Tahera Diamond Corporation

Waste Rock Management Plan

(Part 2, Kimberlite Ore, Coarse Processed Kimberlite and Recovery Circuit Rejects)

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Executive Summary

General

The Jericho Diamond Mine is being developed by Tahera Diamond Corporation (Tahera) in the Canadian Shield, north of Yellowknife. This document is Part 2 of the Waste Rock Management Plan (WMRP). It addresses the stockpiles that will be built to temporarily store kimberlite ore and permanently store coarse processed kimberlite (PK) and recovery circuit rejects (referred to as recovery plant rejects in earlier documents) that will be in place at the end of the operating life of the mine. Part 1, issued in May 2005, addressed the waste rock and overburden stockpiles. Detailed management plans for the fine PK will be provided in the PKCA Management Plan which will be submitted in early 2006.

This document has been prepared as a management tool and to fulfil the requirements of the Jericho Mine Water Licence (NWB1JER0410), Part D, Item 10 and Part H, Item 3 of the water licence. This document is intended primarily for use by Tahera and its designated contractors to ensure that appropriate management procedures are followed during construction and operation of the mine and that appropriate information is obtained by Tahera in relation to mine closure planning.

The plan includes the following:

- Detailed implementation for the construction of kimberlite ore stockpiles, coarse processed kimberlite stockpiles, and recovery circuit rejects stockpile;
- Design criteria and parameters for the processed kimberlite stockpiles;
- Operational volumes of materials for each pile based on processing all of the kimberlite resources;
- Stability assessments based on projected volumes; and
- Monitoring to be done during construction.

Furthermore, the waste rock management plan (Parts 1 & 2):

- Has been developed in accordance with the DIAND "Guidelines for Acid Rock Drainage Protection in the North";
- Describes decision criteria and operating procedures of how coarse processed kimberlite will be placed and managed during construction and mining;
- Includes an annual schedule for ore stockpiling, processed kimberlite generation by type, tonnage and destination over the term of the project; and,
- Includes a description of the methods used to construct the ore stockpiles and processed coarse kimberlite facilities such that generation of acidic drainage and/or metal leaching is limited.

Mine Plan

The mine plan consists of an initial open pit mining plan and, possibly, underground mining to mine between 4.0 and 5.0 million tonnes of kimberlite reserves and resources of which 2.0 to 2.5 million tonnes are classified as reserves and 2.0 to 2.5 million tonnes are classified as resources which will require processing to determine the true economics of the resource and possible reclassification into reserves. This determination will be made in the initial year of mine operations. Tahera now believes that under current market conditions for rough diamonds, this inferred resource kimberlite material will likely be economic, resulting in the processing of all kimberlite resources. As the inferred material is proven to be economic then the mine plan is most economically beneficial to remain as an open pit operation, providing additional 25% kimberlite reserve and resource material. The products discussed in this document consist of kimberlite from the various stages of the mining process.

Waste rock (including granite, till, overburden) management were the subject of WRMP Part 1. Fine PK will be handled as a slurry, and will be discussed in a separate PKCA Management Plan.

Kimberlite Quantities and Physical and Geochemical Properties

The life-of-mine quantities of kimberlite ore and coarse PK will be influenced by the economics of the inferred resources kimberlite material, pit slopes, actual kimberlite ore body configuration and the economic break point, if any, between open pit and underground mining.

Based on the premise that all kimberlite mineable reserves and resources will be fed to the processing plant, the resulting coarse PK is estimated to be approximately 2.0 million m^3. Kimberlite ore is reasonably competent and shows no indication of rapid weathering. The coarse PK is expected to comprise about 80% of the plant feed and with consist of kimberlite gravely sand. The recovery circuit rejects are a minor part of the project mine waste (3 to 5% of the plant feed) and will be comprised mainly of a medium to coarse sand. The remaining 15% will report as a slurry to the PKCA.

Geochemical testing indicated that kimberlite and coarse PK has a low potential to generate acidic or strongly alkaline drainage. However, seepage from these materials could contain slightly elevated concentrations of dissolved salts. The drainage is expected to be slightly alkaline, with pH's in the range of 8.0. The geochemistry of the recovery circuit rejects will be determined as part of the proposed monitoring plans. A precautionary approach has been taken to ensure drainage of any seepage from this material flows to the PKCA.

Kimberlite Ore Stockpiles

The kimberlite ore will only be stockpiled to separate mining and processing operations and provide a surge against weather and mine delays. It is expected that no more than one month's supply will be stockpiled at any given time (<30,000 m^3 of kimberlite).

Coarse PK Stockpile Design

Several disposal areas have been identified for the coarse PK. These areas include a small zone within the southeast part of the PKCA, the upstream toe area of the east and southeast dams, the area immediately west of the Jericho camp facilities within the PKCA watershed and the area immediately south of the east sump.

Stockpiles for coarse PK will be unlined. All runoff from these coarse PK stockpile areas will be captured in either the east sump, pit sumps or within the PKCA itself. Due to the uncertainties in the geochemistry of the recovery circuit rejects, this material will be stockpiled where the leachate runoff is naturally directed to the PKCA.

Foundation conditions at the coarse PK stockpile areas typically consist of bedrock with isolated small pockets of granular colluvial soils or till with, in some locations, a thin veneer of organic soil.

The stockpiles have been designed in order to meet appropriate physical stability criteria and to facilitate access by wildlife. Slopes will, in most cases have 10 to 15 m wide benches at 10 m vertical increments, which will provide an overall average slope of about 2.6H:1V.

Control Measures during Construction and Operation

In addition to placement within the stockpiles described above, minor amounts of coarse PK may be used in the construction of roads, embankments, dikes and dams.

Controls are in place in order to minimize the loss of nitrogen to the kimberlite during mining operations. The use of explosives in all aspects of the mining operation will be closely managed. Wet blast holes have been identified as one of the primary causes of explosives loss to waste rock due to the soluble nature of the bulk ANFO. Although the potential for wet-holes at Jericho is considered to be low due to the land-based nature of this pit and the presence of permafrost throughout the pit, contingency measures will be available to ensure that any wet holes are charged using appropriate methods for minimizing nitrogen losses. The Jericho site will be capable of manufacturing a wet hole emulsion product beginning in 2006 which will assist in minimizing explosive loss to the kimberlite in wet conditions.

The coarse PK stockpiles will be constructed so as to promote stability and generally encourage the aggradation of permafrost into the respective stockpile area. Key actions that may be included during the construction of these facilities include placement of an inspection road (which will act as a frozen berm) at or near stockpile toes and the placement of the initial lift of coarse processed kimberlite in winter, to the extent possible

Any seepage from the stockpiles will be addressed by natural grades to direct local runoff towards the east sump, open pit and/or to the PKCA.

Closure and Reclamation of the Waste Dumps

The target end land use for these areas will be wildlife habitat. Therefore, the aim of the reclamation plan is to promote, to the extent practical, rehabilitation of the land to this use. Key elements of the plan include vegetation prescriptions based on reclamation trials, regrading of most dump slopes and construction of ramps to allow safe caribou transit across the dump slopes. The coarse PK may also be used as a cover on the overburden and waste rock dumps should vegetation trials indicate a suitability of the material as a growth medium. Further details will be provided in the Closure and Restoration Plan (to which updates will be regularly submitted).

Verification and Monitoring Plans

The monthly quantities of ore processed, and the monthly quantities and storage locations of kimberlite ore, coarse PK and recovery circuit rejects will be recorded.

Geochemical monitoring will be carried out to confirm the geochemical properties of the kimberlite, and coarse PK. Results of the solids characterization work will be reported in an annual seepage and waste rock monitoring report.

Annual seepage surveys will be completed at each of the coarse PK stockpiles and related sumps.

A program of regular visual inspections, including an annual inspection by a geotechnical or civil engineer registered in Nunavut, will be implemented so as to evaluate the performance and condition of each stockpile.

Thermistors will be installed at two locations in one of the coarse PK stockpiles early in the life of mine. Temperature data will be collected monthly for a period of at least two years.

Table of Contents

List of Tables

List of Drawings

1 Introduction

The Jericho Diamond Mine is being developed by Tahera Diamond Corporation (Tahera) in the Canadian Shield, north of Yellowknife. This document is Part 2 of the Waste Rock Management Plan (WMRP). It addresses the stockpiles that will be built to temporarily store kimberlite ore and permanently store coarse processed kimberlite (PK) and recovery circuit rejects (referred to as recovery plant rejects in earlier documents) that will be in place at the end of the operating life of the mine. Part 1, issued in May 2005 (SRK 2005), addressed the waste rock and overburden dumps. Detailed management plans for the fine PK will be provided in the PKCA Management Plan to be submitted in early 2006.

This document has been prepared as a management tool and to fulfil the requirements of the Jericho Mine Water Licence (NWB1JER0410), Part D, Item 10 and Part H, Item 3 of the water licence. This document is intended primarily for use by Tahera and its designated contractors to ensure that appropriate management procedures are followed during construction and operation of the mine and that appropriate information is obtained by Tahera in relation to mine closure planning

The plan includes the following:

- Design criteria for the kimberlite ore stockpile, the coarse processed kimberlite stockpiles, and the recovery circuit rejects stockpile;
- Methodology for the construction of each stockpile;
- Operational volumes of materials for each stockpile based on processing all of the kimberlite resources;
- Stability assessments based on projected volumes; and,
- Monitoring to be done during construction and stockpile development.

Furthermore, the waste rock management plan (Parts 1 & 2):

- Has been developed in accordance with the DIAND “Guidelines for Acid Rock Drainage Protection in the North”;
- Describes decision criteria and operating procedures of how coarse processed kimberlite will be placed and managed during construction and mining;
- Includes an annual schedule for ore stockpiling, processed kimberlite generation by type, tonnage and destination over the term of the project; and,
- Includes a description of the methods used to construct the ore stockpiles and processed coarse kimberlite facilities such that generation of acidic drainage and/or metal leaching is limited.

2 Background Information

2.1 Geology

The Jericho Diamond Project is situated in the northern portion of the Slave Geological Province, within the Canadian Shield. The deposit consists of an elongate kimberlite pipe with a length of approximately 300 metres (m), a width of up to 100 m, and a depth of at least 350 m. The kimberlite is hosted by regionally extensive Archean granitic rocks, which vary locally and over very short distances from granodiorite to syenogranite, with associated pegmatite phases. The granitic rocks have been intruded by Proterozoic diabase dykes. Pleistocene glacial sediments occur sporadically throughout the region, and provide a 10 to 20 m cover over the kimberlite pipe.

The Jericho kimberlite was formed from multiple emplacement events, comprising a precursor dyke (JDF2) and three diatreme intrusive stages consisting of a northern (JDF4N), central (JDF6) and southern lobe (JDF4S). The precursor dyke is described as a hypabyssal kimberlite or kimberlite breccia with a finely crystalline, calcite and oxide-rich groundmass hosting macrocrysts of olivine as well as garnet, chrome diopside, ilmenite and mantle xenoliths. The northern and southern lobes are serpentinized, fragmental kimberlites containing olivine macrocrysts, mantle xenoliths as well as xenocrysts and macrocrysts of chrome diopside, phlogopite and ilmenite, and 5 to 10% crustal xenoliths of granodiorite, diabase and limestone. The central lobe is a clast-supported tuffisitic kimberlite, with a serpentinized groundmass hosting olivine macrocrysts, 5 to 10% crustal xenoliths of limestone and granodiorite, and mantle derived material.

The granitic country rock consists of a biotite +/- muscovite granite with associated pegmatite, which varies from weakly foliated to massive. A large diabase dyke crosses through the east side of the kimberlite, and will be encountered during mining. Minor quantities of andesite, aplitic dykes, and quartz veins are found along with the granite. The relative percentage (by length of drill core) of the rock types from the five 1999/2000 geotechnical drill holes are presented in Table 2.1.

Table 2.1: Rock Types by Percentage in 1999/2000 Geotechnical Drill Holes

Rock Type	Percentage	Length of Core (m)
Granite (both massive and foliated)	47	878
Kimberlite	20	384
Pegmatite	16	292
Diabase	13	240
Other	4	84
TOTAL	100	1,878

Sulphide mineralization is extremely rare in both the granitic rocks and kimberlite, and no occurrences of Yellowknife Supergroup Metasediments have been observed in the drill core or surface outcrops in the vicinity of the Jericho deposit.

2.2 Topography and Surficial Soils

The local relief is subdued as a result of previous glaciations, and is characterised by numerous lakes and many small ephemeral streams interspersed among boulder fields, eskers and bedrock outcrops. The water surface elevation in Carat Lake is approximately 470 m, and the topographic highs in the vicinity of the site facilities typically range from approximately 500 to a maximum of 550 m. More resistant rocks in the nearby Willingham Hills (east of the site) lead to small cliffs and elevations of up to 580 m. In the vicinity of the proposed open pit, slopes are gentle, and drainage is towards Carat Lake.

Drilling results and the surficial geological mapping indicate that the foundation conditions at the kimberlite ore and coarse PK stockpile areas consist of bedrock with isolated, thin soil deposits. The soil deposits typically consist of granular colluvium or till with, in some locations, a thin veneer of organic soil. All planned sites are underlain by permafrost.

2.3 Permafrost

Regional permafrost maps, complemented by site-specific thermal data and data from the nearby Lupin Mine, indicate the Jericho Diamond Project lies in a region of continuous permafrost. Permafrost is present everywhere except beneath large lakes. Available data suggests that the permafrost depth is about 450 m, which is consistent with published data from the Jericho area (EBA Engineering Consultants Ltd., 2004). Mining activities are not expected to extend below 300 meters from the surface. Furthermore the deposit is not located under a body of water and as such kimberlite mining should not contain any significant ground water.

In the surficial soils, the active layer typically ranges in thickness from less than one meter in organic soil to slightly more than three meters where well drained granular soils are present. The active layer thickness in exposed rock locally exceeds three meters.

2.4 Mine Plan

The mine plan consists of an initial open pit mining plan to mine 4.0 to 5.0 million tonnes of kimberlite reserves and resources of which 2.0 to 2.5 million tonnes are classified as reserves and 2.0 to 2.5 million tonnes are classified as resources which will require processing to determine the economics of the resource and possible reclassification into reserves. This determination will be made in the initial year of mine operations. If, as expected, given the current robust diamond market, this inferred resource kimberlite material is economic, then all kimberlite material mined will be processed as ore and the kimberlite ore stockpile will be generally less than one month’s plant supply. As the inferred material is proven to be economic, then the mine plan is most economically beneficial to remain as an open pit operation providing an additional 25% kimberlite reserve and resource material. The current management plan for kimberlite ore and coarse PK is based on the combined open pit, underground mining scenario.

Management of the stockpiles for kimberlite ore, coarse PK and recovery circuit rejects are the subject of this detailed plan. The management of the waste rock and overburden are the subject of a previously submitted detailed plan (Part 1 – May 2005). Fine PK will be handled as a slurry and will be discussed in a separate PKCA Management Plan.

The initial years of mining will be by conventional open pit methods with a combination of loaders and off-highway trucks. Loaders and hydraulic shovels with 5 to 10 m^3 buckets will be used. The bench height in the open pit is expected to be 7.5 m, with triple benching to 22.5 m in granite and single benching in less competent materials. The berm widths will typically be 8 m (10 m in overburden). The open pit will be approximately 400 m wide and 500 m long, covering an area of approximately 16 hectares (ha). The depth of permafrost is estimated to be 450m and therefore groundwater seepage into the pit will be limited to flow from the active layer. All of the coarse PK will come from the process plant rejects conveyors in a saturated state.

Should further analysis dictate that underground mining is the preferable method for later years of the mine life the underground would start at the level determined by the economics. Under this scenario, once open pit mining is complete, an underground decline will be driven at a -15% gradient to access the high grade Center lobe kimberlite ore from elevations below the bottom of the open pit. Open benching or sub-level caving will be used to extract the ore. Operating efficiencies and economics experienced during initial open pit operations will dictate the final level for transfer to underground mining.

Three distinct materials will be produced during mining, including:

- Overburden Waste Rock, comprised of a mixture of glacial soils overlying the kimberlite and surrounding waste rock
- Waste rock, comprised of granitic country rock, associated pegmatite phases and diabase dykes
- Kimberlite, of which approximately 80% will result in coarse PK to be stockpiled.

The overburden waste rock and waste rock will be stockpiled in a designated waste dumps and are the subject of Part 1 of the WRMP. Stockpiles for coarse PK or ore are the subject of Part 2 of the WRMP.

2.5 Production Schedule

The production rates for the coarse PK and recovery rejects coarse PK materials have been estimated based on processing all the kimberlite material mined and are summarized in Table 2.2. The percentage estimate for the coarse PK is estimated at 81% of plant ore feed and the coarse kimberlite rejects at 4% of plant feed. The remaining 15% will be fine PK which is pumped to the PKCA plant. These percentages are estimates and may vary +/- a few percentage points depending on actual processing characteristics. The estimated quantity of kimberlite has been included for completeness of materials to be mined.

Table 2.2: Estimated Production Rates for Kimberlite Ore and Processing Products

Year	Annual Production							
	Kimberlite Ore		Coarse PK		Recovery Circuit Rejects		Fine PK	
	Mmt	Mcm	Mmt	Mcm	Mmt	Mcm	Mmt	Mcm
1	0.63	0.39	0.51	0.32	0.03	0.02	0.09	0.06
2	0.72	0.45	0.58	0.36	0.03	0.02	0.11	0.07
3	0.72	0.45	0.58	0.36	0.03	0.02	0.11	0.07
4	0.72	0.45	0.58	0.36	0.03	0.02	0.11	0.07
5	0.72	0.45	0.58	0.36	0.03	0.02	0.11	0.07
6	0.72	0.45	0.58	0.36	0.03	0.02	0.11	0.07
7	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0
Totals*	4.23	2.64	3.43	2.14	0.17	0.11	0.63	0.40

Notes:
1. Mmt = million metric tonnes; Mcm = million cubic metres.
2. Stockpiled coarse PK and recovery circuit rejects are assumed to have a density of 1.6mt/m^3.
3. Stockpiled kimberlite ore is assumed to have a density of 1.6 mt/m^3.
4. Fine PK which is deposited in the PKCA is assumed to have a density of 1.6mt/m^3 to allow totalling of quantities.
5. The actual fine PK density will be addressed in the PKCA Management Plan.
6. Depending on actual processing rates and value economics of resource material and the coarse and fine PK, quantities may change.

3 Coarse PK Stockpile Materials

3.1 General

The kimberlite ore will only be stockpiled to separate mining and processing operations and provide a surge against weather and mine delays. It is expected that no more than one month's supply will be stockpiled at any given time (<30,000 m^3 of kimberlite).

The life-of-mine (LOM) quantities of coarse PK and recovery rejects PK (0.09 Mcm) are provided in Table 3.1 for the total kimberlite processing scenario. The density, taken as the estimated dry density following placement in a PK waste dumps or stockpile, is the basis of the volumetric estimates for each material. As discussed earlier, some of the coarse PK and recovery circuit rejects will be used in the construction of the PKCA structures. In addition, the coarse PK may get used as a cover material over the fine PK at closure. the estimate of coarse PK that might be used may well change as part of subsequent updates to the closure plan. However, based on the values in Table 3.1, 1.77 Mcm of coarse PK and 0.09 Mcm of recovery rejects would require permanent disposal.

Table 3.1: Coarse PK Materials - Total Estimated Quantities and Destinations

Source or Use	Approximate Quantity of Each Material			
	Coarse PK		Recovery Circuit Rejects	
	Tonnes	Volume (m^3)	Tonnes	Volume (m^3)
Produced	3,430,350	2,144,000	169,400	105,875
Used in PKCA Construction	100,000	62,500	20,000	12500
Used for PKCA Closure	500,000	312,500	0	0
Stockpiled	2,830,350	1,769,000	149,400	93,375

Notes:
1. Coarse PK and recovery circuit rejects are assumed at an in-situ density of 1.6mt/m^3
2. Depending on actual processing rates, value economics of resource material, construction requirements and closure requirements, the quantities may change.

The physical and geochemical properties of these materials are discussed in the following sections.

3.2 Physical Characterization

The physical characterization of kimberlite ore and coarse PK materials has been based on data gathered during various drilling and laboratory programs and the assessment of the product streams from the bulk samples of the kimberlite.

3.2.1 Kimberlite Ore

The kimberlite ore will be a run-of-mine product. Its gradation will depend on a variety of factors, but is expected to vary from silt and sand-sized particles to boulders. Observations reported in the EIS indicate the kimberlite is reasonably competent and shows no indication of rapid weathering.

3.2.2 Coarse Processed Kimberlite (Coarse PK)

The coarse PK will comprise a gravely sand made up of about 50 to 93% sand and 7 to 50% fine gravel from mechanical breakdown of the kimberlite ore. Processing plans call for the minimum and maximum particle sizes to be 0.1 mm and 19 mm respectively. The coarse PK is the light fraction from the dense media separation circuit in the processing plant and therefore is made up of the lighter minerals which comprise the majority of the kimberlite. The total tonnage of coarse kimberlite is estimated to be 3.43 million tonnes (mt). The density of the coarse processed kimberlite is expected to be about 1.6 to 1.65 t/m^3, which corresponds to an estimated volume of 2.14 million m^3. A portion of the coarse PK will be used in the construction of the PKCA earthen structures. Furthermore, a layer of coarse PK may be used as a cover surface over the PKCA as part of the closure plan. The final stored volume of the coarse PK will, therefore, be significantly less than 2.35 million m^3.

3.2.3 Recovery Circuit Rejects

Recovery circuit rejects will be produced as a result of kimberlite processing. They will comprise medium to coarse sand with some fine gravel. Particle sizes are expected to range from 1 to 8 mm. This material is the heavy fraction from the dense media separation, minus any diamonds, and is therefore made up of the heavier minerals in the kimberlite, such as ilmenite, chrome diopsite, garnet and phlogopite.

The total tonnage of the recovery circuit rejects is estimated to be approximately 0.17 million mt. The density of the recovery circuit rejects in a stockpile dump is expected to be similar to that of coarse PK, about 1.6 to 1.65 mt/m^3. The volume of the recovery circuit rejects is therefore estimated to be about 0.11 million m^3. Some of the material may be used for general construction purposes.

3.3 Geochemical Characterization

3.3.1 Sampling and Testing Programs

Detailed geochemical characterization of the kimberlite ore and coarse PK, was completed as part of the EIS. The programs included detailed core logging, examination of the development rock, mineralogical characterization, acid base accounting (ABA), solids ICP, leach extraction tests, seepage sampling, and supernatant characterization.

3.3.2 Kimberlite Ore

Petrographic examination of 5 samples from the crushed ore stockpile taken during the bulk sampling phase, indicate varying amounts of carbonate (from 0.5% to 25%) and only trace amounts of sulphides, which occur as pyrite when present (EIS Appendix D.1.4). Fizz testing indicated a strong reaction to weak hydrolchloric acid, confirming the presence of reactive carbonate minerals (EIS Appendix D.1.4).

Results of ABA analysis of 30 kimberlite samples indicated relatively low sulphide concentrations, high neutralization potentials (NP), and neutral to alkaline paste pH's (EIS Appendix D.1.4).

Shake flask extraction tests performed on 9 samples indicated that runoff in contact with stockpiled kimberlite ore will be alkaline, with pH's in the range of pH 8, and alkalinity in the range of 40 mg CaCO3 eq/l. Seepage from this material is expected to have relatively high total dissolved salts concentrations (EIS Appendix D.1.4) and generally low metal concentrations.

In summary, the geochemical testing indicated that kimberlite has a low potential to generate acidic or strongly alkaline drainage. The testing also indicates that runoff in contact with stockpiled kimberlite ore and/or kimberlite waste rock could contain elevated concentrations of total dissolved salts. The drainage is expected to be slightly alkaline, with pH's in the range of 8.0.

3.3.3 Coarse Processed Kimberlite

The diamond recovery process is essentially a mechanical process. Therefore coarse processed kimberlite is expected to be geochemically very similar to the ore. Results of specific tests on this material are summarized below. Mineralogical examination of coarse PK samples indicated that carbonate content ranged from 0.5 to 5% (EIS Appendix D.1.5). One sample had trace levels of disseminated sulphides as pyrite, and the other sample was devoid of sulphides. Results of ABA testing on coarse PK samples indicated that the coarse PK is net acid consuming with an insignificant sulphide content (less than 0.03% as S), very low sulphates (0.01 to 0.05% as S), and high neutralization potentials (EIS Appendix D.1.5). The neutralization potential ranged from 59 to 275 kg CaCo3 eq/mt. Paste pH's were strongly alkaline, ranging from 9.0 to 9.4.

Although supernatant samples were collected from the fine PK, results are mentioned here as an indication the chemistry of water in contact with PK. The chemistry of six fresh and aged PK supernatant samples was characterized by alkaline pH and moderate to elevated alkalinity, chloride, calcium, magnesium, potassium and sodium concentrations (EIS Appendix D.1.5). Heavy metal concentrations were generally very low, however barium, copper, manganese, molybdenum and zinc levels were slightly elevated in some of the samples and aluminum and nickel exceeded the criteria for freshwater aquatic life in more than one of the samples.

Sequential extraction tests on six samples indicated that alkalinity concentrations remained elevated in a second rinse, indicating that alkalinity levels could remain elevated. None of the metals exceeded the criteria for freshwater aquatic life.

3.3.4 Recovery Circuit Rejects

Recovery circuit rejects were not characterized separately in the original geochemical studies for the project and samples of this coarse PK reject stream are no longer available for testing, Sulphides were not observed in the recovery circuit reject materials by SRK in 1999. Nonetheless, it is possible that small amounts of sulphides from the original kimberlite ore, could accumulate in this material, and that light carbonate minerals such as carbonates could become depleted. Therefore, there is a slight potential that this material could be a source of acid generation and/or metal leaching.

As indicated in Table 3.1, the recovery circuit rejects comprise a relatively small amount of material. The leachate from this material will flow directly to the PKCA. Ongoing monitoring and testing of the leachate will determine if there any long-term ARD and water quality issue associated with this material.

4 Design of the Stockpiles

4.1 General Layout of the Stockpiles

The layout of the stockpiles for the kimberlite ore, coarse PK and recovery circuit rejects is illustrated in Drawing WRMP-P2-1 and was selected to:

- Maintain the location of the coarse PK stockpiles in a minimum the number of catchments potentially affected by drainage from the coarse PK dumps and stockpiles;
- Facilitate the operation of existing seepage control structures related to the coarse PK stockpiles by utilizing the east sump and the PKCA drainages;
- Optimize the offsetting impacts associated with the minimized project footprint and conformity with the natural relief in the immediate area; and
- Minimize haul distances and provide access to material for its potential use in reclamation.

The layouts of the stockpiles are approximate and have been based on existing 1-m topographic data. In relatively flat areas, where the stockpiles are close to the assumed catchment lines (as illustrated on Drawing WRMP-P2-2), ground survey methods will be used to accurately define the catchment limits prior to stockpile development.

The kimberlite ore stockpile will be situated immediately east of the plant facility and will be limited to blending piles representing, on average, less than 30,000 m^3 of material. The kimberlite ore stockpile will be graded so that any runoff is directed to the east sump for recycling or pumping to the PKCA.

Several disposal areas have been identified for the coarse PK. These areas include a zone within the southeast part of the PKCA (Area 1), the upstream toe area of the east and southeast dams (Area 2), the area immediately west of the Jericho camp facilities within the PKCA watershed Area 3) and the area immediately south of the east sump (Area 4). Depending on the actual quantities and the direction of surface drainage, the coarse PK stockpile at Area 4 may be amalgamated with Waste Rock Dump #2. However, as will be discussed in Section 5, this potential modification would not occur until later in the life of mine, i.e. when the other three coarse PK stockpile areas have reached their design capacity. Stockpiles for coarse PK will be unlined. All runoff from these coarse PK stockpile areas will be captured in either the east sump, pit sumps or within the PKCA itself.

Due to the uncertainties in the geochemistry of the recovery circuit rejects, this material will be stockpiled in Area 1, so that leachate runoff is naturally directed to the PKCA. In the event that geochemical testing and ongoing monitoring of the recovery circuit rejects demonstrates that there is no long-term ARD and water quality issue associated with this material, deposition of the recovery circuit rejects may shift to one of the other coarse PK stockpiles

4.2 Foundation Conditions at the Stockpiles

4.2.1 Kimberlite Ore Stockpile

Based on site reconnaissance and surficial geological mapping, the foundation conditions at the kimberlite ore stockpile area consist primarily of bedrock, with till under portions of the stockpile. Local permafrost data indicates that all areas are underlain by permafrost conditions.

4.2.2 Coarse PK Stockpile

Coarse PK stockpile Areas 1 and 2 will be integrated with the fine PK in the PKCA, and will therefore be discussed in the PKCA Management Plan. Site reconnaissance and surficial geological mapping indicates that the foundation conditions at coarse PK stockpile Area 3 consist primarily of bedrock. At coarse PK stockpile Area 4, the foundation conditions consist primarily of bedrock with isolated small pockets of granular colluvial soils or till with, in some locations, a thin veneer of organic soil. The small natural pond (East Sump) will be left in place as a water management control structure for the coarse PK drainage and plant area drainage. Local permafrost data indicates that all areas are underlain by permafrost conditions.

4.2.3 Recovery Circuit Rejects

As noted above, the recovery circuit rejects will be stockpiled, at least initially, in Area 1, the development of which will be discussed in the PKCA Management Plan. .

4.3 Stockpile Designs

4.3.1 General

The dimensions and storage capacities of the proposed stockpiles are provided in Table 4.1. Excluding the kimberlite ore stockpile, the total available capacity of the four stockpile areas is 1.94 Mcm. As noted in Table 3.1, the required stockpile capacity is 1.86 Mcm, which is based on 1.77 Mcm of coarse PK and 0.09 Mcm of recovery circuit rejects.

Table 4.1: General Dimensions and Storage Capacities of the Stockpiles

Site	Area (ha)	Approx. Crest Elev. (m)	max Height (m)	Capacity (Mt)	Capacity (Mcm)
Kimberlite Ore Stockpile	2	530	5	0.05	0.03
Coarse PK Stockpile & Recovery Circuit Rejects – Area 1 (south side of PKCA)	4.0	539	23	0.77	0.48
Coarse PK Stockpile – Area 2 (upstream of E and SE dams)	0.9	523	8	0.03	0.02
Coarse PK Stockpile – Area 3 (west of camp facilities)	4.0	539	19	0.50	0.31
Coarse PK Stockpile – Area 4 (south of East Sump)	8.4	539	24	1.81	1.13
Total Available Capacity (excluding live storage at the ore stockpile)				3.10	1.94

Notes:
1. The capacity stated for the kimberlite ore stockpile is based on several blending piles and incorporates less than one month of plant feed at full capacity
2. The recovery circuit rejects stockpile will be developed in stages within Area 1, according to the actual rate of production.

4.3.2 Kimberlite Ore Stockpile

The kimberlite ore stockpile will be a relatively small, “live” stockpile. The stockpile area will be sloped so that any drainage from the area will either flow to the East Sump for transfer to the PKCA or recycle to the process plant.

4.3.3 Coarse PK Stockpiles

Typical sections through the coarse PK stockpiles are provided in Drawing WRMP-P2-2. The overall slopes at these stockpiles will be about 2.6H:1V (21 degrees), though they will be made up of benches. The slope angles between benches are expected to about 1.4H:1V (35 degrees).

The thickness of each lift in the stockpile is expected to be approximately 5 m, but depending on the projected height of the structure and the number of benches, the lift thickness may be modified in order to develop relatively uniform bench heights.

The overall coarse PK stockpile areas will have nominal excess capacity at the final elevations indicated in Table 4.1.

4.3.4 Recovery Circuit Rejects Stockpile

Recovery circuit rejects will be stockpiled at Area 1, within the PKCA drainage area. The development of Area 1 will be discussed in the PKCA Management Plan.

Following evaluation of diamond recovery and geochemical characterization of the solids, deposition of the recovery circuit rejects may shift from Area 1 to a coarse PK stockpile closer to the processing plant (if testing indicates there are no ARD/ML concerns).

4.4 Stability Analysis

4.4.1 General

The stability of the coarse PK stockpiles has been considered in an overall context based on the generally favourable foundation conditions, moderate slope angles and low seismic risk. Stability analyses have been undertaken for the coarse PK stockpile structure located immediately east of the plant facilities (Area 4). This stockpile will have a final height of about 24 m.

4.4.2 Stability Criteria

A typical example of minimum factors of safety for waste rock dumps is provided in Table 4.2, the source of which is the guidelines published by the BC Mine Waste Rock Pile Research Committee in 1991.

Recent changes to the National Building Code of Canada have lead to replacement of the 475-year earthquake with the earthquake having a 2,475-year return period. Both earthquake events have been considered in the stability analyses.

Table 4.2: Guidelines for Minimum Design Factor of Safety – Waste Rock Dumps

Stability Condition	Case A – more severe	Case B – less severe
Stability of Dump Surface Short term (active) Long term (closure)	 1.0 1.2	 1.0 1.1
Overall stability (deep-seated) Short term (active) Long term (closure) Pseudo-static	 1.3 - 1.5 1.5 1.1 - 1.3	 1.1 - 1.3 1.3 1.0
Case A: Low level of confidence in critical analysis parameters Possibly unconservative interpretation of conditions, assumptions Severe consequences of failure Simplified stability analysis method (charts, method of slices) Stability analysis method poorly simulates physical conditions Poor understanding of potential failure mechanism(s)		
Case B: High level of confidence in critical analysis parameters Conservative interpretation of conditions, assumptions Minimal consequences of failure Rigorous stability analysis method Stability analysis method simulates physical conditions well High level of confidence in critical failure mechanism(s)		

4.4.3 Failure Modes

Given the granular nature of the coarse PK, the potential failure surfaces are likely to be relatively shallow and sub-parallel to the slope face.

4.4.4 Method of Analysis

The slope stability analyses were performed using 2-dimensional limit equilibrium analyses and the computer program SLOPE/W, which was developed by GEO-SLOPE International. Factors of safety for the various stability cases were determined using the Bishop and infinite slope methods of analysis.

4.4.5 Geometry and Input Parameters

A maximum height of 24 m was used for the coarse PK stockpile. During operations, the PK stockpile was assumed to have an overall downstream slope of 2.6H:1V (21 degrees), with an inter-bench slope of 1.4H:1V (35 degrees). Other input parameters have been selected based on judgment and are believed to be at or below typical mean values for the respective material (Table 4.3).

Table 4.3: Input Parameters used in the Stability Analyses

Parameter	Moist Unit Weight (kN/m^3)	Effective Strength Parameters		Water Table	Earthquake for Pseudo-Static Assessment
		c (kPa)	phi (degrees)		
Kimberlite	20	0 to 10	30	Elevated in pile	0.013 and 0.06
Till	22	5	32	In stockpile	
Bedrock	Failure surface prevented from intersecting the bedrock				

Two water tables were analysed. One was a "low" water table that was about 15% of the slope height. This water table is believed to be a conservative estimate of the water table during operations, assuming no weathering of the coarse PK occurs. The second was a "high" water table, reflecting the potential for weathering and the development of fines which leads to an elevated water table. This scenario could also apply under transient conditions due to an extended period of exceptional precipitation. The "high" water table was assumed to be about 40% of the slope height. Information gathered during operations will provide insights as to how much weathering, if any, of the coarse PK is likely to occur.

The earthquakes with 475 and 2,475-year return periods coincide with peak ground accelerations of 0.013g and 0.06g, respectively.

4.4.6 Results of Analysis

The results of the stability analyses for kimberlite are summarized in Table 4.4.

The minimum allowable factors of safety have been based on Case B in Table 4.2 for the following reasons:

- Conservative assumptions have been used in the analyses

- The consequences of failure are minimal as they do not involve loss of life or large scale environmental impacts
- The potential failure modes are relatively simple and are well suited to the analytical methods that have been used.

The factor of safety at the face of the stockpile is based on a simple infinite slope analysis. Since the material is end-dumped, the stockpile slope will conform to the angle of repose which in the absence of a water table, means that the dump face has a factor of safety of about 1.

Table 4.4: Summary of Critical Factors of Safety for Kimberlite Stockpile

Stability Condition	Suggested Minimum FOS	Calculated Factor of Safety (FOS)	Comments
Stockpile Surface Short Term	1.0	1.0	Bench face, at angle of repose
Deep Seated			During operations, c = 0 kPa
Short Term	1.3	1.5/1.4	Till foundation (low/high water table)
Pseudo-static	1.0	1.5/1.3	Till foundation, acceleration = 0.013g (low/high water table)
Pseudo-static	1.0	1.5/1.3	Till foundation, acceleration = 0.06g (low/high water table)
Deep Seated			During operations, c = 10 kPa
Short Term	1.3	1.8/1.5	Till foundation (low/high water table)
Pseudo-static	1.0	1.8/1.5	Till foundation, acceleration = 0.013g (low/high water table)
Pseudo-static	1.0	1.5/1.5	Till foundation, acceleration = 0.06g (low/high water table)

4.4.7 Conclusions

Stability analyses were completed for the maximum slope at the coarse PK stockpile using what are believed to be conservative input parameters. In all cases, the calculated factors of safety meet or exceed the minimum allowable values.

The analyses should be reviewed as additional information is obtained in the initial years of the mine operations.

5 Control Measures - Construction and Operations

This section describes the measures that will be implemented to minimize environmental impacts associated with mining and the construction and operation of the dumps and stockpiles.

5.1 Mine Operations related to Ammonia Management

Controls are in place in order to minimize the loss of nitrogen to the kimberlite during mining operations. The use of explosives in all aspects of the mining operation will be closely managed. Wet blast holes have been identified as one of the primary causes of explosives loss to waste rock due to the soluble nature of the bulk ANFO. Although the potential for wet-holes at Jericho is considered to be low due to the land-based nature of this pit and the presence of permafrost throughout the pit, contingency measures will be available to ensure that any wet holes are charged using appropriate methods for minimizing nitrogen losses. The Jericho site will be capable of manufacturing a wet hole emulsion product beginning in 2006 which will assist in minimizing explosive loss to the kimberlite in wet conditions.

5.2 Use of Coarse PK for Construction

Item 3, Schedule D of the Water Licence specifies the waste rock used for construction shall be non-acid generating, and shall meet the physical specifications outlined in specific design reports for each of the major facilities on site.

Geochemical testing indicates that the coarse PK is non-acid generating, with a limited potential for metal leaching. Physical specifications for construction materials are specific to the designated use. The coarse PK will be stockpiled, as a facing material, on the upstream slopes of the east and southeast PKCA dams. In addition, it may also be used as a frozen core material within the PKCA dams if it is found to be geotechnically suitable. Further details will be provided in the PKCA Management Plan, to be issued under separate cover.

5.3 Construction and Operation of Waste Dumps

5.3.1 Coarse PK Stockpiles

The coarse PK will be hauled to the stockpile locations using a front end loader for close proximities and loaded into trucks for longer hauls. The dumps will be developed over the life of the processing operation based on the following procedures:

- Over areas of till outside the PKCA, a layer of granite waste rock will be placed on the tundra to provide physical separation between organic soils and the stockpile material.

- To the extent practical, the granitic pad will be placed in the winter when the tundra is frozen, in order to develop a frozen foundation layer. In addition, where this occurs, the placement of the coarse PK will be managed to lock in the frozen conditions in the foundation layer
- The coarse PK stockpile in the area of the PKCA dams (Area 2) will be placed to avoid the entrapment of significant snow or ice lenses.

The general sequence of stockpile development is expected to be as follows: Areas 1 and 2 will be developed early in the operating life of the mine (additional details are provided in the PKCA Management Plan). Similarly, Area 3 will also be developed early in the mine life either concurrently or immediately following the development of Areas 1 and 2. Area 4 will likely be developed later in the operating life of the mine.

Depending on the actual quantities and the direction of surface drainage, Tahera may wish to amalgamate the coarse PK stockpile at Area 4 with Waste Rock Dump #2. By the time this potential requirement becomes evident, Tahera will have a reasonable understanding of the seepage quantity and quality associated with the coarse PK stockpiles. Furthermore, Tahera will have detailed topographic information over the area of the proposed expansion. It will, therefore, be possible to define the precise footprint of an appropriate eastward expansion of Area 4 towards Waste Rock Dump #2, i.e. so that the catchment of Ash Lake / Key Lake is not affected.

5.3.2 Recovery Circuit Rejects Stockpile

The recovery circuit rejects will be stockpiled in Area 1, which drains naturally into the PKCA. Ongoing monitoring and testing of the leachate will determine if there any long-term ARD and water quality issue associated with this material. Assuming this information confirms that no such issue exists with the recovery circuit rejects, they may be blended with coarse PK and stockpiled in areas close to the processing plant.

6 Closure and Reclamation

The target end land use for the stockpile areas will be wildlife habitat. Therefore the aim of the reclamation plan is to promote, to the extent practical, rehabilitation of the land to this use. Key elements of the plan include vegetation prescriptions based on reclamations trials, regarding of the stockpile slopes, construction of ramps for safe caribou transit across the slopes, and the potential use of coarse PK as a cover for the PKCA.

Details on closure and reclamation of the coarse PK stockpiles, will be presented in the Abandonment and Restoration Plan, Jericho Diamond Project.

7 Verification and Monitoring Plans

7.1 Solids Quantities

As specified in Part K, Item 13 of Water Licence NWB1JER0410, Tahera will record the monthly quantities of ore processed, and the monthly quantities and storage locations of kimberlite ore, coarse PK and recovery circuit rejects.

7.2 Solids Geochemistry

Geochemical monitoring will be carried out to confirm the geochemical properties of the coarse PK and kimberlite.

Coarse PK, fine PK and coarse kimberlite rejects samples will be collected once every two weeks during the first year of processing operations, with the frequency reduced to once per month for the remainder of the operations if it can be demonstrated that there is limited variability in the data. Samples will be submitted for testing of paste pH, reactivity with HCl, and total sulphur. Full ABA analyses, ICP-metals and uranium analyses would be performed on every 5th sample.

Results of the solids characterization work would be reported in an annual seepage and waste rock monitoring report.

7.3 Monitoring of Seepage

To supplement the routine monitoring programs outline in the Site Water Management Plan, an annual seepage survey will also be completed at the toe of each of the PK stockpile dumps, Although seepage is more likely to be detected on the down gradient side of the piles, any areas close to the catchments boundaries will also be checked for seepage. As specified in Water Licence NWB1JER0410, the survey will be completed in July or August. Samples would be submitted for a comprehensive suite of test parameters, including pH, conductivity, ORP, temperature, major ions, acidity, alkalinity, metals and nutrients. Standard QA/QC procedures for water sampling including collection of field, travel and method blanks as well as duplicate samples will be included in the program.

The results of the monitoring programs will be reported in an annual seepage and waste rock monitoring report.

7.4 Visual Inspections

During the active development of each of the coarse PK stockpiles, site staff will carry out daily inspections in relation to the performance and condition of each structure, including slope stability, seepage and conformity to the development footprint. When stockpile activity ceases on an interim or seasonal basis, the inspection frequency will shift to monthly. Following the completion of a stockpile, inspections will continue on a semi-annual basis to closure.

Depending on the performance of each of these facilities, the inspection frequency may have to be increased and possibly supplemented by additional monitoring methods.

Tahera will develop a system for recording and analysing their visual observations, and will assign the responsibility to appropriate personnel for completing and analysing the results of these inspections, for maintaining written records and, where appropriate, for implementing corrective actions.

A geotechnical or civil engineer registered in Nunavut will make an annual inspection of these facilities each summer. His inspection report will be filed in a timely manner so that, if required, construction activity or modifications to these structures can be implemented prior to the next freshet.

7.5 Thermal Monitoring

Thermal monitoring is not critical to the performance of the stockpiles. However, to provide information that will be useful for closure planning and post closure monitoring, thermistors will be installed in one of the coarse PK stockpiles that is constructed early in the operating life of the mine, i.e. probably the stockpile in Area 1, so as to obtain the longest possible data record. The thermistors will be installed in two locations within the stockpile once the stockpile is sufficiently developed. The thermistor readings will be collected on a monthly basis for a period of two years, or at least until a clear pattern has been established. Thereafter the reading frequency can be reduced to quarterly.

This report **"Waste Rock Management Plan, Part 2** (**Kimberlite Ore, Coarse Processed Kimberlite and Recovery Circuit Rejects)"** has been prepared in conjunction with Tahera personnel and by SRK Consulting (Canada) Inc.

Cam Scott, P.Eng.
Principal Engineer

Kelly Sexsmith, P.Geo.
Senior Environmental Geochemist

8 References

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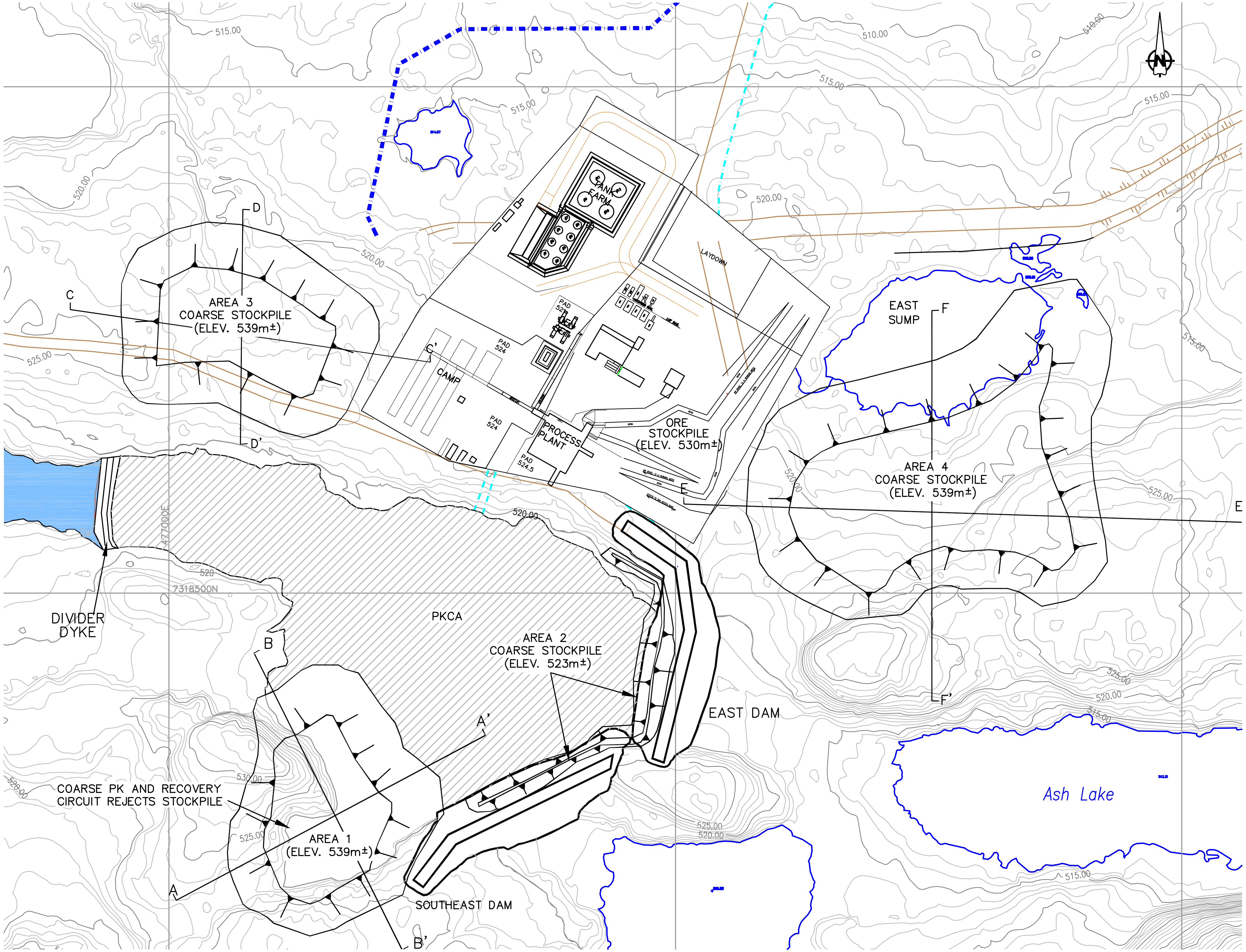
Drawings



NOTES:

1. THE LAYOUTS OF THE STOCKPILES ARE APPROXIMATE AND HAVE BEEN BASED ON EXISTING TOPOGRAPHIC DATA.
2. IN RELATIVELY FLAT AREAS WHERE THE STOCKPILES ARE CLOSE TO THE ASSUMED CATCHMENT LIMIT (I.E. THAT SEPARATES THE STOCKPILE FROM ASH LAKE AND KEY LAKE CATCHMENT), GROUND SURVEY METHODS WILL BE USED TO ACCURATELY DEFINE THE CATCHMENT LIMIT.
3. A BUFFER ZONE WILL BE ESTABLISHED BETWEEN THE STOCKPILE TOE AND THE ASH/KEY LAKE CATCHMENT ON A FIELD FIT BASIS IN AREAS WHERE GROUND SURVEY METHODS ARE REQUIRED (SEE NOTE 2).
4. THE RECOVERY CIRCUIT TAILINGS WILL BE DEPOSITED IN AREA 1. DETAILS WILL BE PROVIDED IN THE PKCA MANAGEMANT PLAN, WHICH WILL BE ISSUED IN EARLY 2006

TAHERA CORPORATION
JERICHO LAKE SOUTHWEST EXTENSION

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Scale of Photography: 1:10 000
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Survey control based on: UTM Projection, NAD 27, Zone 12
Compiled by The ORTHOSHOP, Calgary, October 1995.
WO 7423

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REFERENCE DRAWINGS		REVISIONS					ISSUE AUTHORIZATION			

DETAILED DESIGN

SRK Consulting
Engineers and Scientists

DESIGNED BY: DJ/CS DATE: DEC. 2005	DRAWN BY: JM DATE: DEC. 2005
CHECKED BY: CCS DATE: DEC. 2005	DISCIP. ENGR. DATE:
PROJ. MGR: DATE	PROJ. ENGR. DATE
SRK PROJECT NUMBER: 1CT004.09	

Tahera
Diamond Corporation

JERICHO DIAMOND PROJECT

LAYOUT OF STOCKPILES

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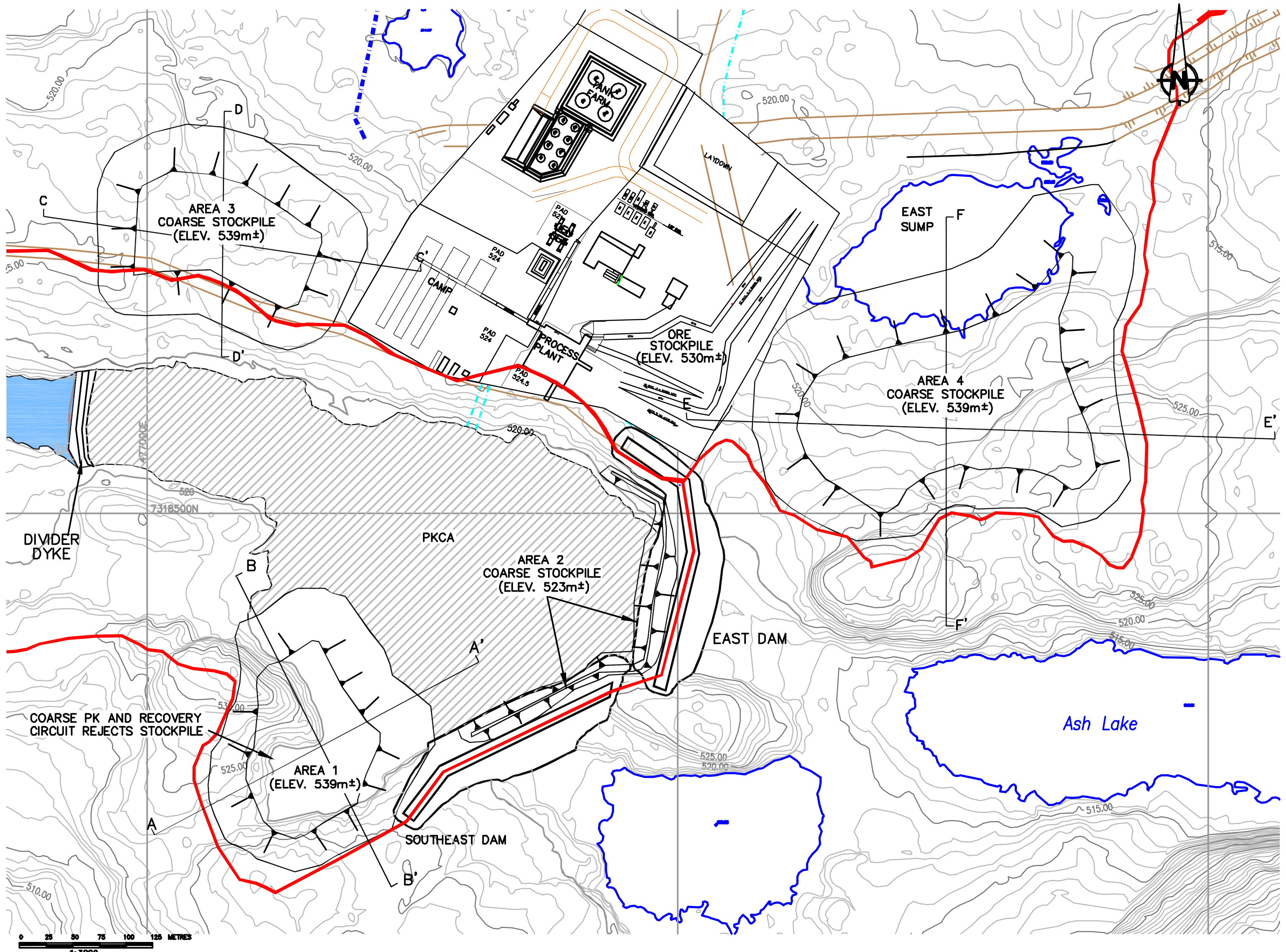

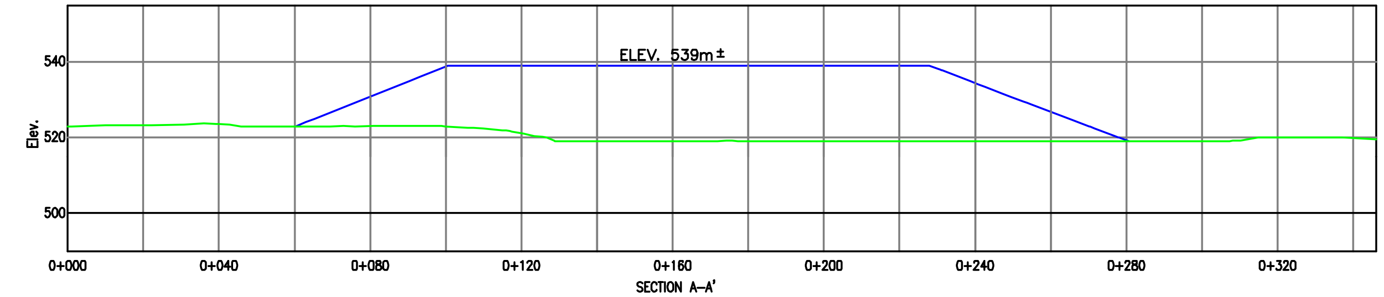

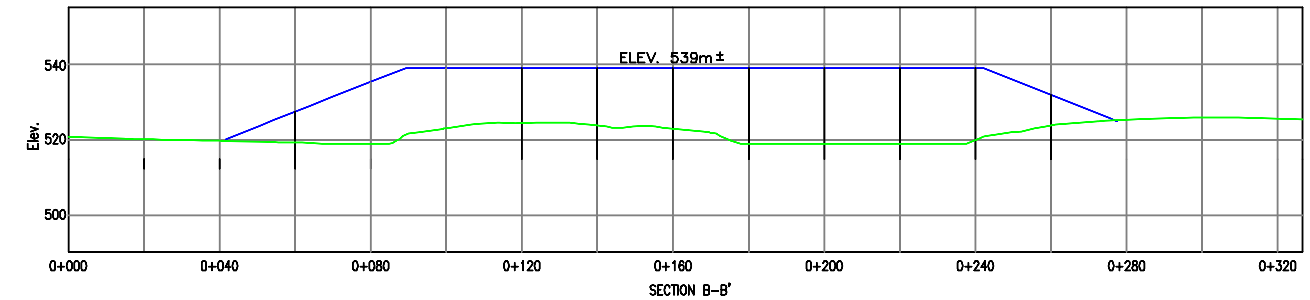

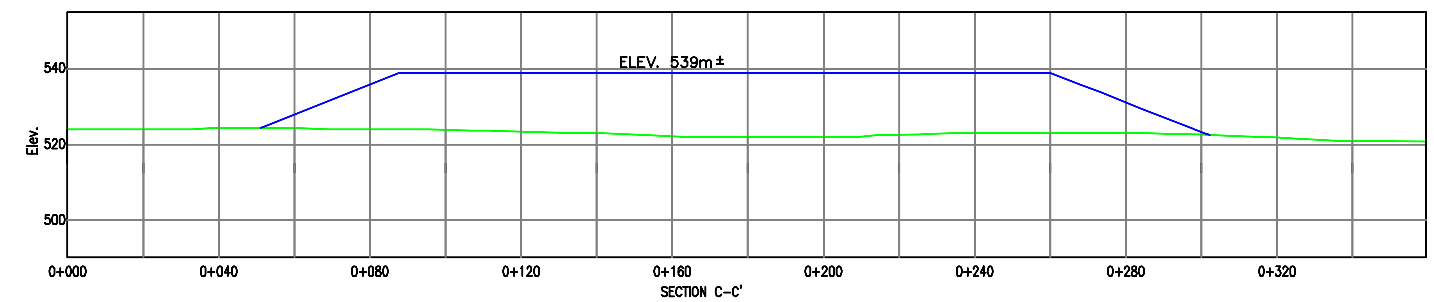

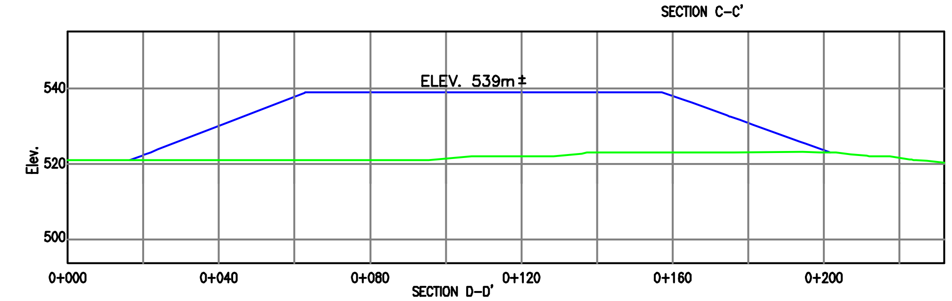

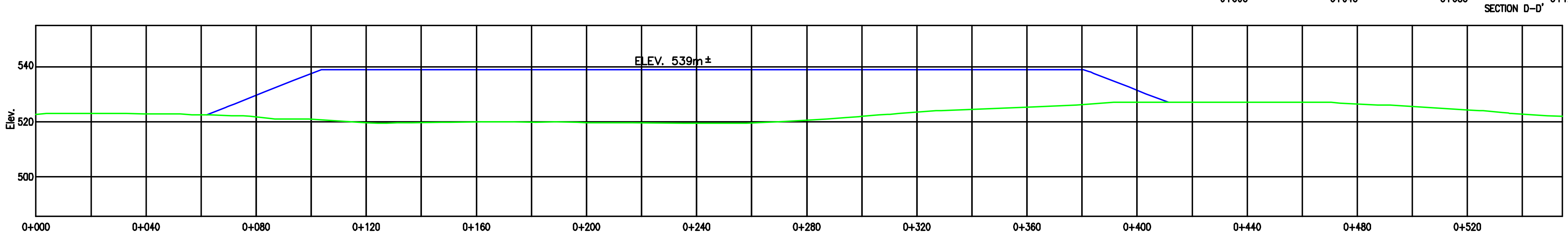

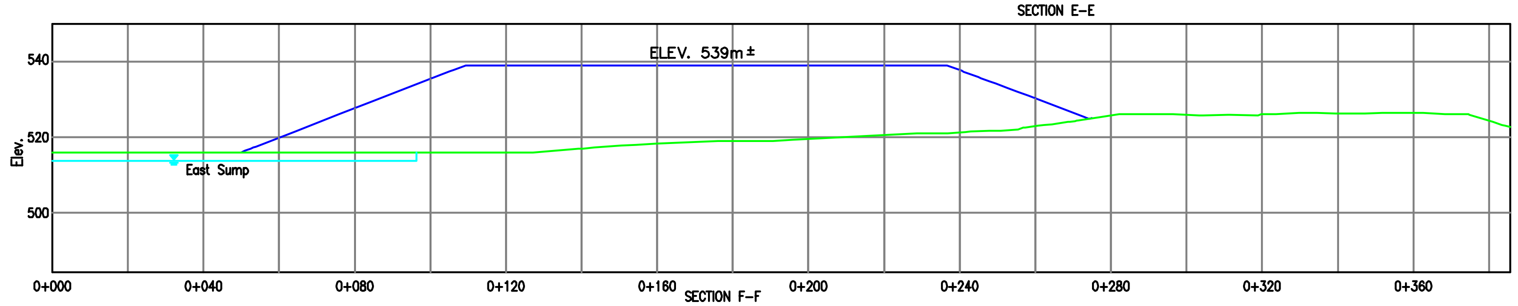

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SECTIONS THROUGH SELECT STOCKPILES

DRAWING NUMBER: WRMP – P2 – 2

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