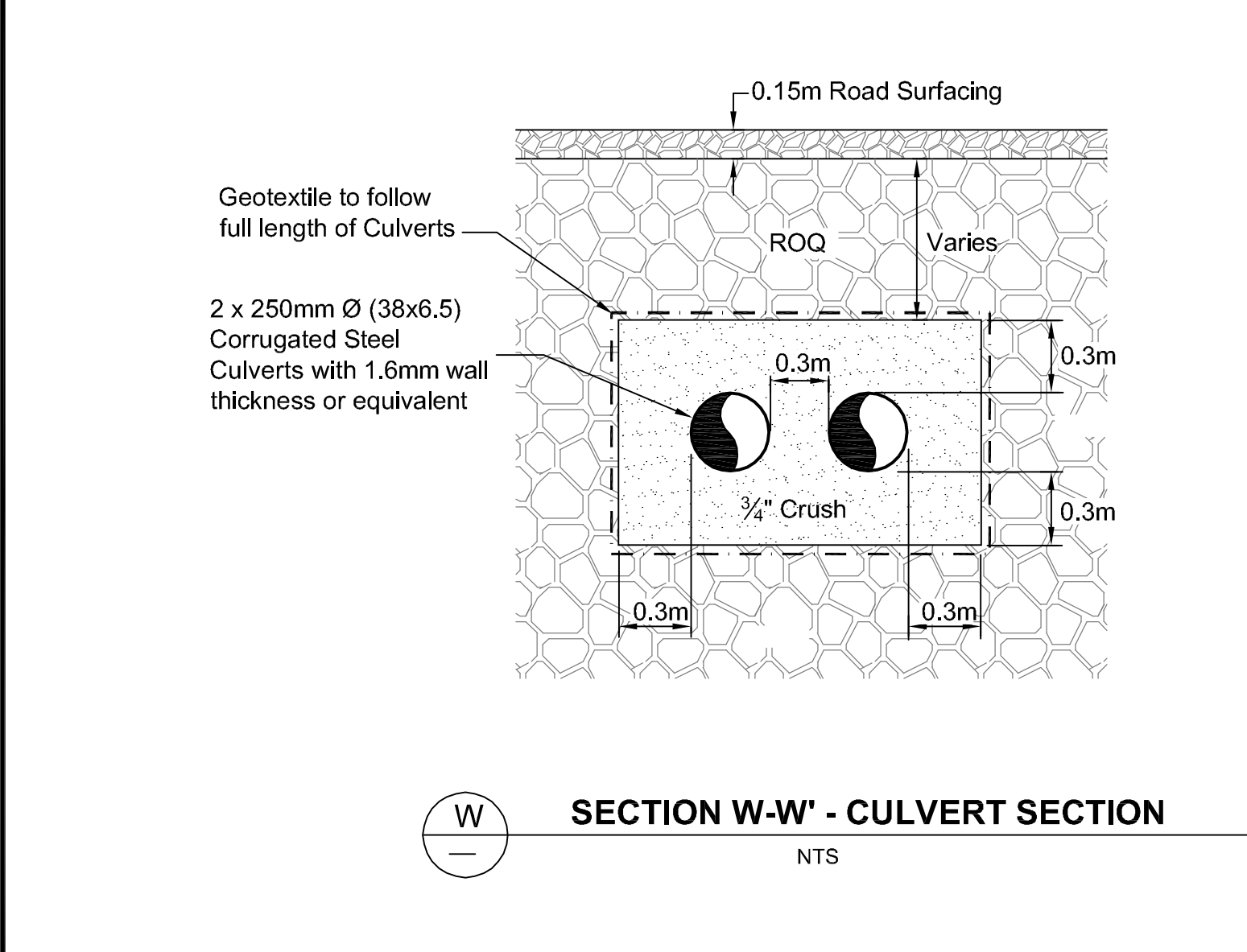
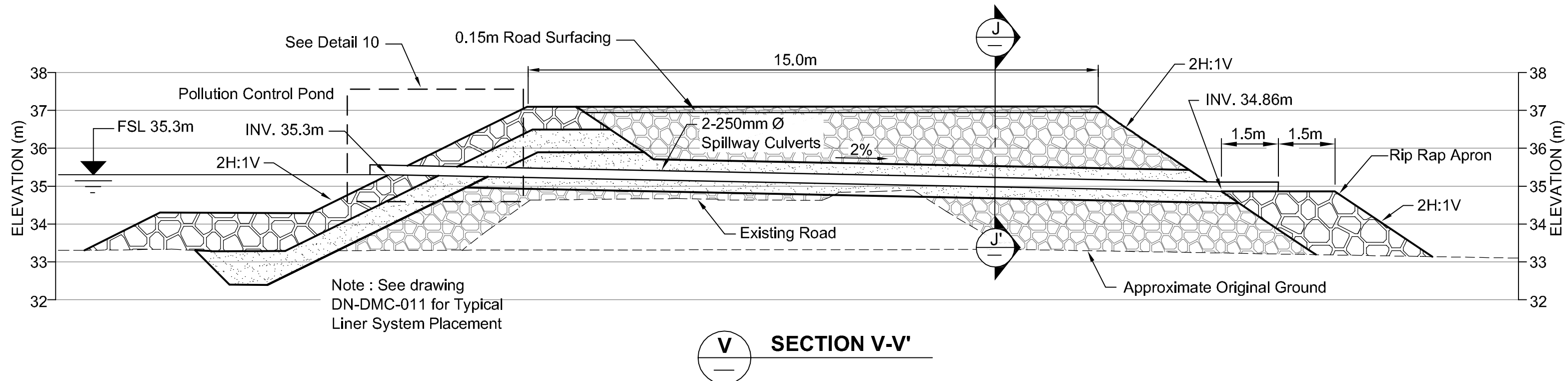
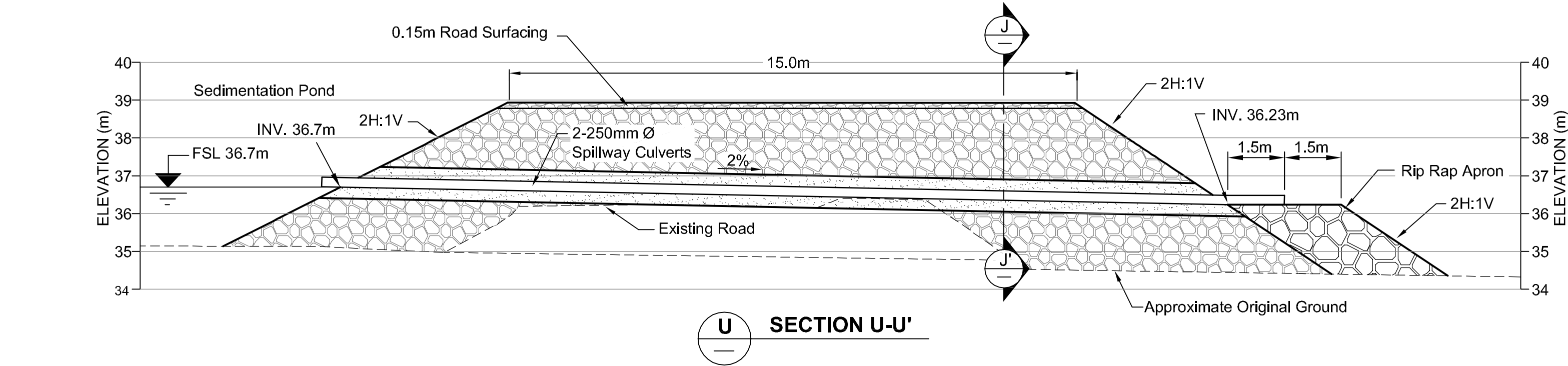
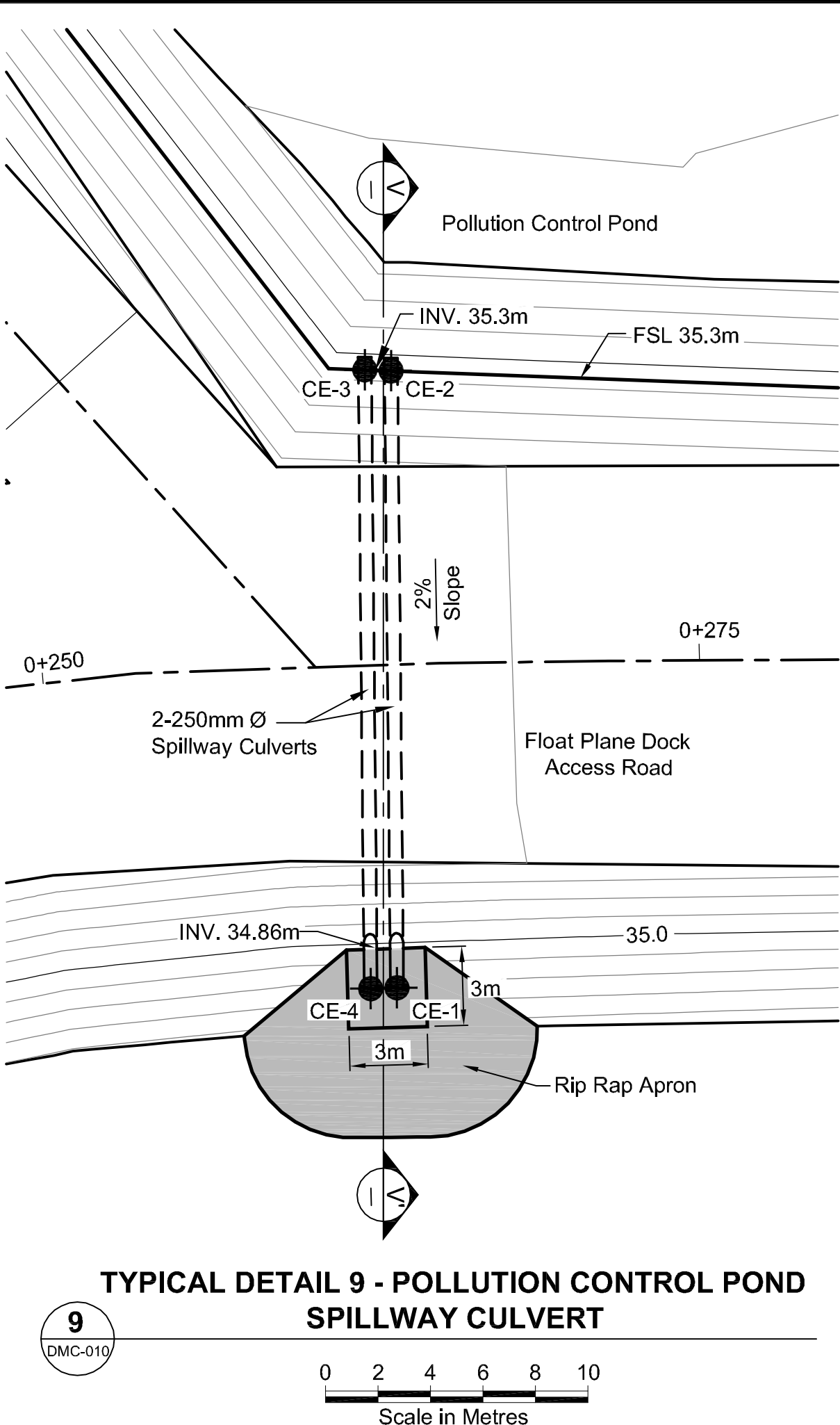
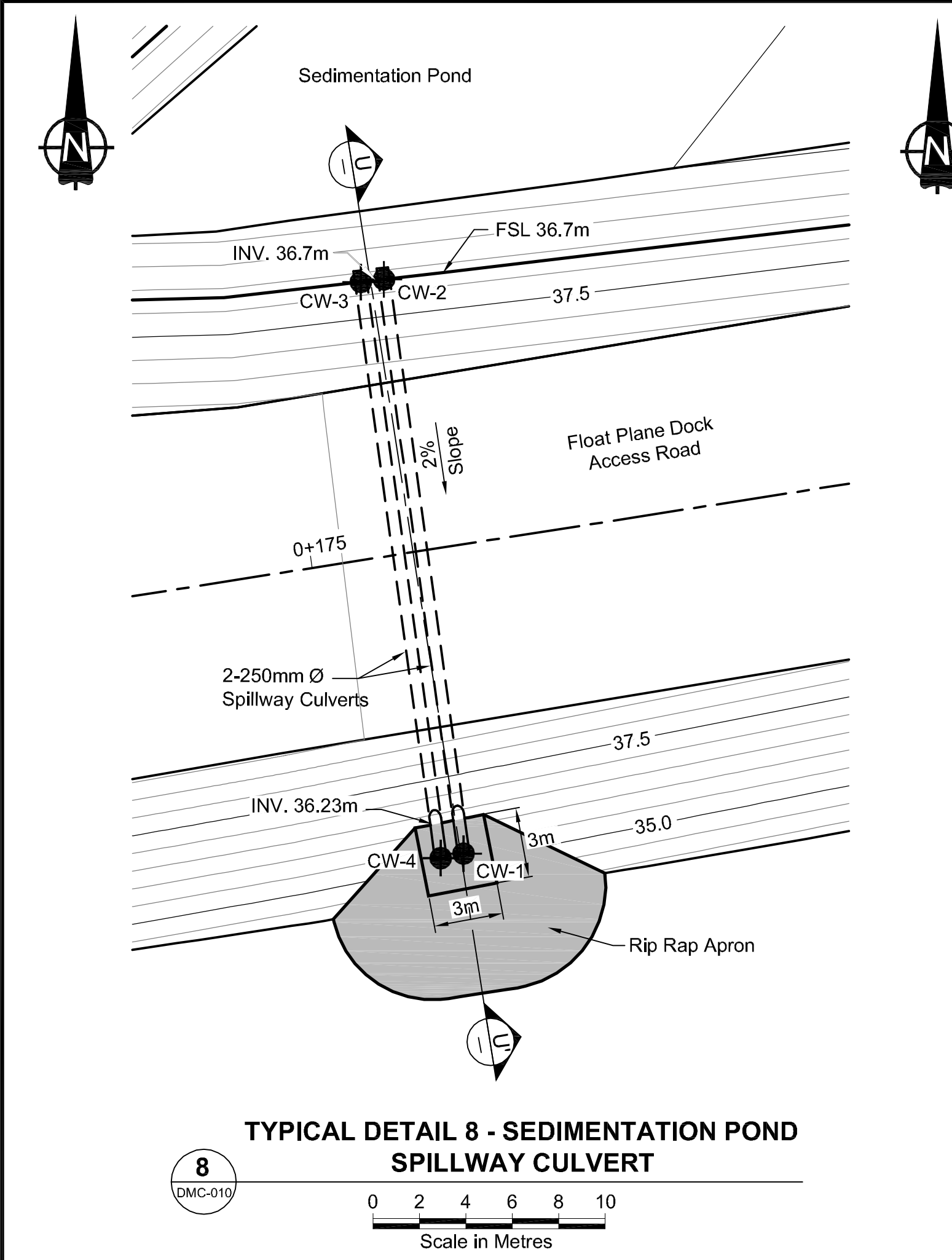
Item	Quantity/Area/Volume		Description
3/4" Finishing Material	Liner Subgrade (0.3 m)	1,100 m ³	Volumes Derived by Eagle Point V7.2
	Overliner (0.3 m)	1,100 m ³	- Side slope 1.5H:1V for fill less than 2m
	Culvert	60 m ³	- Side slope 2H:1V for fill greater than 2m
	Total	2,260 m ³	-Fills are a min. 1.0m
Surfacing Material (1-1/4" Crush)	Berm Surfacing	100 m ³	- Volume derived by merging Topography/As-built to Pad Design surfaces
	Road surfacing	1,200 m ³	
	Total	1,300 m ³	
Run of Quarry Material	Berm	6,600 m ³	
	Road	14,000 m ³	
	Total	26,600 m ³	
Geotextile	Pollution Control Pond	8,200 m ²	12 oz. Non-Woven
	Total	8,200 m ²	
Liner	Pollution Control Pond	2,000 m ²	Textured HDPE 60 or equivalent
	Total	2,000 m ²	
Rip Rap		100 m ³	Spillway Aprons
	Total	100 m ²	
Culverts 4 in total		95 m	250mm Diameter Corrugated Steel Culvert
	Total	95 m	

SEDIMENTATION POND STAKE-OUT TABLE			
ID	Northing	Easting	Elevation (m)
SP-01	7,558,915.40	433,164.14	37.43
SP-02	7,558,965.46	433,119.21	40.26
SP-03	7,558,963.30	433,119.29	39.50
SP-04	7,558,930.28	433,088.97	39.50
SP-05	7,558,913.78	433,070.97	39.49
SP-06	7,558,906.68	433,072.64	39.38
SP-07	7,558,902.40	433,082.52	39.21
SP-08	7,558,919.76	433,151.32	34.24
SP-09	7,558,950.99	433,119.36	35.32
SP-10	7,558,924.38	433,094.87	35.33
SP-11	7,558,911.32	433,079.92	35.42
SP-12	7,558,910.20	433,083.15	35.34

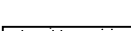
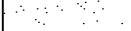


POLLUTION CONTROL POND STAKE-OUT TABLE			
ID	Northing	Easting	Elevation (m)
PP-01	7,558,916.02	433,174.34	37.17
PP-02	7,558,971.42	433,124.60	40.27
PP-03	7,558,956.47	433,146.60	36.00
PP-04	7,558,980.84	433,189.66	36.00
PP-05	7,558,983.10	433,198.43	36.00
PP-06	7,558,982.91	433,234.79	36.00
PP-07	7,558,975.09	433,240.71	36.00
PP-08	7,558,921.36	433,241.22	36.00
PP-09	7,558,916.20	433,234.56	36.00
PP-10	7,558,923.81	433,178.43	33.28
PP-11	7,558,955.84	433,149.30	35.07
PP-12	7,558,979.05	433,191.02	34.88
PP-13	7,558,980.76	433,198.49	34.82
PP-14	7,558,980.92	433,233.79	35.00
PP-15	7,558,974.63	433,239.49	35.39
PP-16	7,558,961.93	433,238.83	35.00
PP-17	7,558,947.61	433,236.97	34.00
PP-18	7,558,923.98	433,235.81	33.31
PP-19	7,558,921.73	433,232.66	33.24

ROAD RAISE STAKE-OUT TABLE			
ID	Northing	Easting	Elevation (m)
RD-01	7,558,935.99	432,929.51	39.80
RD-02	7,558,923.63	432,921.02	39.80
RD-03	7,558,923.18	432,948.38	39.75
RD-04	7,558,910.31	432,940.63	39.75
RD-05	7,558,906.18	432,997.35	39.50
RD-06	7,558,887.56	432,989.00	39.50
RD-07	7,558,902.40	433,035.62	39.50
RD-08	7,558,879.29	433,035.66	39.50
RD-09	7,558,902.93	433,059.98	38.50
RD-10	7,558,883.06	433,061.75	39.17
RD-11	7,558,903.45	433,091.83	39.00
RD-12	7,558,888.55	433,093.64	39.00
RD-13	7,558,899.97	433,162.77	37.50
RD-14	7,558,901.05	433,183.38	37.00
RD-15	7,558,901.20	433,233.97	36.00
RD-16	7,558,917.58	433,260.20	35.50
RD-17	7,558,900.48	433,256.70	35.50
RD-18	7,558,912.91	433,279.21	35.00
RD-19	7,558,898.29	433,275.98	35.00
RD-20	7,558,890.48	433,345.81	33.50
RD-21	7,558,877.55	433,338.66	33.50
RD-22	7,558,878.02	433,365.99	33.00
RD-23	7,558,867.59	433,358.54	33.00
RD-24	7,558,857.68	433,390.74	33.00
RD-25	7,558,850.86	433,385.22	33.00
RD-26	7,558,849.04	433,399.29	32.22
RD-27	7,558,844.88	433,393.00	33.50

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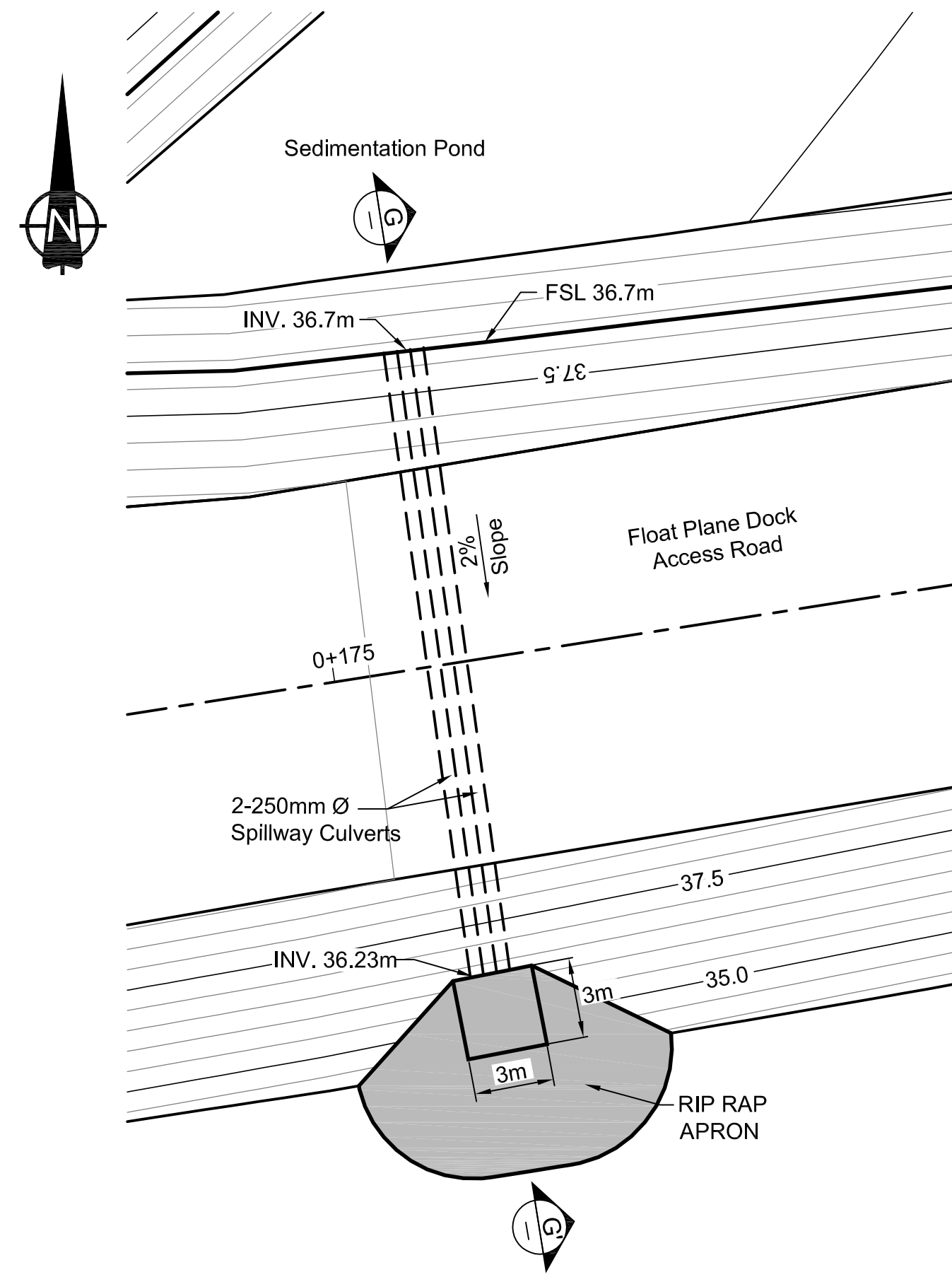


SPILLWAY CULVERT STAKE OUT TABLE			
ID	Northing	Easting	Approx. Elev. (m)
Sedimentation Pond Culvert			
CW-1	7,558,883.65	433,097.91	36.20
CW-2	7,558,908.36	433,094.49	36.71
CW-3	7,558,908.25	433,093.49	36.71
CW-4	7,558,883.45	433,096.93	36.20
Pollution Control Pond Culvert			
CE-1	7,558,896.19	433,178.92	34.83
CE-2	7,558,919.67	433,178.69	35.31
CE-3	7,558,919.71	433,177.69	35.31
CE-4	7,558,896.16	433,177.92	34.83

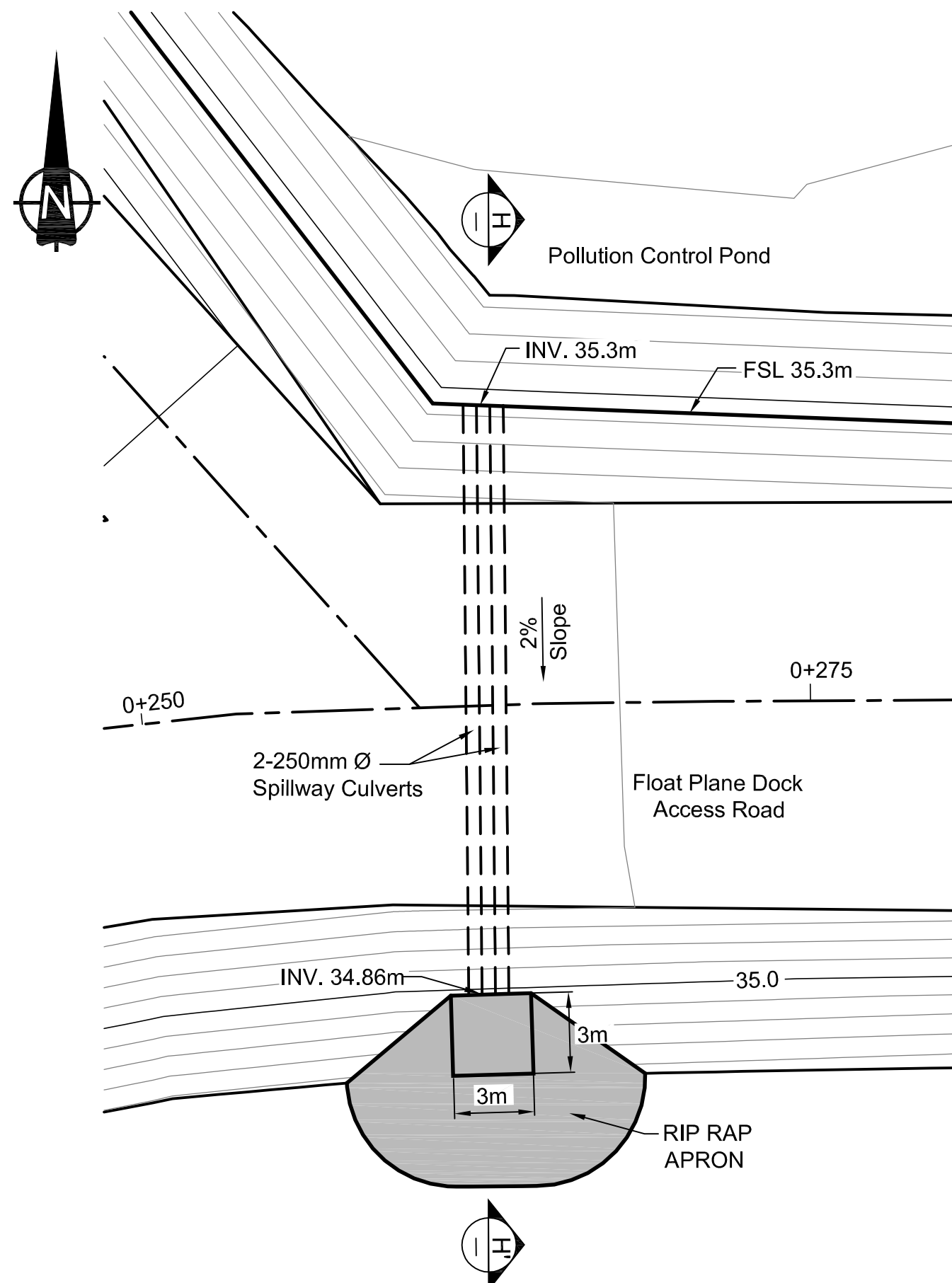
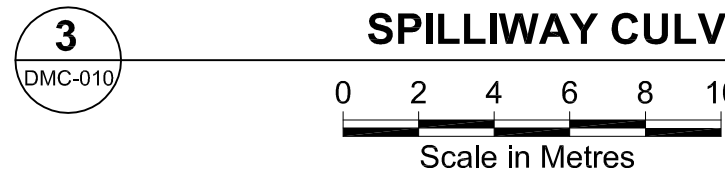
LEGEND			
	¾" Crushed Material	- - - - -	Existing ground surface
	1 ¼" Crushed Material	- - - - -	Textured 60mil HDPE Liner
	Run of Quarry Material	- · - · - · -	12 oz. Non-woven Geotextile
	Rip Rap		

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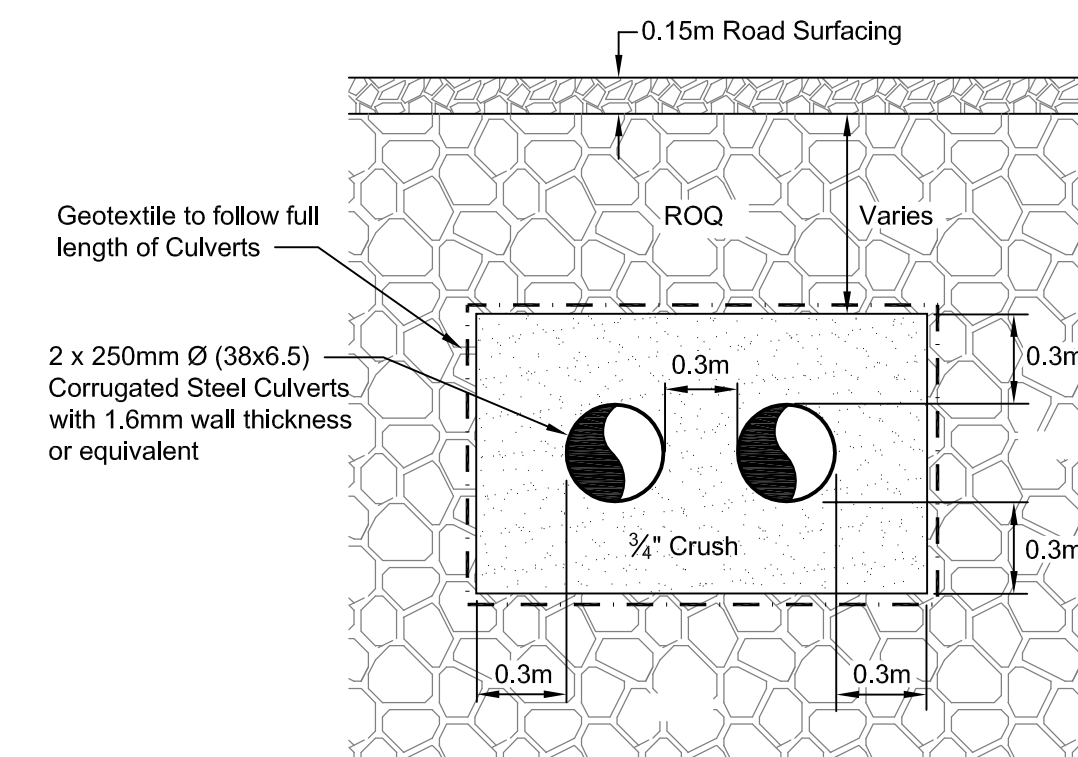
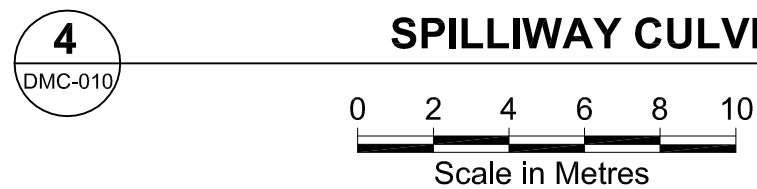
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TYPICAL DETAIL 3 - SEDIMENTATION POND SPILLWAY CULVERT

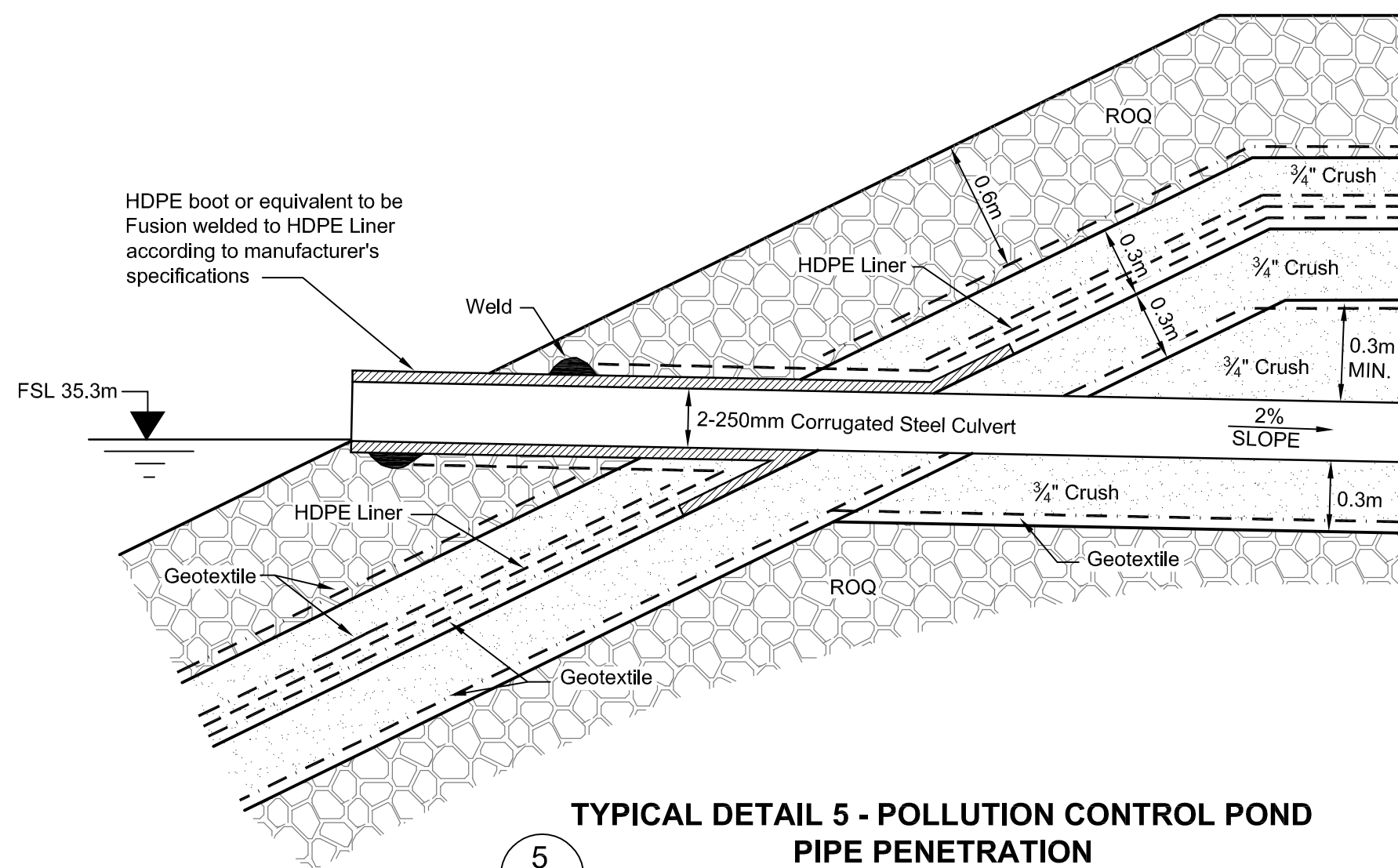


TYPICAL DETAIL 4 - POLLUTION CONTROL POND SPILLWAY CULVERT

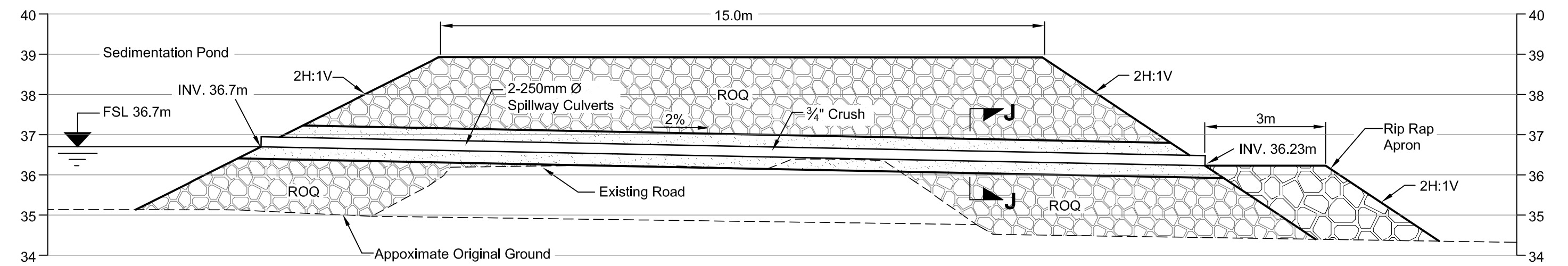
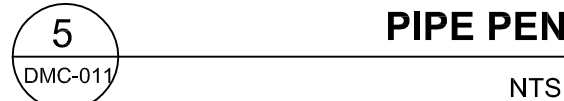


SECTION J-J' - CULVERT SECTION

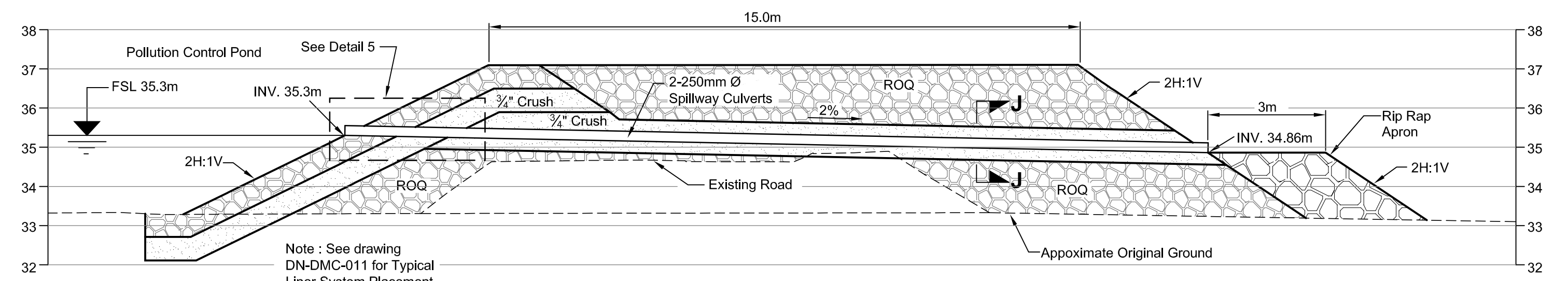
NTS



TYPICAL DETAIL 5 - POLLUTION CONTROL POND PIPE PENETRATION



SECTION G-G'

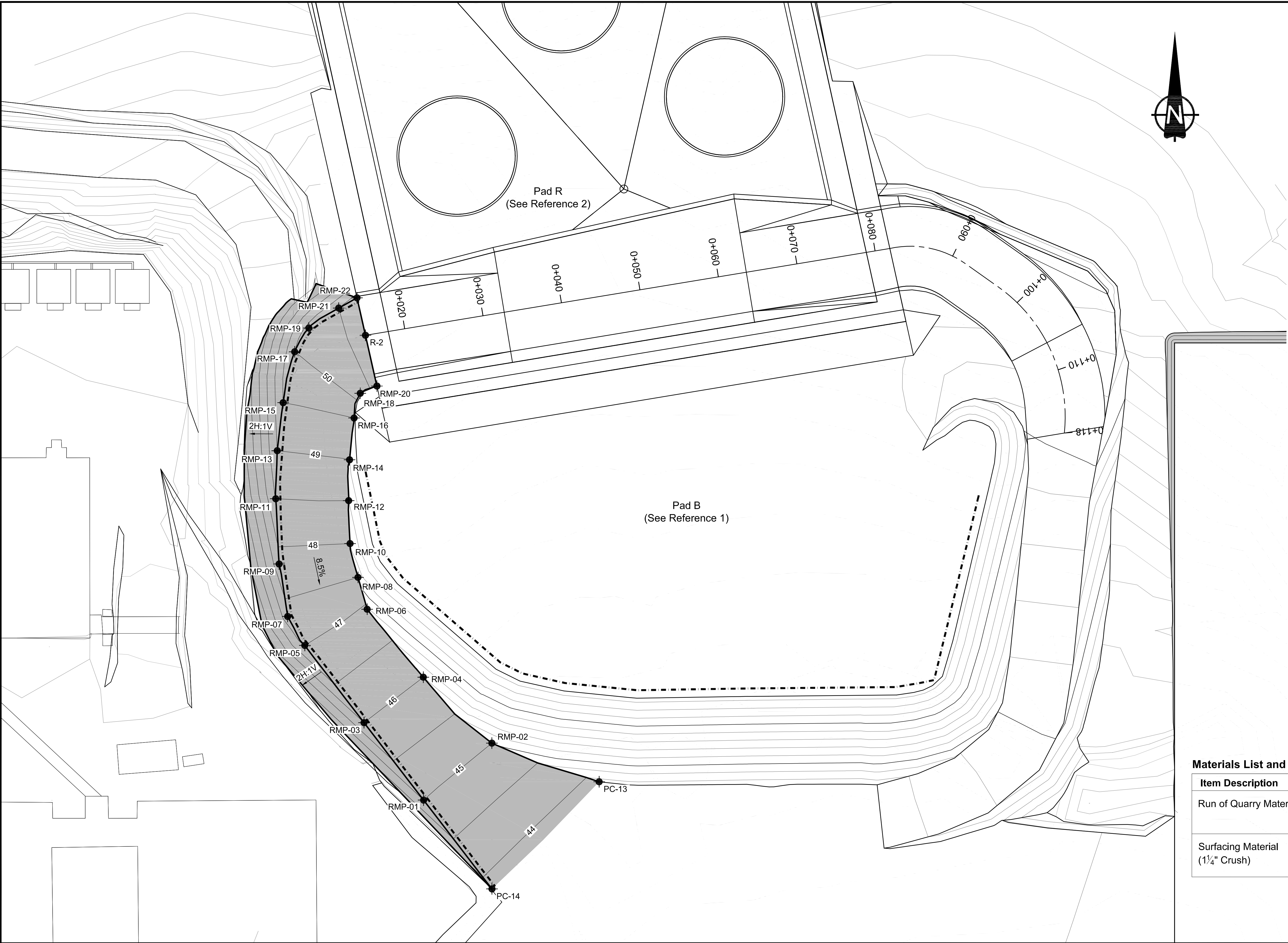


SECTION H-H'

LEGEND			
	1/4" Crushed Material		Existing ground surface
	1 1/4" Crushed Material		Textured HDPE Liner
	Run of Quarry Material		12 oz. Non-woven Geotextile

												DORIS NORTH PROJECT			
								DRAWING TITLE:				Sedimentation and Pollution Control Pond Liner and Spillway Culvert Typical Details			
								NEMONT DRAWING NO.				HB+D-CIV-CIV-OND-0080			
								SHEET				15 OF 15			
								REVISION NO.				A			

DMC-010				Sedimentation and Pollution Ponds Grading Plan											
DRAWING NO.				DRAWING TITLE				DRAWING NO.				DRAWING TITLE			
				REFERENCE DRAWINGS											
								REVISIONS							



LEGEND

- New Raised Access Ramp
- Stake-out Point
- Existing Buildings
- Safety Berms (See Typical Berm Barrier Options Detail on Dwg DN-DMC-03)

NOTES

- This drawing supersedes stakeout points PR-01 and PR-02; PB-23 to 25; and PC-13 and 14 on DN-DMC-01.

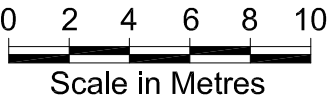
REFERENCES

- For detailed design of the Doris North Camp refer to Engineering Drawings for the Doris North Camp Area, Doris North Project, Nunavut, Canada, Revision 1, SRK 2010.
- For detailed Pad R refer to Engineering Drawings for the Doris North Fuel Tank Farm, Doris Infrastructure Project, Nunavut, Canada, Revision 1, SRK 2010.

PAD R ACCESS RAMP STAKE-OUT TABLE			
ID	Northing	Easting	Elevation (m)
R-2	7,559,177.70	432,988.83	50.70
PC-13	7,559,121.58	433,018.22	43.81
PC-14	7,559,108.11	433,004.73	43.85
RMP-01	7,559,119.27	432,996.14	45.00
RMP-02	7,559,126.43	433,004.73	45.00
RMP-03	7,559,129.01	432,988.65	46.00
RMP-04	7,559,134.72	432,996.11	46.00
RMP-05	7,559,138.71	432,981.21	47.00
RMP-06	7,559,143.26	432,989.05	46.91
RMP-07	7,559,142.35	432,979.05	47.32
RMP-08	7,559,147.27	432,987.89	47.50
RMP-09	7,559,148.95	432,977.97	47.84
RMP-10	7,559,151.51	432,986.89	48.00
RMP-11	7,559,157.15	432,977.55	48.50
RMP-12	7,559,156.91	432,986.72	48.50
RMP-13	7,559,163.19	432,977.74	49.00
RMP-14	7,559,162.05	432,986.83	49.00
RMP-15	7,559,169.22	432,978.48	49.50
RMP-16	7,559,167.30	432,987.40	49.50
RMP-17	7,559,175.62	432,979.93	50.00
RMP-18	7,559,170.40	432,988.18	50.20
RMP-19	7,559,178.61	432,981.71	50.20
RMP-20	7,559,171.32	432,990.27	50.70
RMP-21	7,559,181.11	432,985.47	50.50
RMP-22	7,559,182.40	432,987.77	50.70

Materials List and Quantities

Item Description	Quantity / Area / Volume		
Run of Quarry Material	Ramp	1200 m³	Volumes derived by Eagle Point 7.2.
Surfacing Material (1¼" Crush)	Ramp	150 m³	- Side slopes 2H:1V Unless otherwise noted



DRAWING NO.		DRAWING TITLE		DRAWING NO.		DRAWING TITLE		1	ISSUED FOR CONSTRUCTION	LW	EMR	8AUG10
								NO.	DESCRIPTION	CHK'D	APP'D	DATE
								REVISIONS				

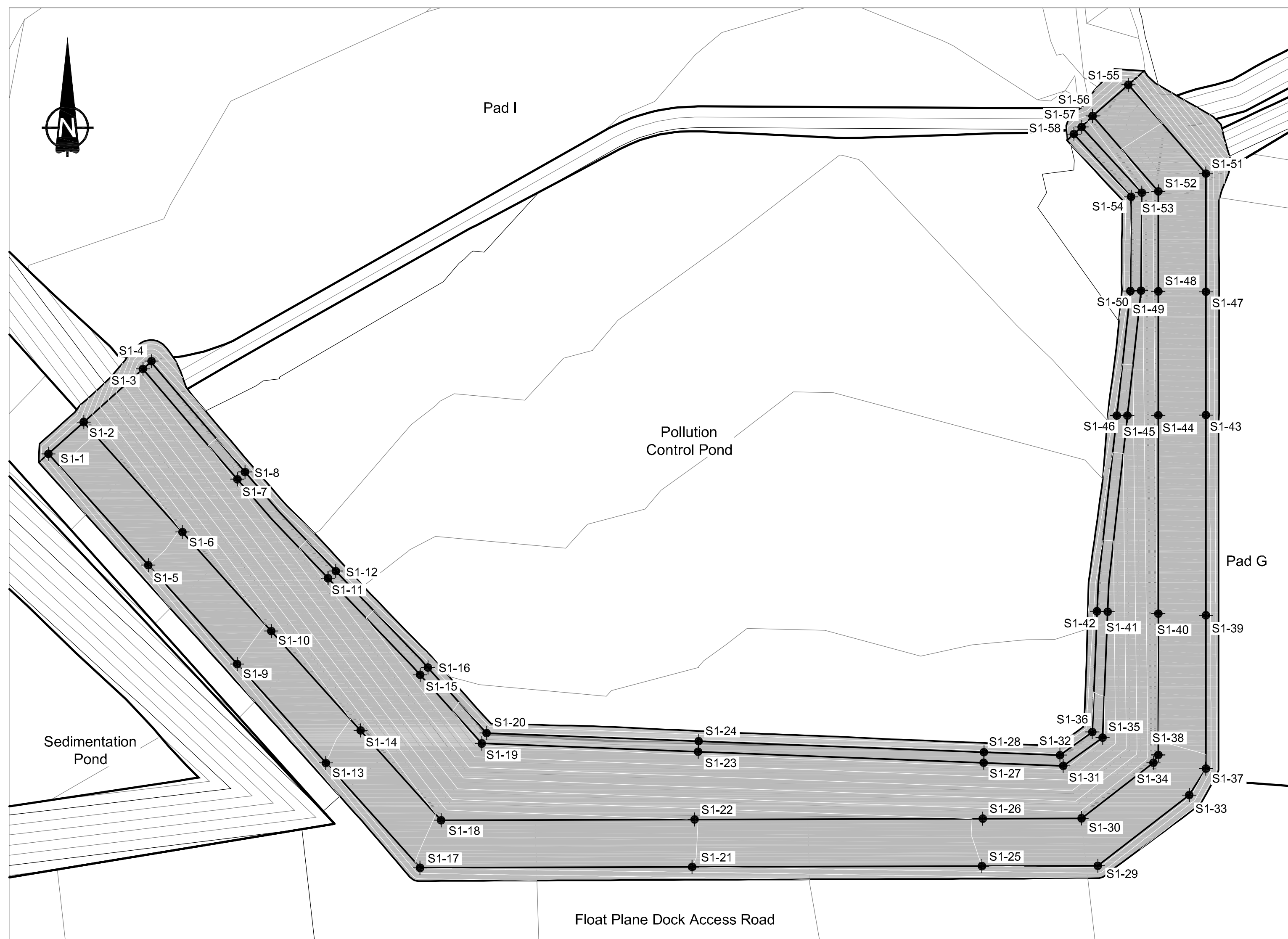
PROFESSIONAL ENGINEERS' STAMP	
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DESIGN: MK	DRAWN: MDDS	REVIEWED: EMR
CHECKED: LW	APPROVED: EMR	DATE: AUG 8, 2010
FILE NAME: DN-DMC-015.dwg		

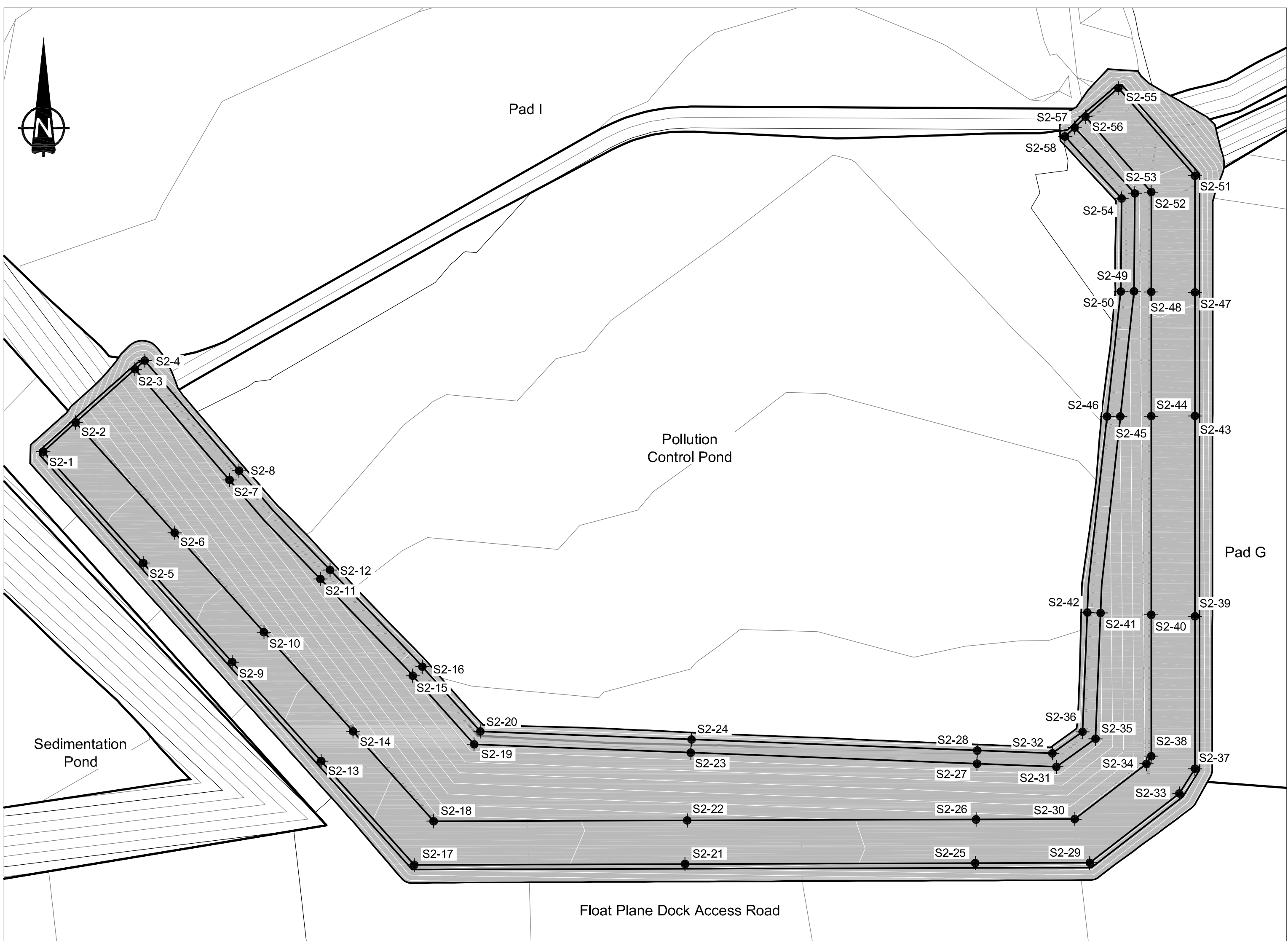
HOPE BAY MINING LIMITED	
SRK JOB NO.: 1CH008 027	SRK DWG NO.: DN-DMC-015

DORIS NORTH PROJECT		
DRAWING TITLE:		
PAD R - RAISED ACCESS RAMP		
NEWMONT DRAWING NO.	SHEET	REVISION NO.
HB+D-CIV-CIV-OND-0082	16 OF 16	1

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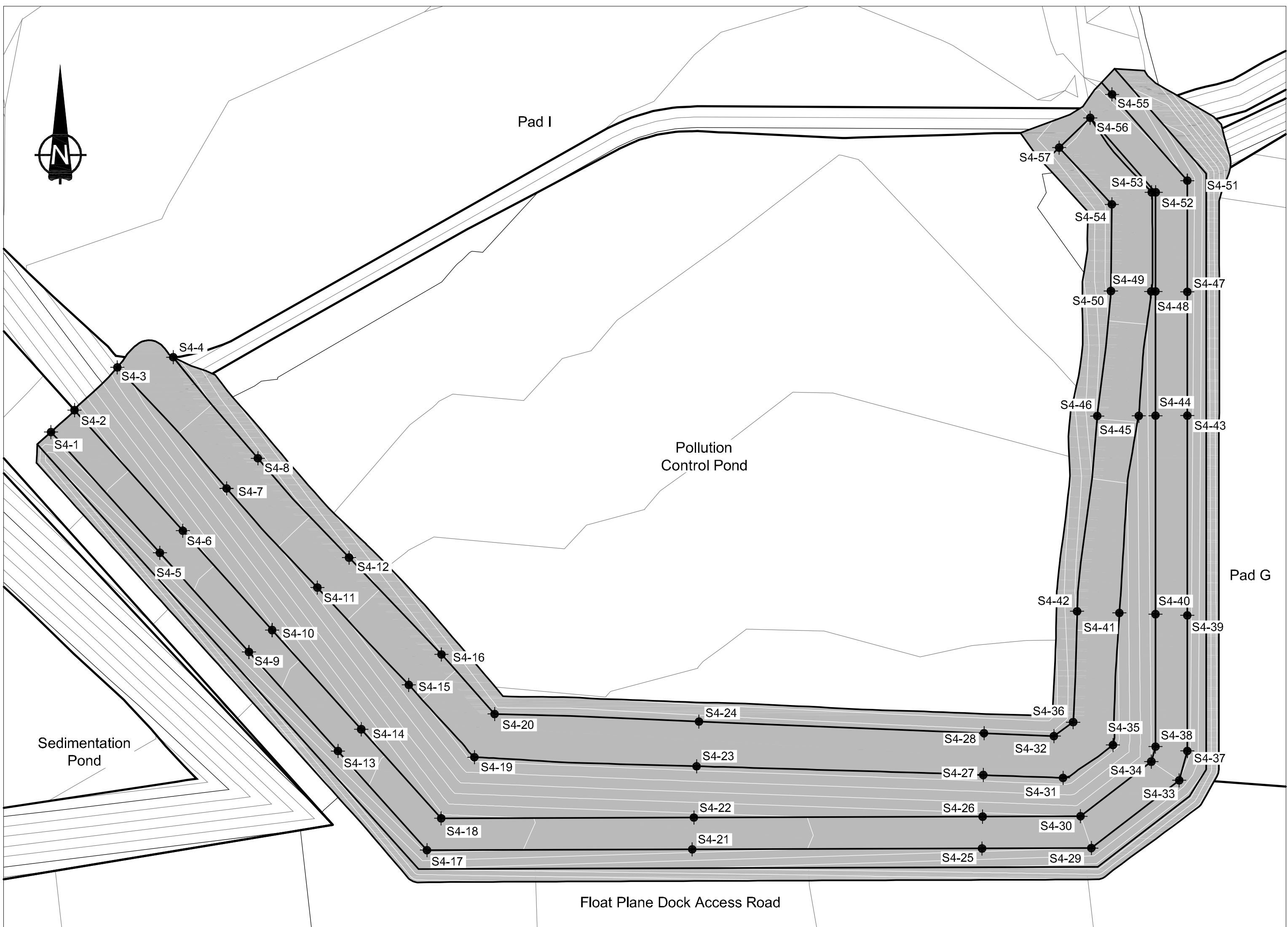


SURFACE 1 - STAKE-OUT TABLE											
ID	Northing	Easting	Elevation (m)	ID	Northing	Easting	Elevation (m)	ID	Northing	Easting	Elevation (m)
S1-1	7,558,950.31	433,137.14	38.06	S1-21	7,558,911.32	433,197.89	35.50	S1-41	7,558,935.41	433,237.11	32.69
S1-2	7,558,953.30	433,140.48	38.06	S1-22	7,558,915.80	433,198.13	35.50	S1-42	7,558,935.45	433,236.11	32.69
S1-3	7,558,958.32	433,146.07	34.28	S1-23	7,558,922.20	433,198.47	32.36	S1-43	7,558,953.97	433,246.39	35.15
S1-4	7,558,958.99	433,146.81	34.28	S1-24	7,558,923.20	433,198.52	32.36	S1-44	7,558,953.95	433,241.90	35.15
S1-5	7,558,939.80	433,146.57	37.50	S1-25	7,558,911.40	433,225.25	35.00	S1-45	7,558,953.93	433,238.98	33.72
S1-6	7,558,942.93	433,149.79	37.50	S1-26	7,558,915.89	433,225.33	35.00	S1-46	7,558,953.93	433,237.97	33.72
S1-7	7,558,947.91	433,154.99	33.87	S1-27	7,558,921.16	433,225.42	32.34	S1-47	7,558,965.60	433,246.39	35.20
S1-8	7,558,948.60	433,155.70	33.87	S1-28	7,558,922.16	433,225.44	32.34	S1-48	7,558,965.65	433,241.90	35.20
S1-9	7,558,930.47	433,154.95	37.00	S1-29	7,558,911.44	433,236.19	34.80	S1-49	7,558,965.71	433,240.27	34.42
S1-10	7,558,933.59	433,158.18	37.00	S1-30	7,558,915.92	433,234.65	34.80	S1-50	7,558,965.67	433,239.26	34.42
S1-11	7,558,938.57	433,163.54	33.28	S1-31	7,558,920.87	433,232.92	32.34	S1-51	7,558,976.75	433,246.39	35.26
S1-12	7,558,939.25	433,164.27	33.28	S1-32	7,558,921.88	433,232.62	32.34	S1-52	7,558,975.07	433,241.90	35.26
S1-13	7,558,921.14	433,163.33	36.50	S1-33	7,558,918.10	433,244.82	34.80	S1-53	7,558,974.96	433,240.34	34.49
S1-14	7,558,924.21	433,166.61	36.50	S1-34	7,558,921.16	433,241.44	34.80	S1-54	7,558,974.57	433,239.33	34.49
S1-15	7,558,929.46	433,172.23	32.63	S1-35	7,558,923.53	433,236.64	32.41	S1-55	7,558,985.15	433,239.06	34.80
S1-16	7,558,930.14	433,172.96	32.63	S1-36	7,558,924.06	433,235.66	32.41	S1-56	7,558,982.20	433,235.69	34.80
S1-17	7,558,911.24	433,172.22	35.97	S1-37	7,558,920.61	433,246.39	34.99	S1-57	7,558,981.16	433,234.66	34.10
S1-18	7,558,915.73	433,174.21	35.97	S1-38	7,558,921.90	433,241.90	34.99	S1-58	7,558,980.48	433,233.92	34.10
S1-19	7,558,922.98	433,178.04	32.38	S1-39	7,558,935.07	433,246.39	35.06				
S1-20	7,558,923.96	433,178.50	32.38	S1-40	7,558,935.24	433,241.90	35.06				



SURFACE 2 - STAKE-OUT TABLE											
ID	Northing	Easting	Elevation (m)	ID	Northing	Easting	Elevation (m)	ID	Northing	Easting	Elevation (m)
S2-1	7,558,950.61	433,137.47	38.36	S2-21	7,558,911.77	433,197.92	35.80	S2-41	7,558,935.41	433,237.05	32.99
S2-2	7,558,953.35	433,140.53	38.36	S2-22	7,558,915.88	433,198.13	35.80	S2-42	7,558,935.46	433,235.81	32.99
S2-3	7,558,958.36	433,146.11	34.58	S2-23	7,558,922.26	433,198.47	32.66	S2-43	7,558,953.97	433,245.94	35.45
S2-4	7,558,959.19	433,147.04	34.58	S2-24	7,558,923.50	433,198.53	32.66	S2-44	7,558,953.95	433,241.83	35.45
S2-5	7,558,940.11	433,146.90	37.80	S2-25	7,558,911.85	433,225.25	35.30	S2-45	7,558,953.93	433,238.92	34.02
S2-6	7,558,942.97	433,149.86	37.80	S2-26	7,558,915.96	433,225.33	35.30	S2-46	7,558,953.92	433,237.67	34.02
S2-7	7,558,947.94	433,155.02	34.17	S2-27	7,558,921.22	433,225.42	32.64	S2-47	7,558,965.60	433,245.94	35.50
S2-8	7,558,948.81	433,155.92	34.17	S2-28	7,558,922.46	433,225.44	32.64	S2-48	7,558,965.65	433,241.83	35.50
S2-9	7,558,930.78	433,155.28	37.30	S2-29	7,558,911.88	433,236.04	35.10	S2-49	7,558,965.71	433,240.21	34.72
S2-10	7,558,933.60	433,158.27	37.30	S2-30	7,558,915.99	433,234.63	35.10	S2-50	7,558,965.68	433,238.96	34.72
S2-11	7,558,938.45	433,163.48	33.58	S2-31	7,558,920.93	433,232.90	32.64	S2-51	7,558,976.59	433,245.94	35.56
S2-12	7,558,939.40	433,164.53	33.58	S2-32	7,558,922.19	433,232.52	32.64	S2-52	7,558,975.05	433,241.83	35.56
S2-13	7,558,921.45	433,163.66	36.80	S2-33	7,558,918.41	433,244.48	35.10	S2-53	7,558,974.93	433,240.28	34.79
S2-14	7,558,924.25	433,166.66	36.80	S2-34	7,558,921.21	433,241.39	35.10	S2-54	7,558,974.45	433,239.03	34.79
S2-15	7,558,929.50	433,172.27	32.93	S2-35	7,558,923.57	433,236.58	32.71	S2-55	7,558,984.85	433,238.73	35.10
S2-16	7,558,930.35	433,173.18	32.93	S2-36	7,558,924.22	433,235.36	32.71	S2-56	7,558,982.15	433,235.63	35.10
S2-17	7,558,911.69	433,172.42	36.27	S2-37	7,558,920.74	433,245.94	35.29	S2-57	7,558,981.12	433,234.62	34.40
S2-18	7,558,915.80	433,174.25	36.27	S2-38	7,558,921.92	433,241.83	35.29	S2-58	7,558,980.28	433,233.70	34.40
S2-19	7,558,923.04	433,178.07	32.68	S2-39	7,558,935.09	433,245.94	35.36				
S2-20	7,558,924.26	433,178.64	32.68	S2-40	7,558,935.24	433,241.83	35.36				

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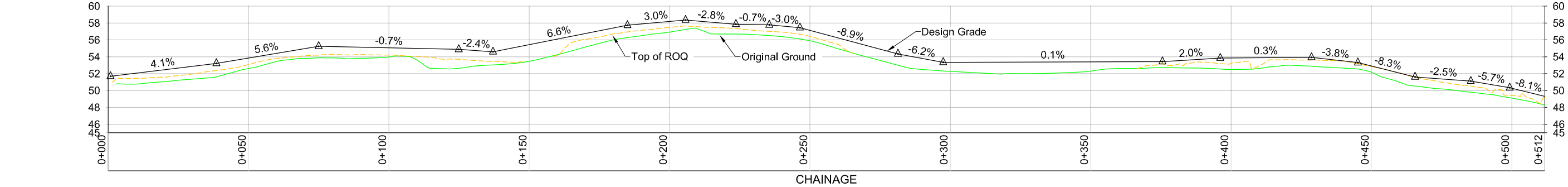


Surface 4 - Top of Rip Rap

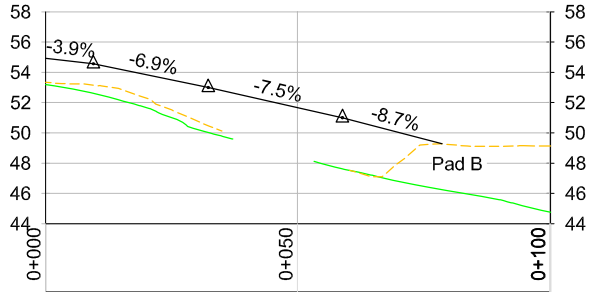
SURFACE 4 - STAKE-OUT TABLE											
ID	Northing	Easting	Elevation (m)	ID	Northing	Easting	Elevation (m)	ID	Northing	Easting	Elevation (m)
S4-1	7,558,952.41	433,137.60	39.26	S4-21	7,558,913.09	433,197.99	36.70	S4-41	7,558,935.37	433,238.22	34.56
S4-2	7,558,954.47	433,139.82	39.26	S4-22	7,558,916.09	433,198.15	36.70	S4-42	7,558,935.52	433,234.24	34.56
S4-3	7,558,958.51	433,143.85	36.68	S4-23	7,558,920.92	433,198.40	34.30	S4-43	7,558,953.96	433,244.61	36.35
S4-4	7,558,959.46	433,149.11	36.15	S4-24	7,558,925.13	433,198.62	34.30	S4-44	7,558,953.94	433,241.61	36.35
S4-5	7,558,941.03	433,147.85	38.70	S4-25	7,558,913.18	433,225.28	36.20	S4-45	7,558,953.94	433,240.05	35.57
S4-6	7,558,943.12	433,150.01	38.70	S4-26	7,558,916.18	433,225.33	36.20	S4-46	7,558,953.92	433,236.14	35.57
S4-7	7,558,947.09	433,154.14	35.78	S4-27	7,558,920.09	433,225.40	34.21	S4-47	7,558,965.62	433,244.61	36.40
S4-8	7,558,949.93	433,157.09	35.78	S4-28	7,558,923.87	433,225.50	34.21	S4-48	7,558,965.65	433,241.61	36.40
S4-9	7,558,931.69	433,156.24	38.20	S4-29	7,558,913.21	433,235.58	36.00	S4-49	7,558,965.65	433,241.22	36.21
S4-10	7,558,933.75	433,158.42	38.20	S4-30	7,558,916.23	433,234.69	36.00	S4-50	7,558,965.69	433,237.41	36.21
S4-11	7,558,937.76	433,162.68	35.21	S4-31	7,558,919.82	433,232.91	34.20	S4-51	7,558,976.09	433,244.61	36.46
S4-12	7,558,940.58	433,165.67	35.21	S4-32	7,558,923.76	433,232.05	34.20	S4-52	7,558,974.99	433,241.64	36.46
S4-13	7,558,922.35	433,164.62	37.70	S4-33	7,558,919.59	433,243.85	36.00	S4-53	7,558,974.99	433,241.26	36.30
S4-14	7,558,924.40	433,166.82	37.70	S4-34	7,558,921.36	433,241.22	36.00	S4-54	7,558,973.86	433,237.51	36.30
S4-15	7,558,928.59	433,171.30	34.58	S4-35	7,558,922.93	433,237.61	34.28	S4-55	7,558,984.22	433,237.52	36.00
S4-16	7,558,931.46	433,174.37	34.58	S4-36	7,558,925.08	433,233.86	34.28	S4-56	7,558,982.01	433,235.47	36.00
S4-17	7,558,913.02	433,173.01	37.17	S4-37	7,558,922.36	433,244.61	36.19	S4-57	7,558,979.21	433,232.54	36.00
S4-18	7,558,916.02	433,174.34	37.17	S4-38	7,558,922.77	433,241.61	36.19				
S4-19	7,558,921.77	433,177.48	34.30	S4-39	7,558,935.14	433,244.61	36.26				
S4-20	7,558,925.84	433,179.38	34.30	S4-40	7,558,935.25	433,241.61	36.26				

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- LEGEND**
- Design Grade
 - Top of Existing ROQ
 - Original Ground
 - Point of Vertical Intersection
 - Grade
 - Route Centerline

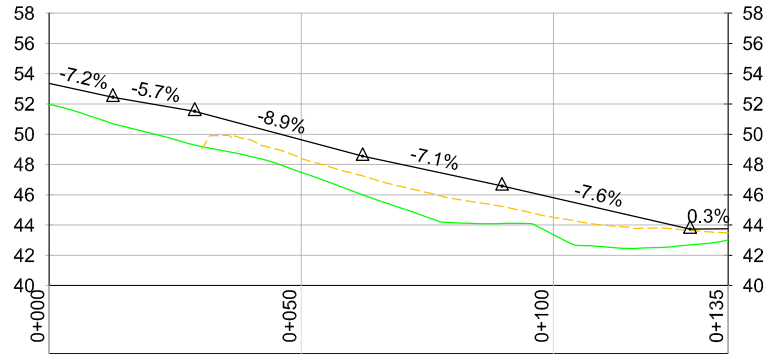


**PROFILE
WEST RAMP**

Horizontal Scale in Metres
Vertical Exaggeration 3X

**PROFILE
NORTH ROAD**

Horizontal Scale in Metres
Vertical Exaggeration 3X



**PROFILE
EAST RAMP**

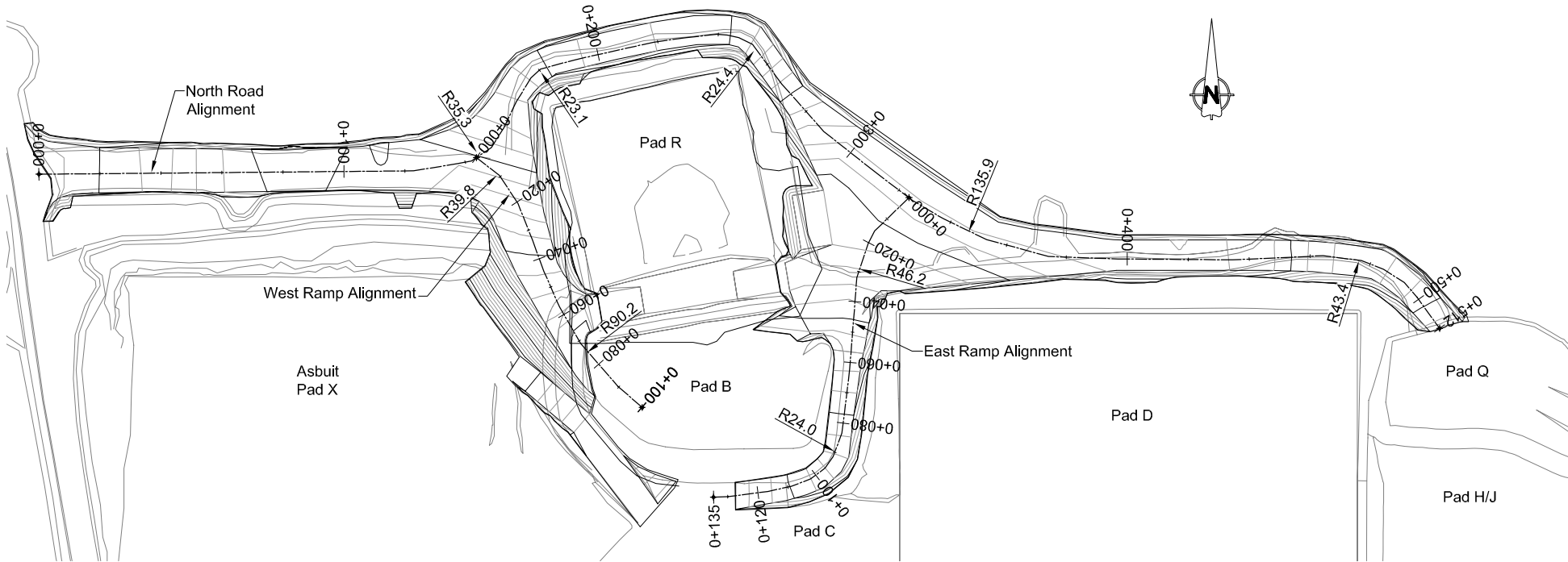
Horizontal Scale in Metres
Vertical Exaggeration 3X

REFERENCE

- For detailed design of the Doris North Camp refer to Engineering Drawings for the Doris North Camp Area, Doris North Project, Nunavut, Canada, Revision 1, SRK 2010.
- For detailed design drawings of the fuel tank farm refer to engineering Drawings for the Doris North Fuel Tank Farm, Doris North Project, Nunavut, Canada, Revision 1, SRK 2010.



NOTES

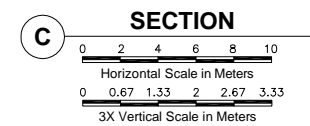
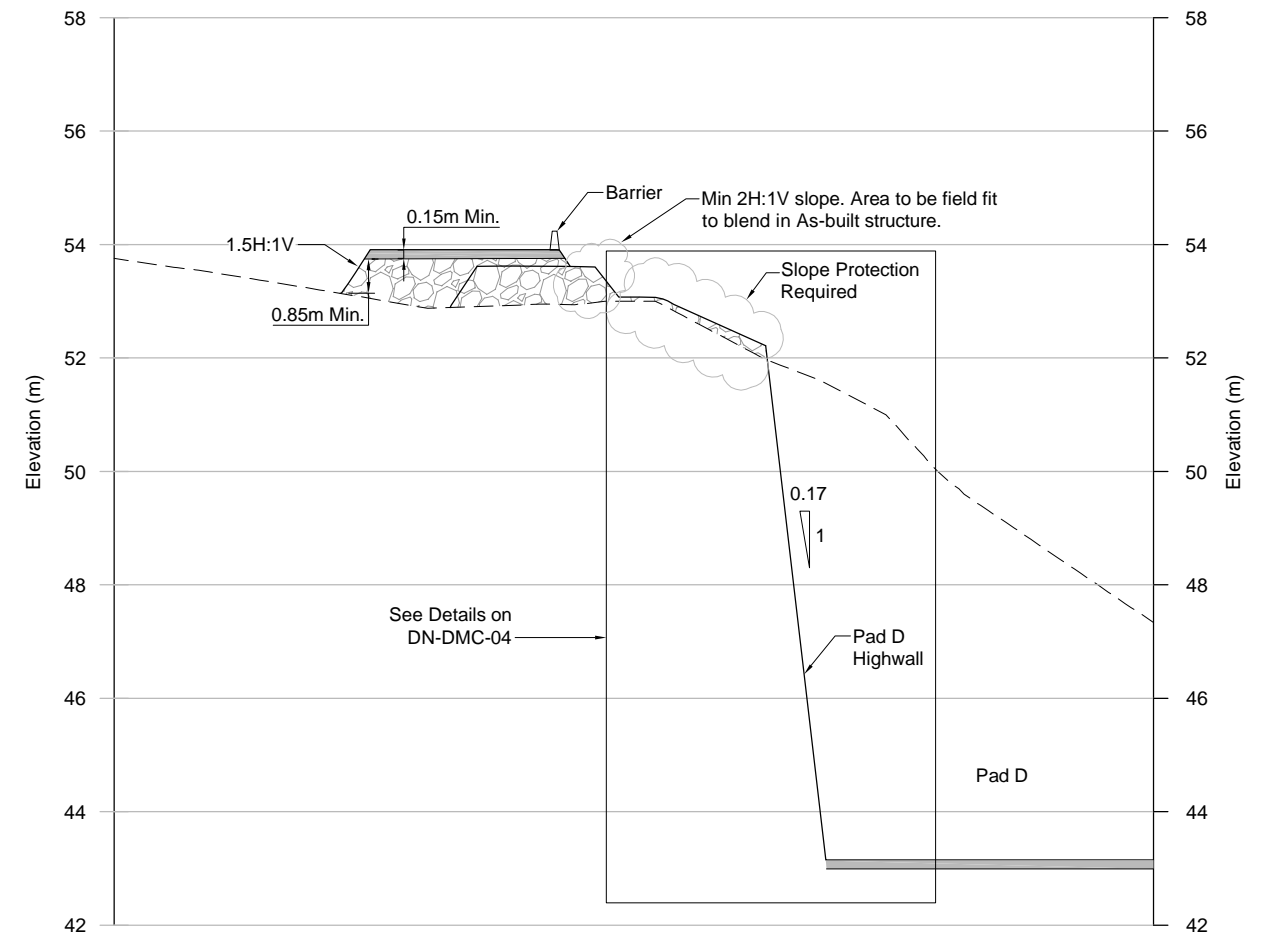
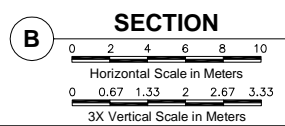
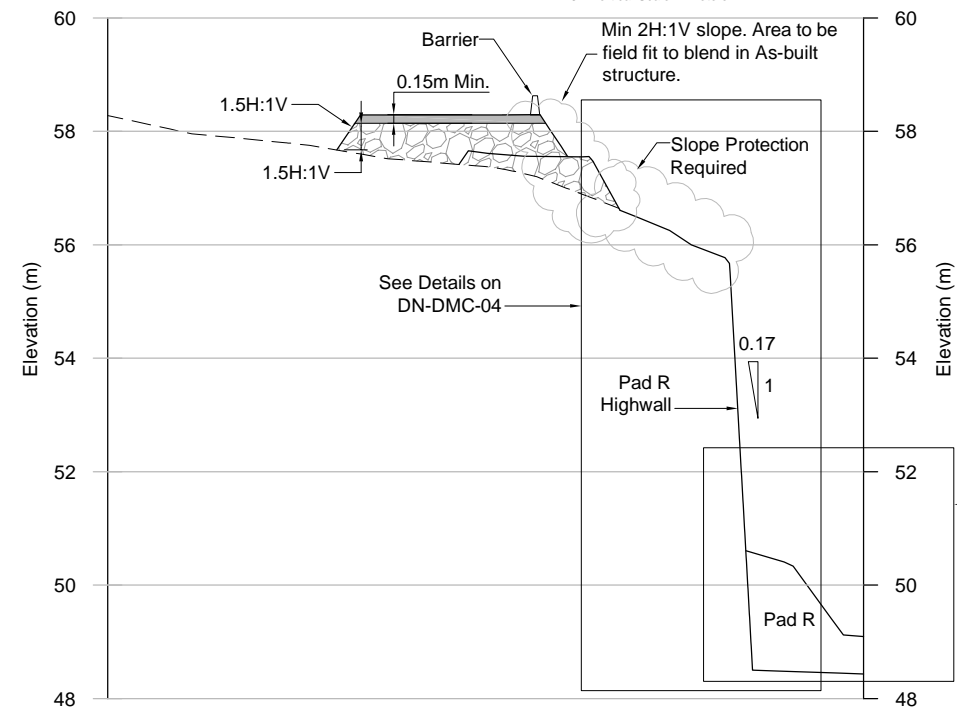
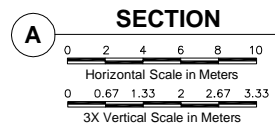
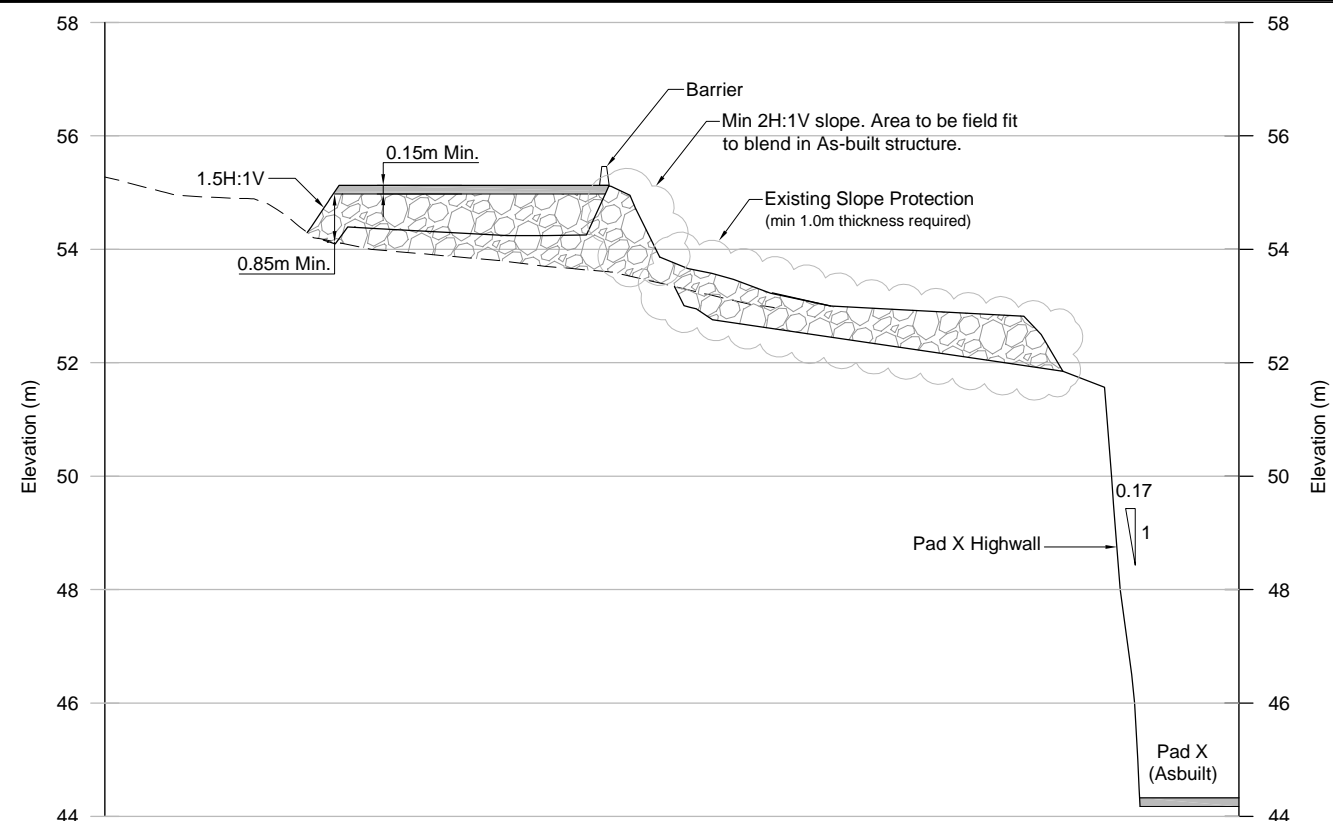
- All dimensions in meters unless noted otherwise
- The tie-ins to Pad R and Pad B should be blended into the existing pads and field fit as required to ensure that grades of less than or equal to 10% are maintained.
- Where the thickness of the pads is greater than 3.0m allow for the placement of barriers.
- Where the road crest is adjacent or above a highwall allow for the placement of barriers.
- The barriers are to consist of boulders larger than 1m in diameter, jersey-barriers (1.82m long X 1.37m high X 0.61m wide) or a rock fill berm 0.5m high. Maximum spacing between barriers is 3.3m.
- Notes on this drawing apply to all other active drawings.



**PLAN VIEW
WINDY CAMP TO PATCH 14**

Scale in Metres

								Original Drawings Stamped and Signed by Engineer			 ENGINEERS AND SCIENTISTS Vancouver			 NORTH AMERICA			Doris North Project		
											DESIGN: JBK			DRAWN: NV			REVIEWED: LW		
											CHECKED: LW			APPROVED: EMR			DATE: Aug. 24, 2010		
											FILE NAME: NORTH ROAD Plan&Profile.dwg			SRK JOB NO.: 1CH008 027			SRK DWG NO.: DN-DMC-20		
																	HOPE BAY MINING LIMITED		
																	DRAWING TITLE: Doris North Access Road Profiles		
																	NEWMONT DRAWING NO. HB+D-CIV-CIV-OND-0110		
																	SHEET 21 of 24		
																	REVISION NO. 0		



REFERENCE

1. For detailed design of the Doris North Camp refer to Engineering Drawings for the Doris North Camp Area, Doris North Project, Nunavut, Canada, Revision 1, SRK 2010.
2. For detailed design drawings of the fuel tank farm refer to engineering Drawings for the Doris North Fuel Tank Farm, Doris North Project, Nunavut, Canada, Revision 1, SRK 2010.

NOTES

1. All dimensions in meters unless noted otherwise.
2. Minimum design thickness of 1.0m must be maintained for all sections of the roads
3. Where the thickness of the roads is greater than 3.0m allow for the placement of barriers.
4. Where the road crest is adjacent or above a highwall allow for the placement of barriers.
5. The barriers are to consist of boulders larger than 1m in diameter, jersey-barriers (1.82 long X 1.37m high X 0.61m wide) or a rock fill berm 0.5m high. Maximum spacing between barriers is 3.3m.
6. Notes in this drawing apply to all other active drawings.

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Original Drawings
Stamped and
Signed by Engineer



DESIGN: JBK	DRAWN: LR	REVIEWED: EMR
CHECKED: LW	APPROVED: EMR	DATE: SEPT. 24,

P FILE NAME: North Road Section A-C.dwg



HOPE BAY MINING LIMITED

SRK JOB NO.: 1CH008 027

SRK DWG NO.:	DN-DMC-21
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Doris North Project

DRAWING TITLE:

Doris North Access Road
Sections (1 of 2)

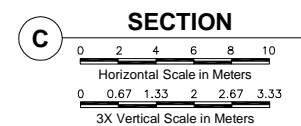
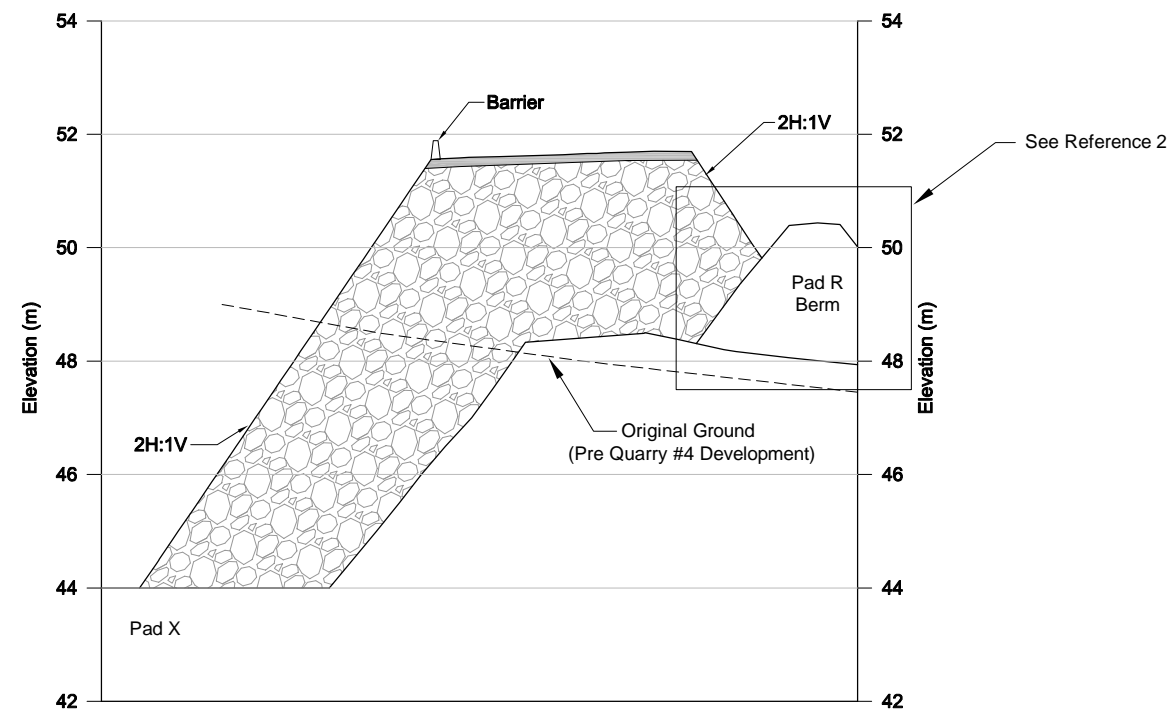
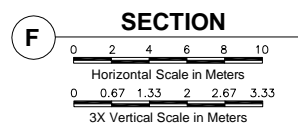
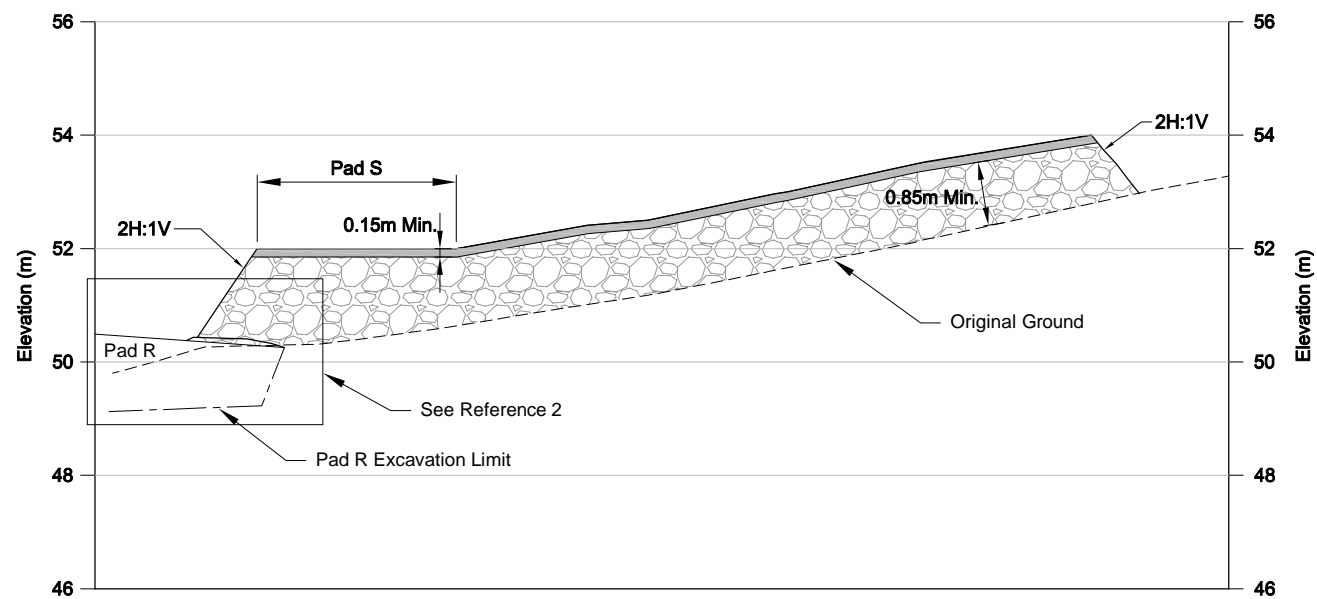
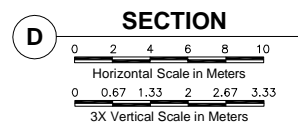
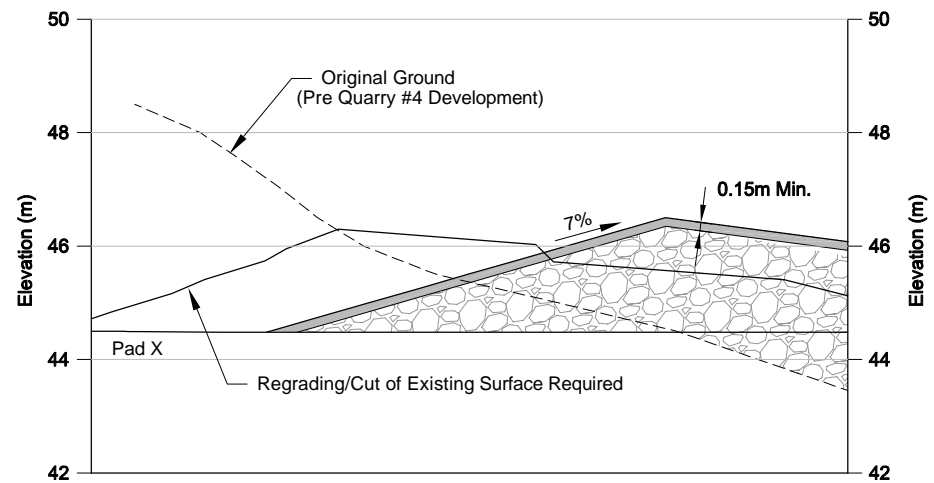
NEMONT DRAWING NO.

HB+D-CIV-CIV-OND-0111





SHEET	1
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2 OF 24

0



LEGEND

- | | |
|---|------------------------|
|  | Original Ground |
|  | Existing Ground |
|  | Surfacing Material |
|  | Run of Quarry Material |

REFERENCE

1. For detailed design of the Doris North Camp refer to Engineering Drawings for the Doris North Camp Area, Doris North Project, Nunavut, Canada, Revision 1, SRK 2010.
2. For detailed design drawings of the fuel tank farm refer to engineering Drawings for the Doris North Fuel Tank Farm, Doris North Project, Nunavut, Canada, Revision 1, SRK 2010.

NOTES

1. All dimensions in meters unless noted otherwise.
2. Minimum design thickness of 1.0m must be maintained for all sections of the roads.
3. Where the thickness of the roads is greater than 3.0m allow for the placement of barriers.
4. Where the road crest is adjacent or above a highwall allow for the placement of barriers.
5. The barriers are to consist of boulders larger than 1m in diameter, jersey-barriers (1.82 long X 1.37m high X 0.61m wide) or a rock fill berm 0.5m high. Maximum spacing between barriers is 3.3m.
6. Notes in this drawing apply to all other active drawings.

[illegible]

Memo

To:	Project File	Date:	December 1, 2010
cc:		From:	Murray McGregor, Maritz Rykaart
Subject:	Doris North Project Waste Rock Pile Stability Analysis	Project #:	1CH008.027.0300

This memo presents the results of a slope stability analyses for the waste rock pile at the Doris North Mill site. The stability analysis was carried out using the Morgenstern-Price method as applied in SLOPE/W. The model is set up using three materials: marine silt and clay, run of quarry foundation pad, and run of mine waste rock. Loading of the waste rock pile will occur at a rate that could outpace freezeback into the waste rock pile and therefore the entire waste rock pile is conservatively assumed to be unfrozen. The typical active layer thickness for uncovered marine silt and clay is about 1 m. However, for the purpose of this analysis, conservative active layer thickness of 2 m was used to compensate for the presence of the rockfill pad over the tundra soils which change the thermal regime.

Table 1 summarizes the material properties used in the analysis taken from the previous Doris Creek Bridge Abutments stability analysis.

Table 1: Material Properties

Parameter		Run of Quarry Foundation Pad	Waste Rock	Marine Silt and Clay Foundation
Saturated Unit Weight (kN/m ³)		20	20	18.5
Degree of Saturation		30%	30%	85%
Porosity		0.30	0.30	0.52
Volumetric Water Content		0.090	0.090	0.442
Unfrozen	Apparent Cohesion c' (kPa)	0	0	0
	Friction angle, ϕ^0	40	39	30
Frozen	Apparent Cohesion c' (kPa)	5	n/a	112
	Friction angle, ϕ^0	40	n/a	26

The analysis is carried out using a critical cross-section of the waste rock pile, taking into consideration the foundation slope and ultimate pile height. This typical section, complete with assigned material zones are presented in Figure 1 (note the overall slope angle is 2H:1V).

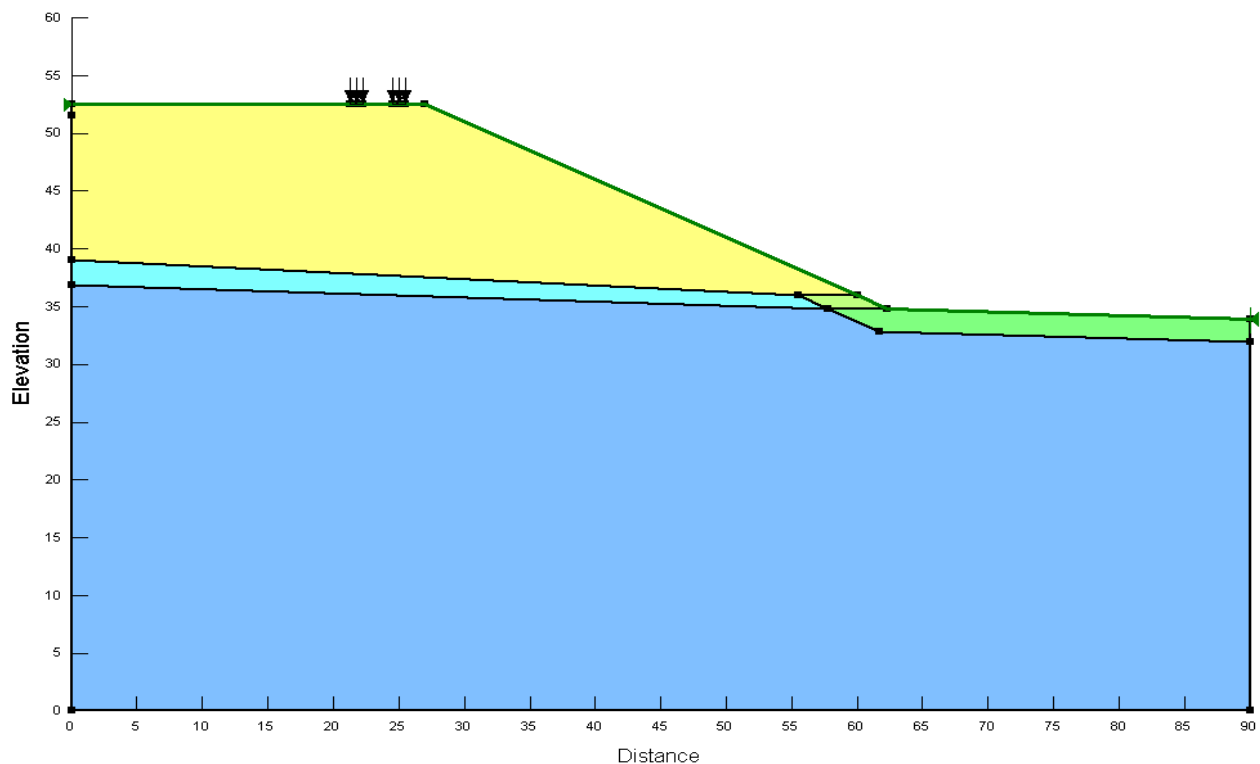


Figure 1: Critical Section of the Waste Rock Pile used in the Slope Stability Analysis

The critical slip surface was evaluated under two conditions; for a free standing waste rock pile without consideration of haul truck wheel loads at the crest, and with wheel loads. A sample calculation for haul truck wheel loading is included as Appendix A. Both rotational slip surfaces and blocks failure modes were considered in each case.

The Project site is located in a stable seismic zone of Canada with low peak ground accelerations. The waste rock piles are temporary, as they will be hauled back underground for ground support within 2 to 4 years of being stockpiled. For these reasons the stability analysis under seismic conditions was not assessed.

Graphic results for the critical slip surfaces of each analysis are presented in Appendix B. In each case where haul truck wheel loads are included, a load induced failure occurs near the crest of the pile. For the case where no wheel loads are considered, the critical slip surface appears as a shallow skin failure along the outer edge of the pile.

Table 2: Calculated Factors of Safety from SLOPE/W Models

Condition	Calculation Method	Factor of Safety	Critical Slip Surface Location
Haul Truck Wheel Loads Considered	Entrance and Exit	1.315	Load induced failure occurs near the crest of the pile.
	Block Specified	1.343	
Free Standing Waste Pile	Entrance and Exit	1.621	Shallow skin failure along the outer edge of the pile
	Block Specified	1.630	

A dump stability rating for the waste rock pile was completed in accordance with the guidelines set by the British Columbia Mine Waste Rock Pile Research Committee in their 1991 publication of “*Mined Rock and Overburden Piles: Investigation and Design Manual*”. For frozen foundation conditions the stability rating of the waste rock pile is 300 (Class I Stability), while for unfrozen foundation conditions the stability rating increases to 500 (Class II Stability). Details of the rating are provided in Appendix C.

The level of stability analysis presented in this memo is in accordance with the stated stability rating assessed for the waste rock pile.

The client should implement measures to ensure proper setback distances for haul trucks from the operating crest of the waste rock pile. Installation of thermistors to monitor foundation frost conditions is recommended to warn against possible onset of unfrozen conditions.

Appendix A

Sample Calculation of Haul Truck Wheel Loading

Subject Vehicle Loading on Waste Rock Piles Calculation Sheet 1 of 1

From Manufacturer Website:

CAT 773 Gross Operating Weight: 222,000 lbs = 100,698 kg

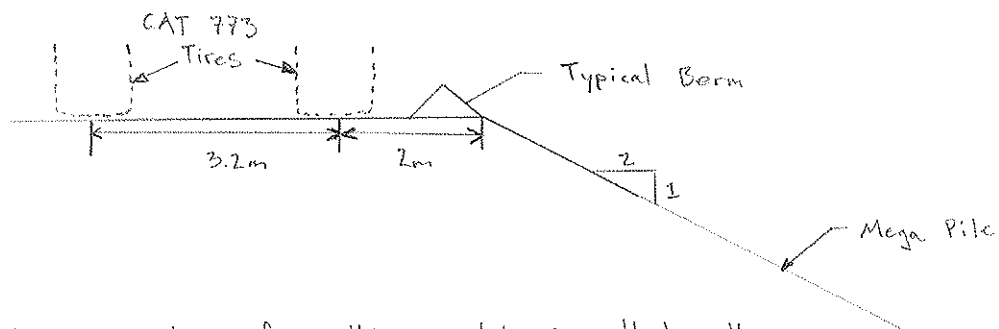
Load Weight Distributions: Front 35% Rear 65%

$$\text{Rear Tire Load: } (100,698 \text{ kg})(65\%) \left(\frac{1 \text{ tire}}{\text{Axle}(2)} \right) \left(\frac{9.81 \text{ N}}{\text{kg}} \right) = 321 \text{ kN}$$

Centerline Front Tire Width: 10.5 ft \approx 3.2 m

Offset from Slope Edge: (Berm width) + ($\frac{1}{2}$ tire width) \approx 2.0 m

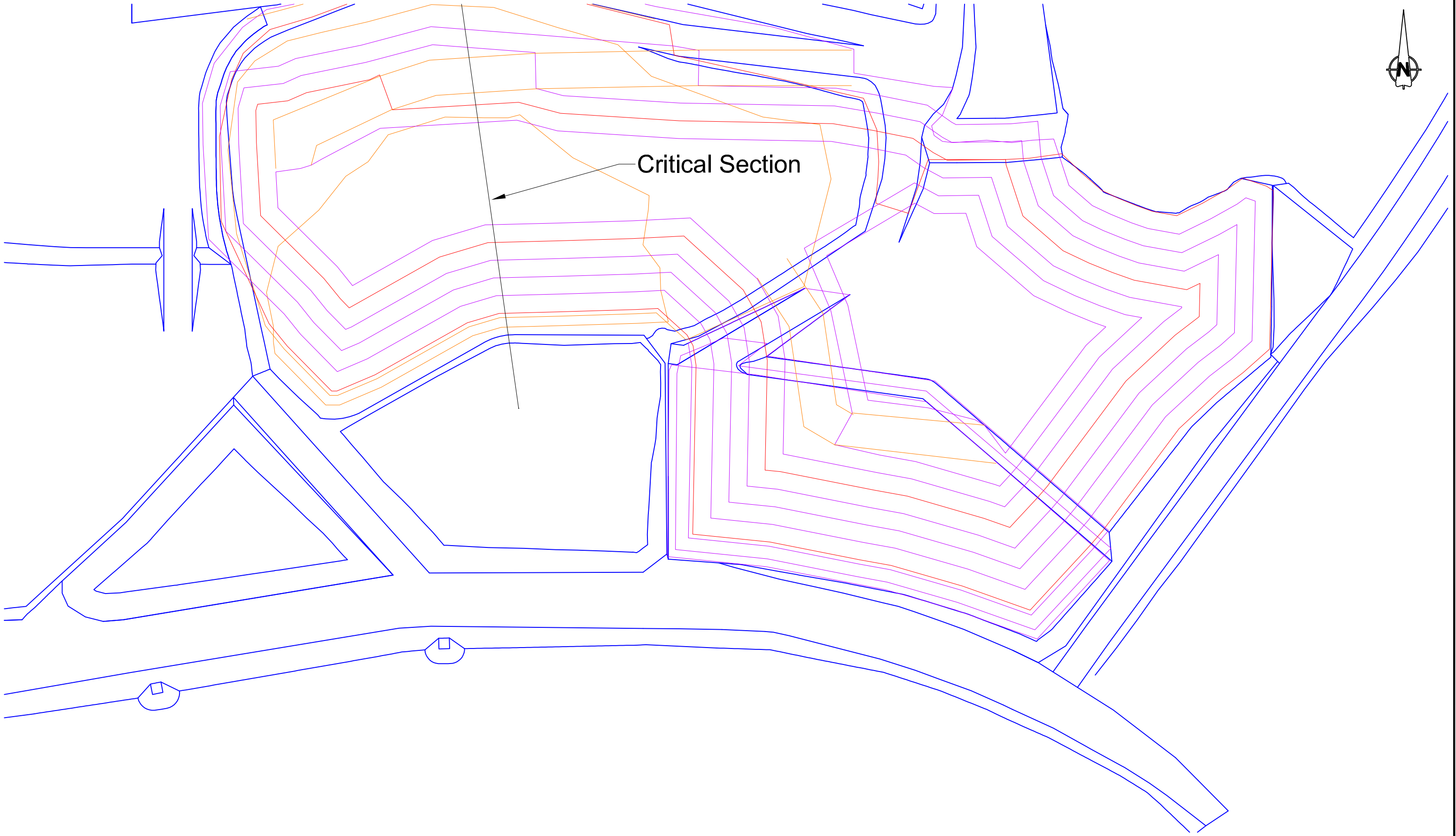
Typical Berm Width = 1 meter minimum



An assumption for this model is that the tires act as equal pressure loads over 1m^2 areas.

Appendix B
Graphic Results of Critical Slip Surfaces

J:\01_SITES\Hope Bay\LD408.027_Phase 1 and 2 Infrastructure Designs\0300_Phase 1 Engineering Design Support\Waste Rock\Slope V Analysis\MegaPiling.dwg

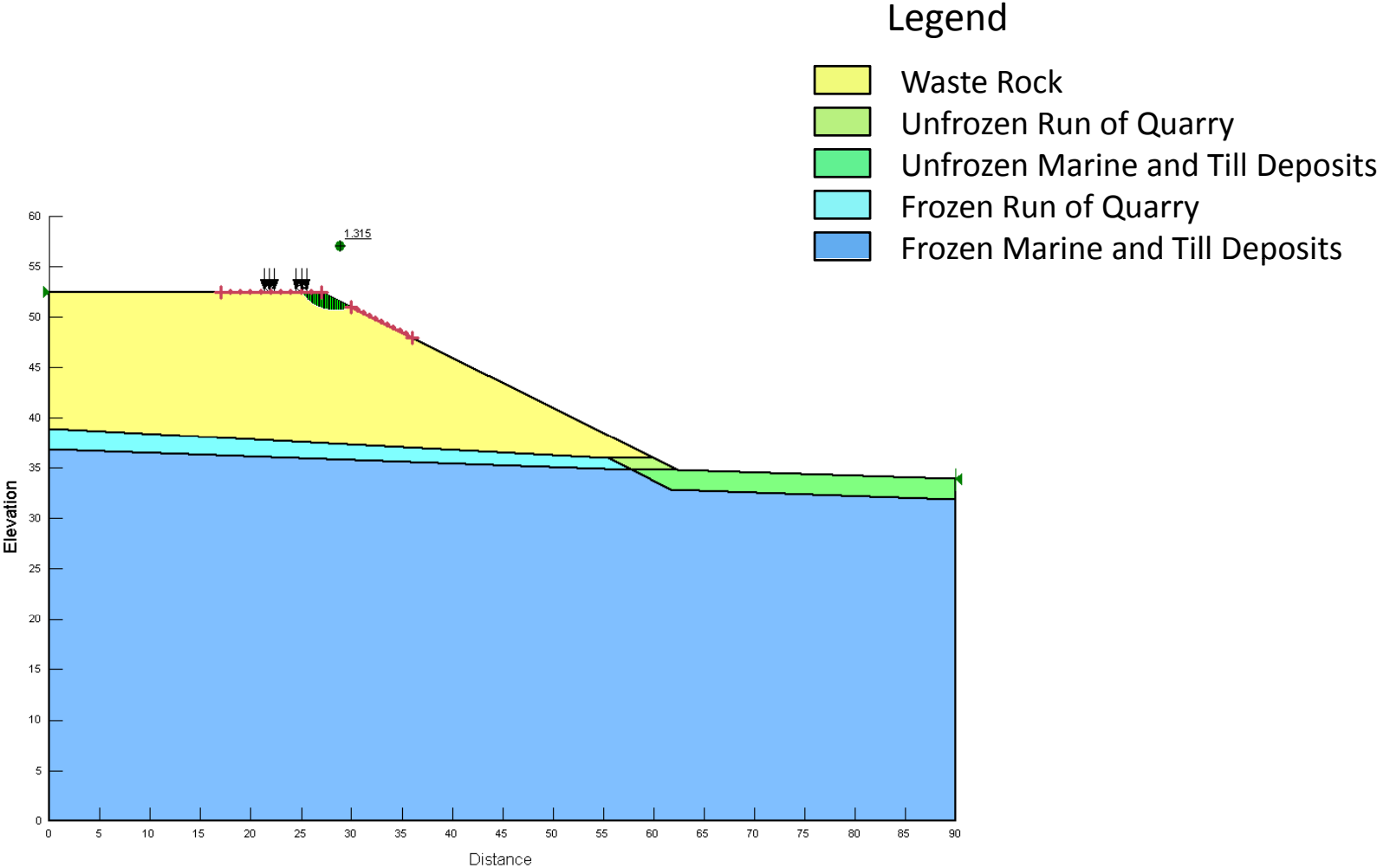


-	-			
NO.	DESCRIPTION	CHK'D	APP'D	DATE
REVISIONS				

HOPE BAY MINING LTD.

Doris North Project		
Waste Pile using all containment area.		
17/11/2010	-	1

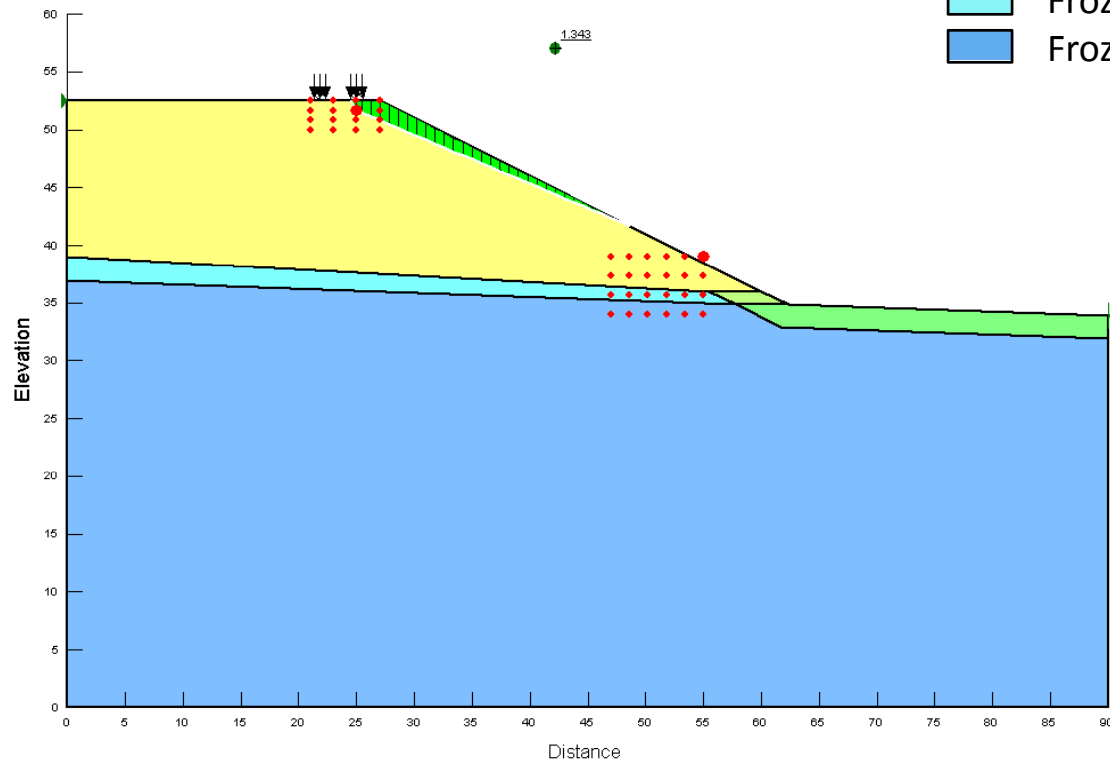
Doris North Waste Pile Section Defined by Entry and Exit
(Morgenstern-Price Method with Haul Truck Loading)



Doris North Waste Pile Section Defined by Blocks (Morgenstern-Price Method with Haul Truck Loading)

Legend

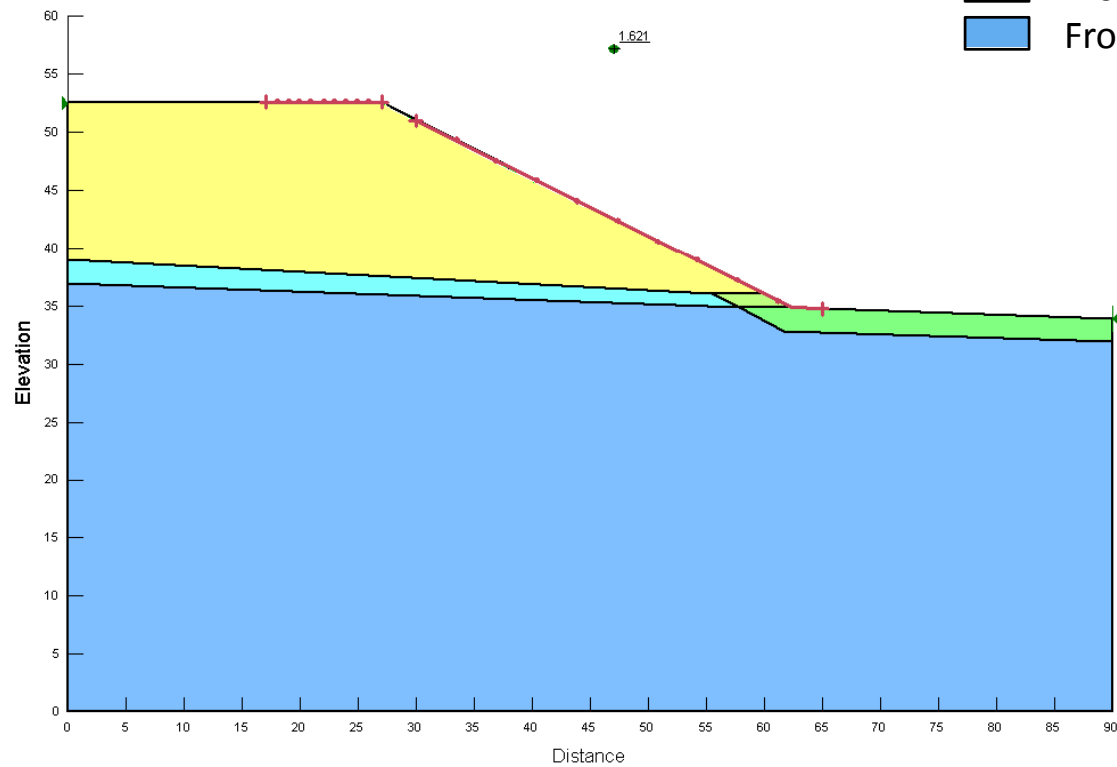
- Waste Rock
- Unfrozen Run of Quarry
- Unfrozen Marine and Till Deposits
- Frozen Run of Quarry
- Frozen Marine and Till Deposits



Doris North Waste Pile Section Defined by Entry and Exit (Morgenstern-Price Method without Haul Truck Loading)

Legend

- Waste Rock
- Unfrozen Run of Quarry
- Unfrozen Marine and Till Deposits
- Frozen Run of Quarry
- Frozen Marine and Till Deposits

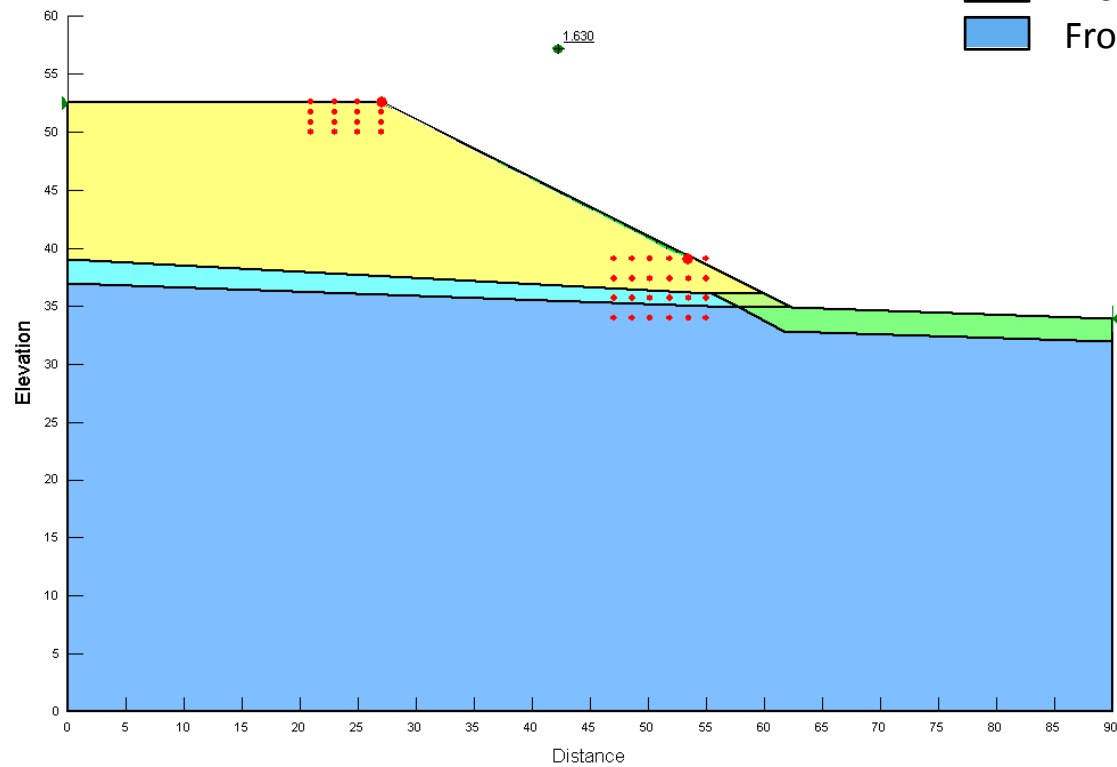


Doris North Waste Pile Section Defined by Blocks

(Morgenstern-Price Method without Haul Truck Loading)

Legend

- Waste Rock
- Unfrozen Run of Quarry
- Unfrozen Marine and Till Deposits
- Frozen Run of Quarry
- Frozen Marine and Till Deposits



Appendix C
Waste Rock Pile Stability Ratings

Subject Doris North Waste Rock Pile Stability Rating Sheet 1 of 1

Stability Factor	Description	Points
Dump Height	Maximum 21m	0
Dump Volume	532,00 tonnes ($\frac{m^3}{1.8 \text{ tonnes}}$) = 290,000 m ³	0
Dump Slope	2:1 = 28.6° Moderate	50
Foundation Slope	1% < 10°	0
Confinement	Unconfined	100
Foundation Type	Competent (frozen) / Weak (unfrozen)	200
Dump Material Quality	Strong - High	0
Construction Method	Lifts < 25m - Favourable	0
Piezometric / Climate	Moderate precipitation (intermediate)	100
Dumping Rate	5 m ³ /linear meter/day (Low)	0
Seismicity	Low	0

Maximum dumping rate:	Frozen Total	300
= 81,000 tonnes / quarter	Unfrozen Total	500
= 27,000 tonnes / month		
= 14,500 m ³ / month		
= 490 m ³ / day		
Dump span \approx 100m		
= 4.9 m ³ / linear meter / day		

Table 1: **Geochemical Classification and Management Recommendations for Proposed Waste Management Units**

Unit	Quantity (tonnes)	No. of Samples	Characteristics	Classification Based on NP/AP (% of samples)			Classification Based on TIC/AP (% of samples)			% Samples with S >0.25%	Classification based on Segregation Criteria*** (% of samples/quantity of rock)		Notes	Management
				non- PAG	uncertain	PAG	non- PAG	uncertain	PAG		non-Mineralized	Mineralized		
Basalt	203,000	98	Sulphur content highly variable, with less than 0.5% in 95% of samples, and localized concentrations up to 6.8% (10 cm vein). NPs were greater than 30 kg CaCO ₃ eq/tonne in 95% of the samples. TICs were typically elevated.	96%	2%	2%	91%	3%	6%	8%	92% 159,000 tonnes	8% 14,000 tonnes	Descriptions for all uncertain and PAG samples noted elevated sulphides.	Low Risk: separate any high sulphide material.
Gabbro	a minor subunit within basalt*	41	Sulphur content low with values between 0.01 and 0.32% in 95% of samples, with a maximum value of 0.74%. NP and TIC were consistently low with median values of 17 and 0.5 kg CaCO ₃ eq/tonne.	85%	10%	5%	8%	25%	67%	12%	0% n/a	100% *30,000 tonnes	Data set is biased toward the spatially clustered samples from 06TDD614.	Moderate Risk due to low NP: store in mineralized pile.
Diabase	143,000	34	Sulphur content consistently low, with all values less than 0.1%. NP and TIC are also low, with median values of 12 and 1.5 kg CaCO ₃ eq/tonne.	100%	0%	0%	62%	24%	15%	0%	100% 203,000 tonnes	0% n/a	Given the consistently low AP, should be managed as non-PAG.	Low Risk: confirm lithology.
Buffer Zone	58,000	24	Sulphur content highly variable, with median values of 0.15%, 95 th percentile values of 1.4%, and maximum values of 4.2%. NP and TIC were greater than 89 and 127 kg CaCO ₃ eq/tonne in 95% of the samples.	96%	4%	0%	100%	0%	0%	29%	71% 41,000 tonnes	29% 17,000 tonnes	Most PAG or uncertain samples contained sulphide or were logged as quartz veins.	Low Risk: separate any high sulphide material.
Alteration Zone	102,000	45	Sulphur content highly variable, with median values of 0.2%, 95 th percentile values of 1.9%, and maximum values of 3.4%. NP and TIC were typically high, but larger number of samples had lower NP values than observed in the buffer zone or the basalt.	87%	11%	2%	93%	3%	3%	46%	0% n/a	100% 102,000 tonnes	Most PAG or uncertain samples contained sulphide or were logged as quartz veins.	Moderate Risk: store in mineralized pile.
Stopes	n/a**	17	Sulphur content highly variable, with median values of 0.27%, 95 th percentile values of 2.3%, and maximum values of 5.4%. NP and TIC were highly variable, ranging from negligible to as high as 400 kg CaCO ₃ eq/tonne	41%	41%	18%	25%	38	38%	53%	n/a	n/a	Most PAG or uncertain samples contained or were logged as quartz veins.	n/a: all material from the stopes will be processed.
Totals	506,000										403,000 tonnes	163,000 tonnes		

Notes: * The gabbro is not defined in the geological model but is considered a minor component of the zone defined as basalt. A search of the geological database indicated that 6% of the core in the deposit area was gabbro. Therefore, conservatively neglecting core that is from ore zones, approximately 30,000 tonnes of gabbro could be present. This is taken from the block model quantities for basalt.

** all of the rock in the stopes is ore and will be processed.

***Segregation criteria based on rock type and then visual percent sulphides. For diabase, gabbro, alteration zone and stopes, rock type is the only criteria considered. For basalt and buffer zone rock the percent of samples with greater than 0.25% sulphur based on lab analyses was used to estimate the percent of material in each category.