



**AGNICO EAGLE**

**MEADOWBANK GOLD MINE**

**2016 WATER MANAGEMENT REPORT AND PLAN UPDATE**

**NOVEMBER 2017**

**VERSION 02**

## **EXECUTIVE SUMMARY**

Agnico-Eagle Mines Ltd. Meadowbank Division (AEM) is operating the Meadowbank Gold Mine (the Mine), located on Inuit-owned surface lands in the Kivalliq region approximately 70 km north of the Hamlet of Baker Lake, Nunavut. The mine is subject to the terms and conditions of both the Project Certificate issued in accordance with the Nunavut Land Claims Agreement Article 12.5.12 on December 30, 2006, and the Nunavut Water Board Water Licence No. 2AM\_MEA1525 issued on July 23, 2015 (NWB, 2015).

This report presents an updated version of the Water Management Plan 2015 and provides a revised site-wide Water Balance. The revised Water Balance determines the demand and storage requirements of water over the life of the mine. The storage strategies and required transfers will be discussed at large. Certain concepts within the water balance, including pit flooding, remain at the conceptual stage for now and will be further detailed in the Final Mine Closure and Reclamation Plan to be submitted one year prior to final closure in accordance with the current Type A Water License.

The necessity of this particular water management update follows the Water Licence 2AM\_MEA1525 Modification Request initiated by AEM regarding the modification of the tailings management strategy which includes the deposition of tailings inside the Goose and Portage Pits. This modification to the plan is part of the mitigation plan developed regarding the situation of the Central Dike Seepage and the recommendations of the Meadowbank Dike Review Board (MDRB, 2017b).

The principal additions to this update are:

- Earlier closure of the South Cell TSF
- Disposal of the Meadowbank tailings inside Goose Pit
- Disposal of the potential Whale Tail Pit tailings inside Portage Pit
- Review of the flooding activities in accordance with new deposition strategy
- The tailings deposition parameters used for the model following the results of the 2016 bathymetries analysis and consolidation analysis performed by SNC-Lavalin;
- The Central Dike seepage status update;

The 2016 Water Management Plan Update also includes the In Pit deposition Water Balance and Water Quality Forecast Update (Appendix B). The Freshet Action Plan and Ammonia Management Plan will be reviewed following the approbation of the modification request by the Nunavut Water Board (NWB).

The Water Management Plan will be updated on a yearly basis as required by the Nunavut Water Board Water License 2AM-MEA1525. Recommendations obtained during the 2016 Meadowbank Annual Report Review will be included in the 2017 Water Management Plan to be issued in March 2018.

**DOCUMENT CONTROL**

Version	Date (YM)	Section	Page	Revision
1	March 2014	ALL	-	Revision for the 2012 Water Management Plan (by SNC) according to the updated Life of Mine and water management strategies
2	March 2015	ALL	-	Revision for the 2013 Water Management Plan (by AEM) according to the updated Life of Mine and water management strategies
3	October 2015	ALL	-	Update of sections according to Water License renewal conditions
4	March 2016	ALL	-	Revision of the 2014 Water Management Plan (by AEM) according to the updated Life of Mine and water management strategies
5	March 2017	ALL	-	Revision of the 2015 Water Management Plan (by AEM) according to the updated Life of Mine and water management strategies
6	November 2017	ALL	-	Revision of the 2016 Water Management Plan (by AEM) according to Water Licence Modification Request related to in-pit disposal

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Environmental Department

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## **Section 1.0 - INTRODUCTION AND BACKGROUND INFORMATION**

### **1.1 INTRODUCTION**

Agnico-Eagle Mines Ltd. (AEM) has been operating its Meadowbank Gold Mine since 2008, officially beginning production in 2010. The mine is located approximately 70km north of the Hamlet of Baker Lake, Nunavut. The mine is subject to the terms and conditions of both the Project Certificate issued in accordance with the Nunavut Land Claims Agreement Article 12.5.12 on December 30, 2006, and the Nunavut Water Board Water Licence No. 2AM-MEA1525 issued on July 23, 2015 (NWB, 2015).

This report presents an updated version of the Water Management Plan 2016 and provides a revised site-wide water balance that determines the demand and storage requirements of water over the life of the mine (LOM). The storage strategies and required transfers will be discussed at large. Certain concepts within the water balance, including pit flooding, remain at the conceptual stage for now and will be further detailed in the Final Mine Closure and Reclamation Plan which is to be submitted one year prior to mine closure in accordance with the Type A Water License.

The necessity of this particular water management update is related to the Nunavut Water Board Water Licence No. 2AM-MEA1525 (NWB, 2015) modification request regarding the integration of in-pit tailings deposition practice to the global Meadowbank tailings management plan. This modification will trigger changes in the surface water management strategy, tailings deposition parameters, tailings management and pit reflooding strategies. This management plan presents the impacts of these modifications on the water management strategy.

Over the summer 2017, AEM assessed that the deposition of tailings inside Goose and Portage Pits was a feasible mitigation measure regarding the current situation observed with the Central Dike seepage. In 2016, following the recommendation of the Meadowbank Dike review Board (MDRB, 2016), AEM evaluated different alternatives for disposing tailings in Meadowbank Mine by performing a Multiple Account Analysis (SNC, 2016) with the support of SNC-Lavalin. In-Pit disposal was designated as the best deposition technic and prefeasibility engineering study was completed in September 2017. AEM is requesting the inclusion of this practice to the NWB through this license modification request as a mitigation measure to continue the operation of the Meadowbank mine under the safest conditions.

Recommendations from the NIRB following their review of the 2016 Annual report will be addressed in the 2017 Annual Reports. This document is presenting the updated water balance from January to September 2017 and the water management strategy until the end of mine life. The Water Management Plan will be updated on a yearly basis as required by the Nunavut Water Board Water License 2AM-MEA1525 (NWB, 2015).

This modification request is also in line with the Whale Tail project under evaluation. This management plan reflects the integration of this deposition technique for the tailings produced

following the mining of the Whale Tail Pit. This section of the Water Management Plan would only be applicable in the case where AEM receives the project certificate from the Nunavut Impact Review Board.

As there is no interaction between the watersheds of the Whale Tail Pit and the Meadowbank site, this report does not include the Whale Tail Project site water management, which is provided in the Whale Tail Pit Water Management Plan (AEM, 2016b). Figure 1.1 shows the Meadowbank Mine and Whale Tail Pit site locations and the Figure 1.2 present the general Meadowbank Mine site layout.

***Figure 1.1: Meadowbank and Whale Tail Pit (Amaruq) Mines Site General Location***





**LEGEND**

- CAPPED TAILINGS
- TAILINGS BEACH
- RECLAIM WATER
- RSF PAG
- RSF NPAG
- DIKE / SADDLE DAM
- ACTIVE PIT
- FLOODING PIT

AGNICO-EAGLE - MEADOWBANK TRACED  
PROJECT 000001 VULT AND  
SECOND WATER TUNNEL  
PROPOSED OUTLINE

DATE: 1/20/2019 BY: JWS  
SCALE: 1:2000 SHEET NO: 3.7

## 1.2 IN-PIT TAILINGS DISPOSAL STUDY

Following the development of the Whale Tail Pit Project, a first phase of the Tailings Facility Extension Project (TSFE) was conducted by SNC-Lavalin in 2015 (SNC, 2015a). The objective was to evaluate the potential expansion of the Meadowbank Tailings Storage Facility (TSF) - North Cell by the construction of internal structures to increase the total storage capacity associated to the mining of the Amaruq ore deposit. The addition of these structures proposed by O’Kane Consultant (OKC, 2016) was sufficient to increase the storage capacity of 8.3M tonnes of tailings into the North Cell.

The second phase of the project was to evaluate at a conceptual level, different options for the storage of additional tailings on site coming from the Whale Tail Pit. Three options were evaluated which included in-pit tailings deposition in Portage Pits A & E, construction of internal structures over the actual TSF and the construction of filtered tailings plant to stored filtered tailings over the North Cell TSF. AEM selected a 28M tonnes of tailings produced scenario’s to compare these difference storage technologies together. This scenario was determined as the best estimate of tailings production associated with the potential approved Whale Tail Pit and any further reasonably foreseeable future development at that time. A Multi-Account Assessment (MAA) session was conducted and the in-pit tailings deposition option was selected as the preferred option (SNC, 2016).

The third phase of the TSFE project consists in developing at a prefeasibility study (PFS) level the In-Pit tailings deposition. In the conceptual study, only Portage Pit A and Portage Pit E were considered for tailings deposition. For the prefeasibility study, Goose Pit is also considered as a potential location for tailings deposition. The in-pit disposal prefeasibility study was done assuming a full capacity scenario where Portage Pit A, Portage Pit E and Goose Pit were filled up to a maximum tailings elevation of 125.6 masl and covered by 8m thick water layer at closure. Through this mandate SNC-Lavalin issued the following technical notes:

- Field Investigation Scope of Work (SNC, 2017b);
- Hydrogeological Field Investigation Factual Report (SNC, 2017c);
- Thermal Modeling Memorandum (SNC, 2017d);
- Hydrogeological Modelling Technical Note (SNC, 2017e);
- Water Balance and Water Quality Forecast (SNC, 2017f)
- Consolidation Memorandum (SNC, 2017g);
- Pit Walls Stability Memorandum (SNC, 2017h);
- Groundwater Monitoring Program (SNC, 2017e).

The appendix B is presenting the Water Balance and Water Quality Forecast associated with this full capacity scenario. However, this water management plan is presenting a scenario where the pits are partially filled with tailings as the tailings produced by the completion of the actual Meadowbank Life of Mine (LOM) and the potential Whale Tail Pit LOM are not sufficient to fill the

pits. However the different strategies developed through the prefeasibility study are meticulously integrated in this management plan.

### 1.3 MINING OPERATION DESCRIPTION

The Meadowbank Gold Mine consists of several gold-bearing deposits within reasonably close proximity to one another. The three main deposits are: Vault (including Phaser and BB Phaser), Portage (South, Center and North Portage deposits), and Goose.

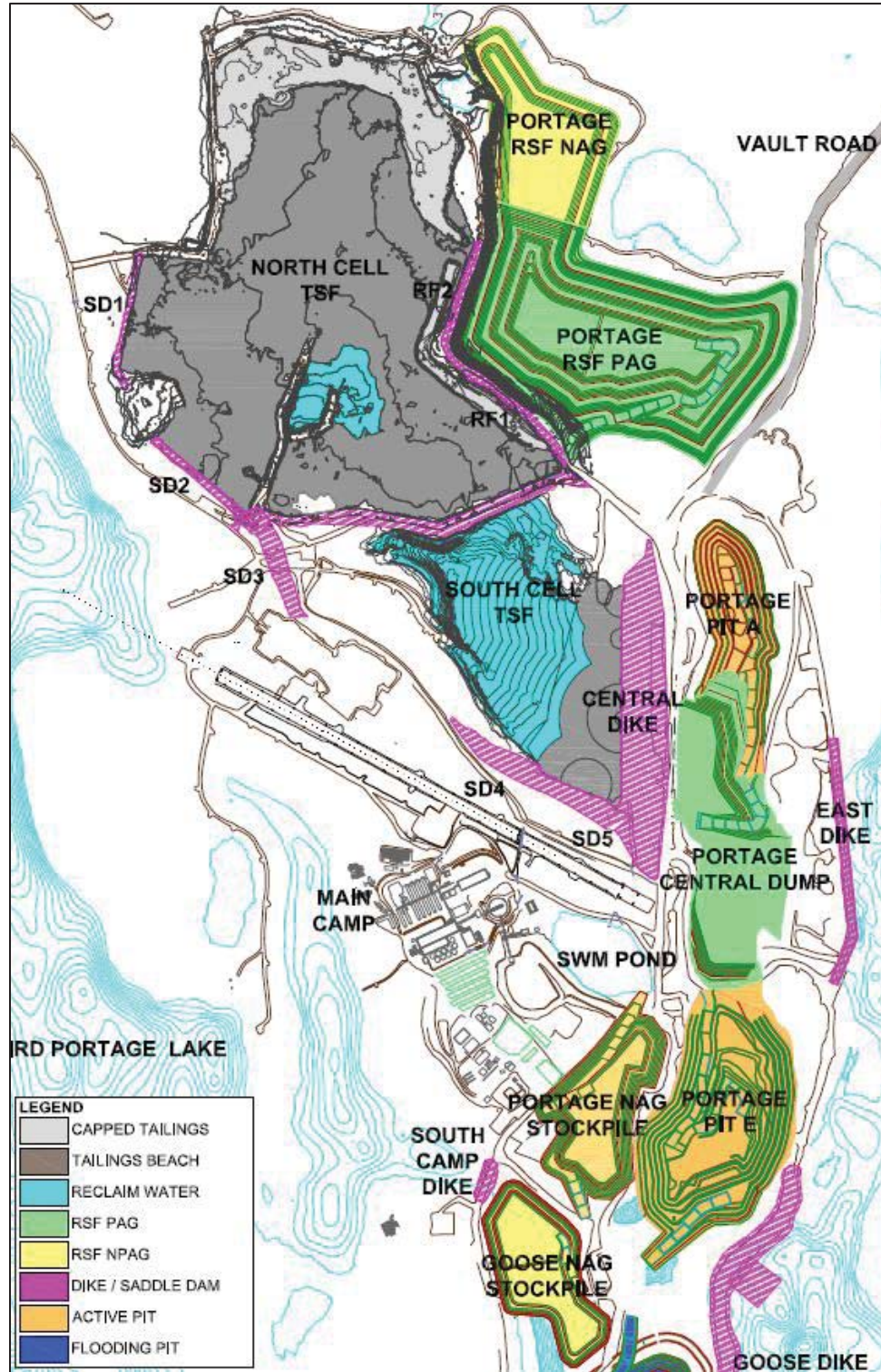
The South Portage deposit is located on a peninsula, and extends northward under Second Portage Lake (2PL) and southward under Third Portage Lake (3PL). The North Portage deposit is located on the northern shore of 2PL. The South, Center and North Portage deposits are mined as a single pit, termed the Portage Pit, which extends approximately 2 km in a north-south direction. The Goose deposit lies approximately 1 km to the south of the Portage deposit, and beneath 3PL. The Vault deposit is located adjacent to Vault Lake, approximately 6 km north of the Portage deposits. A series of dewatering dikes (East, West Channel, Bay-Goose, South Camp and Vault dikes) were required to isolate the mining activities from the lakes. Additional dikes (the Central Dike, Stormwater Dike and Saddle Dams) are required to manage tailings within the dewatered 2PL Arm. East Dike, West Channel, Bay-Goose, South Camp, Vault Dike, Stormwater Dike, Saddle Dam 1, Saddle Dam 2 and the start of Central Dike were all constructed from 2009 - 2014. Regarding the Central Dike; the Cofferdam was built in 2011 up to 110masl, raised to 112masl in 2012, to 120masl in 2013, to 132masl in 2014, then raised to 137masl in 2015, and finally brought to 143masl in 2016. The Saddle Dams 3-4 were constructed up to 140masl in 2015, raised to 143masl in 2016, and finally to 145masl in 2017, (note that SD5 was done in two seasons raised up to 143masl in 2016) and finally to 145masl in 2017. Final elevations will be at 145masl if the current license modification request is approved by NWB. The dikes were and will be constructed primarily using materials produced on site.

#### 1.3.1 Portage Pit Area

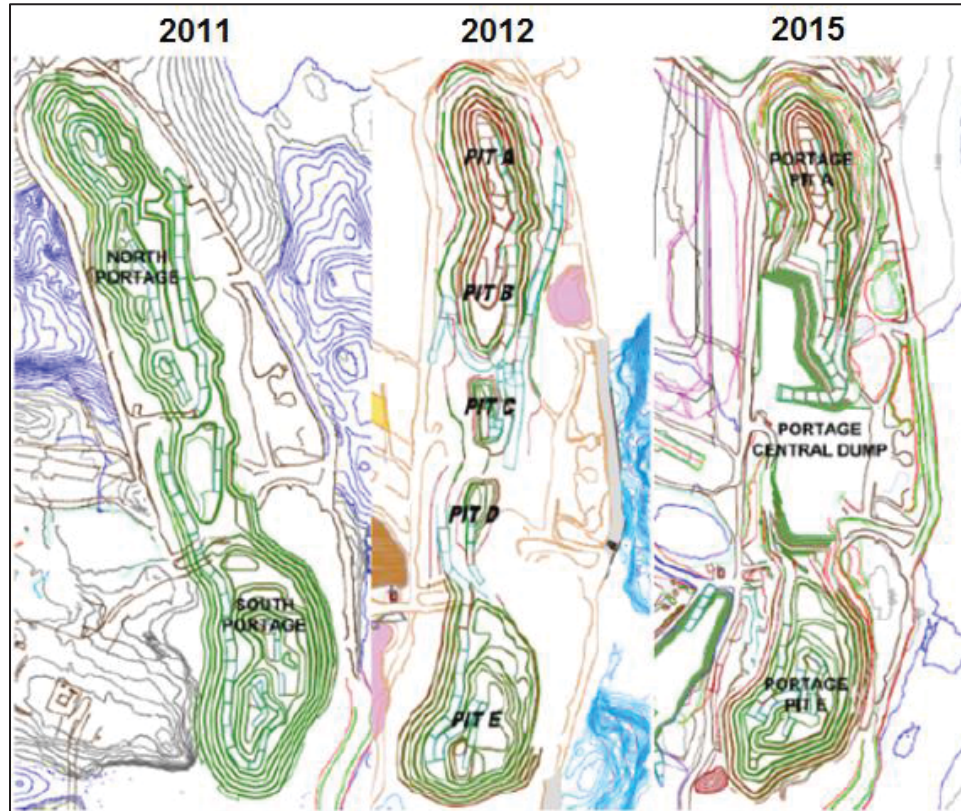
The Portage area located between the Third Portage Lake (3PL) and Second Portage Lake (2PL) contains most of the infrastructure of the Meadowbank mine site including but not limited to the Portage Rock Storage Facility (RSF), North and South Tailings Storage Facilities (NC & SC TSF), the mill, the camp and the Stormwater Management Pond. The East Dike was constructed to isolate the north portion of the Portage Pit from the 2PL. Subsequent renaming of the pits led to the nomenclature for each pit (A, B, C, D and E). Mining in Pits B, C, and D (representing the old Central Portage area) is now completed and they are currently subject to pit infilling operations (which will form part of fish habitat compensation). Mining is still active in Pits A and E. Figure 1.3 shows the current Portage Pit and surrounding infrastructures and Figure 1.4 below presents the evolution of the Portage pit terminology.



Figure 1.3: Portage Pit area map



*Figure 1.4: Portage Pit terminology*



Main water inflow observed in Portage Pit is from the East Dike wall which is associated to the East Dike seepage. This seepage is controlled via two seepage collection points. From the collection points, the water is pumped to a common pipe and discharged back into 2PL since 2014. The discharge is subject to MMER and Water License effluent criteria. The water is discharged through a diffuser located in 2PL. If the seepage does not meet criteria (mainly related to TSS), the pumping is redirected toward the Portage Pit, specifically in the Portage Central Waste Rock area, where the water flows in the rock backfill pores towards Pit B and Pit E in two sumps located at the northern and southern toe of the dump (sampling locations ST-17 and ST-19 respectively). The water is pumped to the South Cell (SC) reclaim pond from those two sumps. Exceptionally, during the summer 2017, water was transferred from Pit A to Pit E as no mining activities was ongoing and AEM wanted to limit the water volume in the South Cell as a mitigation measure of the Central Dike seepage. Another source of pit water was observed in the bottom benches of Pit C and D. These two pits are located in an inferred talik area and also cross a regional fault (Golder, 2009). There are several areas in these pits which are not in permafrost which infers a talik. The water is likely a combination of ground and surface water. AEM is currently monitoring all water quality in sampling locations ST-17 and ST-19 in accordance with the Water License. Pits A and B are located in the permafrost and a minimal amount of water has been observed historically. Some water inflows have been observed from the Pit E south wall during the last years. A major



## 2016 WATER MANAGEMENT PLAN UPDATE

rock fall occurred in September 2015 which was thought to be related to the talik conditions in the shear zone observed on this wall. Water pumped from this area of the Portage Pit was directed to the operational South Cell TSF until the summer 2017 where the water has been stored in the bottom of Pit E, away from the active mining area. Starting in April 2018, all inflow water from Portage Pit will be stored in the Pit A where mining will be completed.

Once the mining of Portage Pit is completed, all dewatering operations will stop and the associated water inflows will contribute to the operation of the tailings deposition process in Portage Pit. The East Dike seepage and any water inflow originating from Pit C and D will also contribute to the in-pit tailings deposition and pit reflooding process during the closure period.

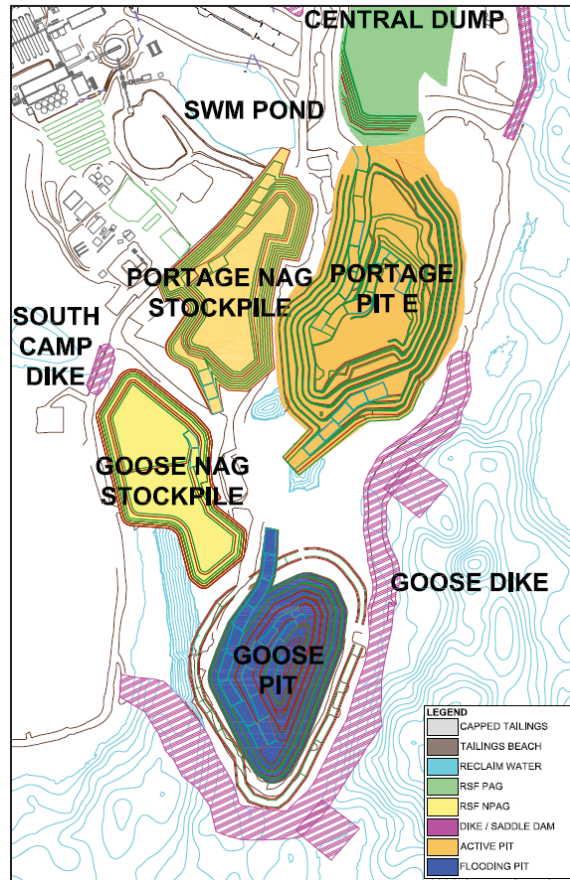
### 1.3.2 Goose Pit Area

The Goose Pit is under 3PL which required the construction of the Goose Dike to isolate the lake from the mining area. Mining in Goose Pit commenced in 2012 and was completed by the end of April 2015. After mining was completed, Goose Pit is being passively re-flooded (only natural runoff and inflow) as part of the closure (refer to the flooding section 2.3 for further details). The Goose Pit area and surrounding infrastructure are illustrated in Figure 1.5.

The majority of the water entering Goose Pit has been observed coming from the South and West wall due to natural inflow from the fractured quartzite rock formation. No major water inflow is observed on the eastern wall associated with the iron formation type rock with small volcanic lenses. Between the quartzite and iron formation, there is a large band of ultramafic rock (soapstone). Most of this pit is located in a talik zone which can explain the water inflow. Some areas of the lower part of the pit are not in permafrost which infers a talik zone. Until mining was completed in April 2015, the water was managed with a system of sumps and trenches along the pit ramp, on the 5109 catch bench and on the working elevation. All water pumped from the Goose Pit was directed to the South Cell Reclaim pond. Since mining has been completed, the inflows are collected in the pit as part of the natural flooding process. Pit water quality is also been monitored during reflooding with sampling station ST-20. The beginning of the active flooding (water transferred from Third Portage Lake) of the Goose pit is planned in 2020. Section 2.3.1 discusses the Goose Pit reflooding.

In 2014, seepage from Central Dike was observed. The seepage is contained at the downstream toe of the dike and a permanent pumping system was installed in 2015. In September 2015, 50,431m<sup>3</sup> of water from the Central Dike D/S Pond were transferred to the Goose pit. This transfer was part of a steady state pumping test performed at that time to understand the nature of the seepage flows. Another water transfer of 284,066m<sup>3</sup> was done from August to September 2017. This transfer was part of the action plan developed by AEM following the Central Dike Trigger Action Response Plan (TARP) alarm level raised from yellow to orange in July 2017. More details about the Central Dike seepage are presented in the section 2.2.4.

*Figure 1.5: Goose Pit area map*



### 1.3.3 Vault Pit Area

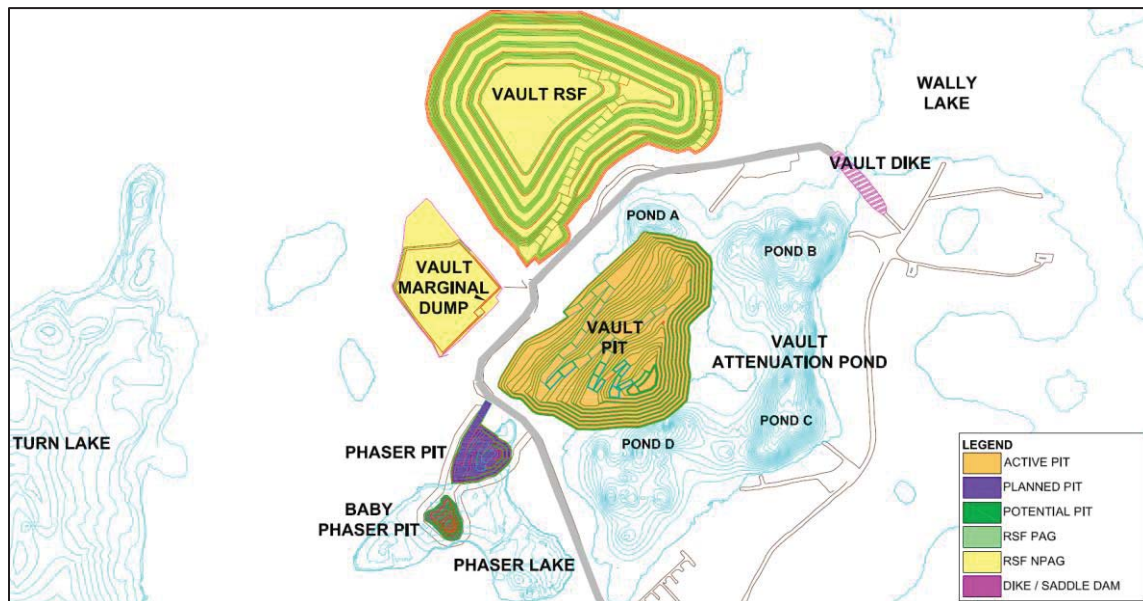
The Vault Pit area contains its own independent infrastructure including but not limited to the Vault RSF, ore and marginal pads, Vault dike, Vault pit, Vault attenuation pond, service building and emergency shelter. The Vault Pit, located under the former Vault Lake required the construction of Vault dike in order to isolate the mining area from Wally Lake and allow dewatering. Dewatering was undertaken in 2013 and 2014. This allowed mining of Vault Pit and the creation of the Vault Attenuation Pond (ATP). The Vault Pit began pre-mining operations in 2013 with active mining starting in 2014. Mining is expected to be completed by the end of the third quarter of 2018. Figure 1.6 illustrates the Vault Pit area and surrounding infrastructure.

The majority of the water migrating into Vault Pit has been observed to be runoff from the surrounding area during the freshet period. Water inflow has been observed on the east wall and most of it is collected in a sump located at the toe of the wall and then pumped into the Vault Attenuation pond. AEM is currently monitoring water quality of the sump in sampling locations

ST-23 in accordance with the Water License to manage that inflow. In 2016 a sump was established in the pond D location to ease runoff water management. Occurrences of small, pressurized, isolated pockets of water are sometimes found while conducting production drilling. The water is managed with a system of sumps and trenches along the pit crest, the main ramp and on the working bench. All water pumped from the Vault Pit is directed to the Vault Attenuation Pond (ATP). The water is subsequently treated for total suspended solids removal (TSS) during summer months (if necessary) and discharged into Wally Lake in accordance with the Water License and the MMER. AEM is currently monitoring water quality of the Vault Attenuation Pond and discharge at sampling locations ST-25 and ST-10 respectively in accordance with the Water License. It is worth mentioning that as of 2017, no water treatment for TSS has been required prior to discharging in Wally Lake as the water met the MMER and Water license criteria.

In 2015, the footprint of the Vault pit was extended following a Life-of-Mine (LOM) exercise. This footprint extension required AEM to review the water management of the Vault Attenuation Pond and change the maximum operation elevation of the different ponds – specifically pond D. The configuration of the Vault Attenuation Pond is presented on Figure 1.6. There are four internal ponds named Pond A, B C & D respectively, which promote natural settling of the suspended solids and contribute to the low TSS levels confirmed by effluent sampling in accordance with MMER and the Water License. The LOM presented in this document includes the mining of Phaser and BbPhaser Pits in 2017-2018. The dewatering of Phaser Lake occurred during summer 2016 to prepare for mining operations initiated in 2017.

**Figure 1.6: Vault Pit area map**



#### 1.3.4 Whale Tail Pit Operations

AEM is currently advancing the plans to develop the new Whale Tail Pit as a satellite deposit to the nearby Meadowbank mine. AEM is working closely with the Nunavut Impact Review Board (NIRB) and the Nunavut Water Board (NWB) on the Whale Tail Pit Project joint permitting process. NIRB/NWB has coordinated the technical review of Whale Tail Pit Project, which is underway; technical meetings, prehearing conference and public hearing conference were held in Baker Lake, Nunavut. The Whale Tail Pit permitting is on schedule, and project certificate is expected to be delivered by Q3 2018.

Following an internal technical study, the Whale Tail satellite deposit at Meadowbank was approved in February 2017 for development, pending the reception of the required permits, which are expected to be received in Q3 2018. In the internal technical study, a conventional open pit mining operation is contemplated to begin extraction of the Whale Tail satellite deposit in Q3 2019. Development of Whale Tail Pit Project would extend the Meadowbank mine life, allowing additional time for AEM to develop and implement an exploration strategy to expand the Whale Tail deposit and to evaluate additional opportunities on the property.

The current management plan is presenting the potential addition of the Whale Tail satellite deposit to the Meadowbank mine life in order to appreciate the impact of the modification of the tailings deposition strategy proposed in this Water Licence Modification Request. However water management of the Amaruq site will not be covered in this report. Refer to the Whale Tail Pit Water Management Plan (AEM, 2016b) for more detail concerning this aspect. This management plan cover only the water management strategy related to the tailings in-pit disposal of the potential Whale Tail Pit ore at the Meadowbank Mine site.

The Whale Tail Pit production plan extend from 2019 to 2022 for a total mill throughput of 8,279,144 tonnes of ore at an average grade of 2.92 g/t. Mining of Whale Tail Pit is a truck-and-shovel open pit operation. Ore will be hauled from Whale Tail Pit to the Meadowbank mill on a road of more than 72.5km. More precisely, three types of ore based on their grade qualities will be milled through a stockpile management process comparable to what is being accomplished at Meadowbank. Milling of the ore will be done at the Meadowbank site and tailings will be stored within the footprint of the approved Meadowbank TSF and potentially inside the Goose and Portage Pits as presented in this management plan.

#### 1.4 LIFE OF MINE DESCRIPTION

The current life-of-mine (LOM) has been updated with the mining surfaces, operational fleet, stockpile situation and milling forecasts. The specifics of the expected monthly milling tonnage are summarized in Table 1.1 seen below. AEM is also presenting the realized processed ore tonnage from January to September 2017 in this table as well as the potential Whale Tail Pit ore tonnage to be processed if AEM receives the Whale Tail Pit project certificate.

*Table 1.1: Current official Meadowbank LOM figures combine with potential Whale Tail Pit LOM –  
Processed ore tonnages*

	2017	2018	2019	2020	2021	2022
January	331,887	279,000	-	273,750	273,750	66,644
February	314,269	252,000	-	273,750	273,750	-
March	279,684	279,000	-	273,750	273,750	-
<b>Q1</b>	<b>925,840</b>	<b>810,000</b>	<b>-</b>	<b>821,250</b>	<b>821,250</b>	<b>66,644</b>
April	328,392	270,000	-	273,750	273,750	-
May	344,962	279,000	-	273,750	273,750	-
June	322,937	270,000	-	273,750	273,750	-
<b>Q2</b>	<b>996,291</b>	<b>819,000</b>	<b>-</b>	<b>821,250</b>	<b>821,250</b>	<b>-</b>
July	336,222	227,530	273,750	273,750	273,750	-
August	326,409	227,530	273,750	273,750	273,750	-
September	275,754	220,191	273,750	273,750	273,750	-
<b>Q3</b>	<b>938,385</b>	<b>675,251</b>	<b>821,250</b>	<b>821,250</b>	<b>821,250</b>	<b>-</b>
October	348,657	-	273,750	273,750	273,750	-
November	337,410	-	273,750	273,750	273,750	-
December	348,657	-	273,750	273,750	273,750	-
<b>Q4</b>	<b>1,034,724</b>	<b>-</b>	<b>821,250</b>	<b>821,250</b>	<b>821,250</b>	<b>-</b>
Total	3,895,240	2,304,251	1,642,500	3,285,000	3,285,000	66,644

#### 1.4.1 Changes from the Water Management Plan 2016

As previously stated, updates to the LOM will lead to additional adjustments of the water management plan. Changes in the LOM plan that affect water management include but are not limited to:

- Updated truck mining fleet;
- Updated stockpile status;
- South Cell (SC) and North Cell (NC) TSF NAG capping volumes (progressive reclamation) and timeframe.

In this water management plan version, revisions/modifications were made to the water balance to integrate the addition of the in-pit deposition process inside Goose and Portage Pits that leads to this update. These include:

- Fresh water consumption revision;
- Total daily mill water requirements;
- Updated tailings deposition plan affecting the North Cell and South Cell deposition calendar;
- Addition of in-pit deposition inside Goose and Portage Pits to the deposition calendar;
- Inclusion of potential Whale Tail Pit processed ore to the deposition calendar;
- Pit water inflow revision based on observed flowmeter data as well as a revision of the pits and TSF run off inflows related to their underlying watersheds (performed by SNC, 2013);
- Flooding sequence and volumes update to take into account the updated run off inflows as well as to optimize flooding activities to reduce the impact on wall stability;
- Seepage section update;
- Changes in tailings dry density as observed through latest bathymetric analysis.

Further details of the modifications/revisions and their effects on the overall water management strategy will be provided in subsequent sections of the Water Management Plan.



## **Section 2.0 - WATER MANAGEMENT PLAN AND WATER BALANCE**

### **2.1 GENERAL WATER MANAGEMENT STRATEGY**

At Meadowbank, five major water inflows are considered in the site water management system: freshwater pumped from Third Portage Lake, natural run off, natural pit groundwater inflow, seepage inflow from the East Dike and freshet water. This water is either utilized or removed from the inflow by the following means: water treatment plant effluent (if treatment necessary to meet discharge criteria) or non-treated effluent from the Vault attenuation pond, water trapped in the capillary voids of the tailings fraction (including ice entrapment for winter months) at the TSF, East Dike seepage discharge into Second Portage Lake, water trapped within the in-pit rock storage facilities area voids and natural flooding (Goose & Portage Pits).

The water balance is subdivided into the following sections: Fresh Water from Third Portage, Reclaim Tailings Water, Mill Water, North and South Cell TSF, Portage Pit, Goose Water Transfers, Model Parameters, East Dike Seepage, Vault Pit, Phaser & BbPhaser Pits and Lake, Vault Pond D, Vault ATP and Vault water transfers. The following sections will discuss each item and their inherent parameters.

The Water Balance is presented in Appendix A of this report.

As per the requirements concerning the water balance in the Water License 2AM-MEA1525 (Part E, condition 7), the Water Management Plan will be updated on an annual basis. The Water Management Plan will include a yearly updated water balance according to the water management strategy and the applicable LOM.

#### **2.1.1 Updated Tailings Deposition Strategy**

The in-pit deposition consists of the deposition of tailings into Goose Pit, Portage Pit A and Pit E following the approval of this modification request. The approval of the modification request will trigger the end of the deposition of tailings in the North and South Cell TSF. The deposition strategy considered for this management plan is divided into the following distinct periods:

- Period 1: Portage/Vault tailings deposition in South Cell TSF and in Goose Pit
- Period 2: Whale Tail tailings deposition in Portage Pit
- Period 3: Pit Closure at the end of operations
- Period 4: Monitoring period
- Period 5: Post closure

Period 2 relies on the submission of the Whale Tail Project Certificate by NIRB and on the approval of the current modification request. In the event AEM does not move forward with the Whale Tail Project, Period 3 will be triggered after the completion of Period 1. Water management global strategy of each period will be presented in the following sections.

#### 2.1.1.1 Period 1: Portage/Vault tailings deposition in South Cell TSF and Goose Pit

Based on the experience acquired during the closure of the North Cell TSF, AEM developed an internal operation guideline related to the minimal water volume required to operate a TSF in Meadowbank. High turbidity levels were observed in the reclaim water when the North Cell TSF water volume – volume of unfrozen water – was below 250,000 m<sup>3</sup>. This situation was observed two times in November 2014 and in October 2015. Back then, these situations lead AEM to switch deposition of tailings from the North Cell TSF to the South Cell TSF in order to continue the operation of the process plant.

When the alarm level of the Central Dike was raised to orange in July 2017, AEM completed water balance sensitivity analyses to evaluate the potential operation of the TSF with a lower water volume over the next year. AEM evaluated that a transfer of 300,000 m<sup>3</sup> would balance the operational risks related to the seepage situation and the operation of the South Cell TSF over the 2017-2018 winter with a lower water volume.

The sensitivity analyses showed that the total water volume of the South Cell TSF will decrease around 540,000 m<sup>3</sup> in April 2018 and more than 60% of this volume will be frozen solid leading to a free water volume of 210,000 m<sup>3</sup>. AEM will need to operate the South Cell TSF below the 250,000 m<sup>3</sup> free water volume self-imposed limit.

AEM established a mitigation plan to reduce the impact of this low free water volume in the South Cell TSF. This action plan is consisting of the:

- Construction of the South Cell Internal Structure during the fall 2017 to prevent tailings beach to reach the reclaim pump during winter 2018;
- Evaluation of the possibility to initiate tailings deposition in Goose Pit in April 2018.

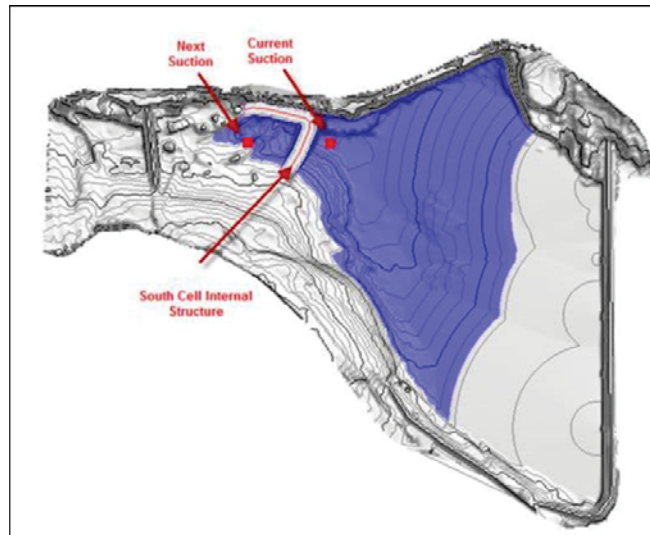
The South Cell Internal Structure layout is presented on the Figure 2.1. This permeable rockfill internal structure in front of the reclaim pump suction will block the migration of tailings toward the reclaim pump area and allow the water to reach the pumping area. Similar structures were built in 2014 in the North Cell TSF and proved their effectiveness.

In the circumstance where the South Cell Internal Structure is not efficient to secure the deposition of tailings in the South Cell TSF, AEM will need to discharge tailings in another storage area. AEM identified the Goose Pit as the best available location.

In order to reflect this strategy, this water management plan presents tailings deposition inside the South Cell TSF until the end of March 2018 and tailings deposition in the Goose Pit from April 2018 to September 2018. During that period of time, 1.5M tonnes of tailings will be stored in the Goose Pit and the water volume inside the Goose pit will vary from 1.5Mm<sup>3</sup> to 2.6Mm<sup>3</sup>. AEM plans on operating the mill during that period of time by consuming 100% of freshwater. This 2.6Mm<sup>3</sup> will be transferred to Portage Pit E during the Period 2 and used during the deposition of the Whale Tail pit tailings in the Portage Pit E. This transfer will reduce the freshwater required at that time. However, if AEM needs to initiate the closure process of Meadowbank mine in 2018, the

water contained inside the Goose Pit will be treated prior to resuming Goose Pit reflooding. Treatment objectives will be to meet CCME or other site specific criteria prior to complete the breaching of the Goose Dike.

**Figure 2.1: South Cell Internal Structure**



#### 2.1.1.2 Period 2: Whale Tail tailings deposition in Goose Pit

According to Whale Tail Pit project presented to the NIRB and NWB previously in 2016 and 2017, AEM was planning the raise of the actual Meadowbank TSF capacity to store the additional 8,279,144 tonnes of tailings produced during the mining of the Whale Tail Pit ore. The geotechnical infrastructures of the South Cell were planned to be raised from elevation 145 to 150m and an upstream dike was planned to be built above the North Cell TSF tailings up to elevation 154m. Following the evaluation of the Central Dike operational risk related to the seepage event and the recommendation of the MDRB, AEM now plans to store the additional tailings inside the Portage Pit.

This new tailings management approach is a modification to the Whale Tail Pit Tailings Management Meadowbank Tailings Storage Facility Management Plan Addendum (AEM, 2016c) presented within the submission documents of the Whale Tail and Haul Road project and will be only applicable upon the reception of the project certificate.

AEM is planning to alternate deposition of tailings in between Portage Pit A and Portage pit E. during Period 2. The Portage Pit is divided in two ponds by the Portage Pit Central Dump as presented on the Figures 2.2 and 2.3. The water balance assumed that the Portage Central Dump is permeable and allows water to travel freely through the rockfill. The waste rock contained inside this dump has a 30% void ratio, and these voids will be filled by water during the deposition of tailings. The Portage Central Dump voids must be filled at the same rate then the Portage Pit A

and E in order to keep a constant water cover over the tailings beach and achieve the deposition of tailings properly. AEM is planning on using 7.5Mm<sup>3</sup> fresh water from 3<sup>rd</sup> Portage Lake (3PL) to achieve this objective during the operation. Flooding of Goose Pit will also be initiated with a 2Mm<sup>3</sup> water transfer from 3PL planned in 2020. Prior to executing this specific transfer, water quality forecasts of the Goose Pit will be evaluated to determine treatment requirements prior to water transfer.

**Figure 2.2: Profile View of Portage Pit A, Pit E and Central Dump**

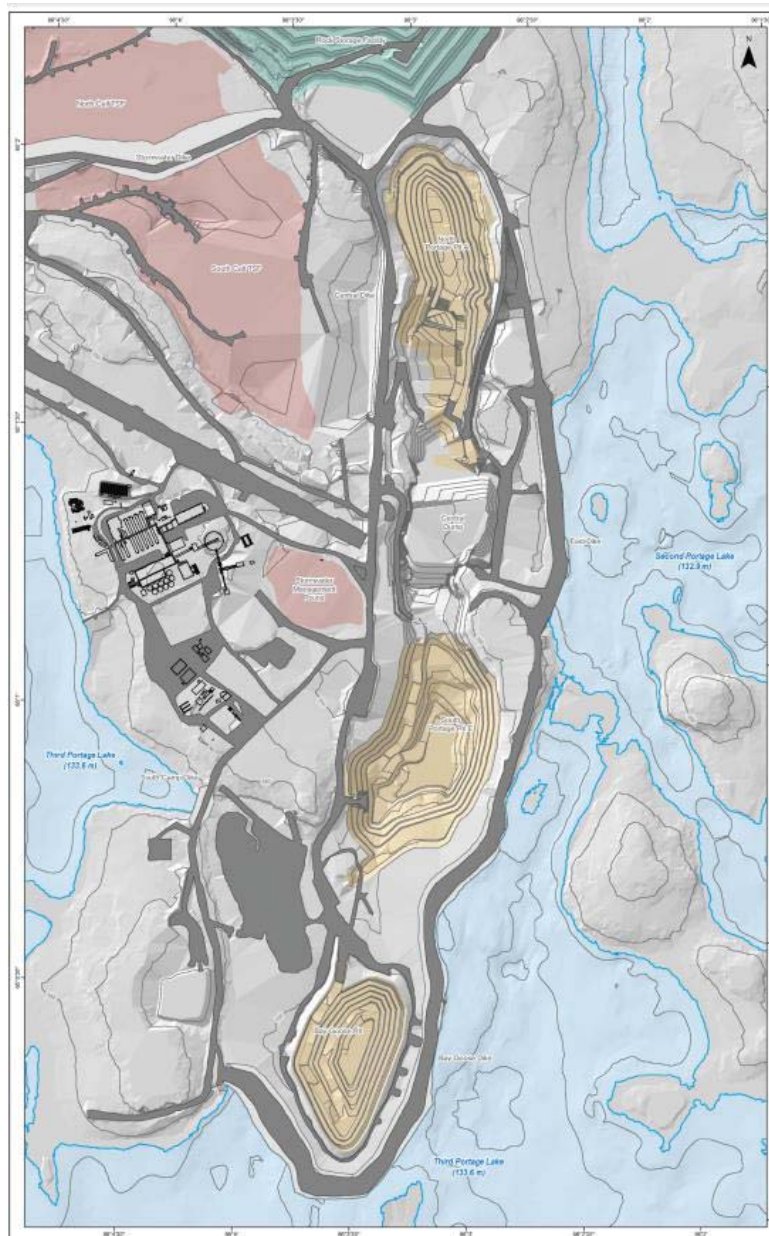
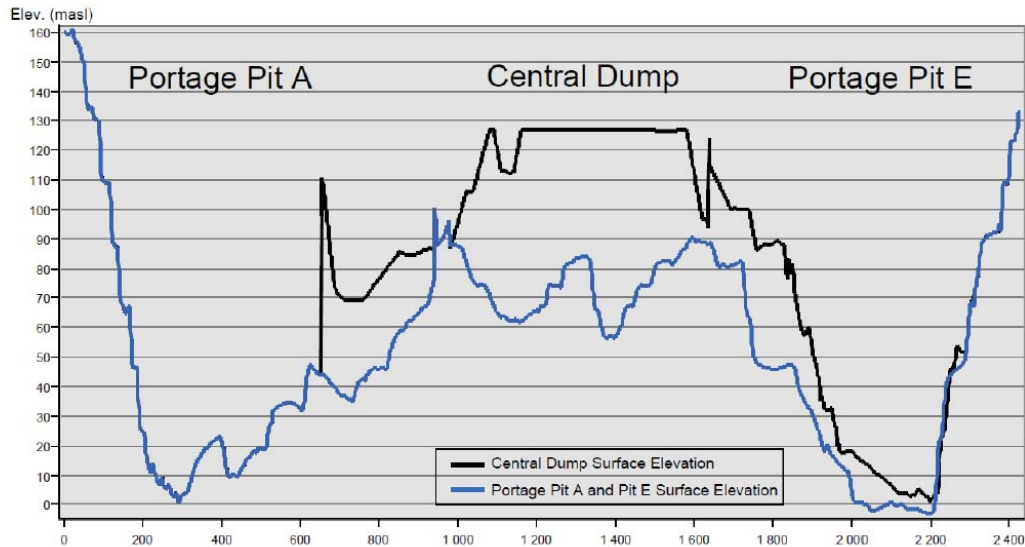


Figure 2.3: Profile View of Portage Pit A, Pit E and Central Dump



#### 2.1.1.3 Period 3: Pit Closure at the end of operations

The in-pit deposition activities are planned to cease in January 2022. Flooding of the Goose and Portage Pits will be resumed during the summer 2020 with the transfer of 24.6Mm<sup>3</sup> of water from 2020 to 2027. Water quality forecasts for the pit water will be evaluated prior to initiating the flooding process and treatment requirements evaluated and executed, if required at that time. Section 3.2 is presenting additional details of the flooding activities and Section 4 is presenting the findings of the water quality forecast completed for the in-pit deposition scenario.

#### 2.1.1.4 Period 4: Monitoring period

Natural flooding of the Goose and Portage Pits will continue from 2027 to 2031. During these four years, AEM will evaluate water quality of the pits prior to Goose Dike breaching in 2031.

#### 2.1.1.5 Period 5: Post closure

Monitoring of the water quality within the pits will be done according to the approved Final Closure Plan.

#### 2.1.2 Fresh Water from Third Portage Lake

Fresh water from Third Portage Lake is pumped, utilizing a fresh water barge, in order to service the camp, mill, maintenance shop and all other fresh water users at Meadowbank. The amount pumped from the barge is tracked and reported in the water balance and as a requirement of the Type A Water License. The two main consumers of fresh water are the mill with an average of 43,046 m<sup>3</sup>/month since the beginning of 2017 (expected average 43,324m<sup>3</sup>/month in 2017) and the camp that averaged 3,373m<sup>3</sup>/month in 2017.



## 2016 WATER MANAGEMENT PLAN UPDATE

It is important to take note that 2017's freshwater consumption at the mill are lower than prior years which was part of a strategy to reduce the volume of free water volume in the reclaim pond to put less pressure on the Central Dike seepage mechanism by reducing the hydraulic gradient in between the South Cell TSF and the Central Dike downstream pond. As mentioned above, this practice increased the level of risk related to the reclaim system operation during winter 2017/2018 as seen in 2013 at the North Cell.

The freshwater going to the mill is used in the milling process and will be discharged with the tailings as slurry. Once in the South Cell TSF, the total water used in the process is made up of 40-70% of reclaim water, 30% of entrapped water within the capillary void space of the tailings and up to 30% of entrapped water within the TSF as ice. The water entrapment within the TSF represents the volume of water loss in the deposition process. The 2016 bathymetry analysis of the South Cell revealed that the annual water entrapment increased to 39% and subsequently to 40% in 2017. According to AEM analysis, these results are the consequence of the tailings deposition mechanism in the South Cell. The annual water entrapment was set at 40% until the end of the operation of the South Cell TSF in March 2018.

To evaluate the capacity of the pits for tailings storage, a one dimensional (1D) geotechnical modelling was carried out by SNC-Lavalin to assess the tailings consolidation in the short and long term as tailings are being deposited in the Portage Pit E (SNC, 2017g). The 1D model was built using the expected tailings production as provided by AEM and the tailings storage volumes developed for Portage Pit E and translated to Pit A and Goose. The model was set up using the existing data obtained from the project site and data from the gold tailings mine with similar properties. Based on the consolidation laboratory testing data obtained from the gold mine with similar tailings properties, the 1D consolidation modelling shows that during in-pit filling the average solid content ranges from 61.2% to 63.7 % with the equivalent tailings dry density ranging from 1.03 tonne/m<sup>3</sup> to 1.11 tonne/m<sup>3</sup>. The water balance presented in this Water Management Plan assumed that tailings, after consolidation, will have a 67% water content during the in-pit deposition process in Goose and Portage Pits. This parameter is considered conservative as it is triggering higher consumption of freshwater during the operation.

The fresh water used in the camp includes laundry facilities, cleaning, cooking and drinking water consumption. The majority of the camp fresh water is returned as sewage treatment effluent to the Stormwater Management Pond which ultimately gets transferred to the active TSF (currently the South Cell and later Goose Pit) and to the Portage Pit from 2020 to 2031 as part of the flooding process at closure.

The total expected fresh water utilization planned from October 2017 to mine closure varies from 60-370m<sup>3</sup>/hr during mill operation, and drops gradually during closure to 4m<sup>3</sup>/hr once the mill has closed or during the 9 months production gap in 2018-2019 prior to Whale Tail Pit ore processing (represents water used by the camp only and does not include pit flooding). The variation seen in the fresh water consumption during the mill operation is optimized to prevent a water deficit in the TSF and allows for adequate reclaim volumes while minimizing the reclaim water transfers

from the TSF to the pits at closure. The higher freshwater consumption flows are planned during the tailings deposition inside Goose Pit. The objective is to build up a 2Mm<sup>3</sup> water volume inside Goose Pit in order to ease the startup of the in-pit deposition of Goose Pit in April 2018 and reduce freshwater consumption during the summer 2019 by transferring this volume in Pit A instead of pumping water from the 3PL.

The ice cover during the winter months on the reclaim pond will vary between 0.0-1.7m in thickness which may represent up to 61% (April 2018) of the total reclaim water volume compared to the 32% ratio observed in April 2015. This shows the large impact of Arctic climate on tailings and water management at Meadowbank. Tables 2.1 and 2.2 present, respectively, the targeted water consumption until the end of the Period 1 and the average yearly water consumption forecasted until the end of the mine life. More details are included in the water balance presented in Appendix A.

Adjustments at the mill and in the water management strategies have led to a revision in fresh water consumption as presented in previous section. Figure 2.4 presents the process plant water consumption per month until the production gap and yearly values are summarized in Table 2.2 for 2017 to 2031, excluding pit reflooding volumes. Refer to Section 2.3 for the pit flooding activities description and freshwater needs.

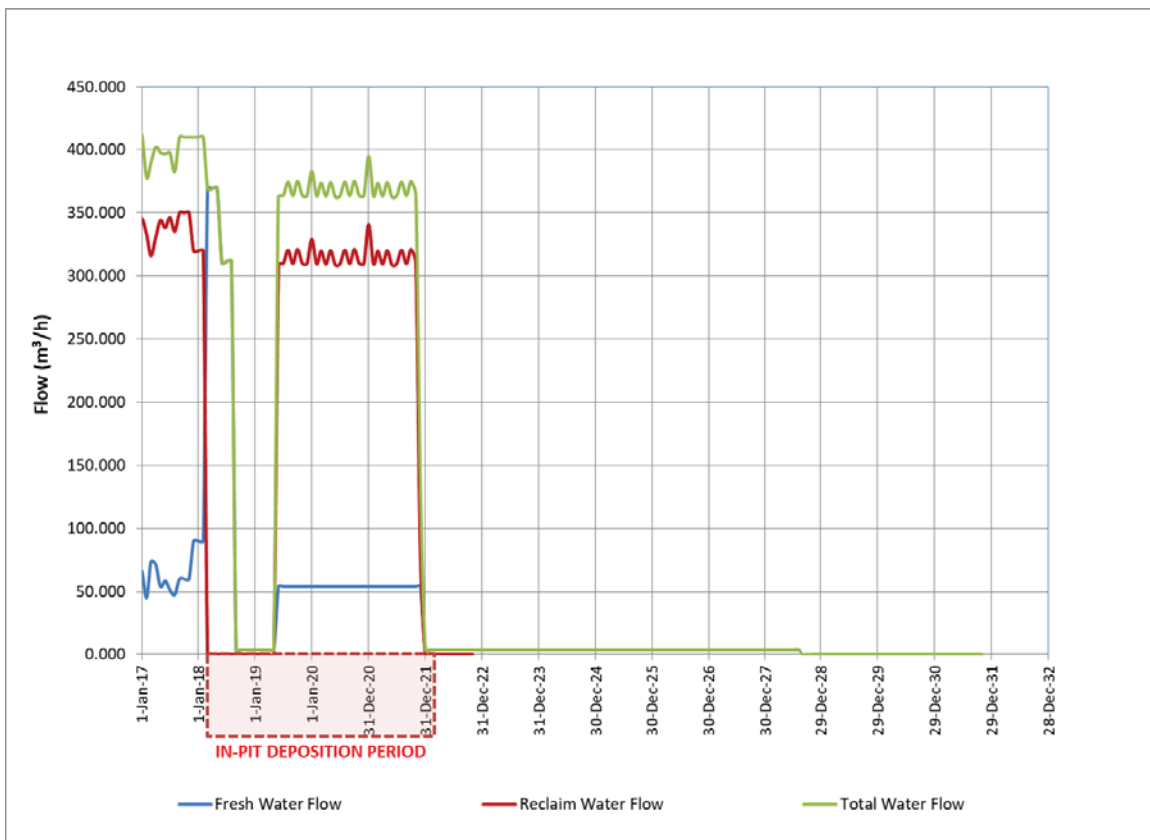
**Table 2.1: Targeted water hourly consumption per month until end of Period 1 – for Mill and Camp Usage**

Month	Fresh Water Flow (m <sup>3</sup> /h)	Reclaim Water Flow (m <sup>3</sup> /h)	Total Water Flow (m <sup>3</sup> /h)
October/17	60	350	410
November/17	60	350	410
December/17	60	350	410
January/18	90	320	410
February/18	90	320	410
March/18	90	320	410
April/18	369	0	369
May/18	369	0	369
June/18	370	0	370
July/18	310	0	310
August/18	311	0	311
September/18	312	0	312
<b>Average</b>	<b>208</b>	<b>168</b>	<b>375</b>

*Table 2.2: Yearly water consumption summary – Mill and Camp Usage*

Year	Average Fresh Water Flow (m <sup>3</sup> /h)	Total Fresh Water (m <sup>3</sup> )	Average Reclaim Water Flow (m <sup>3</sup> /h)	Total Reclaim Water (m <sup>3</sup> )
2017	59	519,683	340	2,977,431
2018	194	1,697,229	80	691,200
2019	29	383,262	157	255,4751
2020	54	473,970	315	2,764,060
2021	54	472,675	315	2,756,507
2022	8	71,875	6	56,118
2023-2031	4	34,675	-	-

*Figure 2.4: Flow to the mill*





### 2.1.3 Reclaim Tailings Water

Reclaim tailings water represents the water reclaimed from the TSF during mill operation. Currently, the pumping system utilizes a mobile pumphouse on skids which retreats on a road as the water level rises in the South Cell TSF. AEM is planning using the same kind of equipment for the operation of the in-pit deposition. The suction line will be placed at the bottom of the ramp and extended as needed according to raise of the water level in the pit. A summary of the reclaim water sent to the mill on an annual basis can be seen in Table 2.2.

Presently the reclaim pumping system installed in the South Cell will continue to supply the mill with reclaim water until end of March 2018. Once in-pit deposition will be initiated, North Cell TSF runoff water inflow will be transferred yearly during summer months into the South Cell, and then from the South Cell to the pits, to maintain a 2m freeboard in the North Cell TSF as required by the TSF designer, the OMS manual and the Water License. This action will be performed yearly (even after the North Cell is capped during closure operations) until 2031 (planned dike breaching if CCME criteria/site specific criteria are met). It should be understood that run off water (non-contact water) from the surrounding North Cell TSF watershed area is captured in the diversion ditches and conveyed to the Interception Sump. From there, it is planned to be transferred into the North Cell or release to the environment if meeting discharge criteria.

The South Cell TSF water management is based on same principles as the North Cell. After the summer of 2017, the reclaim water volume will decrease slowly until the tailings deposition is completed. Some water will need to be transferred to the Portage Pit during the in-pit deposition for the closure phase (i.e. reflooding) and to properly dewater the tailings pond for closure capping. Those reclaim water transfers are included in the pit flooding process. The impact on final pit water quality is considered in the yearly water quality forecast model presented in the section 3.

### 2.1.4 Mill

The LOM figures depicted in Table 1.1 were used to calculate the monthly mill throughput. Based on this, AEM has determined the historical average ore moisture content associated with the mill feed which represents this source of water within the water balance. Table 2.3 illustrates the average moisture content over time until closure. The forecasted average moisture content for 2017-2022 is the average of the measured volume of 2013 to 2015. Note that the moisture content is established as a percentage of mill throughputs.

**Table 2.3: Monthly average moisture content at the mill**

Month	Average Moisture Content (%)
January	0.98%
February	1.53%
March	1.04%
April	1.09%
May	1.08%
June	0.99%
July	1.30%
August	0.98%
September	0.89%
October	0.99%
November	0.72%
December	0.93%
<b>Average</b>	<b>0.99%</b>

#### 2.1.5 North Cell

The North Cell TSF has been in operation since January 2010. Deposition ceased temporarily in the North Cell in November 2014 as the South Cell TSF became operational. Tailings deposition resumed in the North Cell from June to October 2015 to accomplish summer deposition as part of the closure of the North Cell. Progressive closure and capping of the North Cell TSF started in winter 2015. Table 2.4 is presenting the volume of Non Potential Acid Generating (NPAG) material placed over the North Cell TSF since 2015.

**Table 2.4: Monthly average moisture content at the mill**

Year	NPAG material (m <sup>3</sup> )
2015	296,129
2016	280,644
2017	151,116
<b>Total</b>	<b>727,889</b>

Capping will continue to occur progressively during the mining of Portage Pit depending on material availability. As per the design specifications and regulatory requirements, the level of the North Cell reclaim pond must be maintained with a two meter freeboard, with the peripheral

structures at 150.0masl elevation. For the North Cell, the reclaim water must respect a maximum elevation of 148.0masl. A total of 238,762m<sup>3</sup> of water from the North Cell was transferred to the South Cell reclaim pond from June to September 2017.

#### 2.1.6 South Cell

The South Cell area was the Portage Attenuation Pond prior to the November 2014 commencement of tailings deposition. The attenuation pond was designed to contain mine contact water as well as freshet runoff and was discharged to Third Portage Lake via the Water Treatment Plant (WTP) in accordance with the Water License and MMER. In May 2015, AEM proceeded with the dismantlement of the Portage WTP as no additional water was planned to be discharged into 3<sup>rd</sup> Portage Lake through the mine life. As presented earlier, AEM is always looking forward to adapt its water management strategy to reduce freshwater consumption by directing runoff water into the tailings pond. During the in-pit deposition phase, runoff water from the South Cell will be redirected to Goose and Portage Pits. This process will continue during the closure phase, where runoff water will be collected in the Goose and Portage Pits as part of the pit flooding process. The South Cell TSF commenced operation in November 2014 and will be receiving tailings from the mill until March 2018. Closure and capping will be finalized during the closure phase.

#### 2.1.7 Portage Pit

The Portage Pit is divided in sub-pits (A, B, C, D & E) and their associated pushback areas. Currently, Portage Pit contains a central waste rock storage area which extends from Pit C to D with a second section located in Pit B. The Portage Pit natural inflow has been revised from the 2012 SNC Water Management Plan (SNC, 2013) with measured on site data from 2013 to 2015. This inflow includes runoff water, groundwater and the part of the East Dike seepage water which is pumped back to Second Portage Lake when discharge criteria are met. Field observations revealed an inflow observed originating from the bottom benches of Pit C and D. Since these areas are completed and backfilled with rockfill, water can accumulate in the rockfill porosity voids thus leading to a reduction in Portage Pit water outflow. AEM believes that the water inflow is filling up the porosity voids of the Portage Central Dump to some extent. It is anticipated that additional inflow could occur at the bottom of Pit A and E as there will be an increased hydraulic gradient compared to the surrounding water (from possible groundwater and surface water from Second Portage Lake). Furthermore, water inflows were observed from the Pit E south wall during the year 2015. A major rockfall occurred in September 2015 which was thought to be related to the talik conditions of the shear zone observed on this wall.

During the summer 2017, all water pumped from the Portage Pit A was transferred to the bottom of Portage Pit E. This modification to the water management strategy was part of the Central Dike seepage mitigation plan. The objective was to reduce water inflow in the South Cell TSF to reduce the hydraulic gradient through the Central Dike as much as possible and limit seepage flow.

## 2016 WATER MANAGEMENT PLAN UPDATE

Tailings deposition is planned to be initiated in July 2019 in Portage Pit E according to the reception of the Whale Tail Pit project certificate. AEM assumed that the runoff water, Stormwater Management Pond water, East Dike Seepage, South Cell TSF reclaim water and runoff water will be accumulated in the Portage Pit. These water transfers will be done according to the location of the tailings deposition. Tailings will be discharged in Portage Pit E from July 2019 to June 2020, then in Portage Pit A from July 2020 to December 2020 and finally in Portage Pit E until the end of the actual life of mine in January 2022. Other water transfers from Third Portage Lake (3PL) will be required to initiate progressive Portage Pit flooding during operation. The objective of the 3PL water transfers during operation is to always to keep a 20m water cover over the tailings beach at all time. As the Portage Central Dump is permeable, AEM is expecting that the reclaim water cover over Pit A and Pit E tailings beach will flow inside the Portage Central Dump if the rockfill voids are not already filled with water. A 2Mm<sup>3</sup> water transfer from Goose Pit and 4Mm<sup>3</sup> from 3PL will be required to initiate the progressive flooding of the Portage Pit to mitigate that risk. The Table 2.5 is presenting the Portage Pit annual water inflow planned from July 2019 to January 2022.

**Table 2.5: Annual water inflow in Portage Pit during Period 2**

	South Cell Runoff (m <sup>3</sup> )		Stormwater Management Pond (m <sup>3</sup> )		Runoff (m <sup>3</sup> )		Infiltration (m <sup>3</sup> )		East Dike Seepage (m <sup>3</sup> )		Goose Pit transfer (m <sup>3</sup> )		3rd Portage Lake (m <sup>3</sup> )		Net Process water (m <sup>3</sup> )	
	Pit A	Pit E	Pit A	Pit E	Pit A	Pit E	Pit A	Pit E	Pit A	Pit E	Pit A	Pit E	Pit A	Pit E	Pit A	Pit E
2019	221,969	-	-	11,590	31,531	35,232	14,720	10,672	-	89,784	2,000,000	-	-	-	-	304,167
2020	486,864	-	11,590	23,085	55,308	61,799	29,280	21,228	89,784	89,784	-	-	-	2,000,000	304,167	304,167
2021	486,864	-	23,085	11,590	55,308	61,799	29,200	21,170	74,820	104,748	-	-	-	2,000,000	253,472	354,864
2022	-	-	-	-	-	-	2,480	1,798	-	14,964	-	-	-	-	-	12,341
Total	1,195,697	-	34,675	46,265	142,147	158,830	62,680	54,752	164,604	299,280	2,000,000	-	-	4,000,000	557,639	975,539

This new version of the water balance is presenting an infiltration volume that varies based on elevation of the water inside the pit. Half of the infiltration volume is measured above 129masl and no flow observed above 129.9masl.

Table 2.6 is presenting the Portage Pit annual water outflow from July 2019 to January 2022. The two outflows identified in the water balance are the water reclaimed to the process plant and the water entrapped within the tailings based on the water content of the tailings after consolidation (67%). Reclaim water will always be pumped from the pit were tailings are not discharged. For example, if tailings are discharged inside Portage Pit E, water will be reclaimed from the Portage Pit A. This strategy was put in place in order to optimize reclaim water quality and use the Portage Central Dump as a natural filter to promote settlement of fine particulates of the slurry in the active deposition pit.

**Table 2.6: Annual water outflow in Portage Pit during Period 2**

	Reclaim Water (m <sup>3</sup> )		Entrapped Water (m <sup>3</sup> )	
	Pit A	Pit E	Pit A	Pit E
2019	1,383,262	-	-	1,095,000
2020	1,380,798	1,383,262	1,095,000	1,095,000
2021	1,613,746	1,150,314	912,500	1,277,500
2022	56,118	-	-	44,430
Total	4,433,924	2,533,576	2,007,500	3,511,930

Tailings beach elevation will reach elevation 76masl in January 2022. Once flooding will be complete the water cover above the tailings will be 57m thick.

During the closure phase, active pit flooding will be triggered. The pumping systems will be decommissioned and replaced by the infrastructure required for the pit flooding process. Refer to Section 2.3 for the pit flooding activities description.

#### 2.1.8 Goose Pit

Mining in the Goose Pit was completed in April 2015. The inflow values have been revised from the 2012 SNC Water Management Plan (SNC, 2013). It was observed that the pit inflow diminishes during the winter due to the freezing of the pit walls. The volume cannot be measured but is reconciled with the water level measured by survey at each month end. The values for the 2017 Goose Pit inflow have been adjusted based on SNC revised run off inflows update (SNC 2015). When referring back to the initial estimates originating from the 2012 SNC Water Management Plan (SNC 2013), an increase was observed in the water inflow during the mining of the bottom benches of Goose which could be attributable to an increased hydraulic head as vertical mining progressed. This new version of the water balance is presenting an infiltration volume that varies based on elevation of the water inside the pit. Half of the infiltration volume is measure above elevation 129mals and no flows observes above elevation 129.9masl.

No more water is pumped from Goose Pit to the South Cell as the mining of this pit is completed and the inflows (runoff and groundwater) are collected in the pit as part of the pit flooding process. As mentioned previously, AEM has monitored (and will continue to do so) the flooding rate since Goose Pit mining was completed. Pit water quality is also been monitored during reflooding with sampling station ST-20.

A total of 365,575 m<sup>3</sup> of runoff and groundwater inflows were stored in the pit so far in 2017. A water transfer of 284,954 m<sup>3</sup> was done from the South Cell TSF in August and September 2017. More detail regarding the Central Dike seepage mitigation plan is presented in the section 2.2.4.

## 2016 WATER MANAGEMENT PLAN UPDATE

AEM is planning to store Meadowbank tailings in the Goose Pit from April to September 2018. This change to the tailings management plan is done in accordance with the Central Dike Seepage mitigation plan and the recommendation of the MDRB. Reclaiming activity of the process water will be stopped during the deposition of tailings inside Goose Pit. The water volume contained in the pit will then increase from 1.5M to 2.6Mm<sup>3</sup> in six months and the water elevation will increase from 82 to 104m. Tailings beach elevation will reach elevation 83m in September 2018. Once flooding will be completed, the water cover above the tailings will be 51m thick.

The Table 2.7 and 2.8 are presenting the Goose Pit water inflow and outflow from April to September 2018. After the completion of the Period 1, 90% of the inflow will have been entrapped inside the tailings according to the consolidation model developed by SNC (SNC, 2017g). AEM is planning to transfer 600,000m<sup>3</sup> of water from the South Cell TSF from April to June 2018. This water will be needed to keep the water cover at a minimum of 20m thick during the deposition process.

**Table 2.7: Annual water inflow in Goose Pit during Period 1**

	Stormwater Management Pond (m <sup>3</sup> )	Runoff (m <sup>3</sup> )	Infiltration (m <sup>3</sup> )	South Cell transfer (m <sup>3</sup> )	Net Process water (m <sup>3</sup> )
2018	34,675	23,187	160,674	600,000	276,713

**Table 2.8: Annual water outflow in Goose Pit during Period 1**

	Reclaim Water (m <sup>3</sup> )	Entrapped Water (m <sup>3</sup> )
2018	-	996,167

Once the deposition of tailings will be completed, residual water inside the Goose Pit will be transferred to Portage Pit A prior to resuming deposition of tailings. These transfers are planned during the warmest months of the year to avoid operational issues. First transfer of 200,000m<sup>3</sup> is planned in October 2018 and a second transfer of 2.4Mm<sup>3</sup> is planned from May to October 2019. In the event that AEM does not receive the project certificate for the Whale Tail Project, residual process water inside the Goose Pit will be treated as per water quality forecasting requirements in order to meet CCME criteria or other site specific criteria at closure, prior to initiate reflooding activities. Refer to Section 2.3 for the pit flooding activities description.

### 2.1.9 Vault Pit & Phaser Pit

This section has not been updated for this Water Management Plan version as this modification request does not impact Vault and Phaser Pits water management.

### 2.1.10 Water Transfers

Water transfers from various locations around the site are required to reduce freshwater consumption, optimize basin storage, optimize the water balance in general and maintain the

good working order of the different facilities around the mine site. They are also required to prevent off site environmental impacts.

#### 2.1.11 TSF Water Transfers

In order to optimize the tailings deposition sequence, maintain an adequate reclaim pond (operating volume, dike structure protection and water quality), minimize freshwater consumption and perform closure of each cell, water transfers within the tailing storage facilities and pits are required throughout their operating life and in closure. Table 2.9 summarizes the water transfers required around the North Cell and South Cell TSF for adequate water management of these infrastructures from 2017 to 2022.

In 2018, water transfers from the South Cell to the pit (Gosse Pit and Portage Pit A) will be undertaken to promote freeze back of the tailings. The Central Dike seepage, Interception Sump, WEP, SD3-4-5, and ST-16 water are included as transfers into the TSF. All these transfers were recorded in previous years in order to improve the accuracy of the water balance and maintain adequate reclaim pond levels. These transfers are planned through time until the end of operation.

Water transfers from SD3-4-5 to the TSF are required to keep the dike downstream toes free of water. These transfers added to 45,638m<sup>3</sup> in 2017 and are expected to be stable in the upcoming years.

Water transfers from the Stormwater Management Pond (SMP) to the South Cell TSF will stop in 2017 and future transfer will be done in the pit were tailings will be discharged. Regular transfers from the SMP take place twice yearly from 2016 to the closure in 2022. These transfers ensure there is always capacity in the pond to contain runoff water as well as the onsite Sewage Treatment Plant effluent. The transfers from SMP will be directed to the Portage Pit until planned camp closure to play part in the pit flooding process.

The diversion ditches (East and West), located around the perimeter of the North Cell TSF and the Portage RSF, are designed to collect the non-contact water runoff from the surrounding water shed. The ditches are divided in two sections – the west and east sections, to divert non-contact water respectively to Third Portage Lake and to NP1 Lake. On the west end of the diversion ditches, an interception sump was constructed in March 2014 and was completed in 2015. The interception sump has been put in place mainly to control the water quality, in terms of total suspended solids. The interception sump aims to collect runoff water from the west section of the diversion ditches and to retain it until the total suspended solids have reached the criteria allowing discharge to the environment. AEM plans, as per the water balance to pump until end of mine life the entire water accumulation from the Interception Sump into the North Cell. This was done in order to plan the maximum transfers required from North to South Cell and to properly design the required pumping station. However, AEM will promote natural drainage of non-contact water into 3<sup>rd</sup> Portage Lake as much as possible to reduce the overall pumping activities on site, ensuring that water quality meets the required Water License criteria. Water volumes ponding in Waste



Extension Pool (WEP) and Waste Rock Seepage Pond (ST-16) are also planned to be transferred to the North Cell TSF until closure of the mine site.

The Central Dike seepage is included in the water balance in accordance with the 1:1 ratio (South Cell reclaim water to seep water) based on the conclusion of the steady flow test performed during the 50,431m<sup>3</sup> water transfer to Goose Pit in October 2015 and the mass balance exercise completed on a yearly basis by AEM. At the end of each month, the volumes pumped back from the downstream seep location to the South Cell are accounted and compared to the seep volumes leaking out of the South Cell. These seep volumes are calculated through a mass balance based on the South Cell TSF surveyed water elevation. The actual real ratio is monitored through time and used to validate the 1:1 ratio currently used. The Central Dike Seepage mitigation plan is including the complete dewatering of the South Cell in September 2018. AEM is expecting to see the seepage flow to cease at this point in time.

**Table 2.9: North Cell TSF and South Cell TSF water transfers**

North Cell and South Cell TSF Water Transfers - During Operations (m <sup>3</sup> )												
Source	Interception Sump	WEP + SD1	ST-16	North Cell	SD3 + SD4-5	Portage Pit	CD D/S	South Cell	SMP	South Cell	South Cell	South Cell
Discharge	North Cell	North Cell	North Cell	South Cell	South Cell	South Cell	South Cell	CD D/S	South Cell	Goose Pit	Pit A	Pit E
2017	189,560	16,020	50,206	251,666	45,638	144,758	3,623,739	3,763,519	71,433	284,954	0	0
2018	171,214	15,569	19,236	387,053	0	0	Assumed 1:1 ration		0	600,000	523,615	0
2019	171,214	15,569	19,236	387,053	0	0	0	0	0	0	486,864	0
2020	171,214	15,569	19,236	387,053	0	0	0	0	0	0	486,864	0
2021	171,214	15,569	19,236	387,053	0	0	0	0	0	0	486,864	0
2022	171,214	15,569	19,236	387,053	0	0	0	0	0	0	486,864	0

Table 2.10 is presenting the water transfer required during the deposition of tailings inside Goose and Portage Pits. This table summarizes the information presented in the previous section.

**Table 2.10: Goose Pit and Portage Pit TSF water transfers**

Goose Pit and Portage Pit TSF water transfers - During Operations (m <sup>3</sup> )						
Source	SMP	SMP	SWP	Goose	South Cell	3PL
Discharge	Pit A	Pit E	Goose	Pit A	Pit A	Pit E
2017		0	32,461	200,000	0	
2018			34,675	2,400,000	523,615	
2019		11,590	23,085		486,864	
2020	11,590	23,085			486,864	2,000,000
2021	23,085	11,590			486,864	2,000,000
2022		34,675			486,864	



#### 2.1.12 Portage Water Treatment Plant

In May 2015, the Portage water treatment plant (WTP) was dismantled as no more transfers from the former Portage Attenuation Pond will need to be treated and discharged into Third Portage Lake (3PL).

#### 2.1.13 Vault Treatment Plant

This section has not been updated for this Water Management Plan version as this modification request does not impact Vault and Phaser Pits water management.

#### 2.1.14 Phaser Lake dewatering

This section has not been updated for this Water Management Plan version as this modification request does not impact Vault and Phaser Pits water management.

#### 2.1.15 Stormwater Management Pond

The Stormwater Management Pond (SWP) is a small, shallow and fishless, water body that can be seen in Figure 1.5, adjacent to Portage Pit. Treated sewage effluent is discharged to this lake before being transferred to the active TSF (South Cell). The pond also collects freshet flows within its catchment area. A snow dump is located beside this pond since 2016 and an increase in runoff water has been observed since then. Table 2.9 and 2.10 are summarizing the water transfer planned during operation. It was assumed that SWP water will be transfer to the Portage Pit until the closure of the mine site.

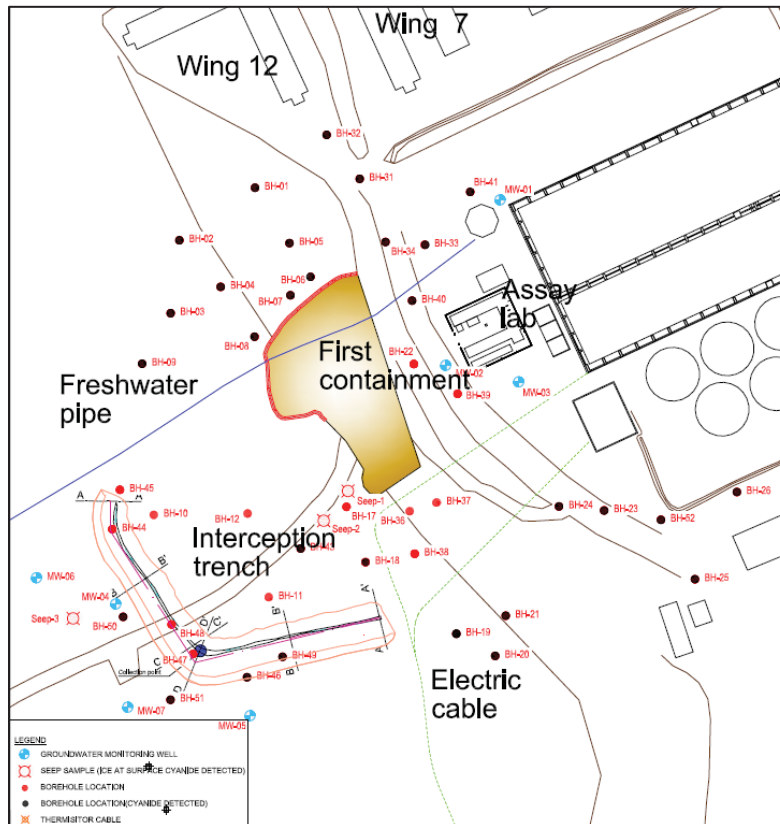
### 2.2 SEEPAGE COLLECTION SYSTEMS

#### 2.2.1 Mill Seepage Collection system

In November 2013, AEM observed seepage discharging west of the access road in front of the Assay lab shown on Figure 2.5. After an investigation, which included initial sampling, drilling of wells and monitoring, contaminants, namely cyanide and copper were identified. The source was determined to be leaking from internal containment structures within the mill. Third Portage Lake (3PL), approximately 200 m to the west, was identified as a possible sensitive receptor. Remedial measures were undertaken immediately and this included construction of an impermeable interception/collection trench downstream of the seepage flow path. A comprehensive monitoring network and plan was implemented which included installation of monitoring wells, a recovery well (MW 203) and a sampling program (including Third Portage Lake). To date no contaminants have been detected in 3PL. Repairs (sealing) were completed within the mill (containment structures) in 2014 to eliminate the source of contaminants. Seepage collected in the trench and recovery well is pumped back to the mill to be used as process water (much the same as reclaim water from the TSF's). The pumping occurs in the warmer months beginning

when freshet commences. The recovery well is pumped year round when water available. No flow of water has been pumped during winter months in the trench because of frozen conditions. Table 2.11 shows the pumped volumes for 2017. AEM observed an increase of the flow to the trench in 2017 (22,428 m<sup>3</sup>) compared to 2016 (11,078 m<sup>3</sup>). AEM is currently investigating the situation.

**Figure 2.5: Mill Seepage Area**



*Table 2.11: Mill Seepage 2017 pumped volumes*

Month	2017 Mill seepage pumped volumes back to the mill (m <sup>3</sup> )
January	0
February	0
March	0
April	0
May	3,025
June	3,973
July	4,961
August	3,782
September	6,687
October	-
November	-
December	-
<b>Total</b>	<b>22,428</b>

#### 2.2.2 ST-16 RSF Seepage management

Refer to the Freshet Action Plan (Appendix D) for the history, long term monitoring plan and remedial actions for this seepage location. The pumping system installed in 2014 is still in operation. Seepage was monitored in accordance with the Freshet Action Plan and 50,206m<sup>3</sup> was pumped back to the North Cell TSF in 2017. Table 2.12 presents the volume of water pumped back to the North Cell TSF from the ST-16 location. There was a higher volume pumped in 2017 (50,206m<sup>3</sup>), compared to 2016 (26,340m<sup>3</sup>). According to AEM, this volume increase is related to higher rainfall observed in 2017. The Figure 2.6 presents the water management strategy developed in 2016 developed to deal with the contact water from the Portage Rock Storage Facility. The infrastructure added in 2016 consists of the two sumps located behind the Portage waste dump (WEP-1 and WEP-2) to collect contact water. All water collected from these sumps is pumped back in the ST-16 sump system and then transferred to the North Cell reclaim pond. Low contaminant levels are still observed by the sampling program. More details will be provided in the 2017 Freshet management plan update.

Figure 2.6: RSF seepage area

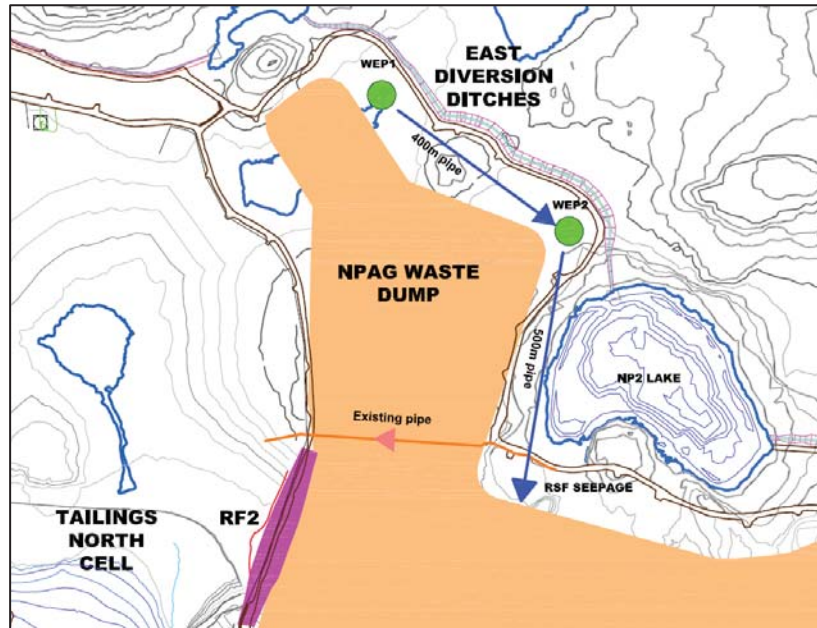


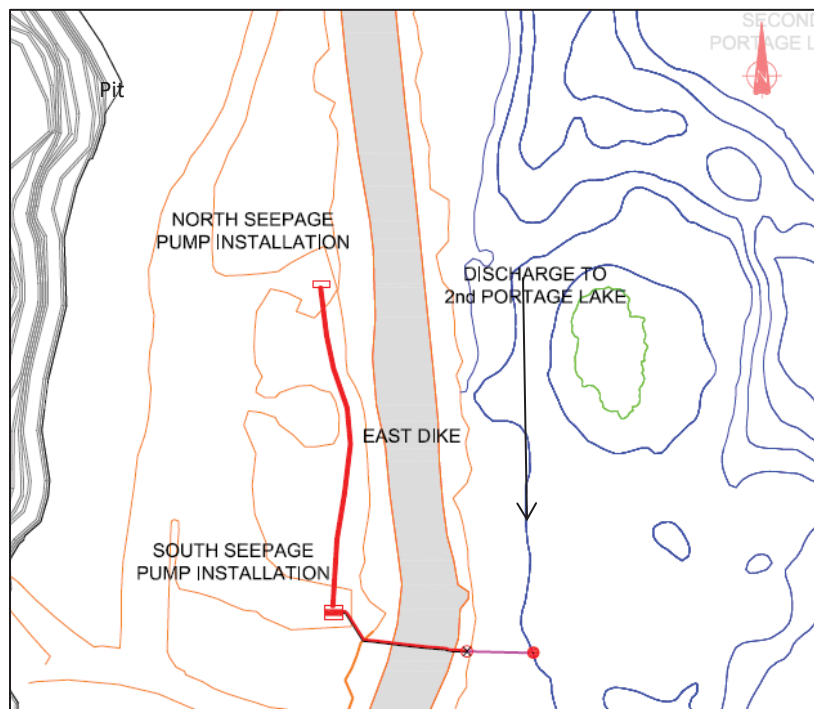
Table 2.12: ST-16 RSF Seepage 2017 pumped volumes

Month	2017 RSF seepage pumped volumes back to NC TSF (m <sup>3</sup> )
January	0
February	0
March	0
April	0
May	16,692
June	20,881
July	5,025
August	4,804
September	2,804
October	
November	
December	
<b>Total</b>	<b>50,206</b>

### 2.2.3 East Dike Seepage Collection

As previously stated, the East Dike Seepage Collection system collects seepage originating from Second Portage Lake (2PL). Seepage from 2PL traverses through the East Dike in two discrete locations and is collected and discharged back, as a combined flow, through a diffuser, to 2PL (in accordance with the Water License and the MMER criteria). Once mining of South Portage Pit area is completed, the East Dike seepage will remain in the Portage Pit as part of the in-pit disposal and pit flooding operations (closure plan). The monthly flow observed in Table 2.13 indicates the 2017 monthly volume discharged to 2PL. If water quality does not meet license or MMER criteria, due to increased TSS during freshet period and large precipitation events in summer, the seepage water is pumped to the mined out areas of the Portage Pit. In 2017, seepage water did not meet license and MMER criteria from May to August 2017 and discharge to 2PL was stopped during that period of time. The total volume returned to Second Portage Lake in 2017 was 66,995m<sup>3</sup>. The historical monthly average of 14,964m<sup>3</sup> has been applied in the water balance until 2031. The discharge into 2PL is planned to cease in September 2018 after Portage Pit mining will be completed. This seepage water volume is included as water inflow during the in-pit deposal process or considered as part of natural reflooding during the closure phase.

**Figure 2.7: East dike pumping system**



As stated in section 2.2 and above, when the discharge is redirected towards the Portage Pit, it is done so specifically in the Portage Central Waste Rock area, where the water flows through the

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deposited rock of the Portage Central Dump. The “voids” in the rock store some of this water; any remaining water flows to the two sumps located at the toe of the Portage Central Dump (which are respectively named sampling locations ST-17 and ST19). From this point, the water is considered Portage Pit inflow regardless of the proportion coming from East Dike Seepage as it is mixed with contact water and groundwater.

**Table 2.13: East Dike Seepage 2017 pumped volumes**

Month	2017 East Dike seepage pumped volumes back to 2PL (m <sup>3</sup> )
January	12,848
February	11,162
March	12,321
April	12,141
May	4,435
June	0
July	0
August	0
September	14,087
October	-
November	-
December	-
<b>Total</b>	<b>66,995</b>

### 2.2.4 Central Dike Seepage

Once tailings deposition started in the South Cell in November 2014, daily inspections of the downstream toe of Central Dike were undertaken as part of the geotechnical inspection program. A small volume of water located against the downstream toe of Central Dike was noticed at that time. This water was contained between the West road and the Central Dike downstream toe. AEM utilized piezometers, thermistors and a ground water well to monitor the dike integrity, the foundation temperatures and the piezometric levels within the structure and its foundation.

On April 14<sup>th</sup> 2015, AEM started pumping at the D/S toe of the dike to lower the water level. The water was pumped back to the South Cell TSF. Water quality was closely monitored to foresee any changes from initial conditions in terms of turbidity and clarity. A flowmeter was also installed to monitor the volume of water pumped. By July 7<sup>th</sup>, 2015 pumping was still on going with a larger pump. The water quality (clarity/turbidity) at the D/S toe is also visually assessed by the Engineering technical personnel during their daily inspection.



Monthly samples are collected as per the Water license (station STS-5) and include analysis for metals, cyanide and major anions. The concentration of some parameters, namely copper, cyanide, sulfates, to name a few, confirms a link between the water ponding at the D/S and the SC reclaim water.

Following the annual site visit of the Meadowbank Dike Review Board in July 2015, steady flow test was performed as recommended by the Board (MDRB, 2015a). SNC performed two specific chemical mass balances to evaluate the ratio of reclaim water, ground water and runoff in the water pumped from the Central Dike D/S pond back into the South Cell TSF (SNC, 2015b). A transfer to Goose Pit was also done to evaluate the same ratio by monitoring the drawdown in the South Cell during the transfer. SNC identified that 50,000 m<sup>3</sup> of seepage transfer from the downstream toe to Goose Pit was possible without compromising water quality at closure (using CCME guidelines for the protection of aquatic life). The 1:1 ratio was confirmed by this test inferring that the seepage water source was the South Cell reclaim water. Other recommendations from the Boards was to assess that the South Cell can be filled as intended, review the seepage model and identify at a conceptual level the mitigation option for the tailings future discharge (MDRB, 2015a).

In September 2015, a second meeting was held with the MDRB to reassess the situation and present result of the seepage model developed by Golder and steady flow pump test performed with SNC. A series mitigation measures were defined and it was confirmed that the Central Dike could be operated safely under certain conditions and agrees that tailings deposition in the South Cell can be resumed (MDRB, 2015b).

In early November 2015, the downstream pond operational level was to be set at 115masl following Golder's recommendations (Golder, 2015). At the same time, a permanent and winterized pumping system was put in place to manage and track the water volumes through the winter. The deposition in South Cell TSF restarted on October 28<sup>th</sup>, 2015. Within the first two weeks of deposition, the seepage flow dropped from 800m<sup>3</sup>/h to 400m<sup>3</sup>/h and then has been stable between 400 to 600 m<sup>3</sup>/h since that time.

In November 2015, Golder conducted a revision of the Central Dike seepage model as mentioned above. AEM observed that the seepage flow was not decreasing as predicted and new information needed to be integrated to the model following field investigation campaigns realized in 2015. The findings of the model were presented to the MDRB in September 2016 (MDRB, 2016). The Board was pleased by the work done and recommended to proceed with a new field investigation campaign to confirm the assumption of the new model which was completed in June 2017.

In the meantime, a new electric pumping system was installed in 2016 to replace the diesel unit previously installed to increase robustness of the pumping installation. Pumping has continued until present day and will continue until TSF closure.

During winter 2017, Golder reviewed seepage model with the updated information from the last year and reevaluate the seepage flow assumption through time (Golder, 2017a). Field

instrumentation campaign was designed following this model update to fill some data gaps identified. Model was presented to the MDRB in March 2017 (MDRB, 2017a).

On July 15<sup>th</sup>, 2017 a sudden rise in turbidity was observed at the Central Dike Downstream Seepage Pond (sampling station ST-S-5). In the following days, turbidity readings continued to be high. An increase in turbidity was observed on the field and a sludgy orange deposit was identified on shoreline rock. A review of all instrumentation data was conducted following the July 18<sup>th</sup> inspection and only one instrument was showing unexpected behavior; a piezometer directly in the seepage pond showing temperature spikes. On July 22<sup>nd</sup>, AEM sampled the orange precipitate at the bottom of the pond for mineralogy and chemical analysis. Aerial investigation of the South Cell TSF was performed during the morning of July 23<sup>rd</sup>. A large deformation in the tailings beach was identified in front of SD4 with smaller depressions surrounding this deformation. The Portage Pit was inspected and no seepage reporting to the pit wall or change in coloration or turbidity inside pit sumps was observed. The average seepage flow measured was around 575m<sup>3</sup>/h in July 2017 compared to 450m<sup>3</sup>/h predicted by the Central Dike seepage model updated by Golder in 2017. AEM organized a meeting with the MDRB on July 28<sup>th</sup> to reevaluate the alert level of the Central Dike in accordance with the Tailings Storage Facility Operation Maintenance and Surveillance Manual (TSF OMS) and the Central Dike Trigger Action Response Plan. The alert level was raised from yellow to orange during this meeting and an action plan was developed to address the situation. The communication plan set in the TSF OMS has also been respected to notify applicable stakeholders.

AEM identified the risk of tailings migration out of the South Cell TSF and established a sampling monitoring program to evaluate the nature of the Central Dike D/S pond orange precipitate. This program consisted of:

- Sampling, on a weekly basis, the South Cell reclaim water, Central Dike D/S pond and Portage Pit A sump;
- Sampling the orange precipitate in the Central Dike D/S pond and perform mineralogy and chemical analysis, and;
- Sampling of the tailings in front of SD4 and compare it to the grey sediment in the Central Dike D/S pond in order to evaluate the nature of the sediment.

Visual inspections were done on a daily basis couple with daily instrumentation interpretation. AEM also performed a bathymetry of the depressions in front of SD4 to evaluate its size and proliferation. This major depression was inspected on a weekly basis via aerial inspections.

Following the recommendation of the MDRB, AEM initiated the evaluation of changing the global water and tailings management strategy of the South Cell TSF. The Board was pleased with the short term action plan developed by AEM and recommended promoting tailings deposition in front of SD4 as soon as possible.

The bathymetry of the tailings depression by Saddle Dam 4 was completed on July 28<sup>th</sup>. The depression has dimensions of 30x36x1m for a volume of 1,080 m<sup>3</sup>. Tailings deposition in the

deformation area was successfully completed around mid-August 2017. It was observed during the aerial inspection of August 14<sup>th</sup> that a significant tailings beach covered the toe of SD4 and the depression area.

An update on the Central Dike seepage situation was done during the MDRB annual meeting #22 held in Meadowbank from September 4<sup>th</sup> to 7<sup>th</sup>. Given the concern with the under-seepage at Central Dike, the Board reiterated that the preferred option for the Whale Tail operation will be in-pit disposal in the mined out Portage and Goose Pits. The Board also agreed to reduce the volume of water inside the South Cell TSF in order to reduce the hydraulic gradient towards the Central Dike downstream pond and consequently the seepage flow rate (MDRB, 2017b).

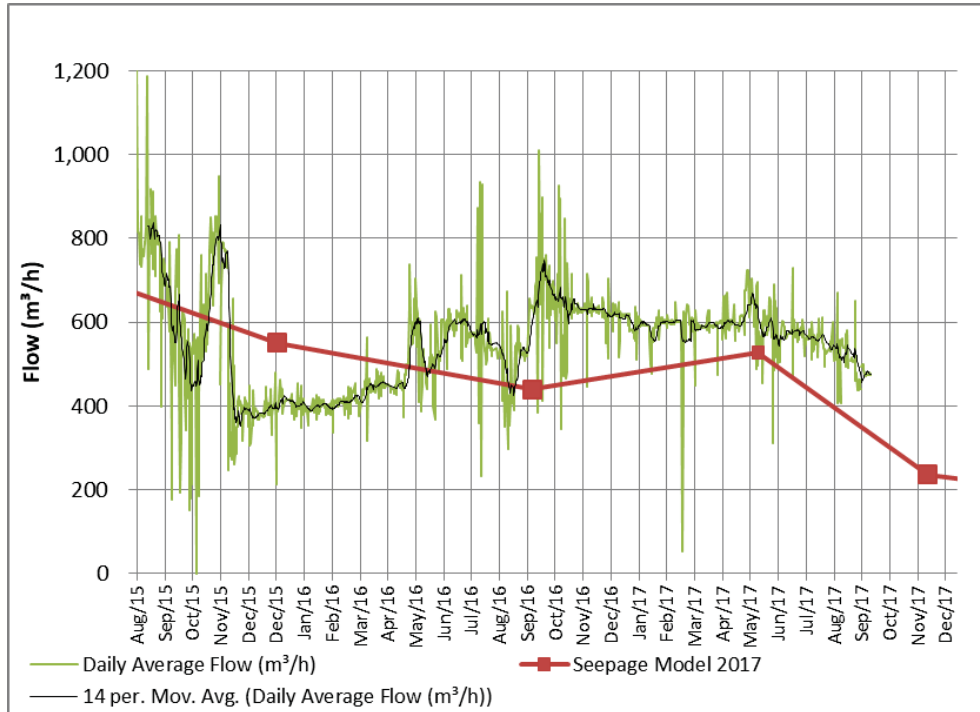
AEM moved forward with a water transfer from the Central Dike downstream pond towards Goose Pit. A total of 284,065 m<sup>3</sup> was pumped from August 29<sup>th</sup> to September 19<sup>th</sup>. The Central Dike seepage flow rate reduced from 525 to 475m<sup>3</sup>/h following the water transfer, remaining above the Golder seepage model forecast (Golder, 2017).

On September 28<sup>th</sup>, the analysis of the data collected during the sampling program revealed that the orange precipitate was the result of a biological process leading to the production of a ferric precipitate. Rises in turbidity and new ferric precipitate events will likely continue to happen in future years until pit flooding is completed.

The Central Dike seepage situation is under control as AEM has the pumping capacity to deal with the seepage flow rate, the integrity of the infrastructure has not been compromised, no tailings was found outside the perimeter of the South Cell TSF and the nature of the orange precipitate was identified as a biological iron precipitate. Variations of temperature observed on the piezometer in the Central Dike downstream pond were explained also be the occurrence of the biological reaction. The sustained tailings beach in front of SD4 shown that the depression was localized and non-sustained event. AEM is considering the opportunity of discharging tailings in Goose Pit as recommended by the MDRB in April 2018 and stop operation of the South Cell TSF.

Table 2.14 presents the water pumped from the Central Dike D/S pond to the South Cell TSF so far in 2017. The figure 2.8 shows the Central Dike seepage pumping flow rate compared to the Golder seepage analysis (Golder, 2017).

*Figure 2.8: Central Dike seepage pumping system*



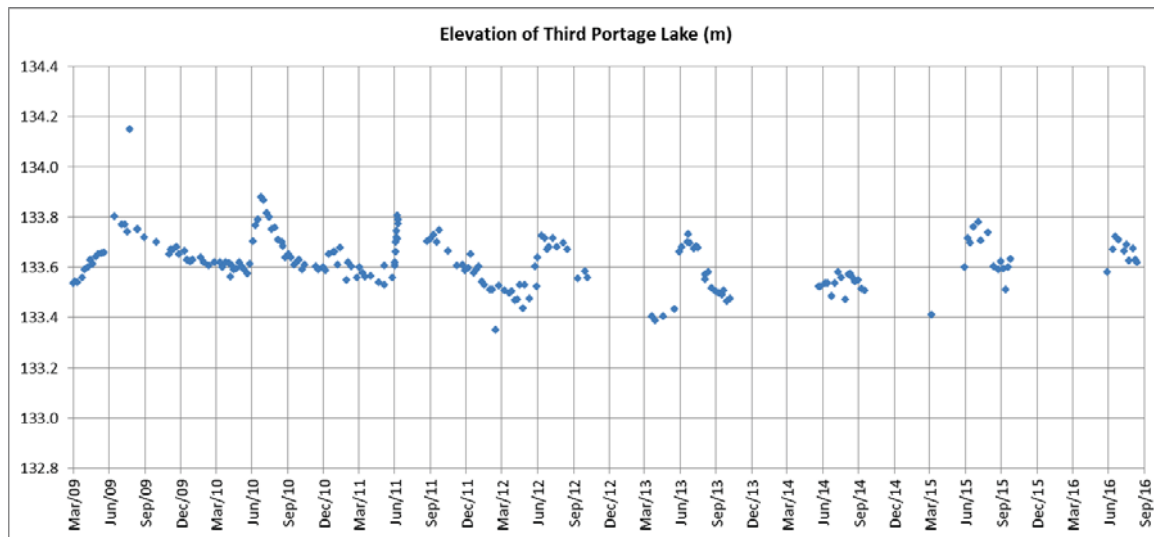
**Table 2.14: Central Dike Seepage 2017 pumped volumes**

Month	2017 Central Dike seepage pumped volumes back to SC TSF (m³)	2017 Central Dike seepage pumped volumes back to Goose Pit (m³)
January	514,587	0
February	406,884	0
March	536,263	0
April	453,079	0
May	372,155	0
June	648,114	0
July	422,908	0
August	329,029	26,889
September	80,500	258,065
October	-	-
November	-	-
December	-	-
<b>Total</b>	<b>3,763,519</b>	<b>284,954</b>

## 2.3 PIT FLOODING

The volumes of water needed for pit flooding, part of the overall closure plan, is dependent on the water elevation of Third Portage Lake (3PL). The Goose dike can only be breached when the level of the flooded pits reaches the same elevation as 3PL and pit water quality meets CCME/site specific criteria concentrations. According to 3PL elevation data from 2013-2016 this elevation would be 133.6masl. Figure 2.9 shows the elevation data recorded since 2009.

**Figure 2.9: Distribution of TPL elevation surveyed data**



The current flooding technique proposed for Portage and Goose Pits is to use a combination of pumps and siphons to achieve the pumping rates prescribed by the water balance which conforms to the approved volume stipulated in the Water License. Details of the complete flooding system will be available in the Final Reclamation and Closure Plan. In the previous Water Management Update, AEM was considering a total of 32.0Mm<sup>3</sup> of freshwater to be transferred from 3<sup>rd</sup> Portage Lake to accomplish the required pit flooding for Portage and Goose Pits. By implementing the tailings deposition practice in Meadowbank, water required for flooding decreases to 24.6Mm<sup>3</sup> including the water used during the operation to flood the Portage Pit and operate in-pit deposition with a constant water cover over the tailings beach. This is representing a global reduction of 7.4Mm<sup>3</sup> of freshwater.

As Goose Pit tailings deposition is completed in September 2018, 2.6Mm<sup>3</sup> of water from Goose Pit will be transfer to Portage Pit to initiate in-pit deposition. Active flooding of Goose Pit is planned to commence in 2020 with a transfer of 2.0Mm<sup>3</sup>. In-pit deposition will cease in the Portage Pit in January 2022. Pit flooding of the Portage Pit will commence in June 2022. At water elevation 131.0 masl both Portage and Goose Pits will join to become one waterbody. Reflooding will continue to the natural Third Portage Lake water elevation at approximately 133.6masl. At this level the dikes can be breached; however this is dependent on pit water quality. The current objective is to ensure the water meets CCME Guidelines for the Protection of Aquatic Life and/or

site specific criteria for parameters not listed in the CCME guidelines before the dike is breached. The first phase of the flooding sequence is planned to be completed in June 2027. Four years of monitoring is planned at that point to evaluate the water quality in the pits. During this time, water runoff will be diverting into the pits to finish the flooding to the 3PL elevation. Breach of the Goose Dike is planned for 2031.

The treatment requirements of the reclaim water will be determined as per the In-Pit Tailings Deposition Water Balance and Water Quality Forecast completed by SNC (September, 2017 – See Appendix B) This report is presenting the water quality under a full capacity scenario where all the pits are filled up to elevation 125.6m. However, SNC reviewed the water quality forecast for this water management plan and predicts that arsenic, chromium, copper, selenium, fluoride, ammonia and total  $N_{\text{equivalent}}$  may require treatment to reach CCME criteria based on the completely mixed assumption.

AEM is committed to updating the Water Quality Forecast Model, using up to date, year over year data, on a yearly basis until, and possibly after, the cessation of mine operations. The water transfers between Portage and Goose Pits could also be revised in the future depending on mining plan updates and water balance changes.

To reach the water elevation of 133.6m, a volume of  $45,6\text{Mm}^3$  needs to be filled. As previously stated,  $24,6\text{Mm}^3$  originates from 3<sup>rd</sup> Portage Lake,  $11,3\text{Mm}^3$  balance will be made up from the natural pit water inflows including runoff and precipitation combined with reclaim water, and the residual volume of  $9,7\text{Mm}^3$  would be occupied by tailings. The difference from the 2016 Water management plan (AEM, 2016a) is related to storage of tailings in each pit and by postponing the closure date which allows storage of runoff water for a longer period of time. Note that AEM feels that this approach is conservative, with respect to TSF runoff, as water quality of the runoff should be able to be re-directed to Third Portage Lake five years after capping which is consistent with the initial function of the diversion ditch system (however please note that the runoff from the capped TSF's will be directed to the pits until the water quality meets closure criteria). Please refer to Table 2.15 for the reflooding sequence per year for all pits. Nothing has changed for Vault, Phaser and BB Phaser Pits.



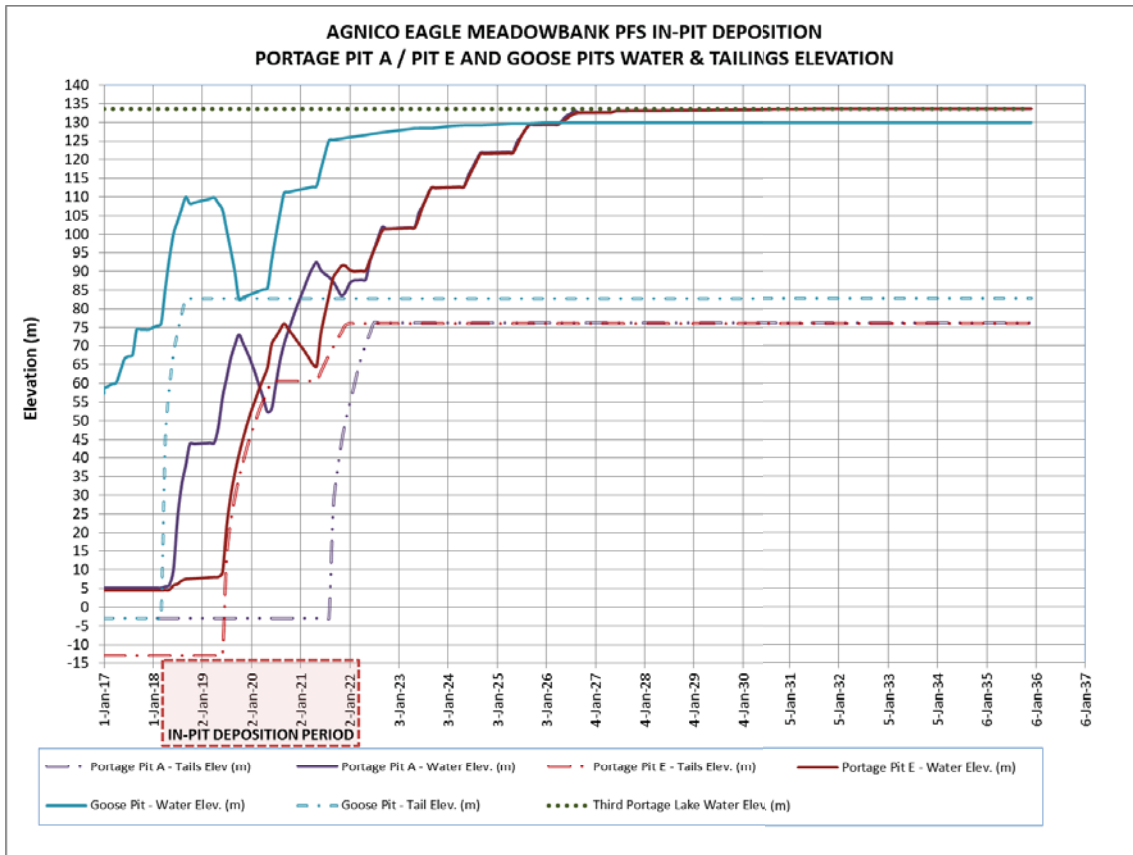
**Table 2.15 : Pit flooding profile**

Pit Flooding profile									
Year	Volumes pumped from 3 <sup>rd</sup> Portage lake				Volumes pumped from Wally lake				Total flooding water (m <sup>3</sup> )
	To Portage Pit A (m <sup>3</sup> )	To Portage Pit E (m <sup>3</sup> )	To Goose pit (m <sup>3</sup> )	From 3PL (m <sup>3</sup> )	To Vault pit (m <sup>3</sup> )	To Vault Attenuation Pond (m <sup>3</sup> )	To Phaser pit (m <sup>3</sup> )	From Wally Lake (m <sup>3</sup> )	
2016	0	0	0	0	0	0	0	0	0
2017	0	0	0	0	0	0	0	0	0
2018	0	0	0	0	0	0	0	0	806,275
2019	0	0	0	0	4,131,994	0	0	4,131,994	9,032,319
2020	0	2,000,000	2,000,000	4,000,000	4,131,994	0	0	4,131,994	9,525,428
2021	0	2,000,000	1,500,000	3,500,000	4,131,994	0	0	4,131,994	9,032,319
2022	1,600,000	2,400,000	0	4,000,000	4,131,994	0	0	4,131,994	9,032,319
2023	1,600,000	2,400,000	0	4,000,000	4,131,994	0	0	4,131,994	9,032,319
2024	1,600,000	2,400,000	0	4,000,000	0	0	0	4,131,994	9,032,319
2025	1,600,000	2,400,000	0	4,000,000	0	476,342	0	3,735,476	5,062,105
2026	1,600,000	2,400,000	0	4,000,000	0				
2027	165,000	535,000	0	700,000	0				
<b>Total</b>	<b>8,165,000</b>	<b>16,535,000</b>	<b>3,500,000</b>	<b>28,200,000</b>	<b>28,051,098</b>	<b>476,342</b>	<b>0</b>	<b>28,527,440</b>	<b>60,555,403</b>

As prescribed in the Nunavut Water Board Water License No. 2AM-MEA1525 (Part E, Conditions 1 and 2), the use of water from Third Portage Lake, for all purposes, including flooding of the pits, shall not exceed a total 2,350,000 m<sup>3</sup> per year from the License approval date to December 31 2017, followed by a maximum 4,935,000 m<sup>3</sup> starting in 2018 through to the expiry of the License 2AM-MEA1525. The use of water from Wally Lake shall not exceed a total 4,185,000 m<sup>3</sup> per year starting in 2018 through the expiry of the License 2AM-MEA1525. As per the recommendations and requirements concerning the water use, the Meadowbank Water Management Plan will be updated on an annual basis. The Water Management Plan includes a pit flooding strategy meeting the requirements outlined in the Nunavut Water Board Water License No. 2AM-MEA1525.

AEM will provide at least 30 days notice to the Nunavut Water Board and Inspector prior to starting the flooding of each pit from water obtained from Third Portage Lake and Wally Lake.

Figure 2.10: Goose pit and Portage Pit re flooding



### 2.3.1 Goose Pit Flooding

Goose Pit flooding started in 2015 by allowing the natural inflow volume (runoff, groundwater, precipitation and possible Bay Goose dike seepage) of 383,800m<sup>3</sup> to remain within the pit. Goose Pit flooding continued in 2016 by again allowing the inflow volume of 352,431 m<sup>3</sup> to remain within the pit, 8% more than the our model (SNC, 2015b) for this particular year. AEM expects that future yearly run offs fall under the model values because the model does not account for lowering the hydraulic gradient which should lower groundwater flows. In April 2018, dewatering of the South Cell will be initiated with a transfer of 600,000 m<sup>3</sup> toward Goose Pit. Transfers from 3PL to Goose Pit are planned from 2020 to 2021 in order to reach 130.0masl at the same moment than the Portage Pit. At this point, the Goose water will join the Portage Pit water to form one water body. Figure 2.10 depicts the Goose Pit flooding curve. Goose Pit volumes between 131masl and 133.6masl are included as part of Portage flooding volumes.

Artificial flooding – from 3PL – will end in August 2021 after which natural pit inflow will allow for the level to reach the 3PL lake elevation in 2031. If water quality meets all closure criteria including CCME guidelines and site specific criteria, the Goose dike will then be breached. Refer to Section 3 for the pit water quality forecast model.

### 2.3.2 Portage Pit Flooding

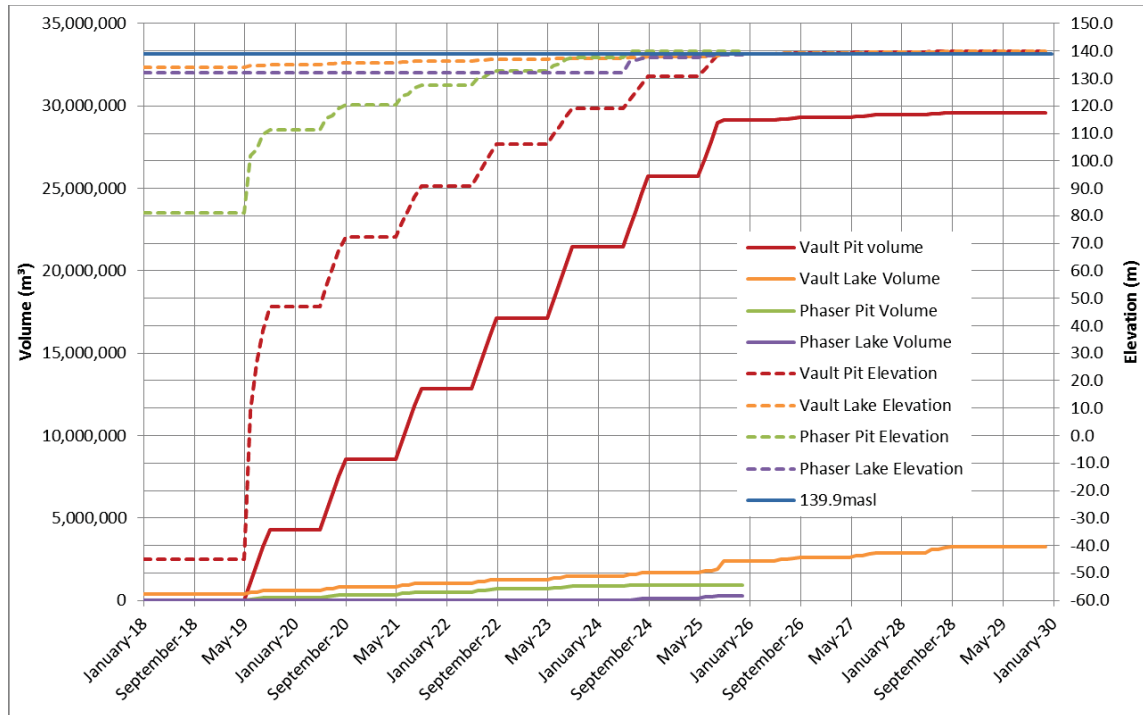
Portage Pit A reflooding will begin in July 2018 with 523,615m<sup>3</sup> transferred and treated (if required) from the South Cell. All runoff water from the North and South Cell TSF will be transferred in Portage Pit A from 2019 to 2031. In 2020, 2Mm<sup>3</sup> transferred from 3PL to the Portage Pit E will be done in order to flood the Portage Pit and keep the tailings beach covered by a 20m water cover during the tailings deposition inside Portage Pit. A second transfer from 3PL toward Pit E of 1.5Mm<sup>3</sup> will be required in 2021 for the same reason. Table 3.15 presents transfers planned from 3<sup>rd</sup> Portage Lake to the Portage Pit from 2020 to 2027 to complete the total artificial flooding to elevation 131masl. From this point, runoff water and other pit inflows will be used to complete flooding of both pits until elevation 133.6masl is reached at the end of 2031. See Figure 2.10 to view the pit reflooding curve which includes all water sources used to reflood the pit, including both South Cell reclaim transfers and 3<sup>rd</sup> Portage lake transfers. Refer to Section 3 for the pit water quality forecast model.

### 2.3.3 Vault Pit Flooding

The Vault pit area is composed of many basins in the former lake and different pit elevations that are all linked together. The flooding of Vault and Phaser is more complex and requires water transfers from basin to basin. Reflooding from Wally Lake of the Vault area will commence in 2019 and will continue until the end of summer 2024 using a siphon system similar to the one planned in Goose and Portage. This active flooding will occur at an annual rate of 4,131,994m<sup>3</sup> and finally 3,259,134m<sup>3</sup> in 2025. Like Portage and Goose, from 2025 to 2029 the natural inflow will then allow Vault pit to reach 139.9masl (natural Wally Lake water level). The reflooding of Vault area with natural inflow consists of approximately 0.5Mm<sup>3</sup> yearly from freshet, precipitation, groundwater inflow. The flooding curves for the Vault area are represented in Figure 2.11. The final elevation of the reflooding will be 139.9masl for Phaser and Vault Lake. At this point the Vault dike will be breached provided the water meets CCME criteria and/or site specific criteria for parameters not included in the CCME Guidelines. Refer to Table 2.15 for the yearly cumulative volumes required to complete the flooding process. Refer to section 3 of this present report for the pit water quality forecast model.

Unlike Vault Pit, Phaser Pits and Lake are planned to be flooded exclusively from their watershed runoff inflows until the target elevation of Wally is reached in summer 2027. From there, those same inflows will be used conjointly with the Vault ATP inflows to flood to the same target elevation as the Vault ATP area – 139.9masl (Wally Lake level).

Figure 2.11: Vault and Phaser Pits flooding



## 2.4 WATER MANAGEMENT STRUCTURES

As per the Water License 2AM-MEA1525 (Part E, Condition 10) AEM will conduct weekly inspections of all water management structures during periods of flow. This program commenced in 2016 and was added to the weekly inspections already undertaken as per the Freshet Action Plan (Appendix D) at water conveyance structures during flow periods. Records of the inspections will be available for review by an Inspector upon request.

### **Section 3.0 - MEADOWBANK WATER QUALITY FORECASTING UPDATE**

The water balance and water quality forecast report was prepared by SNC-Lavalin (SNC, 2017f) was initially done using the full capacity scenario presented in the section 1.2. This report is also presented in the appendix B. AEM requested to SNC to update in a second time the water quality forecast with the actual Meadowbank LOM and with the addition of the potential Whale Tail Pit Project. This update was completed in respect with the continuation of a series of yearly water quality modelling forecast reports that commenced in 2012. AEM is planning continuing this practice until mine closure as per the Water License part E item 7. The purpose is to identify through a mass balance approach the contaminants of concern during the pit flooding process and determine if water treatment will be required on site for closure activities when comparing the final contaminant levels to the CCME guidelines and/or site specific criteria for parameters that are not included in the CCME Guidelines. Each yearly update builds on the previous year as new monitoring data is added at the site. Forecasted model values of the prior years are compared with the actual sample results from the following years for model calibration purposes.

This management plan is presenting two different water quality forecast. The one presented in the table 3.1 is showing the water quality forecast associated with the LOM and water balance used in this water management plan. SNC-Lavalin developed this water quality forecast especially for the case presented in this management plan.

Considering the scenario presented in this Water management plan, SNC identified seven contaminants: arsenic, chromium, copper, selenium, fluoride, chromium, ammonia and total  $N_{equivalent}$  as parameters which may require treatment. These parameters may be of concern prior to dike breaching, treatment options for their removal during or after the pit flooding process will need to be examined and will be assessed in greater detail during the preparation of the final closure and reclamation plan. These contaminants originate from the process water transferred in the pits in 2018 and also from products of the milling process of Whale Tail Pit ore.

SNC-Lavalin also developed a water quality forecast that present a full capacity scenario. This scenario includes tailings deposition inside Portage and Goose Pit up to elevation 125.6m with a water cover of 8m. This report is presented in the Appendix B and presents the water balance and water quality forecast associated with the full capacity scenario.

## 2016 WATER MANAGEMENT PLAN UPDATE

Table 3.1: Water Quality Forecast of Reclaim Water in Portage Pit A, Pit E and Goose Pit

PARAMETERS	UNITS	CCME GUIDELINES	3rd PORTAGE LAKE (avg. Summer 2015)	FORECASTED CONCENTRATIONS									
				AT END OF DEPOSITION JANUARY 2022				AT END OF MONITORING PERIOD DEC. 2031					
				PORTAGE PIT A	PORTAGE PIT E	MIXED PORTAGE PIT	GOOSE PIT	PORTAGE PIT A	PORTAGE PIT E	MIXED PORTAGE PIT	GOOSE PIT	MIXED PITS	
Alkalinity	mg CaCO <sub>3</sub> /L	n/a	9.1	89	76	n/a	21	20	22	21	25	22	
Hardness	mg CaCO <sub>3</sub> /L	n/a	12.05	836	718	n/a	67	109	134	124	66	116	
Total dissolved solids	mg/L	n/a	22.1	2123	1744	n/a	233	264	322	299	243	291	
Total Aluminium (Al)	mg/L	0.10	0.0075	0.26	0.21	n/a	0.04	0.04	0.04	0.04	0.03	0.04	
Total Silver (Ag)	mg/L	0.00025	0.0000	0.00050	0.00020	n/a	0.00042	0.00006	0.00006	0.00006	0.00057	0.00014	
Total Arsenic (As)	mg/L	0.005	0.0005	0.621	0.579	n/a	0.002	0.071	0.098	0.088	0.001	0.074	
Total Barium (Ba)	mg/L	n/a	0.003658	0.1340	0.1198	n/a	0.0094	0.0188	0.0236	0.0217	0.0101	0.0200	
Total Cadmium (Cd)	mg/L	0.00004	0.0000	0.00006	0.00003	n/a	0.00010	0.00001	0.00001	0.00001	0.00016	0.00003	
Total Chromium (Cr)	mg/L	0.001	0.0001	0.008	0.007	n/a	0.000	0.001	0.001	0.001	0.000	0.001	
Total Copper (Cu)	mg/L	0.002	0.000595	0.767	0.608	n/a	0.077	0.087	0.106	0.098	0.061	0.093	
Total Iron (Fe)	mg/L	0.30	0.0173	1.47	1.30	n/a	0.18	0.20	0.24	0.23	0.24	0.23	
Total Lead (Pb)	mg/L	0.001	0.0000	0.002	0.002	n/a	0.000	0.000	0.000	0.000	0.000	0.000	
Total Manganese (Mn)	mg/L	n/a	0.0016	0.114	0.086	n/a	0.100	0.020	0.021	0.020	0.172	0.043	
Total Mercury (Hg)	mg/L	0.000026	0.000003	0.000018	0.000012	n/a	0.000012	0.000007	0.000005	0.000006	0.000018	0.000008	
Total Molybdenum (Mo)	mg/L	0.073	0.0002	0.110	0.069	n/a	0.027	0.013	0.013	0.013	0.023	0.014	
Total Nickel (Ni)	mg/L	0.025	0.0006	0.068	0.061	n/a	0.003	0.009	0.011	0.010	0.003	0.009	
Total Selenium (Se)	mg/L	0.001	0.0000	0.011	0.004	n/a	0.004	0.001	0.001	0.001	0.004	0.001	
Total Strontium (Sr)	mg/L	n/a	0.013225	0.431	0.310	n/a	0.076	0.062	0.066	0.064	0.060	0.064	
Total Thallium (Tl)	mg/L	0.0008	0.0000	0.0005	0.0003	n/a	0.0009	0.0003	0.0003	0.0003	0.0016	0.0005	
Total Uranium (U)	mg/L	0.015	0.000049	0.002	0.001	n/a	0.001	0.000	0.000	0.000	0.001	0.000	
Total Zinc (Zn)	mg/L	0.03	0.001500	0.005	0.003	n/a	0.003	0.003	0.002	0.002	0.004	0.002	
Chloride	mg/L	120	0.7925	96	70	n/a	14	12	13	12	12	12	
Fluoride (F)	mg/L	0.12	0.07925	0.30	0.22	n/a	0.14	0.11	0.10	0.11	0.15	0.11	
Sulphate (SO <sub>4</sub> )	mg SO <sub>4</sub> /L	n/a	5.1	1717	1371	n/a	179	198	242	225	156	214	
Total Cyanide (CNI)	mg/L	0.005	0.0005	1.028	2.462	n/a	0.000	0.000	0.000	0.000	0.000	0.000	
Total Ammonia (NH <sub>3</sub> + NH <sub>4</sub> )	mg N/L	1.83	0.015	15.1	10.7	n/a	2.3	1.7	2.1	1.9	1.9	1.9	
Nitrate (NO <sub>3</sub> )	mg N/L	2.94	0.033	2.66	1.83	n/a	0.43	0.48	0.39	0.43	0.36	0.42	
Total N equivalent	mg N/L	0.35	0.048	17.8	12.6	n/a	2.8	2.2	2.5	2.4	2.2	2.3	
Dissolved Aluminium (Al)	mg/L	0.1	0.0018	0.123	0.093	n/a	0.019	0.021	0.019	0.020	0.020	0.020	
Dissolved Silver (Ag)	mg/L	0.00025	0.0000	0.00046	0.00019	n/a	0.00020	0.00006	0.00005	0.00005	0.00018	0.00007	
Dissolved Arsenic (As)	mg/L	0.005	0.0005	0.6198	0.5780	n/a	0.0015	0.0707	0.0981	0.0873	0.0013	0.0742	
Dissolved Barium (Ba)	mg/L	n/a	0.0037	0.1330	0.1191	n/a	0.0092	0.0187	0.0235	0.0216	0.0100	0.0198	
Dissolved Cadmium (Cd)	mg/L	0.00004	0.0000	0.00005	0.00003	n/a	0.00010	0.00001	0.00001	0.00001	0.00016	0.00003	
Dissolved Chromium (Cr)	mg/L	0.001	0.0001	0.0020	0.0020	n/a	0.0002	0.0003	0.0004	0.0004	0.0001	0.0003	
Dissolved Copper (Cu)	mg/L	0.002	0.0005	0.696	0.552	n/a	0.070	0.079	0.096	0.089	0.056	0.084	
Dissolved Iron (Fe)	mg/L	0.3	0.0050	1.3	1.1	n/a	0.0	0.2	0.2	0.2	0.0	0.2	
Dissolved Lead (Pb)	mg/L	0.001	0.0000	0.001	0.001	n/a	0.000	0.000	0.000	0.000	0.000	0.000	
Dissolved Manganese (Mn)	mg/L	n/a	0.0012	0.107	0.082	n/a	0.066	0.020	0.018	0.019	0.113	0.033	
Dissolved Mercury (Hg)	mg/L	0.000026	0.0000	0.000016	0.000011	n/a	0.000012	0.000006	0.000005	0.000005	0.000018	0.000007	
Dissolved Molybdenum (Mo)	mg/L	0.073	0.0002	0.106	0.066	n/a	0.026	0.012	0.012	0.012	0.023	0.014	
Dissolved Nickel (Ni)	mg/L	0.025	0.0005	0.022	0.019	n/a	0.002	0.004	0.004	0.004	0.003	0.004	
Dissolved Selenium (Se)	mg/L	0.001	0.0000	0.011	0.004	n/a	0.004	0.001	0.001	0.001	0.004	0.001	
Dissolved Strontium (Sr)	mg/L	n/a	0.0135	0.422	0.304	n/a	0.074	0.061	0.065	0.063	0.059	0.062	
Dissolved Thallium (Tl)	mg/L	0.0008	0.000005	0.0005	0.0003	n/a	0.0009	0.0003	0.0003	0.0003	0.0016	0.0005	
Dissolved Uranium (U)	mg/L	0.015	0.000045	0.0021	0.0011	n/a	0.0006	0.0003	0.0003	0.0003	0.0005	0.0003	
Dissolved Zinc (Zn)	mg/L	0.03	0.000625	0.0035	0.0022	n/a	0.0025	0.0016	0.0011	0.0013	0.0039	0.0017	

AEM is committed to implementing the recommendations provided in the SNC Water Modelling Report in 2017 submitted with the 2016 Water Management Plan (AEM, 2016a) in March 2016 and beyond. These are:

- Continue the current monitoring program of the water in the South Cell TSF Reclaim Pond in 2017 for cyanide, total and dissolved metal scan, ammonia, nitrate, chloride, sulfates, total dissolved solids (TDS) and total suspended solids. It is understood that this recommendation is required as per the water license.
- Regular monitoring of pit water quality (Portage and Goose) should also be undertaken, when the site can be safely accessed, and analyzed for cyanide, total and dissolved metals, ammonia, nitrate, chloride, fluoride, sulfates, total dissolved solids (TDS) and total suspended solids. This information will be useful in developing and calibrating a water quality forecast model of the pit water quality based on loadings from surface runoff and possible underground water seepage.



- If possible quantify the seepage flows or volumes entering the Portage and Goose Pits. The study should also attempt to evaluate the seepage rate into the pits as a function of the hydraulic difference between the water level in the pit and in Third Portage Lake.
- Once transfer of South Cell Reclaim Water begins to the Portage Pit, regular (at least monthly) monitoring of all outflows of the TSF Reclaim Pond for all parameters should be undertaken, including TSS to ensure low level during transfer.
- In order to validate the assumption of a well-mixed system in Portage and Goose Pits, it is recommended to sample and analyze the water at different depths before, during and after the pits are filled with water from South Cell TSF and/or Third Portage Lake, when or if it is safe to do so. Furthermore, it may be useful to evaluate the assumption of a well-mixed versus stratified pit water quality prior to mixing Portage and Goose Pits.
- Once Portage and Goose Pits are hydraulically connected, it is recommended to sample the water at different points in the pit area in order to evaluate the mixing efficiency over the entire area. The samples should be taken at different depths over the entire area of the flooded pits before and after the filling season.
- Continue to sample and analyze as per the Water License requirement the Vault Pit and Vault Attenuation Pond and include ammonia and nitrate in the list of parameters to analyze for.
- Perform a bench scale water treatment test to evaluate the contaminant removal efficiency using treatment approaches such as lime neutralization, coagulation/flocculation with aluminium sulphate or ferric sulphate, and coagulation/flocculation with proprietary coagulants designed for metal removal.

This version of the Meadowbank Water Management Plan Report as part of the Water Licence modification request includes in appendix the updated water quality model and the comparison of predicted and measured water quantity and quality.

## **Section 4.0 - 2016 INTEGRATED DEPOSITION PLAN**

A Tailings Deposition Plan prepared by AEM has been used to update last year's model until the completion of the deposition in the South Cell in March 2018. The 2017 bathymetry was compared to the 2013 to 2016 bathymetries. The analysis revealed that ice entrapment and tailings dry density observed during the winter 2015-2016 was consistent with what was observed during winter 2016-2017. Average tailings dry density measured was down to 1.30t/m<sup>3</sup> instead of the average of 1.43t/m<sup>3</sup> observed in the South Cell during the previous year. Sub-aerial and sub-aqueous beach angles are also consistent meaning that the global deposition strategy implemented in 2015 is still efficient.

A simplified deposition plan was produced for the in-pit deposition phase and a flat geometry assumption was used for the disposal of the tailings inside Goose and Portage Pits. An extensive deposition plan will be submitted upon the approval of the Water License modification request. This assumption was considered acceptable as AEM planned a minimum water cover of 20m above the tailings beach during the in-pit deposition process which should compensate for any slopping of the tailings beach is observed during that period.

The deposition strategy considered for this management plan is divided into the following distinct periods:

- Period 1: Portage/Vault tailings deposition in South Cell TSF and in Goose Pit
- Period 2: Whale Tail tailings deposition in Portage Pit
- Period 3: Pit Closure at the end of operations
- Period 4: Monitoring period
- Period 5: Post closure

The deposition strategy was described in detail in the section 3.1.1 to ease the reading of the report and will not be covered again in this section. Closure water management for the TSF was updated to optimize the pit flooding process. These activities are detailed in the section 3.2. The deposition plan associated with this Water Management Plan update is presented in the 2016 Mine Waste Rock and Tailings Management Report & Plan Update (AEM, 2017).

## **Section 5.0 - CONCLUSION**

This report presents an updated/revised water management plan for the Meadowbank mine based on the AEM 2016 Water Management Plan (AEM, 2016a) submitted to the NWB as part of the AEM 2015 Annual Report. This Water Management Plan updated is part of a Water Modification requested by AEM to the Nunavut Water Board (NWB) concerning the Meadowbank project. AEM wants to initiate deposition of tailings inside the Goose and Portage Pits and start the closure of the South Cell TSF earlier than planned. These modifications to the management plan are done in accordance with the recommendation of the Meadowbank Dike Review Board (MDRB, 2017b) related to the situation of the Central Dike Seepage.

The Alert Level of the Central Dike was raised to orange following the following observations in July 2017:

- A sudden rise in turbidity was observed at sampling station ST-S-5;
- An orange precipitate settled at the bottom of the Central Dike Downstream Pond;
- A 1,080 m<sup>3</sup> depression was observed in the tailings beach located in front of SD4;

In addition to these observations, the seepage flow did not follow the one predicted in the Golder Central Dike seepage model reviewed in 2017. An increase of 45% of the Central Dike seepage flow was measured year to date in between data collected in 2016 and 2017.

AEM initiated an action plan to address the situation after presenting the situation to the MDRB. The nature of the precipitate was determined after several chemical and mineralogical analyses. AEM concluded that a bacterial reaction occurred in the seepage water leading to the orange ferric precipitate inside the Central Dike downstream pond. It was also determined that the turbidity events correlated with the precipitate formation. AEM also modified the deposition of tailings in the SD4 area and covered the depression. No future depressions were observed after this action.

The MDRB visited the site in September 2017 and were pleased by how AEM addressed the situation. Given the concern with the under-seepage at Central Dike, the Board concluded that the preferred option for operations would be in-pit disposal in the mined out Portage and Goose Pits. The Board also agreed to the reduction in water volume inside the South Cell TSF in order to reduce the hydraulic gradient toward Central Dike downstream pond and consequently the seepage flow rate.

Moving forward with these recommendations, AEM evaluated the potential of including the in-pit disposal as early than April 2018 to store Meadowbank Mine tailings inside Goose Pit from April to September 2018 and initiate closure of the South Cell TSF by dewatering the reclaim pond in summer 2018. This change to the plan will promote freeze back of the South Cell TSF and will reduce and stop the Central Dike seepage. Finally, following the reception of the Whale Tail Project Certificate, AEM is now planning storage of the 8.2M tonnes of Whale Tail Pit tailings inside the Portage Pit.

Validation and updates of the site parameters (i.e. runoff and pit inflows) was conducted with the data collected so far in 2017. In addition, further updates/modifications/revisions to the mine plan (LOM), site wide water management, tailings deposition plans and operating schedule were evaluated in preparing this report.

The water balance presented has been optimized to reduce freshwater consumption as much as possible, secure operation of the tailings pond during winter 2018 and minimize water treatment requirements at closure.

Pit flooding volumes and sequencing (including Portage and Goose Pits) was reviewed according to deposition of tailings inside Goose and Portage Pits. To reach water elevation 133.6m, a volume of 45,6Mm<sup>3</sup> needs to be filled. As previously stated, 24,6Mm<sup>3</sup> originates from 3<sup>rd</sup> Portage Lake, 11.3Mm<sup>3</sup> balance will be made up from the natural pit water inflows including runoff and precipitation combined with reclaim water, and the residual volume of 9,7Mm<sup>3</sup> is occupied by the tailings. This represents a global freshwater consumption reduction of 7.7Mm<sup>3</sup> compared to the flooding volumes forecasted in the 2016 Water Management Plan (AEM, 2016a).

The entire pit flooding process will be completed by the end of 2027. Once water quality in the flooded pits meet CCME Guidelines for the Protection of Aquatic Life and/or site specific criteria for parameters not listed in the CCME Guidelines, dike breaching of the surrounding structures will occur to reconnect the Portage and Goose areas to Second Portage Lake (2031) and Vault area to Wally Lake (2029). AEM plans at least four years of monitoring to assess the pit water quality prior to breaching. It should be understood that the dikes will not be breached unless the water quality meets the CCME or other site specific criteria.

A water quality forecasting model was completed by SNC Lavalin for the life of mine presented in this report. The mandate of this report is to analyze the water quality during the operating life of the mine and at closure after the pit are flooded to determine the needs of treating the potential contaminants of concern. Based on current water quality and the updated water balance including in-pit disposal, the report identifies that arsenic, chromium, copper, selenium, fluoride, chromium, ammonia and total N<sub>equivalent</sub> may require removal treatment in order for the pit water quality to meet CCME criteria in 2031. AEM is committed to updating this forecast on a yearly basis.

## **Section 6.0 - RECOMMENDATIONS**

This section presents a series of recommendations in order to improve on the current water management strategies and water balance. It is AEM's intent to implement all recommendations listed.

- Continue to monitor and include any new flow monitoring locations/devices for any additional or new inflows observed in 2017.
- Develop detailed tailings deposition plan for Goose and Portage Pits following the approval of the modification request.
- Continue to update the deposition plans of the North and South Cell TSF as needed to maximize water use and availability as well as increasing the accuracy of the models including but not limited to bathymetric readings.
- Validate new tailings parameters with 2017 North and South Cells bathymetries.
- Conduct the water quality modelling analysis on a yearly basis based on updated water quality results and water balance through the life of mine.
- Continue development of the sediment flux model to evaluate erosion of geotechnical structures on site for the closure, primarily for TSS control: diversion ditches, rock storage facilities, capping of the tailings storage facilities, dikes and dams.
- Evaluate opportunities to reduce contaminants concentration in the reclaim pond prior to closure.
- Continue follow up of the Central Dike seepage flow and adjust pumping station capacity in function of the flow variation.
- Implement 2016 Meadowbank water quality forecasting (SNC, 2017j) recommendations.

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## APPENDIX A – WATER BALANCE

Project ID	Project Name	Month	Year	# Days	BMS	L/H	Milestones										Performance Metrics									
							M1		M2		M3		M4		M5		M6		M7		M8		M9		M10	
							Start	End	Start	End	Start	End	Start	End	Start	End	Start	End	Start	End	Start	End	Start	End	Start	End
							Actual	Planned	Actual	Planned	Actual	Planned	Actual	Planned	Actual	Planned	Actual	Planned	Actual	Planned	Actual	Planned	Actual	Planned	Actual	Planned
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MEADOWBANK GOLD MINE  
2016 WATER MANAGEMENT PLAN UPDATE

Project ID		Project Name		Project Manager		Project Status		Project Location		Project Start Date		Project End Date		Project Duration (Days)		Project Budget (USD)		Project Actual Cost (USD)		Project Variance (USD)		Project Risk Level		Project Complexity		Project Scope		Project Description		Project Notes		Project Comments		Project Actions		Project Tasks		Project Milestones		Project Deliverables		Project Outputs		Project Results		Project Metrics		Project KPIs		Project Indicators		Project Trends		Project Forecasts		Project Projections		Project Assumptions		Project Constraints		Project Dependencies		Project Risks		Project Opportunities		Project Challenges		Project Solutions		Project Outcomes		Project Impacts		Project Benefits		Project Costs		Project Revenue		Project Profit		Project ROI		Project NPV		Project IRR		Project Payback Period		Project Break-Even Point		Project Sensitivity Analysis		Project Scenario Analysis		Project Monte Carlo Simulation		Project Risk Register		Project Risk 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Firmness		Project Risk Determination		Project Risk Resolve		Project Risk Willpower		Project Risk Force		Project Risk Power		Project Risk Strength		Project Risk Might		Project Risk Vigor		Project Risk Energy		Project Risk Enthusiasm		Project Risk Excitement		Project Risk Eagerness		Project Risk Zeal		Project Risk Vigor		Project Risk Alacrity		Project Risk Promptness		Project Risk Quickness		Project Risk Speed		Project Risk Agility		Project Risk Flexibility		Project Risk Adaptability		Project Risk Resilience		Project Risk Tolerance		Project Risk Endurance		Project Risk Persistence		Project Risk Steadfastness		Project Risk Firmness		Project Risk Determination		Project Risk Resolve		Project Risk Willpower		Project Risk Force		Project Risk Power		Project Risk Strength		Project Risk Might		Project Risk Vigor		Project Risk Energy		Project Risk Enthusiasm		Project Risk Excitement		Project Risk Eagerness		Project Risk Zeal		Project Risk Vigor		Project Risk Alacrity		Project Risk Promptness		Project Risk Quickness		Project Risk Speed		Project Risk Agility		Project Risk Flexibility		Project Risk Adaptability		Project Risk Resilience		Project Risk Tolerance		Project Risk Endurance		Project Risk Persistence		Project Risk Steadfastness		Project Risk Firmness		Project Risk Determination		Project Risk Resolve		Project Risk Willpower		Project Risk Force		Project Risk Power		Project Risk Strength		Project Risk Might		Project Risk Vigor		Project Risk Energy		Project Risk Enthusiasm		Project Risk Excitement		Project Risk Eagerness		Project Risk Zeal		Project Risk Vigor		Project Risk Alacrity		Project Risk Promptness		Project Risk Quickness		Project Risk Speed		Project Risk Agility		Project Risk Flexibility		Project Risk Adaptability		Project Risk Resilience		Project Risk Tolerance		Project Risk Endurance		Project Risk Persistence		Project Risk Steadfastness		Project Risk Firmness		Project Risk Determination		Project Risk Resolve		Project Risk Willpower		Project Risk Force		Project Risk Power		Project Risk Strength		Project Risk Might		Project Risk Vigor		Project Risk Energy		Project Risk Enthusiasm		Project Risk Excitement		Project Risk Eagerness		Project Risk Zeal		Project Risk Vigor		Project Risk Alacrity		Project Risk Promptness		Project Risk Quickness		Project Risk Speed		Project Risk Agility		Project Risk Flexibility		Project Risk Adaptability		Project Risk Resilience		Project Risk Tolerance		Project Risk Endurance		Project Risk Persistence		Project Risk Steadfastness		Project Risk Firmness		Project Risk Determination		Project Risk Resolve		Project Risk Willpower		Project Risk Force		Project Risk Power		Project Risk Strength		Project Risk Might		Project Risk Vigor		Project Risk Energy		Project Risk Enthusiasm		Project Risk Excitement		Project Risk Eagerness		Project Risk Zeal		Project Risk Vigor		Project Risk Alacrity		Project Risk Promptness		Project Risk Quickness		Project Risk Speed		Project Risk Agility		Project Risk Flexibility		Project Risk Adaptability		Project Risk Resilience		Project Risk Tolerance		Project Risk Endurance		Project Risk Persistence		Project Risk Steadfastness		Project Risk Firmness		Project Risk Determination		Project Risk Resolve		Project Risk Willpower		Project Risk Force	
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# MEADOWBANK GOLD MINE

## 2016 WATER MANAGEMENT PLAN UPDATE

Month-Year	# Days/Year	Year	S/W	NORTH CELL					Transfer to NC				
				13.0 d ha									
				Runoff to NC	Interflow to NC	Runoff to NC (17.5 d)	Runoff to NC (17.5 d)	Water risk to NC (17.5 d)					
3 MONTH CELL													
PERIOD 1: 1997-2016													
PERIOD 2: 1997-2016													
PERIOD 3: 1997-2016													
PERIOD 4: 1997-2016													
PERIOD 5: 1997-2016													
PERIOD 6: 1997-2016													
PERIOD 7: 1997-2016													
PERIOD 8: 1997-2016													
PERIOD 9: 1997-2016													
PERIOD 10: 1997-2016													
PERIOD 11: 1997-2016													
PERIOD 12: 1997-2016													
PERIOD 13: 1997-2016													
PERIOD 14: 1997-2016													
PERIOD 15: 1997-2016													
PERIOD 16: 1997-2016													
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PERIOD 97: 1997-2016													
PERIOD 98: 1997-2016													
PERIOD 99: 1997-2016													
PERIOD 100: 1997-2016													

## 2016 WATER MANAGEMENT PLAN UPDATE

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## 2016 WATER MANAGEMENT PLAN UPDATE

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Month	Year	Non-Storm Water										Storm Water										All Systems									
		Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)	Flow (m³/s)
January	2016	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
February	2016	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
March	2016	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
April	2016	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
May	2016	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
June	2016	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
July	2016	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
August	2016	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
September	2016	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
October	2016	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
November	2016	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
December	2016	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0

## 2016 WATER MANAGEMENT PLAN UPDATE

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## 2016 WATER MANAGEMENT PLAN UPDATE

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MEADOWBANK GOLD MINE  
2016 WATER MANAGEMENT PLAN UPDATE

APPENDIX B IN-PIT TAILINGS DEPOSITION WATER BALANCE AND WATER QUALITY  
FORECAST



MEADOWBANK GOLD MINE  
2016 WATER MANAGEMENT PLAN UPDATE

 <b>SNC • LAVALIN</b>	<b>TECHNICAL NOTE</b> <b>In-Pit Tailings Deposition Water Balance and Water Quality Forecast</b>	Prepared by: A.L. Nguyen Reviewed by: M.H. Picard		
		Rev.	Date	Page
	643541-5000-40ER-0002	B00	Sep. 12, 2017	i

**Title of document:** **IN-PIT TAILINGS DEPOSITION WATER BALANCE AND WATER QUALITY FORECAST**

**Client:** **AGNICO EAGLE – MEADOWBANK MINE SITE**

**Project:** **TSFE PROJECT – IN-PIT DEPOSITION PREFEASIBILITY STUDY**

*Prepared by:* Anh-Long Nguyen, Eng.

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*Reviewed by:* Marie-Hélène Picard, Eng.

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*Approved by:* Dominic Tremblay, Eng.

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 <b>SNC • LAVALIN</b>	<b>TECHNICAL NOTE</b> <b>In-Pit Tailings Deposition Water Balance and Water Quality Forecast</b>	Prepared by: A.L. Nguyen Reviewed by: M.H. Picard		
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#	Revision			Pages Revised	Remarks
	Prep.	App.	Date		
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## 1.0 Introduction

Agnico Eagle is looking to extend the life of the Meadowbank Mine by constructing and operating Whale Tail Pit, a satellite deposit on the Amaruq property, as a continuation of mine operations and milling at the Meadowbank Mine.

In order to accommodate the tailings produced from the development of the Whale Tail Pit Project, a first phase of the Tailings Storage Facility Extension Project (TSFE) was conducted in 2015/2016. The objective was to evaluate the potential expansion of the Meadowbank TSF - North Cell by the construction of internal structures to increase the total storage capacity associated to the mining of the Amaruq ore deposit. This addition of these structures proposed by O'Kane Consultant (O'Kane, 2015 & 2016) was sufficient to increase the storage capacity of 8.3M tonnes of tailings into the North Cell.


The second phase of the project was to evaluate at a conceptual level different options for the storage of additional tailings on site coming from the Whale Tail Pit and future ore bodies. Three options were evaluated which included in-pit tailings deposition in Portage Pits A & E, internal structures tailings deposition over North and South Cells and filtered tailings deposition over North and South Cells. A Multi-Account Assessment (MAA) session was conducted and the in-pit tailings deposition option was selected as the preferred option to store tailings waste produced from Whale Tail Mine and future ore bodies in addition to its current TSF (SLI 2016a).

The third phase of the project consists in developing a prefeasibility study (PFS) design of the in-pit deposition. In the conceptual study, only Portage Pit A and Pit E were considered for tailings deposition. For the pre-feasibility study, Goose Pit is also considered as a location for tailings deposition. The PFS design of the in-pit deposition will also assess the maximum amount of tailings that can be stored in Goose Pit and Portage Pit A and Pit E to determine if the storage volume available is sufficient for anticipated and possible future tailings production volumes.

The PFS design of the in-pit deposition includes the following studies:

- 1D Tailings Consolidation Modeling Assessment of the tailings in the pit in order to assess the in-site tailings density;
- A Hydrogeological Modeling of groundwater flow in and around the Portage and Goose Pits, including a 3D contaminant transport model;
- Review Pit Wall Stability during in-pit deposition;
- Update and refinement of the water and tailings mass balance around Portage and Goose Pits;
- Update of the water quality forecast model;
- Development of deposition strategy
- Development of closure strategy;
- Development of infrastructures required for in-pit deposition.

The following technical note presents the PFS design of the water and mass balance, the water quality forecast, the deposition strategy and the infrastructures required for in-pit deposition. Results from the 1D tailings consolidation modeling assessment and the hydrogeological modeling are taken into account in the update of the water and mass balance and water quality forecast.

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## 2.0 Design Basis

### 2.1 Summary

The design parameters considered for the PFS design of the in-pit tailings deposition of tailings in Portage and Goose Pits are presented in Table 2-1.

**Table 2-1 : Operating Parameters for In-Pit Tailings Deposition**

Parameter	Units	Values	Source
In-pit tailings capacity requirements	t	28,000,000 minimum (total amount required based on conceptual study design parameter)	SLI (2016b)
Mill throughput rate per day (dry)	TPD	9,000	AEM (2017a)
Tailings production tonnage profile		Refer to section 2.2	AEM (2017a)
Tailing slurry solid concentration from the mill	% w/w	54	AEM
Tailings slurry specific gravity	t/m <sup>3</sup>	1.56	Calculated
Tailings solid specific gravity		3.0	AEM
Tailings solid particle size (P80)	µm	80	AEM
Reclaim water flow	m <sup>3</sup> /h	Adjusted to maintain water cover over the tailings; maximum 230	SLI
Fresh water requirement for camp site	m <sup>3</sup> /d	95	AEM
Moisture content in ore (assumed values based on previous water balance)	%	Jan: 0.98%; Feb: 1.53%; Mar: 1.04%; Apr: 1.09%; May 1.08%; Jun: 0.99%; Jul: 1.30%; Aug: 0.98%; Sep: 0.89%; Oct: 0.99%; Nov: 0.72%; Dec: 0.93%	AEM
Minimum reclaim pond volume	m <sup>3</sup>	250,000	AEM
Tailings slurry in-situ dry density (in-situ after consolidation)	t/m <sup>3</sup>	Refer to section 2.3	SLI
Water Content in the deposited tailings (in-situ after consolidation)	%	Refer to section 2.3	SLI
Deposition Slope	%	for modelling purposes, assume a flat geometry	SLI

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Parameter	Units	Values	Source
Pit Volumes <ul style="list-style-type: none"> <li>Portage Pit A (up to elev. 133 m)</li> <li>Portage Pit E (up to elev. 133 m)</li> <li>Goose Pit (up to elev. 130 m)</li> </ul>	m <sup>3</sup>	Refer to Section 2.6 <ul style="list-style-type: none"> <li>13,452,984</li> <li>20,988,815</li> <li>6,967,170</li> </ul>	AEM (2017b)
Catchment Areas	ha	Refer to Section 2.4	AEM / SLI
Precipitation/evaporation values	mm	Refer to Section 2.4	AEM / SLI
Pit infiltration		Refer to section 2.5	SLI
Minimum water cover depth	m	3	SLI (2014)
Ice thickness	m	2	SLI (2014)
Maximum tailings elevation	m	125.6 m (8 m below the Third Portage Lake level (133.6 m) to prevent tailings re-suspension)	SLI (2016)

## 2.2 In-Situ Tailings Dry Density

In the conceptual study for the in-pit deposition, an in-situ tailings dry density of 1.0 t/m<sup>3</sup> following consolidation was selected (SLI 2016). The use of this value is conservative and would represent possibly the highest tailings storage volume required. This value was selected to account for the high rate of addition of tailings in the pit, which could lead to high pore water pressures resulting in very low density consolidated deposit.

SLI conducted a 1D tailings consolidation modeling assessment using the computer program FSConsol (GWP Software Inc.) while considering the expected properties of the tailings based on literature data (SLI 2017a). The model was evaluated under ideal sub-aqueous deposition condition. The results indicated that under these operating conditions, the average in-situ dry tailing density will range from 1.03 to 1.11 t/m<sup>3</sup>. It is important to note that this model was based on literature values only since no specific data on the Whale Tail tailings were available. Characterization and testing on the Whale Tail tailings will be performed in the summer of 2017. The results will be used to confirm these assumptions.


For the purpose of the PFS design and in order to provide a conservative analysis, the water/mass balance model and water quality forecast model will continue to consider an average in-situ dry tailings density of **1.0 t/m<sup>3</sup>**.

Assuming a dry solid specific gravity of 3.0 and an in-situ tailings density of 1.0 t/m<sup>3</sup>, the water content in the deposited tailings after consolidation is evaluated at **67% w/w** of the mass of dry tailings deposited.

## 2.3 Tonnage Profile

For the purpose of the PFS design for in-pit deposition, Table 2-2 presents the mill throughput tonnage profile considered in the development of the water/mass balance around Portage Pit and Goose Pit based on the operating parameters listed in Table 2-1 and an in-situ tailings dry density of 1.0 t/m<sup>3</sup>. The total tonnage shown in



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the table is the maximum amount of Portage/Vault, Whale Tail and future ore bodies tailings that can be stored in Goose Pit and Portage Pit.

**Table 2-2 : Tailings Throughput Tonnage Profile (AEM 2017a)**

Year	Tailings Throughput per Year (tons dry solid/year) Note 1	Source of Tailings	Deposition Location
2018	2,420,216	Portage/Vault	South Cell TSF
2019	1,583,570 1,642,499	Portage/Vault Whale Tail	Goose Pit
2020	3,285,000	Whale Tail	Goose Pit Portage Pit A
2021	3,285,000	Whale Tail	Portage Pit A and/or Pit E
2022	3,285,000	Whale Tail	Portage Pit A and/or Pit E
2023	3,285,000	Future Ore Bodies	Portage Pit A and/or Pit E
2024	3,285,000	Future Ore Bodies	Portage Pit A and/or Pit E
2025	3,285,000	Future Ore Bodies	Portage Pit A and/or Pit E
2026	3,285,000	Future Ore Bodies	Portage Pit A and/or Pit E
2027	3,285,000	Future Ore Bodies	Portage Pit A and/or Pit E
2028	2,457,000	Future Ore Bodies	Portage Pit A and/or Pit E
<b>Total</b>	<b>4,003,786 11,497,499 18,882,000</b>	<b>Portage/Vault Whale Tail Future Ore Bodies</b>	

Note 1: Conceptual tonnage/year for the purposes of the PFS.

## 2.4 Surface Runoff

Table 2-3 presents the site run-off hydrology for a typical average year considered in the evaluation of the water/mass balance around Portage and Goose Pit. It is assumed that the volume of snowfall accumulated between the months of October and May will be handled as additional snowmelt volume in the month of June during spring runoff.



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Table 2-4 summarizes the catchment areas and the net surface runoff volumes considered in the water/mass balance model for in-pit deposition. Figure 2-1 presents the evaluation of the catchment areas used in the PFS around Portage Pit A, Portage Pit E, Portage Central Dump and Goose Pit.


**Table 2-3 : Site Run-Off Hydrology for a Typical Average Year**

Month	Rainfall	Snowfall Water Equivalent	Evapo-Transpiration	Snow Sublimation	Lake Evaporation	Net precipitation on ground or over pond	Net precipitation used for model
	mm	mm	mm	mm	mm	mm	mm
Jan	0.0	8.2	0	9	0	0.0	0.0
Feb	0.0	2.2	0	9	0	0.0	0.0
Mar	0.0	3.6	0	9	0	0.0	0.0
Apr	0.0	3.9	0	9	0	0.0	0.0
May	0.0	15.6	0	9	0	6.6	0.0
Jun	20.3	2.6	2.8	0	8.8	20.1	50.9
Jul	40.3	5.2	32	0	99.2	13.5	13.5
Aug	61.2	7.9	32.4	0	100.4	36.7	36.7
Sep	24.2	5.8	12.7	0	39.5	17.3	17.3
Oct	0.0	22.2	0	9	0.1	13.2	0.0
Nov	0.0	5.6	0	9	0	0.0	0.0
Dec	0.0	20.0	0	9	0	11.0	0.0

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**Table 2-4 : Catchment Areas and Net Surface Runoff Volumes**

Sectors	North Cell TSF	South Cell TSF	Portage Pit A + Portion of Central Dump	Portage Pit E + Portion of Central Dump	Goose Pit
<b>Catchment Area</b>	<b>152.9 ha</b>	<b>84.3 ha</b>	<b>46.7 ha</b>	<b>52.2 ha</b>	<b>19.6 ha</b>
<b>Month</b>	<b>m<sup>3</sup>/month</b>	<b>m<sup>3</sup>/month</b>	<b>m<sup>3</sup>/month</b>	<b>m<sup>3</sup>/month</b>	<b>m<sup>3</sup>/month</b>
Jan	0	0	0	0	0
Feb	0	0	0	0	0
Mar	0	0	0	0	0
Apr	0	0	0	0	0
May	0	0	0	0	0
Jun	77,826	42,909	23,777	26,568	9,968
Jul	20,642	11,381	6,306	7,046	2,644
Aug	56,114	30,938	17,144	19,156	7,187
Sep	26,452	14,584	8,081	9,030	3,388
Oct	0	0	0	0	0
Nov	0	0	0	0	0
Dec	0	0	0	0	0
<b>Total</b>	<b>181,034</b>	<b>99,811</b>	<b>55,308</b>	<b>61,799</b>	<b>23,187</b>

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**Figure 2-1: Catchment Areas for Portage and Goose Pit**



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## 2.5 Pit Infiltration

Table 2-5 presents the pit infiltration flow rates used in the water/mass balance model. These values were estimated using the actual volumes pumped from the pits in 2015 minus the average runoff precipitation (SLI 2017b).

The East Dike seepage flows is based on the value used by AEM in their annual Water Management Plan updates.

**Table 2-5 : Assumed Pit Infiltration Flow Rates**

Location	Infiltration Flow
Portage Pit A	80 m <sup>3</sup> /d
Portage Pit E	58 m <sup>3</sup> /d
Goose Pit	878 m <sup>3</sup> /d
East Dikes Seepage	14,964 m <sup>3</sup> /mth

## 2.6 Pit Filling Curve

The pit filling curves were evaluated based on the latest topography data and accounts for the waste rock dump deposited in Portage Pit A, Pit E and Goose Pit.

Figure 2-2 presents the pit filling curve considered in the PFS design for in-pit deposition. Two curves are presented for each pit:

- > One curve shows the free water storage volumes. This curve considers the water storage volume available in the pit as well as in the void space in the waste dump.
- > One curve shows the total storage volume available in the pits only for water and tailings. For the model, it is assumed that a negligible amount of tailings solids can migrate through the waste dump.

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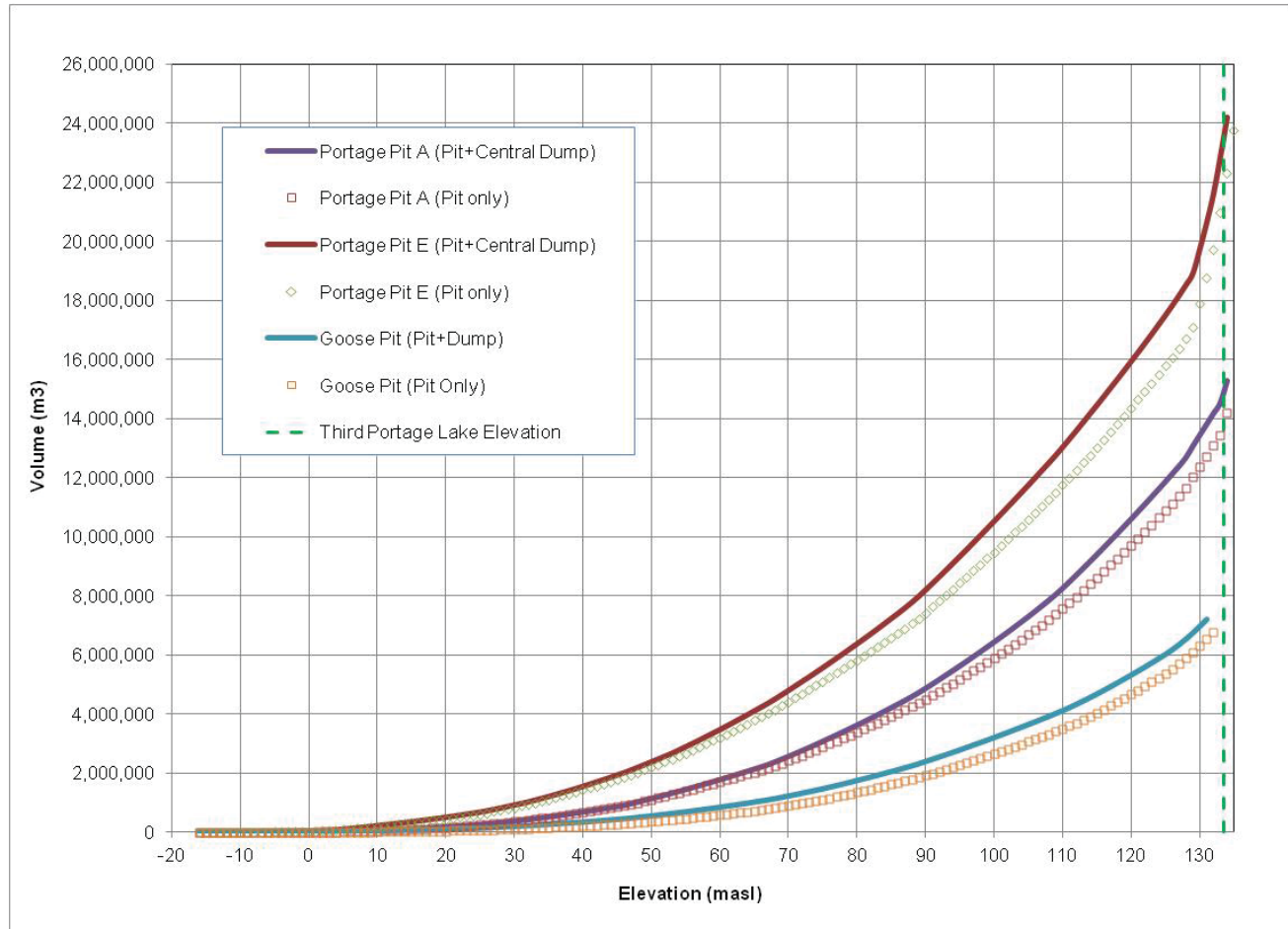
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**Figure 2-2: Pit Filling Curve****Notes:**

- The solid lines indicate the total available volume in the pit and include the void volume in the dump that deposited in the pits.
- The dashed lines indicate the available volume in the pit only.



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### 3.0 In-Pit Deposition Strategy

The in-pit deposition consists of the deposition of tailings into Goose Pit, Portage Pit A and Pit E. The deposition strategy considered for the PFS design is divided into the following distinct periods:

- > Period 1: Portage/Vault tailings deposition in South Cell TSF and in Goose Pit
- > Period 2: Whale Tail tailings deposition in Goose Pit
- > Period 3: Whale Tail and Future Ore Bodies Tailings deposition in Portage Pit, alternating between Portage Pit A and Pit E
- > Period 4: Pit Closure at the end of operations
- > Period 5: Monitoring period
- > Period 6: Post closure

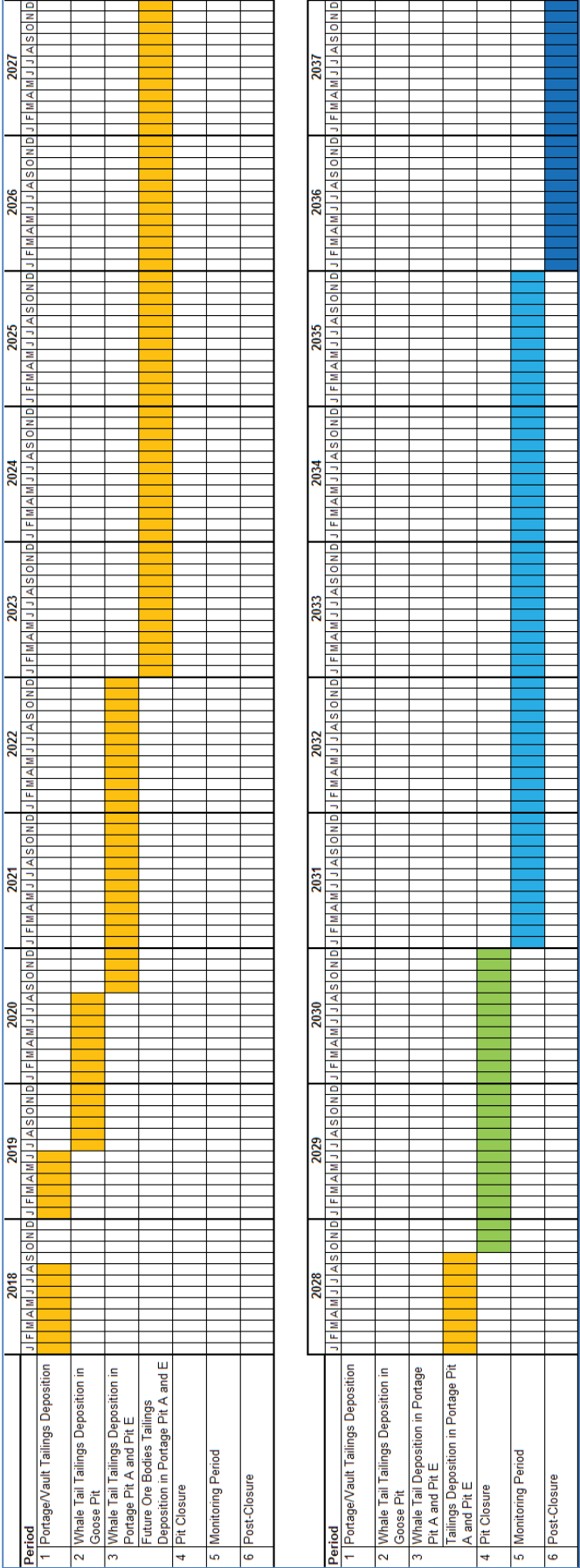
The in-pit deposition strategy was developed based on the following general assumptions:

- i. It is assumed that water can flow between Portage Pit A and Pit E via the Portage Central Dump once the water level in the pit is above 90 masl.
- ii. Tailings are first deposited in Goose Pit. For the purpose of the PFS study, it is assumed that the pit is filled until the tailings elevation reach about 125 masl.
- iii. Once Goose Pit is filled, tailing deposition continues in Portage Pit A. Tailings are deposited in Pit A until elevation 80 masl to limit the amount of reclaim water that could flow from Pit A to Pit E through Central dump.
- iv. Portage Pit E is then filled with tailings up to elevation 80 masl.
- v. Deposition continues in Portage Pit, alternating between Pit A and Pit E until the tailings reaches an elevation of 125 masl in order to limit the hydraulic gradients between the pits and ensuring a minimum water cover over the tailings.
- vi. During deposition, reclaim water is pumped to the mill from either Portage Pit A or Pit E. Reclaim water is pumped from the pit where no deposition is occurring to ensure that low Total Suspended Solids (TSS) are returned to the mill.
- vii. During deposition, to ensure that the water level in Goose Pit remains below 130 masl, water from Goose Pit is transferred to Portage Pit E every summer.
- viii. North Cell and South Cell TSF runoff are transferred to Portage Pit E during in-pit deposition.
- ix. Stormwater Management Pond water is transferred to the pit where tailings deposition is occurring.
- x. East Dike Seepage water is transferred to either Portage Pit A or Pit E during in-pit deposition. The seepage is transferred to the pit where tailings deposition is occurring.

Figure 3-1 presents the preliminary project timeline while table 3-1 presents the detail in-pit deposition strategy based on an in-situ tailings dry density of  $1.0 \text{ t/m}^3$  after consolidation in the pits. For Period 3, tailings deposition will occur in Portage Pit, alternating between Portage Pit A (period 3A) and Portage Pit E (period 3B).

Figure 3-1 presents a plan and section view of the Portage and Goose Pits. A process flow diagram (PFD) of the in-pit deposition in Goose Pit, Portage Pit A and Pit E can be found in Appendix 1.

Figure 3-1: Preliminary Project Timeline



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**Table 3-1 : In-Pit Deposition Strategy**

Period	North Cell TSF	South Cell TSF	Portage Pit A	Portage Pit E	Goose Pit
<b>Period 1:</b> <b>Portage/Vault</b> <b>Tailings</b> <b>Deposition</b>  <b>January 2018</b> <b>to</b> <b>June 2019</b>	Input: Surface water from the NC TSF, Interception sump, SD1 and WSF Output: Surface water transfer to SC TSF  <u>Activity:</u> Start reclamation of the North Cell.	Deposition: Continue deposition of Vault tailings in South Cell TSF (January 2018 – August 2018) Input: Surface water from NC and SC TSF Reclaim Pond. Input: Stormwater Mgmt Pond Water Output: Reclaim water pumped to Mill	Input: Pit surface runoff and pit infiltration.  <u>Note:</u> East Dike seepage pumped to 2PL.  <u>Activity:</u> Install tailings piping into the pit	Input: Pit surface runoff and pit infiltration.  <u>Activity:</u> Install reclaim pumps and pipeline in Portage Pit E. Bring electrical power to reclaim pump.	Deposition: Deposition in Goose Pit from January 2019 to June 2019. Input: Surface runoff and pit infiltration. Input: Stormwater Mgmt Pond Water Output: Transfer water to Portage Pit A (as required) to maintain water level during deposition. <u>Activity:</u> Installation of tailings pipelines to Goose Pit in 2018. Installation water transfer pump station.

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Period	North Cell TSF	South Cell TSF	Portage Pit A	Portage Pit E	Goose Pit		
<b>Period 2:</b> <b>Whale Tail</b> <b>Tailings</b> <b>Deposition in</b> <b>Goose Pit</b> <b>(Max Tails. Elev.)</b>  <b>July 2019</b> to <b>August 2020</b>	Input: Surface water from the NC TSF, Interception sump, SD1 and WSF Output: Surface water transfer to SC TSF.  <u>Activity:</u> Continue reclamation of the North Cell.	Input: Surface water from SC. Input: Surface water from NC. Output: Surface water to Portage Pit E.  <u>Activity:</u> Start reclamation of the South Cell.	Input: Pit surface runoff and pit infiltration. Input: 3PL water.  <u>Note:</u> East Dike seepage pumped to 2PL.	Input: Pit surface runoff and pit infiltration. Input: NC and SC runoff Input: 3PL water. Output: Reclaim water pumped to Mill.  <u>Activity:</u> Install tailings piping into the pit	Deposition tailings  Input: Surface runoff and pit infiltration. Input: Stormwater Mgmt Pond Output: Transfer water to Portage Pit E (as required) to maintain water level during deposition.	Whale  Tail	

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Period	North Cell TSF	South Cell TSF	Portage Pit A	Portage Pit E	Goose Pit
<b>Period 3A</b> <b>Whale Tail and Future Ore Bodies Tailings Deposition in Portage Pit A</b>	Input: Surface water from the NC TSF, Interception sump, SD1 and WSF Output: Surface water transfer to SC TSF <u>Activity:</u> Continue reclamation of the North Cell.	Input: Surface water from SC. Input: Surface water from NC. Output: Surface water to Portage Pit E <u>Activity:</u> Continue reclamation of the South Cell.	Deposition Whale Tail and Future Ore Bodies tailings Input: Pit surface runoff and pit infiltration. Input: 3PL water. Input: Stormwater Mgmt Pond Input East Dike seepage Output: Water to Pit E via Central Dump.	Input: Pit surface runoff and pit infiltration. Input: 3PL water. Input: NC and SC runoff Input: Goose Pit runoff Input: Pit A water from Central Dump Output: Reclaim water pumped to Mill.	Input: Surface runoff and pit infiltration. Output: Transfer to Pit E to maintain water level < 130 m.
<b>September 2020 to September 2028 (intermittent)</b>					

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Period	North Cell TSF	South Cell TSF	Portage Pit A	Portage Pit E	Goose Pit
<b>Period 3B</b> <b>Whale Tail and Future Ore Bodies Tailings Deposition in Portage Pit E</b>  <b>September 2021 to March 2028 (intermittent)</b>	Input: Surface water from the NC TSF, Interception sump, SD1 and WSF Output: Surface water transfer to SC TSF  <u>Activity:</u> End reclamation of the North Cell. Monitoring of NC water quality	Input: Surface water from SC. Input: Surface water from NC. Output: Surface water to Portage Pit E  <u>Activity:</u> End reclamation of the South Cell. Monitoring of SC water quality	Input: Pit surface runoff and pit infiltration. Input: 3PL water. Input: Pit E water via Central Dump Output: Water to Pit E via Central Dump. Output: Reclaim water pumped to Mill.	Deposition Whale Tail and Future Ore Bodies tailings Input: Pit surface runoff and pit infiltration. Input: Stormwater Mgmt Pond Input East Dike seepage Input: NC and SC runoff Input: Goose Pit runoff Input: Pit A water from Central Dump Output: Water to Pit A via Central Dump	Input: Surface runoff and pit infiltration. Output: Transfer to Pit E to maintain water level < 130 m.
<b>Period 4: Pit Closure</b>  <b>October 2028 to December 2030</b>	Input: Surface water from the NC TSF, Interception sump, SD1 and WSF Output: To 3PL  <u>Note:</u> Closure completed	Input: Surface water from SC. Output: To 3PL  <u>Note:</u> Closure completed	Input: Pit surface runoff and pit infiltration. Input: East Dike seepage  <u>Activity:</u> Treatment of reclaim water in Pit Monitor water quality.	Input: Pit surface runoff and pit infiltration. Input: East Dike seepage  <u>Activity:</u> Treatment of reclaim water in Pit Monitor water quality.	Input: Surface runoff and pit infiltration.  <u>Activity:</u> Treatment of reclaim water in Pit Monitor water quality.  <u>Note:</u> Once water level > 130 m, assume zero infiltration flow.



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Period	North Cell TSF	South Cell TSF	Portage Pit A	Portage Pit E	Goose Pit
<b>Period 5:</b> <b>Monitoring Period</b>  <b>January 2031 to December 2035</b>	<u>Note:</u> Closure completed Surface water directed toward 3PL.	<u>Note:</u> Closure completed Surface water directed toward 3PL.	Input: Pit surface runoff and pit infiltration. Input: East Dike seepage  <u>Activity:</u> Monitor water quality.	Input: Pit surface runoff and pit infiltration. Input: East Dike seepage  <u>Activity:</u> Monitor water quality.	Input: Surface runoff and pit infiltration.  <u>Activity:</u> Monitor water quality.  <u>Note:</u> Once water level > 130 m, assume zero infiltration flow.
<b>Period 6:</b> <b>Post-Closure</b> <b>As of January 2036</b>	Closure completed	Closure completed	Closure completed	Closure completed	Closure completed



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## TECHNICAL NOTE

### In-Pit Tailings Deposition Water Balance and Water Quality Forecast

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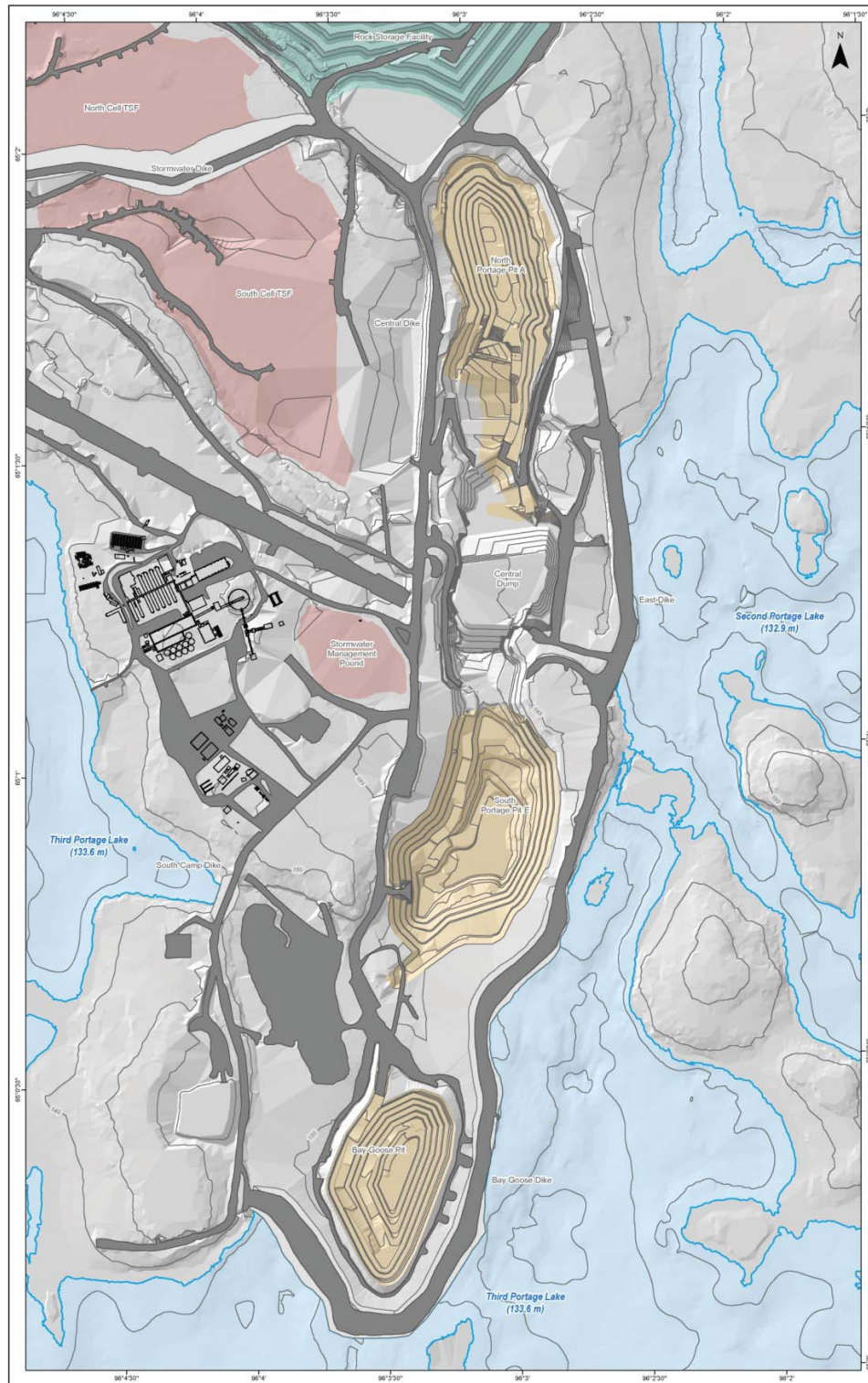
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Figure 3-2: Plan View of the Portage and Goose Pit Area




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## 4.0 Pit Closure Strategy

For the PFS design, the closure strategy retained at the end of operation consists of pit flooding and dike breaching once the water quality is met. In fact, the ultimate objective for closure is to return the existing surrounding lakes to pre-mining state by joining the in-pit water bodies to the surrounding receiving environment. To achieve this objective, the following steps will have to be realised:

- > In-pit tailings deposition to an elevation up to 125.6 masl. This maximum tailings elevation was assumed in order to achieve a water cover of about 8 m above the tailings at closure. This water cover depth will ensure that the tailings will not be re-suspended due to wave effect and ice formation and limit access of aquatic life to it, thus removing the necessity of a granular cover over the tailings.
- > Treatment of the reclaim water to remove total/dissolved metals and other parameters of concern;
- > Pit flooding with Third Portage Lake water, if required;
- > During the monitoring period, natural runoff will be allowed to enter and fill the Portage and Goose Pit until the water elevation is close to the water elevation of Third Portage Lake (133.6 masl).
- > Dike breaching once the water quality meets site-specific closure criteria.

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## 5.0 Water and Mass Balance Model

### 5.1 Description

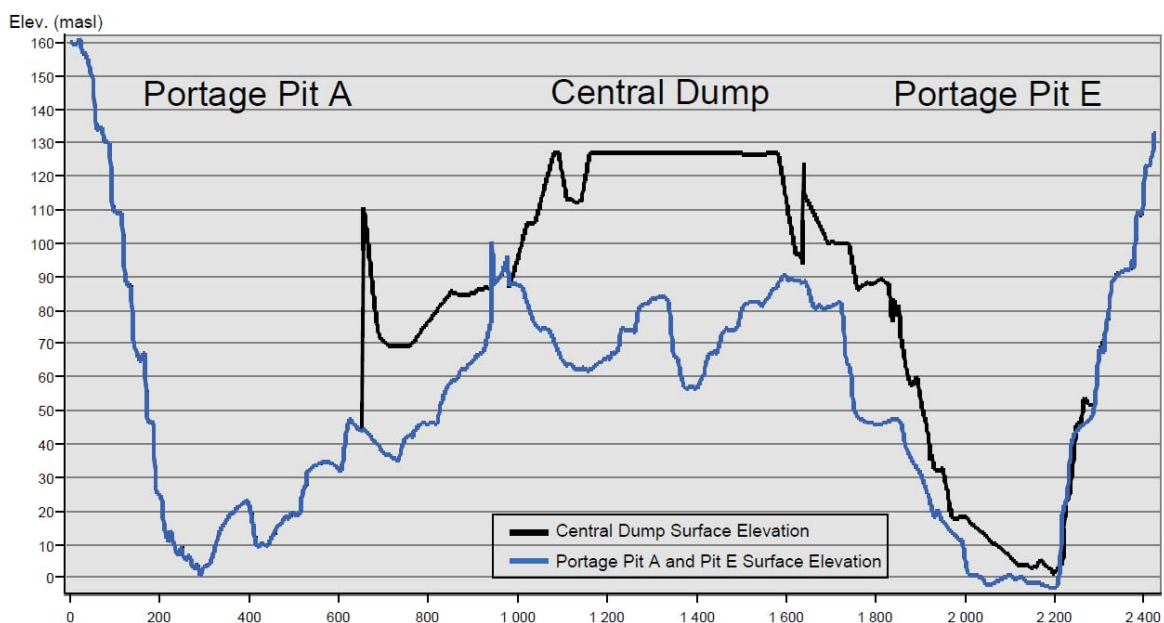
A water/mass balance model was developed for the PFS design of the in-pit deposition in order to evaluate the following:


- > Maximum quantity of tailings that can be deposited in the pits considering a maximum tailings elevation of 125.6 masl;
- > Mass, volume and elevation the consolidated tailings will occupy in each pit;
- > Elevation of the water in each pit during in-pit deposition and at closure;
- > Volume of fresh water required to maintain a water cover over the deposited tailings during in-pit deposition and for pit filling at closure;
- > Reclaim water flow back to the mill while maintaining a minimum water cover over the tailings;
- > Water quality forecast of different parameters in the reclaim water (i.e. water stored in the pits during deposition) during deposition and following closure.

The water/mass balance was developed based on the different inputs and outputs streams into each pit as described in Table 3-1. The model is based on a monthly time step and starts in January 2018. The water/mass balance model includes deposition of Portage/Vault tailings in the South Cell TSF and Goose Pit, and Whale Tail tailings in Goose Pit, and Whale Tail and future ore bodies tailings in Portage Pit A and Pit E.

Furthermore, the water/mass balance model also takes into account that Portage Pit A and Pit E are hydraulically connected via the Portage Central Dump. Figure 5-1 presents a section view of Portage Pit A, Pit E and the Central Dump. The model allows water to flow from one pit to the other when there is a difference in water elevation between the pits. Once the water elevation in Pit A and Pit E are more or less the same, water is allowed to transfer between the pits to maintain the same water elevation in both pits.

**Figure 5-1: Profile View of Portage Pit A, Pit E and Central Dump**



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## 5.2 Assumptions


The following main assumptions were made for the development of the water/mass balance for the PFS design of the in-pit deposition:

1. In order to simplify the model, 100% conservation of water and mass is assumed. No chemical or natural degradation is taken into consideration, except for cyanide. Cyanide degradation is considered only during the summer months (June to September);
2. For this analysis, no treatment will take place at the North or South Cells TSF Reclaim Pond or at the Portage or Goose Pits during operations and closure;
3. The water quality of the Mill Effluent is assumed to be constant over time for all parameters, except for ammonia, chloride, sulfates and total dissolved solids (TDS). For ammonia, the water quality for this parameter will continue to vary due to the hydrolysis of cyanate to ammonia. For chloride, the water quality for this parameter will continue to increase due to the continued use of calcium chloride as a dust suppressant in the mill and crusher. For sulfates, the oxidation of sulphide in the ore will continue to contribute to the sulfate loading in the Mill Effluent. The overall TDS in the Mill Effluent will continue to increase due to the increase in ammonia, chloride and sulfate.
4. The water quality for the runoff and infiltration streams entering in the system is assumed to be constant over time for all parameters.
5. Water will start flowing between Portage Pit A and Pit E through Portage Central Dump once the water elevation in the pit is greater or equal to 90 masl. Water is assumed to flow through Central Dump between Portage Pit A and Pit E, irrespective of the tailings elevation. No reduction of the Central Dump permeability is accounted for in the model.
6. No solid tailings are assumed to migrate into the waste dump in Goose Pit and Portage Pit A and Pit E. Only water is allowed to flow through and accumulate in the waste dump.
7. Flows from surface waters, pit infiltration and East Dike seepage into the Portage Pit A, Pit E and Goose Pit are considered in the model. The flows are assumed constant throughout the year. When the water elevation is greater than 129 masl, it is assumed that the pit infiltration and East Dike seepage flow is reduced by 50% since the hydraulic gradient between the pit and the Second and Third Portage Lake will be lower.
8. Runoff water from the North and South Cells TSF will be transferred to Portage Pit E until the end of in-pit deposition. By that time, the closure of North and South Cells TSF is assumed to be completed and the runoff from this area can be transferred to Third Portage Lake.
9. Starting volumes and forecasted water quality in the South Cell TSF, Portage Pit A, Portage Pit E and Goose Pit are based on the results obtained from the Meadowbank Water Quality Forecasting Update for the 2016 Water Management Plan (SLI 2017c) for the month of December 2017.

## 5.3 Inputs/Outputs of Water/Mass Balance

### 5.3.1 Input and Output Streams


Table 5-1 summarizes the input and outputs considered in the water/mass balance around Portage Pits A and E and Goose Pit, as well as around the South Cell TSF during the period of In-Pit Tailings Deposition.

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**Table 5-1 : Summary Input and Output Streams used in Water/Mass Balance Model**

Area	Input Streams	Output Streams
<b>North Cell TSF</b>	Surface water runoff Interception sump to NC WEP & SD1 to NC Waste rock seepage to NC	Runoff to South Cell TSF
<b>South Cell TSF</b>	North Cell runoff South Cell runoff Stormwater Management Pond** Tailings Water from the Mill*	Reclaim water to the Mill South Cell runoff to Portage Pit E
<b>Portage Pit A</b>	Transfer from Third Portage lake Portage Pit A runoff Portage Pit A infiltration Tailings Water from Mill* East Dike Seepage*** Stormwater Management Pond*** Transfer from Portage Pit E via Central Dump	Reclaim water to Mill** Water transfer to Pit E via Central Dump
<b>Portage Pit E</b>	Transfer from Third Portage lake Portage Pit E runoff Portage Pit E infiltration Tailings Water from Mill* South Cell runoff Goose Pit East Dike Seepage*** Stormwater Management Pond***	Reclaim water to Mill** Water transfer to Pit A via Central Dump
<b>Goose Pit</b>	Transfer from Third Portage lake Goose Pit runoff Goose Pit infiltration Tailings Water from Mill* Stormwater Management Pond***	Transfer to Pit E when required to maintain water elevation below 130 m during in-pit deposition.
<b>Notes:</b> * Applicable only when tailings are deposited in the area. ** Reclaim water transferred to mill from pit where no deposition is occurring. *** For the purpose of the model, stream will be transferred to the pit where tailings deposition is occurring.		



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### 5.3.2 Water Quality Data

Table 5-2 presents the water quality data for the Mill Effluent and tailings leaching rate used in the mass balance to evaluate the water quality forecast in Goose Pit, Portage Pit A and Pit E. Table 5-3 and 5-4 present the water quality data used around North and South Cells and around Portage Pit and Goose Pit respectively.

The water quality data are based on the following information:

- > Mill Effluent when processing Portage/Vault ore: Average results from 4 samples taken of the mill effluent in 2016;
- > Leaching of tailings from Portage/Vault ore: Average results from SFE leach tests on tailings conducted in 2016;
- > Mill Effluent when processing Whale Tail ore: Average results from metallurgical test obtained from “Combined Ore” samples taken in Mar 2015 and May 2016;
- > Leaching of tailings from Whale Tail ore: Average results from metallurgical test obtained from “Combined Ore” samples taken in Mar 2015 and May 2016;
- > Water quality data from Portage RSF, Saddle Dam 1 sump, Saddle Dam 3 sump and East Dike Seepage is based on average water quality results obtained from sampling conducting in 2015 and 2016;
- > Stormwater Management Pond water quality is based on analytical results from samples taken in 2013;
- > Third Portage Lake water quality data is based on the average results taken from sample in the summer 2015;
- > Pit infiltration water quality data to Portage Pit and Goose Pit is based on samples taken at groundwater monitoring well E3 on 2016-07-03 and MW03-01 on 2010-08-26, respectively;
- > Natural runoff is assumed to have similar quality as Third Portage Lake water;
- > The starting water quality data used for North Cell, South Cell, Portage Pit and Goose Pit is based on the 2016 water quality forecast model results for the month of December 2017.

Table 5-5 presents the CCME guidelines and Water License discharge criteria to Third Portage Lake at Meadowbank. The values present in this table are used for the PFS design to identify parameters of concern during in-pit deposition and at closure.



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**Table 5-2 : Mill Effluent Water Quality Data and Leaching Rate**

PARAMETERS	UNITS	MILL EFFLUENT WHALE TAIL	LEACHING OF TAILS WHALE TAILS (kg/ton)	MILL EFFLUENT PORTAGE/VAULT	LEACHING OF TAILS PORTAGE/VAULT (kg/ton)
Alkalinity	mg CaCO <sub>3</sub> /L	102	5.47E-02	66	3.50E-02
Hardness	mg CaCO <sub>3</sub> /L	1345	5.43E-01	1313	1.85E-01
Total dissolved solids	mg/L	Summer: +3664 Winter: +4037	1.18E+00	Summer: +1564 Winter: +1937	0.00E+00
Total Aluminium (Al)	mg/L	0.764	4.41E-05	0.326	1.53E-04
Total Silver (Ag)	mg/L	0.001	8.67E-09	0.005	1.08E-06
Total Arsenic (As)	mg/L	0.452	5.88E-04	0.026	5.28E-06
Total Barium (Ba)	mg/L	0.080	1.18E-04	0.128	1.32E-05
Total Cadmium (Cd)	mg/L	0.00004	1.03E-08	0.000	0.00E+00
Total Chromium (Cr)	mg/L	0.041	3.00E-08	0.001	7.75E-08
Total Copper (Cu)	mg/L	3.569	2.89E-06	3.569	2.40E-06
Total Iron (Fe)	mg/L	1.710	1.03E-03	0.832	2.42E-04
Total Lead (Pb)	mg/L	0.010	2.33E-08	0.002	8.50E-08
Total Manganese (Mn)	mg/L	0.161	5.53E-05	0.013	1.47E-05
Total Mercury (Hg)	mg/L	0.000005	6.67E-09	0.000	5.00E-09
Total Molybdenum (Mo)	mg/L	0.115	4.36E-05	0.966	4.92E-05
Total Nickel (Ni)	mg/L	0.319	9.33E-06	0.024	7.00E-07
Total Selenium (Se)	mg/L	0.008	6.67E-07	0.166	1.17E-05
Total Strontium (Sr)	mg/L	0.70	1.79E-04	2.130	2.70E-04
Total Thallium (Ti)	mg/L	0.00002	3.33E-09	0.000	3.80E-08
Total Uranium (U)	mg/L	0.003	2.79E-07	0.013	3.67E-06
Total Zinc (Zn)	mg/L	0.006	1.00E-06	0.003	1.00E-06
Chloride	mg/L	Summer: +75 Winter: +300	3.20E-02	Summer: +75 Winter: +300	0.00E+00
Fluoride (F)	mg/L	0.19	1.07E-04	0.645	3.25E-04

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PARAMETERS	UNITS	MILL EFFLUENT WHALE TAIL	LEACHING OF TAILS WHALE TAILS (kg/ton)	MILL EFFLUENT PORTAGE/VAULT	LEACHING OF TAILS PORTAGE/VAULT (kg/ton)
Sulphate (SO <sub>4</sub> )	mg SO <sub>4</sub> /L	Summer: +3500 Winter: +3500	8.47E-01	Summer: +1400 Winter: +1400	2.70E-01
Total Cyanide (CNt)	mg/L	19	5.84E-03	18	0.00E+00
Total Ammonia (NH <sub>3</sub> + NH <sub>4</sub> )	mg N/L	Summer: +40 Winter: +40	3.60E-03	Summer: +40 Winter: +40	4.95E-03
Nitrate (NO <sub>3</sub> )	mg N/L	7	4.00E-04	13	8.05E-04
Dissolved Aluminium (Al)	mg/L	0.279	4.41E-05	0.119	1.53E-04
Dissolved Silver (Ag)	mg/L	0.001	8.67E-09	0.005	1.08E-06
Dissolved Arsenic (As)	mg/L	0.452	5.88E-04	0.026	5.28E-06
Dissolved Barium (Ba)	mg/L	0.077	1.18E-04	0.122	1.32E-05
Dissolved Cadmium (Cd)	mg/L	0.00004	1.03E-08	0.000	0.00E+00
Dissolved Chromium (Cr)	mg/L	0.0065	3.00E-08	0.000	7.75E-08
Dissolved Copper (Cu)	mg/L	3.240	2.89E-06	3.240	2.40E-06
Dissolved Iron (Fe)	mg/L	1.397	1.03E-03	0.679	2.42E-04
Dissolved Lead (Pb)	mg/L	0.0058	2.33E-08	0.0004	8.50E-08
Dissolved Manganese (Mn)	mg/L	0.161	5.53E-05	0.008	1.47E-05
Dissolved Mercury (Hg)	mg/L	0.000005	6.67E-09	0.000	5.00E-09
Dissolved Molybdenum (Mo)	mg/L	0.101	4.36E-05	0.943	4.92E-05
Dissolved Nickel (Ni)	mg/L	0.056	9.33E-06	0.021	7.00E-07
Dissolved Selenium (Se)	mg/L	0.008	6.67E-07	0.169	1.17E-05
Dissolved Strontium (Sr)	mg/L	0.676	1.79E-04	2.045	2.70E-04
Dissolved Thallium (Ti)	mg/L	0.00001	3.33E-09	0.000	3.80E-08
Dissolved Uranium (U)	mg/L	0.003	2.79E-07	0.012	3.67E-06
Dissolved Zinc (Zn)	mg/L	0.003	1.00E-06	0.001	1.00E-06

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**Table 5-3 : Water Quality Data for Streams around North and South Cell TSF**

PARAMETERS	UNITS	RECLAIM ST-21 NORTH CELL	SOUTH CELL	PORTAGE RSF TO NORTH CELL	SADDLE DAM 1 SUMP TO NORTH CELL	SADDLE DAM 3 SUMP TO SOUTH CELL	THIRD PORTAGE LAKE
Alkalinity	mg CaCO <sub>3</sub> /L	0	124	68	56	40	9
Hardness	mg CaCO <sub>3</sub> /L	0	1417	176	182	235	12
Total dissolved solids	mg/L	0	3038	301	315	379	22
Total Aluminium (Al)	mg/L	0.00	0.65	0.26	0.37	0.24	0.01
Total Silver (Ag)	mg/L	0.00	0.01	0.00	0.00	0.00	0.00
Total Arsenic (As)	mg/L	0.00	0.04	0.03	0.02	0.00	0.00
Total Barium (Ba)	mg/L	0.00	0.13	0.02	0.02	0.04	0.00
Total Cadmium (Cd)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00
Total Chromium (Cr)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00
Total Copper (Cu)	mg/L	0.00	2.90	0.03	0.01	0.02	0.00
Total Iron (Fe)	mg/L	0.00	1.47	0.97	1.17	2.58	0.02
Total Lead (Pb)	mg/L	0.00	0.00	0.00	0.00	0.01	0.00
Total Manganese (Mn)	mg/L	0.00	0.06	0.52	0.29	1.53	0.00
Total Mercury (Hg)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00
Total Molybdenum (Mo)	mg/L	0.00	0.87	0.01	0.01	0.00	0.00
Total Nickel (Ni)	mg/L	0.00	0.02	0.04	0.03	0.25	0.00
Total Selenium (Se)	mg/L	0.00	0.16	0.00	0.00	0.00	0.00
Total Strontium (Sr)	mg/L	0.00	2.22	0.15	0.00	0.00	0.01
Total Thallium (Ti)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00
Total Uranium (U)	mg/L	0.00	0.02	0.01	0.00	0.00	0.00
Total Zinc (Zn)	mg/L	0.00	0.01	0.00	0.11	0.01	0.00
Chloride	mg/L	0.00	433.20	10.12	7.56	19.83	0.79
Fluoride (F)	mg/L	0.00	1.15	0.19	0.21	0.35	0.08
Sulphate (SO <sub>4</sub> )	mg SO <sub>4</sub> /L	0.00	3115.69	33.44	145.72	182.00	5.10

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PARAMETERS	UNITS	RECLAIM ST-21 NORTH CELL	SOUTH CELL	PORTAGE RSF TO NORTH CELL	SADDLE DAM 1 SUMP TO NORTH CELL	SADDLE DAM 3 SUMP TO SOUTH CELL	THIRD PORTAGE LAKE
Total Cyanide (CNT)	mg/L	0.00	2.02	0.00	0.01	0.01	0.00
Total Ammonia (NH <sub>3</sub> + NH <sub>4</sub> )	mg N/L	0.00	79.45	0.56	0.75	1.30	0.01
Nitrate (NO <sub>3</sub> )	mg N/L	0.00	12.91	8.39	8.62	7.77	0.03
Dissolved Aluminium (Al)	mg/L	0.00	0.38	0.26	0.37	0.24	0.00
Dissolved Silver (Ag)	mg/L	0.00	0.01	0.00	0.00	0.00	0.00
Dissolved Arsenic (As)	mg/L	0.00	0.03	0.00	0.02	0.00	0.00
Dissolved Barium (Ba)	mg/L	0.00	0.12	0.02	0.02	0.04	0.00
Dissolved Cadmium (Cd)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00
Dissolved Chromium (Cr)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00
Dissolved Copper (Cu)	mg/L	0.00	2.63	0.03	0.01	0.02	0.00
Dissolved Iron (Fe)	mg/L	0.00	1.00	0.21	1.17	2.58	0.01
Dissolved Lead (Pb)	mg/L	0.00	0.00	0.00	0.00	0.01	0.00
Dissolved Manganese (Mn)	mg/L	0.00	0.05	0.64	0.29	1.53	0.00
Dissolved Mercury (Hg)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00
Dissolved Molybdenum (Mo)	mg/L	0.00	0.85	0.01	0.01	0.00	0.00
Dissolved Nickel (Ni)	mg/L	0.00	0.02	0.04	0.03	0.25	0.00
Dissolved Selenium (Se)	mg/L	0.00	0.16	0.00	0.00	0.00	0.00
Dissolved Strontium (Sr)	mg/L	0.00	2.15	0.15	0.00	0.00	0.01
Dissolved Thallium (Ti)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00
Dissolved Uranium (U)	mg/L	0.00	0.02	0.01	0.00	0.00	0.00
Dissolved Zinc (Zn)	mg/L	0.00	0.00	0.00	0.11	0.01	0.00


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**Table 5-4 : Water Quality Data for Streams around Portage and Goose Pit**

PARAMETERS	UNITS	EAST DIKE SEEPAGE TO PORTAGE	STORMWATER MANAGEMENT POND	THIRD PORTAGE LAKE	PORTAGE PIT ST-19	GOOSE PIT ST-20	PORTAGE PIT INFILTRATION	GOOSE PIT INFILTRATION WATER
Alkalinity	mg CaCO <sub>3</sub> /L	29	0	9	156	69	74	From MW03-01 sample 2010- 08-26
Hardness	mg CaCO <sub>3</sub> /L	40	0	12	517	266	129	77
Total dissolved solids		42	0	22	782	427	271	340
Total Aluminium (Al)	mg/L	0.04	0.00	0.01	3.35	0.73	0.22	0.015
Total Silver (Ag)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00	0.001
Total Arsenic (As)	mg/L	0.00	0.00	0.00	0.25	0.00	0.01	0.001
Total Barium (Ba)	mg/L	0.01	0.00	0.00	0.04	0.02	0.02	0.015
Total Cadmium (Cd)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00	0.001
Total Chromium (Cr)	mg/L	0.00	0.00	0.00	0.10	0.01	0.00	0.000
Total Copper (Cu)	mg/L	0.00	0.00	0.00	0.01	0.11	0.00	0.002
Total Iron (Fe)	mg/L	0.10	0.00	0.02	11.12	1.30	0.61	0.600
Total Lead (Pb)	mg/L	0.00	0.00	0.00	0.01	0.00	0.00	0.000
Total Manganese (Mn)	mg/L	0.01	0.00	0.00	0.42	0.09	0.09	0.550
Total Mercury (Hg)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00	0.000
Total Molybdenum (Mo)	mg/L	0.00	0.00	0.00	0.16	0.03	0.03	0.015
Total Nickel (Ni)	mg/L	0.00	0.00	0.00	0.08	0.03	0.03	0.005
Total Selenium (Se)	mg/L	0.00	0.00	0.00	0.00	0.01	0.00	0.001
Total Strontium (Sr)	mg/L	0.00	0.00	0.01	0.01	0.22	0.24	0.000
Total Thallium (Ti)	mg/L	0.01	0.00	0.00	0.00	0.00	0.00	0.005
Total Uranium (U)	mg/L	0.00	0.00	0.00	0.00	0.01	0.00	0.000
Total Zinc (Zn)	mg/L	0.00	0.00	0.00	0.02	0.01	0.00	0.009
Chloride	mg/L	0.87	0.00	0.79	40.54	50.15	8.40	5.70
Fluoride (F)	mg/L	0.07	0.00	0.08	0.78	0.64	0.42	0.20

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PARAMETERS	UNITS	EAST DIKE SEEPAGE TO PORTAGE	STORMWATER MANAGEMENT POND	THIRD PORTAGE LAKE	PORTAGE PIT ST-19	GOOSE PIT ST-20	PORTAGE PIT INFILTRATION	GOOSE PIT INFILTRATION WATER
Sulphate (SO4)	mg SO4/L	10.04	0.00	5.10	347.66	211.24	16.40	87
Total Cyanide (CNT)	mg/L	0.00	0.00	0.00	0.02	0.00	0.03	0.00
Total Ammonia (NH <sub>3</sub> + NH <sub>4</sub> )	mg N/L	0.01	9.60	0.01	6.06	2.96	2.20	0.08
Nitrate (NO <sub>3</sub> )	mg N/L	0.42	0.07	0.03	18.02	2.76	4.67	0.09
Dissolved Aluminium (Al)	mg/L	0.04	0.00	0.00	0.01	0.01	0.00	0.030
Dissolved Silver (Ag)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00	0.000
Dissolved Arsenic (As)	mg/L	0.00	0.00	0.00	0.03	0.00	0.01	0.001
Dissolved Barium (Ba)	mg/L	0.01	0.00	0.00	0.04	0.02	0.02	0.015
Dissolved Cadmium (Cd)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00	0.001
Dissolved Chromium (Cr)	mg/L	0.00	0.00	0.00	0.10	0.01	0.00	0.000
Dissolved Copper (Cu)	mg/L	0.00	0.00	0.00	0.00	0.10	0.00	0.002
Dissolved Iron (Fe)	mg/L	0.10	0.00	0.01	0.02	0.04	0.04	0.050
Dissolved Lead (Pb)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00	0.001
Dissolved Manganese (Mn)	mg/L	0.01	0.00	0.00	0.17	0.06	0.09	0.360
Dissolved Mercury (Hg)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00	0.000
Dissolved Molybdenum (Mo)	mg/L	0.00	0.00	0.00	0.11	0.03	0.03	0.015
Dissolved Nickel (Ni)	mg/L	0.00	0.00	0.00	0.03	0.03	0.03	0.005
Dissolved Selenium (Se)	mg/L	0.00	0.00	0.00	0.00	0.01	0.00	0.001
Dissolved Strontium (Sr)	mg/L	0.00	0.00	0.01	0.01	0.21	0.19	0.000
Dissolved Thallium (Ti)	mg/L	0.01	0.00	0.00	0.00	0.00	0.00	0.005
Dissolved Uranium (U)	mg/L	0.00	0.00	0.00	0.00	0.01	0.00	0.000
Dissolved Zinc (Zn)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00	0.011

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**Table 5-5 : Discharge Criteria**

PARAMETERS	UNITS	CCME GUIDELINES (based on 3PL)	WATER LICENSE, MAX. AVG CONC. (to 3PL)
Alkalinity	mg CaCO <sub>3</sub> /L	n/a	n/a
Hardness	mg CaCO <sub>3</sub> /L	n/a	n/a
Total dissolved solids	mg/L	n/a	1400
Total Aluminium (Al)	mg/L	0.1	1.5
Total Silver (Ag)	mg/L	0.00025	n/a
Total Arsenic (As)	mg/L	0.005	0.3
Total Barium (Ba)	mg/L	n/a	n/a
Total Cadmium (Cd)	mg/L	0.00004	0.002
Total Chromium (Cr)	mg/L	0.001	n/a
Total Copper (Cu)	mg/L	0.002	0.1
Total Iron (Fe)	mg/L	0.3	n/a
Total Lead (Pb)	mg/L	0.001	0.1
Total Manganese (Mn)	mg/L	n/a	n/a
Total Mercury (Hg)	mg/L	0.000026	0.0004
Total Molybdenum (Mo)	mg/L	0.073	n/a
Total Nickel (Ni)	mg/L	0.025	0.2
Total Selenium (Se)	mg/L	0.001	n/a
Total Strontium (Sr)	mg/L	n/a	n/a
Total Thallium (Ti)	mg/L	0.0008	n/a
Total Uranium (U)	mg/L	0.015	n/a
Total Zinc (Zn)	mg/L	0.03	0.4
Chloride	mg/L	120	1000
Fluoride (F)	mg/L	0.12	n/a
Sulphate (SO <sub>4</sub> )	mg SO <sub>4</sub> /L	n/a	n/a
Total Cyanide (CNT)	mg/L	0.005	0.5
Total Ammonia (NH <sub>3</sub> + NH <sub>4</sub> )	mg N/L	1.83	16
Nitrate (NO <sub>3</sub> )	mg N/L	2.94	20
Dissolved Aluminium (Al)	mg/L	0.1	1
Dissolved Silver (Ag)	mg/L	0.00025	n/a
Dissolved Arsenic (As)	mg/L	0.005	0.3
Dissolved Barium (Ba)	mg/L	n/a	n/a
Dissolved Cadmium (Cd)	mg/L	0.00004	0.002
Dissolved Chromium (Cr)	mg/L	0.001	n/a
Dissolved Copper (Cu)	mg/L	0.002	0.1
Dissolved Iron (Fe)	mg/L	0.3	n/a
Dissolved Lead (Pb)	mg/L	0.001	0.1
Dissolved Manganese (Mn)	mg/L	n/a	n/a
Dissolved Mercury (Hg)	mg/L	0.000026	0.0004
Dissolved Molybdenum (Mo)	mg/L	0.073	n/a
Dissolved Nickel (Ni)	mg/L	0.025	0.2



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PARAMETERS	UNITS	CCME GUIDELINES (based on 3PL)	WATER LICENSE, MAX. AVG CONC. (to 3PL)
Dissolved Selenium (Se)	mg/L	0.001	n/a
Dissolved Strontium (Sr)	mg/L	n/a	n/a
Dissolved Thallium (Ti)	mg/L	0.0008	n/a
Dissolved Uranium (U)	mg/L	0.015	n/a
Dissolved Zinc (Zn)	mg/L	0.03	0.4

## 5.4 Results from Water/Mass Balance Model

### 5.4.1 In-Pit Deposition of Tailings

The results from the water/mass balance model around Portage Pit A and Pit E and Goose Pit for the In-Pit Tailings Deposition option are summarized in the following figures:

- > Figure 5-2: Tonnage and Cumulative Tailings Deposited in Portage Pit A and Pit E and Goose Pit
- > Figure 5-3: Estimated Yearly Filling Rate of Tailings in Portage Pit A and E and Goose Pit
- > Figure 5-4: Estimated Water and Tailings Elevations in Portage Pit A and E and Goose Pit
- > Table 5-6: Updated Mill Throughput Tonnage Profile


As shown in the Figures and in Table 5-6, it is possible to store an additional 4 MT of Portage/Vault tailings in Goose Pit and a minimum of 28 MT of Whale Tail and future ore bodies tailings in Goose Pit, Portage Pit A and Pit E. The maximum amount of Whale Tail and future ore bodies tailings that can be stored in all three pits is estimated at **30.3 MT** if we assume to fill all the pits with tailings up to an elevation of 125 masl with an in-situ tailings density after consolidation of 1.0 t/m<sup>3</sup>.

Per the 1D tailings consolidation modeling (SNC 2017a), the in-situ tailings density at the end of deposition was estimated at 1.11 t/m<sup>3</sup>. With this value, an additional 3 MT of tailings can be stored in the pits, which is equivalent to an additional 11 to 12 months of operation. It is important to note that this value was assessed using literature values only since no specific data on the Whale Tail tailings were available. Characterization and testing on the Whale Tail tailings will be performed in the summer of 2017. The results will be used to confirm these assumptions.

Figure 5-3 shows that the tailings filling rate in Goose Pit, Portage Pit A and Pit E is high, especially during the first year of deposition. Based on experience on other mine sites, when the tailings deposition is higher than 5 m/year, the tailings will not have sufficient time to consolidate and release its trapped water. This results in lower in-situ tailings densities, which is confirmed with the 1D modeling (SLI 2017a).


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PARAMETERS	UNITS	EAST DIKE SEEPAGE TO PORTAGE	STORMWATER MANAGEMENT POND	THIRD PORTAGE LAKE	PORTAGE PIT ST-19	GOOSE PIT ST-20	PORTAGE PIT INFILTRATION	GOOSE PIT INFILTRATION WATER
Sulphate (SO4)	mg SO4/L	10.04	0.00	5.10	347.66	211.24	16.40	87
Total Cyanide (CNT)	mg/L	0.00	0.00	0.00	0.02	0.00	0.03	0.00
Total Ammonia (NH <sub>3</sub> + NH <sub>4</sub> )	mg N/L	0.01	9.60	0.01	6.06	2.96	2.20	0.08
Nitrate (NO <sub>3</sub> )	mg N/L	0.42	0.07	0.03	18.02	2.76	4.67	0.09
Dissolved Aluminium (Al)	mg/L	0.04	0.00	0.00	0.01	0.01	0.00	0.030
Dissolved Silver (Ag)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00	0.000
Dissolved Arsenic (As)	mg/L	0.00	0.00	0.00	0.03	0.00	0.01	0.001
Dissolved Barium (Ba)	mg/L	0.01	0.00	0.00	0.04	0.02	0.02	0.015
Dissolved Cadmium (Cd)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00	0.001
Dissolved Chromium (Cr)	mg/L	0.00	0.00	0.00	0.10	0.01	0.00	0.000
Dissolved Copper (Cu)	mg/L	0.00	0.00	0.00	0.00	0.10	0.00	0.002
Dissolved Iron (Fe)	mg/L	0.10	0.00	0.01	0.02	0.04	0.04	0.050
Dissolved Lead (Pb)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00	0.001
Dissolved Manganese (Mn)	mg/L	0.01	0.00	0.00	0.17	0.06	0.09	0.360
Dissolved Mercury (Hg)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00	0.000
Dissolved Molybdenum (Mo)	mg/L	0.00	0.00	0.00	0.11	0.03	0.03	0.015
Dissolved Nickel (Ni)	mg/L	0.00	0.00	0.00	0.03	0.03	0.03	0.005
Dissolved Selenium (Se)	mg/L	0.00	0.00	0.00	0.00	0.01	0.00	0.001
Dissolved Strontium (Sr)	mg/L	0.00	0.00	0.01	0.01	0.21	0.19	0.000
Dissolved Thallium (Ti)	mg/L	0.01	0.00	0.00	0.00	0.00	0.00	0.005
Dissolved Uranium (U)	mg/L	0.00	0.00	0.00	0.00	0.01	0.00	0.000
Dissolved Zinc (Zn)	mg/L	0.00	0.00	0.00	0.00	0.00	0.00	0.011

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**Table 5-5 : Discharge Criteria**

PARAMETERS	UNITS	CCME GUIDELINES (based on 3PL)	WATER LICENSE, MAX. AVG CONC. (to 3PL)
Alkalinity	mg CaCO <sub>3</sub> /L	n/a	n/a
Hardness	mg CaCO <sub>3</sub> /L	n/a	n/a
Total dissolved solids	mg/L	n/a	1400
Total Aluminium (Al)	mg/L	0.1	1.5
Total Silver (Ag)	mg/L	0.00025	n/a
Total Arsenic (As)	mg/L	0.005	0.3
Total Barium (Ba)	mg/L	n/a	n/a
Total Cadmium (Cd)	mg/L	0.00004	0.002
Total Chromium (Cr)	mg/L	0.001	n/a
Total Copper (Cu)	mg/L	0.002	0.1
Total Iron (Fe)	mg/L	0.3	n/a
Total Lead (Pb)	mg/L	0.001	0.1
Total Manganese (Mn)	mg/L	n/a	n/a
Total Mercury (Hg)	mg/L	0.000026	0.0004
Total Molybdenum (Mo)	mg/L	0.073	n/a
Total Nickel (Ni)	mg/L	0.025	0.2
Total Selenium (Se)	mg/L	0.001	n/a
Total Strontium (Sr)	mg/L	n/a	n/a
Total Thallium (Ti)	mg/L	0.0008	n/a
Total Uranium (U)	mg/L	0.015	n/a
Total Zinc (Zn)	mg/L	0.03	0.4
Chloride	mg/L	120	1000
Fluoride (F)	mg/L	0.12	n/a
Sulphate (SO <sub>4</sub> )	mg SO <sub>4</sub> /L	n/a	n/a
Total Cyanide (CNT)	mg/L	0.005	0.5
Total Ammonia (NH <sub>3</sub> + NH <sub>4</sub> )	mg N/L	1.83	16
Nitrate (NO <sub>3</sub> )	mg N/L	2.94	20
Dissolved Aluminium (Al)	mg/L	0.1	1
Dissolved Silver (Ag)	mg/L	0.00025	n/a
Dissolved Arsenic (As)	mg/L	0.005	0.3
Dissolved Barium (Ba)	mg/L	n/a	n/a
Dissolved Cadmium (Cd)	mg/L	0.00004	0.002
Dissolved Chromium (Cr)	mg/L	0.001	n/a
Dissolved Copper (Cu)	mg/L	0.002	0.1
Dissolved Iron (Fe)	mg/L	0.3	n/a
Dissolved Lead (Pb)	mg/L	0.001	0.1
Dissolved Manganese (Mn)	mg/L	n/a	n/a
Dissolved Mercury (Hg)	mg/L	0.000026	0.0004
Dissolved Molybdenum (Mo)	mg/L	0.073	n/a
Dissolved Nickel (Ni)	mg/L	0.025	0.2

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PARAMETERS	UNITS	CCME GUIDELINES (based on 3PL)	WATER LICENSE, MAX. AVG CONC. (to 3PL)
Dissolved Selenium (Se)	mg/L	0.001	n/a
Dissolved Strontium (Sr)	mg/L	n/a	n/a
Dissolved Thallium (Ti)	mg/L	0.0008	n/a
Dissolved Uranium (U)	mg/L	0.015	n/a
Dissolved Zinc (Zn)	mg/L	0.03	0.4

## 5.4 Results from Water/Mass Balance Model

### 5.4.1 In-Pit Deposition of Tailings

The results from the water/mass balance model around Portage Pit A and Pit E and Goose Pit for the In-Pit Tailings Deposition option are summarized in the following figures:

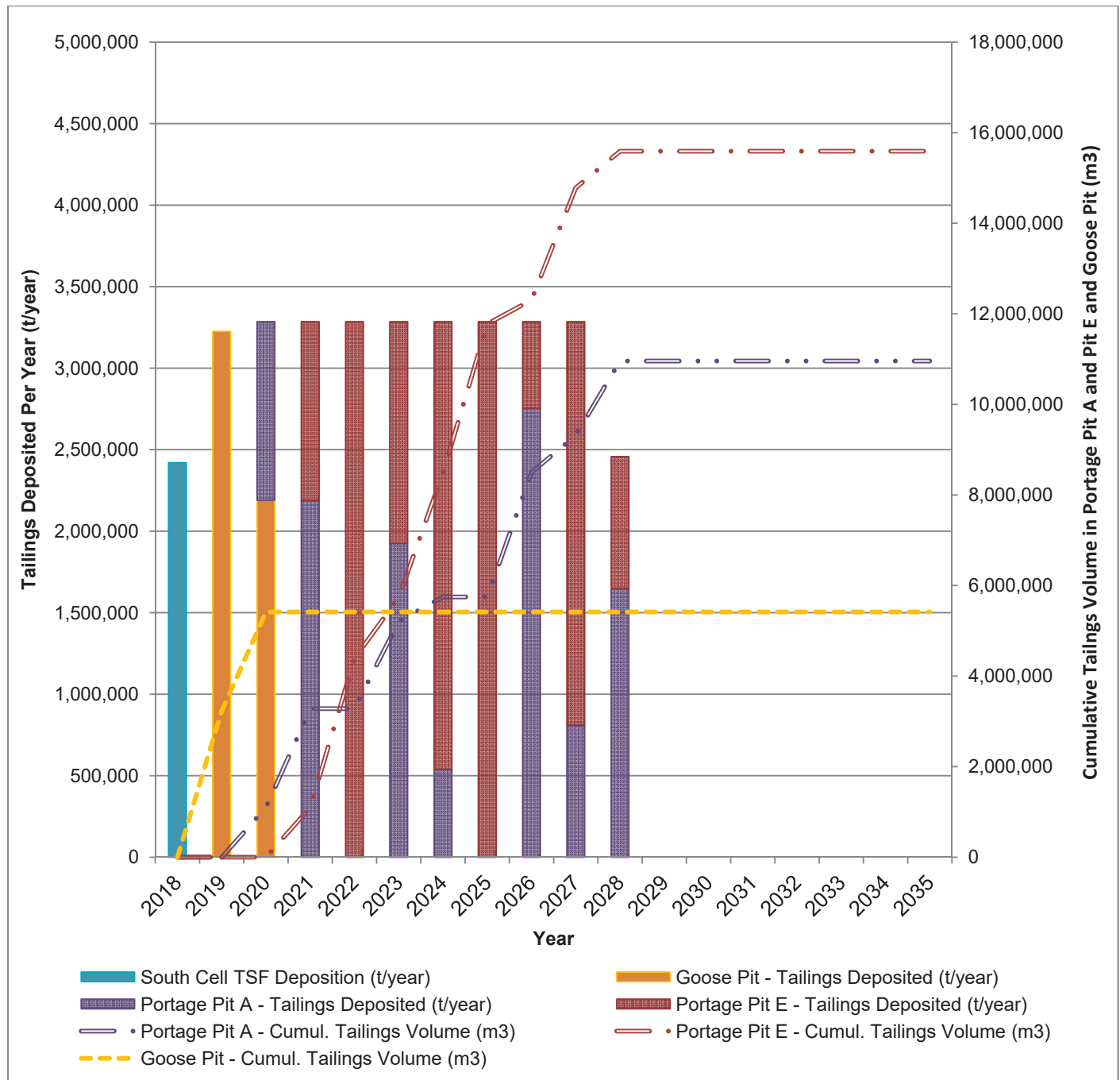
- > Figure 5-2: Tonnage and Cumulative Tailings Deposited in Portage Pit A and Pit E and Goose Pit
- > Figure 5-3: Estimated Yearly Filling Rate of Tailings in Portage Pit A and E and Goose Pit
- > Figure 5-4: Estimated Water and Tailings Elevations in Portage Pit A and E and Goose Pit
- > Table 5-6: Updated Mill Throughput Tonnage Profile

As shown in the Figures and in Table 5-6, it is possible to store an additional 4 MT of Portage/Vault tailings in Goose Pit and a minimum of 28 MT of Whale Tail and future ore bodies tailings in Goose Pit, Portage Pit A and Pit E. The maximum amount of Whale Tail and future ore bodies tailings that can be stored in all three pits is estimated at **30.3 MT** if we assume to fill all the pits with tailings up to an elevation of 125 masl with an in-situ tailings density after consolidation of 1.0 t/m<sup>3</sup>.

Per the 1D tailings consolidation modeling (SNC 2017a), the in-situ tailings density at the end of deposition was estimated at 1.11 t/m<sup>3</sup>. With this value, an additional 3 MT of tailings can be stored in the pits, which is equivalent to an additional 11 to 12 months of operation. It is important to note that this value was assessed using literature values only since no specific data on the Whale Tail tailings were available. Characterization and testing on the Whale Tail tailings will be performed in the summer of 2017. The results will be used to confirm these assumptions.

Figure 5-3 shows that the tailings filling rate in Goose Pit, Portage Pit A and Pit E is high, especially during the first year of deposition. Based on experience on other mine sites, when the tailings deposition is higher than 5 m/year, the tailings will not have sufficient time to consolidate and release its trapped water. This results in lower in-situ tailings densities, which is confirmed with the 1D modeling (SLI 2017a).

**Figure 5-2: Tonnage and Cumulative Volume of Tailings in Portage Pit A & E and Goose Pit**





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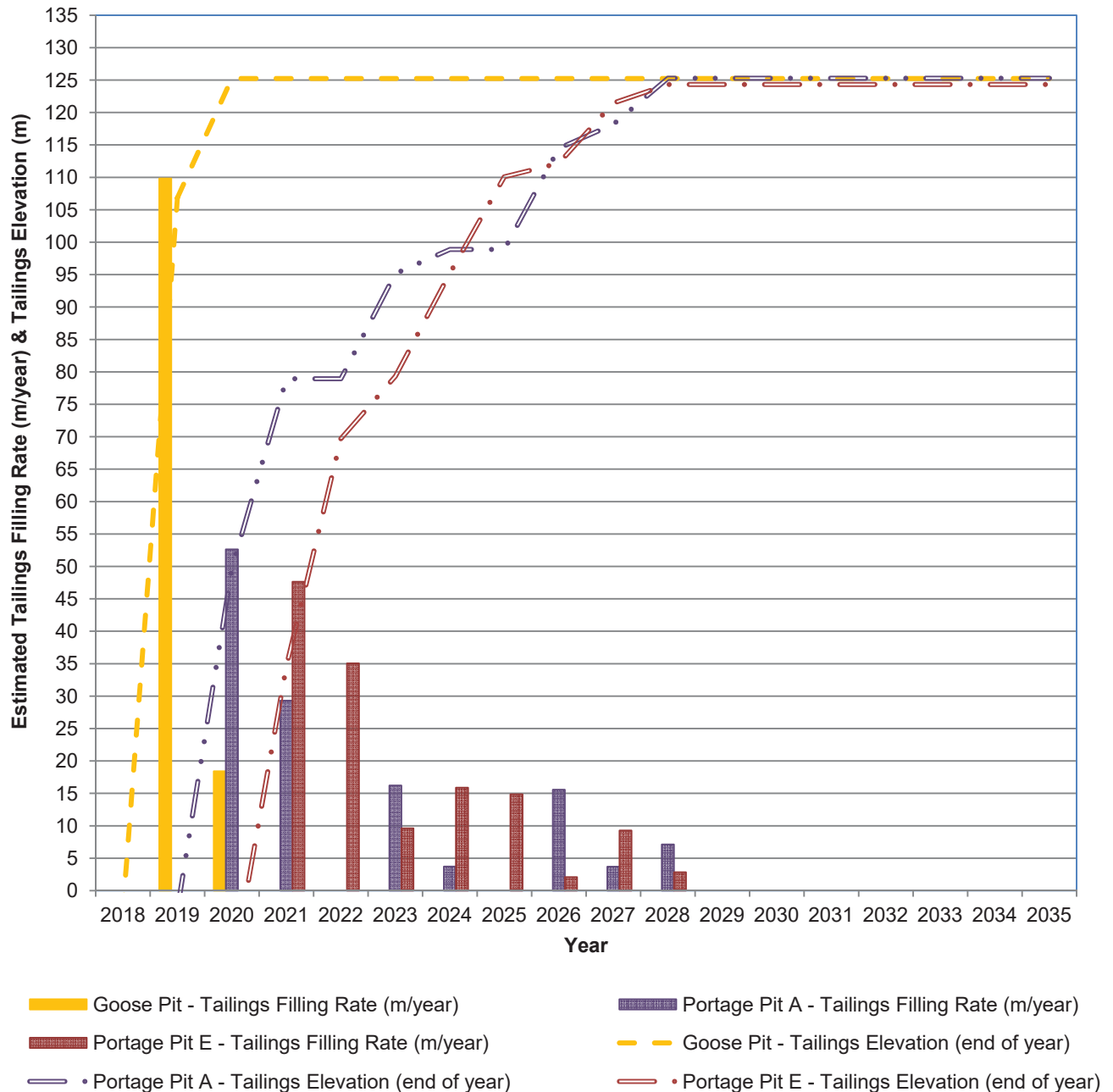
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Figure 5-3: Estimated Yearly Tailings Filling Rate in Portage Pit A and E and Goose Pit





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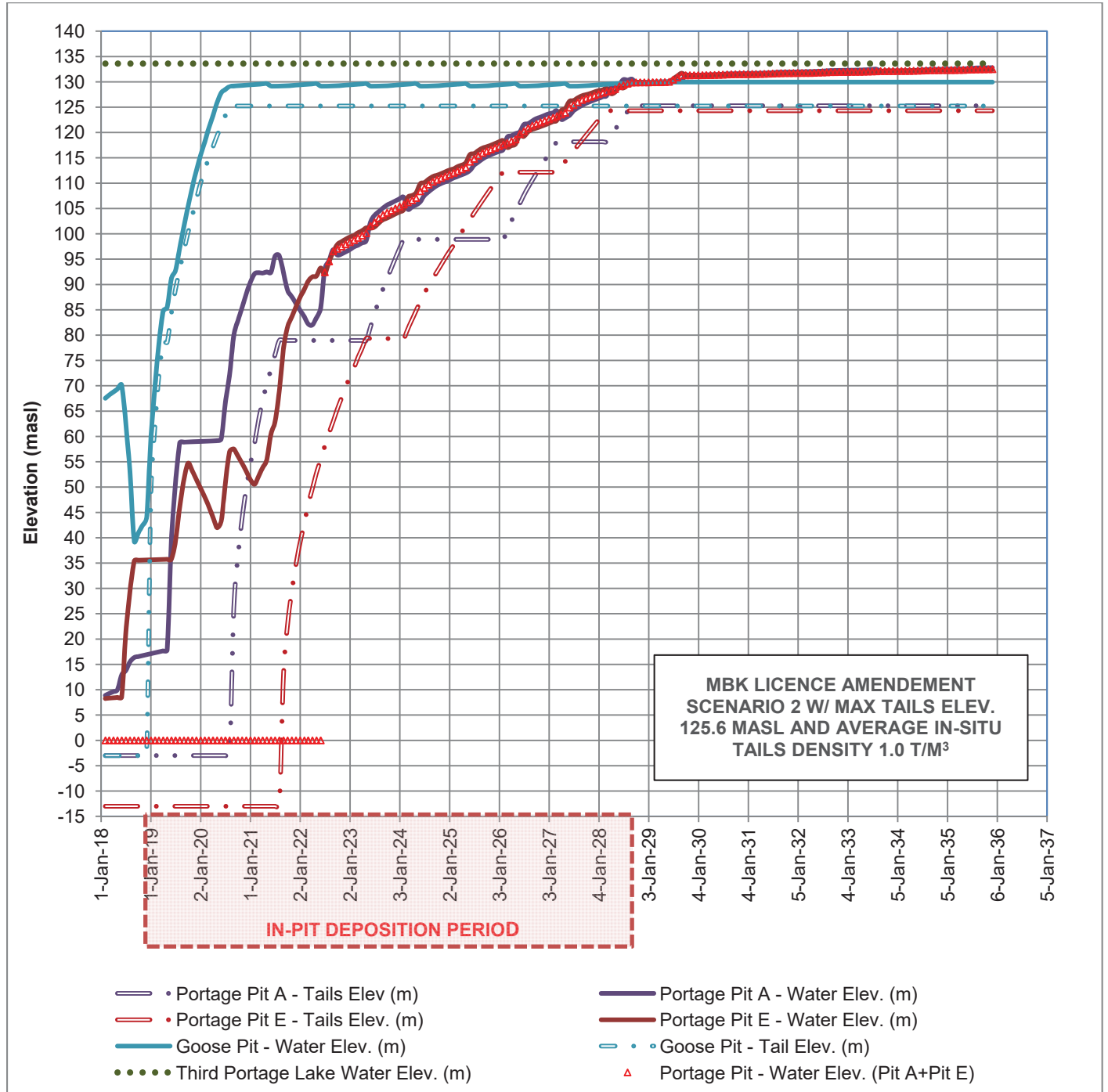
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Figure 5-4: Estimated Water and Tailings Elevations in Portage Pit A and E and Goose Pit






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**Table 5-6 : Tailings Deposition Tonnage Profile**

Year	Source of Tailings	Period 1 South Cell TSF (t/year)	Period 1 & 2 Goose Pit (t/year)	Period 3A Portage Pit A (t/year)	Period 3B Portage Pit E (t/year)	Total per Year (t/year)
2018	Portage/Vault	2,420,216				<b>2,420,216</b>
2019	Portage/Vault Whale Tail		1,583,570 1,642,499			<b>1,583,570</b> <b>1,642,499</b>
2020	Whale Tail		2,190,000	1,095,000		<b>3,285,000</b>
2021	Whale Tail			2,187,000	1,098,000	<b>3,285,000</b>
2022	Whale Tail				3,285,000	<b>3,285,000</b>
2023	Future Ore Bodies			1,926,000	1,359,000	<b>3,285,000</b>
2024	Future Ore Bodies			538,525	2,746,475	<b>3,285,000</b>
2025	Future Ore Bodies				3,285,000	<b>3,285,000</b>
2026	Future Ore Bodies			2,754,000	531,000	<b>3,285,000</b>
2027	Future Ore Bodies			810,000	2,475,000	<b>3,285,000</b>
2028	Future Ore Bodies			1,647,000	810,000	<b>2,457,000</b>
<b>Sub- Total</b>	<b>Portage/Vault</b>	<b>2,420,216</b>	<b>1,583,570</b>			<b>4,003,786</b>
	<b>Whale Tail</b>		<b>3,832,499</b>	<b>3,282,000</b>	<b>4,383,000</b>	<b>11,497,499</b>
	<b>Future Ore Bodies</b>			<b>7,675,525</b>	<b>11,206,475</b>	<b>18,882,000</b>
<b>Total</b>		<b>2,420,216</b>	<b>5,416,069</b>	<b>10,957,525</b>	<b>15,589,475</b>	
		<b>Portage/Vault Tailings</b> <b>Whale Tail &amp; Future Ore Bodies Tailings</b>				<b>4,003,786</b> <b>30,379,499</b>


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#### 5.4.2 Reclaim Water and Fresh Water Consumption

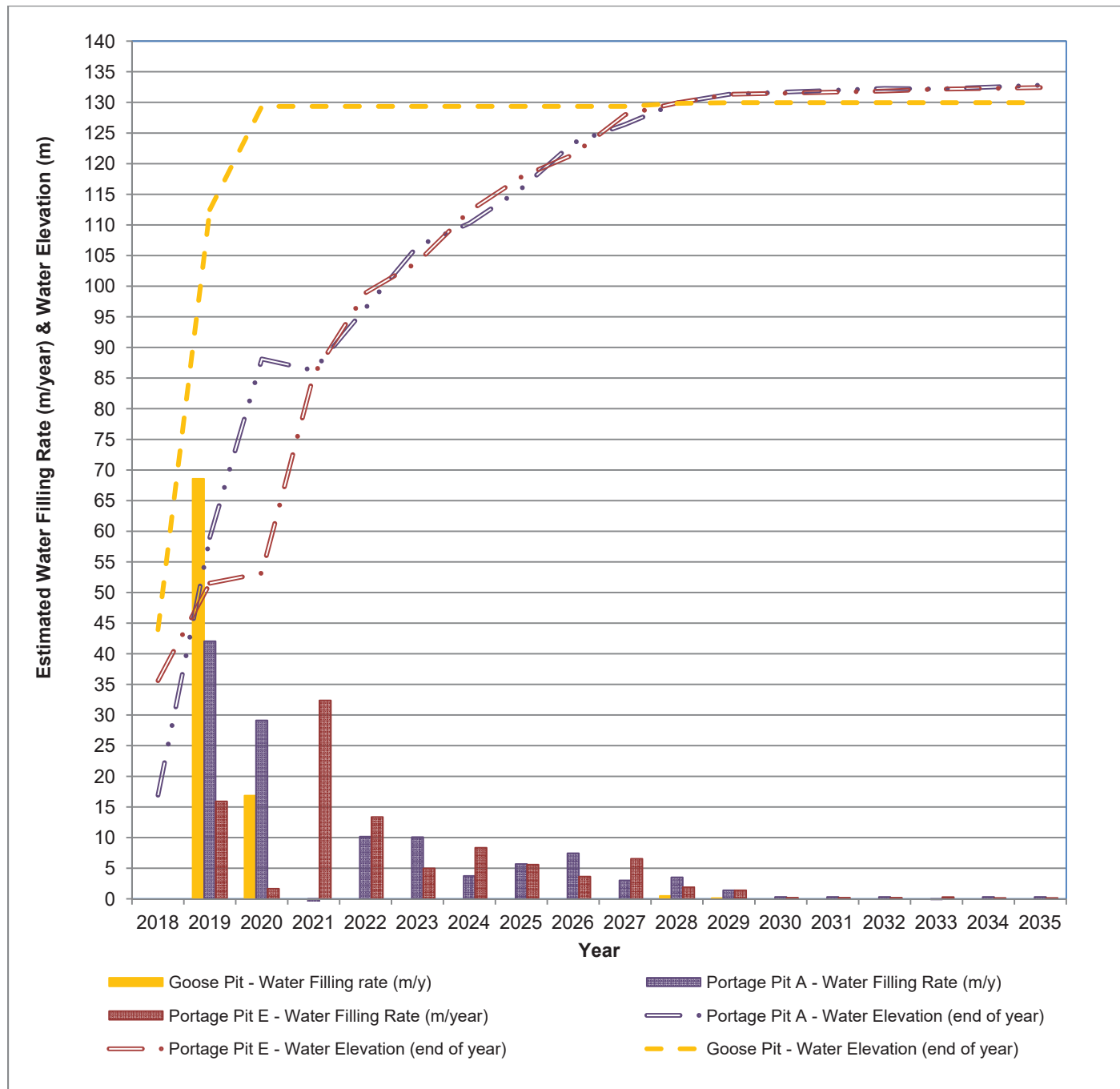
In developing the water/mass balance for in-pit deposition, the following key operating parameters were considered:


- > Reclaim water is pumped from Portage Pit A or Pit E to the mill at a constant daily average flow of 230 m<sup>3</sup>/h (5520 m<sup>3</sup>/day);
- > Reclaim water is pumped from either Portage Pit A or Pit E. Water is only pumped from the inactive pit to ensure that a low Total Suspended Solids (TSS) in the reclaim water;
- > Prior to the start of deposition in Goose Pit, if required, water is transferred to Portage Pit E to lower the starting water elevation to about 40 to 45 masl. This will ensure that the water elevation does not exceed 130 masl at the end of deposition in Goose Pit;
- > During in-pit deposition, water is transferred from Goose Pit to Portage Pit E every summer to ensure its water elevation remained below 130 masl.

As shown in Figure 5-4, the variations in water elevation during in-pit deposition can be very high due to the deposition of slurry in the pit and the volume of water pumped back to the mill. Figure 5-5 presents the changes in water elevation over a year. Based on the model, the large changes in water elevation in Portage Pit A and Pit E occurs at the start of the in-pit deposition. At most, the water level can increase by 30 to 40 m/year. Assuming a 4 m difference have to be maintain between the water elevation and the reclaim pump, the pump skid will have to be moved up the ramp 7 to 10 times / year.

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**Figure 5-5: Estimated Yearly Changes in Water Elevation in Portage Pit A and E and Goose Pit**



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### 5.4.3 Fresh Water Consumption


In developing the water/mass balance for in-pit deposition, the following key operating parameters were considered with regard to fresh water consumption (i.e. from Third Portage Lake):

- > A minimum water cover of 3 m is maintained during in-pit deposition by adding Third Portage Lake water to Portage Pit A and Pit E when required.
- > Third Portage Lake is also added during pit closure in order that the water elevation reaches 133.6 masl by the end of the monitoring period (i.e. end of 2035).
- > Fresh water consumption at the mine site camp is assumed constant during in-pit deposition, pit closure and monitoring period.
- > Additional fresh water is added to the process to obtain a 54% w/w tailings slurry. The amount of fresh water added is evaluated based on the mill throughput, the slurry solid content, the volume of reclaim water pumped from the pits and the water content in the ore.

Table 5-7 presents the preliminary yearly fresh water consumption evaluated for in-pit deposition from 2018 to 2035. The estimated fresh water consumption includes the consumption required at the mill, the mine site camp and for pit filling.

**Table 5-7 : Preliminary Yearly Fresh Water Consumption during In-Pit Deposition**

Year	Phase	Mill and Camp (m <sup>3</sup> /year)	Portage Pit A (m <sup>3</sup> /year)	Portage Pit E (m <sup>3</sup> /year)	Goose Pit (m <sup>3</sup> /year)	Total per Year (m <sup>3</sup> /year)
2018	Portage/Vault Tailings to South Cell TSF	581,017				581,017
2019	Portage/Vault & Whale Tail Tailings to Goose Pit	905,359	1,500,000	1,500,000		3,905,359
2020	Whale Tail Tailings to Goose Pit and Pit A	778,554	1,500,000	1,150,000		3,428,554
2021	Whale Tail and Future Ore Bodies Tailings to Portage Pit A and Pit E	784,023	1,500,000			2,284,023
2022		784,023	1,500,000			2,284,023
2023		784,023				784,023
2024		778,554				778,554
2025		784,023				784,023
2026		784,023				784,023
2027		784,023				784,023
2028		593,830				593,830
2029	Pit Closure	34,675		1,500,000		1,534,675
2030	Pit Closure	34,675				34,675
2031	Monitoring	34,675				34,675
2032	Monitoring	34,675				34,675
2033	Monitoring	34,675				34,675
2034	Monitoring	34,675				34,675
2035	Monitoring	34,675				34,675
<b>Total</b>		<b>8,584,176</b>	<b>6,000,000</b>	<b>4,150,000</b>	<b>0</b>	<b>18,734,176</b>

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## 5.5 Water Quality Forecast

Table 5-8 presents the forecasted reclaim water Quality in Goose Pit, Portage Pit A, Portage Pit E at the end of the In-Pit Tailings Deposition (September 2028) and at the end of the Monitoring Period (December 2035), assuming that no active in-situ water treatment system is in place during Operations and Closure. Note that the water and mass balance model considers an in-situ tailings density of  $1.0 \text{ t/m}^3$ . Thus, the model accounts for the volume of water released from the tailings into the water column during deposition based on this in-situ tailings density.

For the purpose of the PFS design, CCME guidelines were used as a benchmark, however final site-specific closure limits will be developed through review of the final closure plan by regulatory agencies.

At the end of tailings deposition in Goose Pit and Portage Pit, many dissolved heavy metal concentrations are forecasted to be significantly higher than the CCME guidelines (i.e. 10% higher than guidelines; values highlighted in red in Table 5-8).

At the end of the Monitoring Period, even when a mixed pit conditions for Goose Pit, Portage Pit A and Portage Pit E is considered, many parameters remain higher than the CCME guidelines, including arsenic, copper, iron, cadmium, chromium, lead and selenium.

Table 5-9 presents the equilibrium concentrations of different heavy metals at the end of the monitoring period in Portage Pit, Goose Pit and mixed pits condition. The equilibrium concentrations were evaluated using the USGS geochemical modeling tool PHREEQC (USGS 2015). At equilibrium, many of the metals should precipitate out of solution, like arsenic, iron and copper. However, according to this evaluation, certain metals will remain higher than the CCME guidelines in the mixed Portage Pit, Goose Pit and mixed pits scenario after pit flooding and monitoring period, including silver, chromium, molybdenum, selenium, thallium, fluoride and total ammonia, and cadmium in Goose Pit only.


Long term consolidation of the tailings in the pit could also release pore water with similar reclaim water quality properties and may increase the concentration of these contaminants in the pit water following in-pit deposition, pit flooding and closure. However, the 1D tailings consolidation model suggests that the final in-situ tailings density could reach as high as  $1.08$  to  $1.1 \text{ t/m}^3$  one year following the end of deposition, and does not increase significantly in the following years (SNC 2017a).

Contaminants within the tailings pore water could also diffuse to the environment following closure due to concentration gradients between the tailings pore water and the water column above the tailings. This could lead to a higher contaminant concentration at the surface of the tailings compare to the concentration in the water column.

In order to meet the CCME guidelines and/or final site-specific closure limits with regard to total metals in the Portage and Goose Pits water following in-pit deposition and pit closure, active in-situ water treatment will be required at closure. The objective of this treatment system is to precipitate the dissolved metals out of solution and allow the metal precipitate to settle out in the pits.

With regard to total cyanide, it is forecasted to be higher than the CCME guidelines. However, by the end of the monitoring period, most of the cyanide would volatilize and the final concentrations are forecasted to be well below the criteria guidelines.

Forecasted ammonia concentrations are more elevated than the CCME guideline. This parameter can be removed through a variety of treatment methods, such as in-situ aeration during the summer months, chemical oxidation or biological treatment.

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Chloride, fluoride, and nitrate concentrations are also forecasted to be slightly more elevated than CCME guidelines at the end of deposition. At the end of the monitoring period, only fluoride will remain slightly more elevated than CCME guidelines.

The total nitrogen equivalent, which is the sum of total ammonia and nitrate concentrations, is also forecasted to be higher than the threshold concentration in terms of nutrient concentration that are typically adopted for adopted for an oligotrophic lake (Nurnberg 1996). Third Portage Lake is considered as a highly oligotrophic lake. The CCME guidelines do not have a specific criterion for this parameter.

Further investigation and discussion are required to review the potential impacts these parameters (F, SO<sub>4</sub>, ammonia and nitrate) could have on Third Portage Lake water quality once the dikes are breached.

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**Table 5-8 : Forecasted Reclaim Water Quality in Portage and Goose Pits**

Parameters	Units	CCME Guidelines	At End of Deposition – September 2028					At End of Monitoring Period – December 2035				
			Portage Pit A	Portage Pit E	Mixed Portage Pit	Goose Pit		Portage Pit A	Portage Pit E	Mixed Portage Pit	Goose Pit	Mixed Pits
Alkalinity	mg CaCO <sub>3</sub> /L	n/a	160	130	142	102		123	86	99	90	98
Hardness	mg CaCO <sub>3</sub> /L	n/a	1609	1273	1412	742		1178	797	930	644	892
Total dissolved solids	mg/L	n/a	3860	3060	3391	1817		2820	1909	2227	1581	2141
Total Aluminium (Al)	mg/L	0.10	0.41	0.33	0.36	0.22		0.31	0.21	0.24	0.19	0.24
Total Silver (Ag)	mg/L	0.00025	0.00039	0.00036	0.00037	0.00149		0.00030	0.00026	0.00027	0.00134	0.00041
Total Arsenic (As)	mg/L	0.005	1.336	1.049	1.168	0.495		0.971	0.649	0.761	0.427	0.717
Total Barium (Ba)	mg/L	n/a	0.2694	0.2131	0.2364	0.1173		0.1975	0.1336	0.1559	0.1020	0.1487
Total Cadmium (Cd)	mg/L	0.00004	0.00009	0.00009	0.00009	0.00037		0.00007	0.00006	0.00006	0.00034	0.00010
Total Chromium (Cr)	mg/L	0.001	0.015	0.012	0.014	0.006		0.011	0.008	0.009	0.005	0.008
Total Copper (Cu)	mg/L	0.002	1.343	1.061	1.178	0.645		0.976	0.659	0.770	0.556	0.741
Total Iron (Fe)	mg/L	0.30	2.80	2.23	2.46	1.53		2.06	1.40	1.63	1.35	1.60
Total Lead (Pb)	mg/L	0.001	0.004	0.003	0.003	0.001		0.003	0.002	0.002	0.001	0.002
Total Manganese (Mn)	mg/L	n/a	0.206	0.179	0.191	0.444		0.155	0.121	0.133	0.404	0.169
Total Mercury (Hg)	mg/L	0.000026	0.000048	0.000043	0.000045	0.000041		0.000038	0.000028	0.000032	0.000038	0.000033
Total Molybdenum (Mo)	mg/L	0.073	0.139	0.112	0.123	0.112		0.102	0.071	0.082	0.097	0.084
Total Nickel (Ni)	mg/L	0.025	0.139	0.109	0.121	0.056		0.102	0.068	0.080	0.048	0.076
Total Selenium (Se)	mg/L	0.001	0.006	0.005	0.006	0.012		0.005	0.004	0.004	0.010	0.005
Total Strontium (Sr)	mg/L	n/a	0.653	0.522	0.576	0.390		0.484	0.332	0.385	0.337	0.378
Total Thallium (Ti)	mg/L	0.0008	0.0008	0.0008	0.0008	0.0035		0.0010	0.0008	0.0009	0.0032	0.0012
Total Uranium (U)	mg/L	0.015	0.002	0.002	0.002	0.002		0.002	0.001	0.001	0.002	0.001
Total Zinc (Zn)	mg/L	0.03	0.006	0.006	0.006	0.008		0.005	0.004	0.005	0.008	0.005
Chloride	mg/L	120	150	124	135	72		110	77	88	62	85
Fluoride (F)	mg/L	0.12	0.37	0.31	0.34	0.37		0.30	0.23	0.25	0.34	0.27
Sulphate (SO <sub>4</sub> )	mg SO <sub>4</sub> /L	n/a	3012	2377	2640	1375		2190	1476	1725	1188	1654
Total Cyanide (CNI)	mg/L	0.005	1.511	0.499	0.296	0.000		0.000	0.000	0.000	0.000	0.000
Total Ammonia (NH <sub>3</sub> + NH <sub>4</sub> )	mg N/L	1.83	22.6	17.9	19.9	11.2		16.5	11.5	13.2	9.6	12.8
Nitrate (NO <sub>3</sub> )	mg N/L	2.94	3.74	3.08	3.35	2.13		2.91	2.00	2.32	1.84	2.25



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Parameters	Units	CCME Guidelines	At End of Deposition – September 2028				At End of Monitoring Period – December 2035			
			Portage Pit A	Portage Pit E	Mixed Portage Pit	Goose Pit	Portage Pit A	Portage Pit E	Mixed Portage Pit	Goose Pit
Total N equivalent	mg N/L	0.35 (**)	26.3	21.0	23.2	13.3	19.4	13.5	15.6	11.5
Dissolved Aluminium (Al)	mg/L	0.1	0.206	0.169	0.184	0.132	0.155	0.108	0.124	0.115
Dissolved Silver (Ag)	mg/L	0.00025	0.00033	0.00029	0.00031	0.00064	0.00025	0.00019	0.00022	0.00056
Dissolved Arsenic (As)	mg/L	0.005	1.3357	1.0486	1.1674	0.4949	0.9704	0.6483	0.7606	0.4265
Dissolved Barium (Ba)	mg/L	n/a	0.2680	0.2119	0.2351	0.1165	0.1965	0.1329	0.1550	0.1013
Dissolved Cadmium (Cd)	mg/L	0.00004	0.00009	0.00008	0.00009	0.00037	0.00007	0.00006	0.00006	0.00034
Dissolved Chromium (Cr)	mg/L	0.001	0.0029	0.0023	0.0026	0.0012	0.0022	0.0015	0.0017	0.0010
Dissolved Copper (Cu)	mg/L	0.002	1.220	0.964	1.070	0.586	0.887	0.598	0.699	0.505
Dissolved Iron (Fe)	mg/L	0.3	2.6	2.0	2.3	1.1	1.9	1.3	1.5	0.9
Dissolved Lead (Pb)	mg/L	0.001	0.002	0.002	0.002	0.001	0.002	0.001	0.001	0.001
Dissolved Manganese (Mn)	mg/L	n/a	0.198	0.169	0.181	0.314	0.149	0.111	0.124	0.284
Dissolved Mercury (Hg)	mg/L	0.000026	0.000047	0.000040	0.000043	0.000042	0.000037	0.000027	0.000031	0.000038
Dissolved Molybdenum (Mo)	mg/L	0.073	0.134	0.108	0.118	0.109	0.098	0.068	0.078	0.094
Dissolved Nickel (Ni)	mg/L	0.025	0.042	0.033	0.037	0.020	0.031	0.021	0.025	0.018
Dissolved Selenium (Se)	mg/L	0.001	0.006	0.005	0.006	0.012	0.005	0.004	0.004	0.011
Dissolved Strontium (Sr)	mg/L	n/a	0.640	0.512	0.565	0.382	0.473	0.325	0.377	0.331
Dissolved Thallium (Ti)	mg/L	0.0008	0.0008	0.0008	0.0008	0.0035	0.0010	0.0008	0.0009	0.0032
Dissolved Uranium (U)	mg/L	0.015	0.0021	0.0018	0.0019	0.0022	0.0016	0.0012	0.0013	0.0019
Dissolved Zinc (Zn)	mg/L	0.03	0.0049	0.0048	0.0048	0.0089	0.0040	0.0034	0.0036	0.0082


Notes:

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Cells highlighted in red indicated forecasted concentrations that are 10% times higher than the CCME guidelines.

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Value based on the threshold concentration considered for an oligotrophic lake in terms of nutrient concentration (Nurnberg 1996).

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**Table 5-9 : Forecasted Reclaim Water Quality in Portage and Goose Pits at Equilibrium**

			At End of Monitoring Period – December 2035					
			Mixed Portage Pit		Goose Pit		Mixed Pits	
Parameters	Units	CCME Guidelines	Mass Balance	Equil. Conc.	Mass Balance	Equil. Conc..	Mass Balance	Equil. Conc..
pH		6.5 to 9.0	7.5 est.	7.9	7.5 est.	7.9	7.5 est.	7.9
Alkalinity	mg CaCO <sub>3</sub> /L	n/a	99	26	90	27	98	26
Hardness	mg CaCO <sub>3</sub> /L	n/a	930	860	644	586	892	823
Total dissolved solids	mg/L	n/a	2227	-	1581	-	2141	-
Total Aluminium (Al)	mg/L	0.10	0.24	0.00040	0.19	0.00044	0.24	0.00041
Total Silver (Ag)	mg/L	0.00025	0.00027	0.00027	0.0013	0.00130	0.0004	0.00040
Total Arsenic (As)	mg/L	0.005	0.761	0.00075	0.427	0.00023	0.717	0.00065
Total Barium (Ba)	mg/L	n/a	0.1559	0.00059	0.1020	0.00098	0.1487	0.00062
Total Cadmium (Cd)	mg/L	0.00004	0.00006	0.000015	0.00034	0.000056	0.00010	0.000023
Total Chromium (Cr)	mg/L	0.001	0.009	0.0050	0.005	0.0024	0.008	0.0046
Total Copper (Cu)	mg/L	0.002	0.770	0.00044	0.556	0.00032	0.741	0.00042
Total Iron (Fe)	mg/L	0.30	1.63	7.51E-09	1.35	6.99E-09	1.60	7.45E-09
Total Lead (Pb)	mg/L	0.001	0.002	2.67E-07	0.001	1.05E-07	0.002	2.43E-07
Total Manganese (Mn)	mg/L	n/a	0.133	5.52E-11	0.404	3.69E-11	0.169	5.26E-11
Total Mercury (Hg)	mg/L	0.000026	0.000032	0.0000249	0.000038	0.0000103	0.000033	0.0000237
Total Molybdenum (Mo)	mg/L	0.073	0.082	0.0794	0.097	0.0934	0.084	0.0813
Total Nickel (Ni)	mg/L	0.025	0.080	0.0100	0.048	0.0046	0.076	0.0092
Total Selenium (Se)	mg/L	0.001	0.004	0.0039	0.010	0.0104	0.005	0.0048
Total Strontium (Sr)	mg/L	n/a	0.385	0.385	0.337	0.337	0.378	0.378
Total Thallium (Ti)	mg/L	0.0008	0.0009	0.00090	0.0032	0.00317	0.0012	0.00120
Total Uranium (U)	mg/L	0.015	0.001	0.00136	0.002	0.00192	0.001	0.00144
Total Zinc (Zn)	mg/L	0.03	0.005	0.00021	0.008	0.00025	0.005	0.00022
Chloride	mg/L	120	88	88	62	62	85	85
Fluoride (F)	mg/L	0.12	0.25	0.254	0.34	0.338	0.27	0.265
Sulphate (SO <sub>4</sub> )	mg SO <sub>4</sub> /L	n/a	1725	1724	1188	1187	1654	1653
Total Cyanide (CNT)	mg/L	0.005	0.000	1.24E-05	0.000	1.53E-08	0.000	1.10E-05
Total Ammonia (NH <sub>3</sub> + NH <sub>4</sub> )	mg N/L	1.83	13.2	13.2	9.6	9.6	12.8	12.8
Nitrate (NO <sub>3</sub> )	mg N/L	2.94	2.3	2.3	1.8	1.8	2.3	2.3
Total N equivalent	mg N/L	0.35 (**)	15.6	15.56	11.5	11.5	15.0	15.0


Notes:

xxx

Cells highlighted in red indicated forecasted concentrations that are 10% times higher than the CCME guidelines.

\*\*

Value based on the threshold concentration considered for an oligotrophic lake in terms of nutrient concentration (Nurnberg 1996).

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## 6.0 Infrastructure Requirements

### 6.1 General

In order to implement in-pit deposition at Meadowbank, the following infrastructure will be required on site:

- > New pipeline to transfer the tailings to Goose Pit, Portage Pit A and Pit E;
- > New pipeline to transfer reclaim water from the pits to the mill and between the pits;
- > Reclaim water pumping stations;
- > Reclaim water treatment system (for pit closure);
- > Central Dump monitoring wells.

### 6.2 Pipelines

Figure 6-1 presents an overview of the tailings pipeline routing to Goose Pit, Portage Pit A and Pit E, while Figures 6-2 to 6-4 present the approximate ground profile where the pipelines will be installed toward Goose Pit, Portage Pit A and Pit E respectively. The profiles shown on these figures are preliminary only and will be optimized to avoid any sudden rises and low points in the next phase of the project.

No changes are expected to the existing tailings and reclaim water pipeline from the mill to tie-in points located just to the north of the access road that runs along the south of the North and South Cells TSF. From the tie-in points, a new tailings pipeline will be installed and follow the North/South Cells TSF access road. The new tailings pipeline will then cross either aboveground or under the Goose/Portage Pit west road. The pipeline can then be sent to Goose Pit, Portage Pit E and Pit A.

The new reclaim water pipeline will also follow the same routing as the tailings pipelines for Portage Pit A and Pit E.

Table 6-1 summarizes the new pipelines required for in-pit deposition while Figure 6-5 presents a general overview of the pipelines. A general site layout can be found in Appendix 2.

**Table 6-1 : Summary of New Pipelines for In-Pit Deposition**

Item	New Pipeline	Diameter (in)	Approx. Length (m)	Material
1	Tailings to Goose and Portage Pits (header)	14	500	HDPE DR11
2	Tailings to Goose Pit	14	1800	HDPE DR11
3	Tailings to Portage Pit E	14	900	HDPE DR11
4	Tailings to Portage Pit A	14	900	HDPE DR11
5	Reclaim water from Portage Pit A/Pit E (header)	14	500	HDPE DR11
6	Reclaim water from Portage Pit A	14	900	HDPE DR11
7	Reclaim water from Portage Pit E	14	900	HDPE DR11
8	Goose Pit to Portage Pit E	8	720	HDPE DR11
9	Reclaim water to Water Treatment (for pit closure)	14	850	HDPE DR11
10	Treated reclaim water to pit (for pit closure)	14	850	HDPE DR11



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## TECHNICAL NOTE

### In-Pit Tailings Deposition Water Balance and Water Quality Forecast

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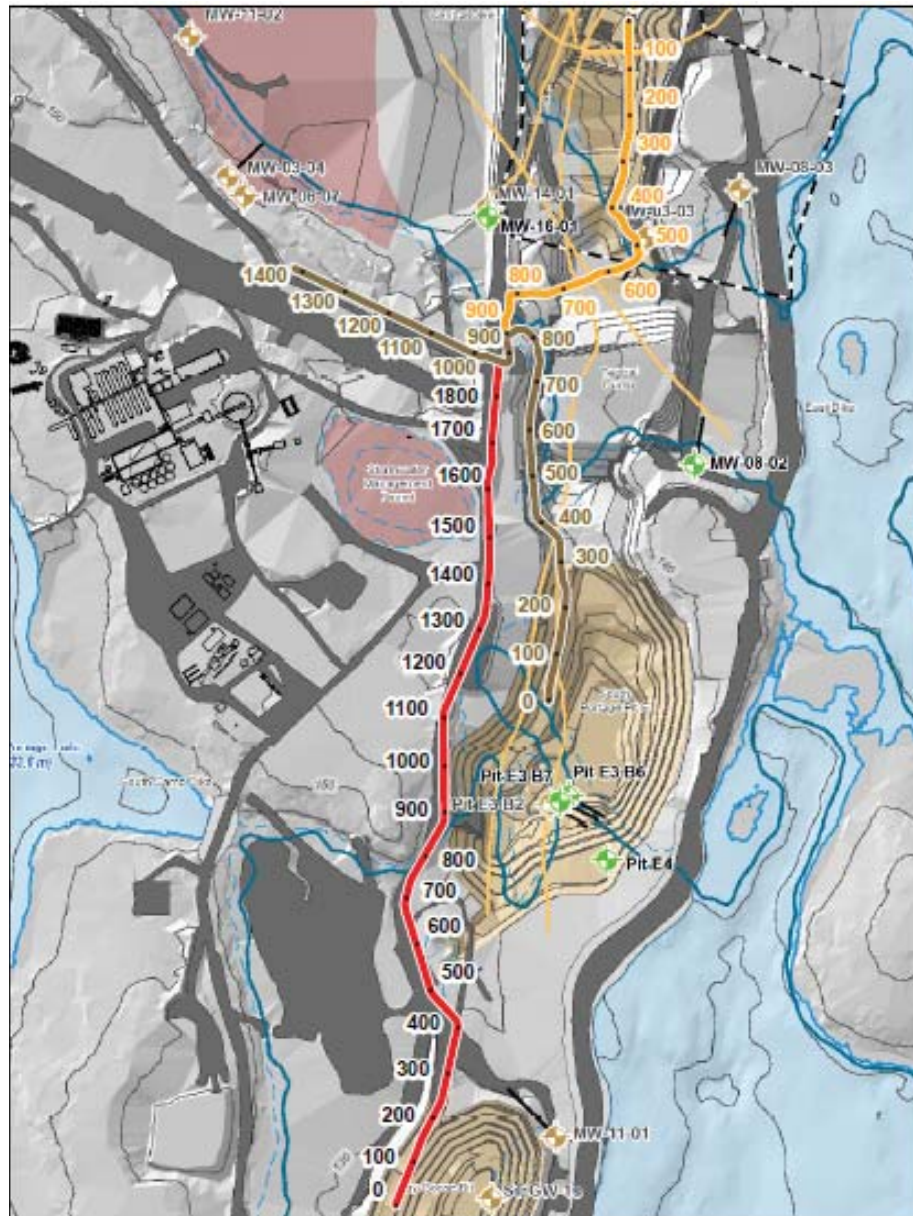
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**Figure 6-1: Tailings Pipeline Routing Overview**



**Notes:**

- Red line: Tailings to Goose Pit
- Brown line: Tailings to Portage Pit E
- Orange line: Tailings to Portage Pit A



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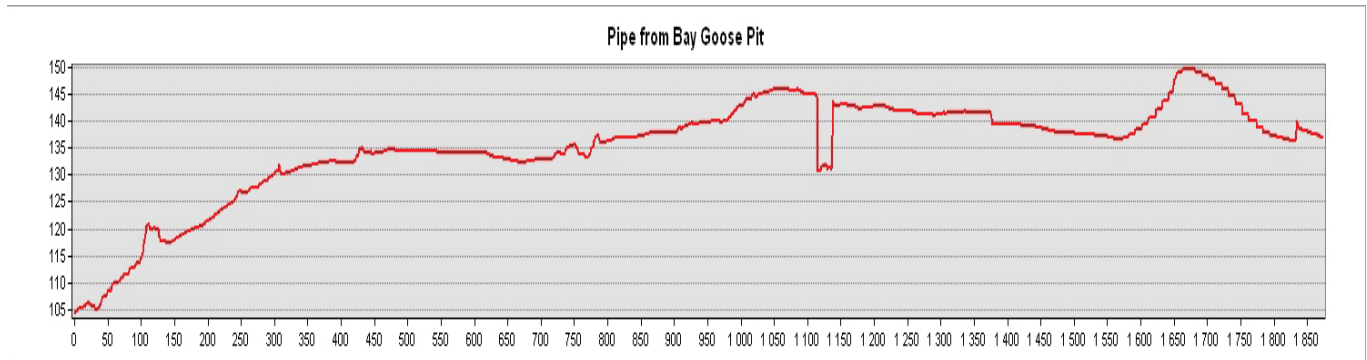
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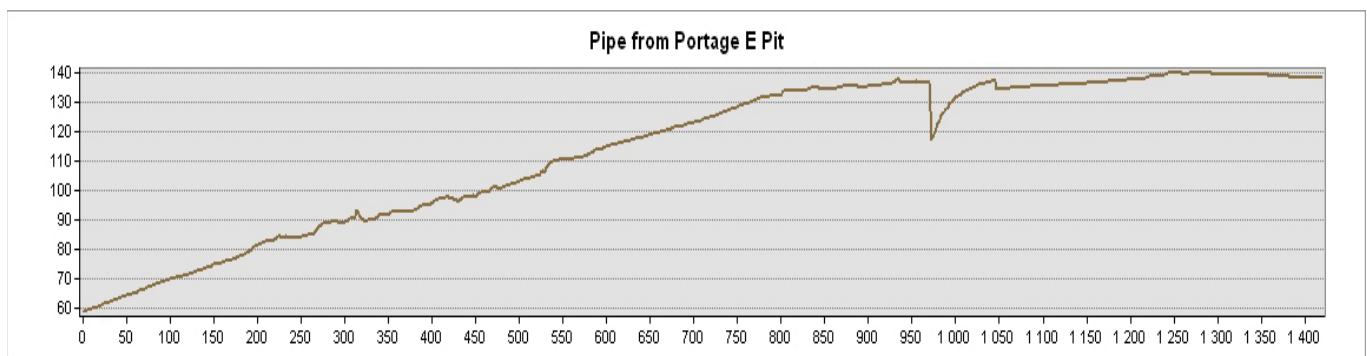
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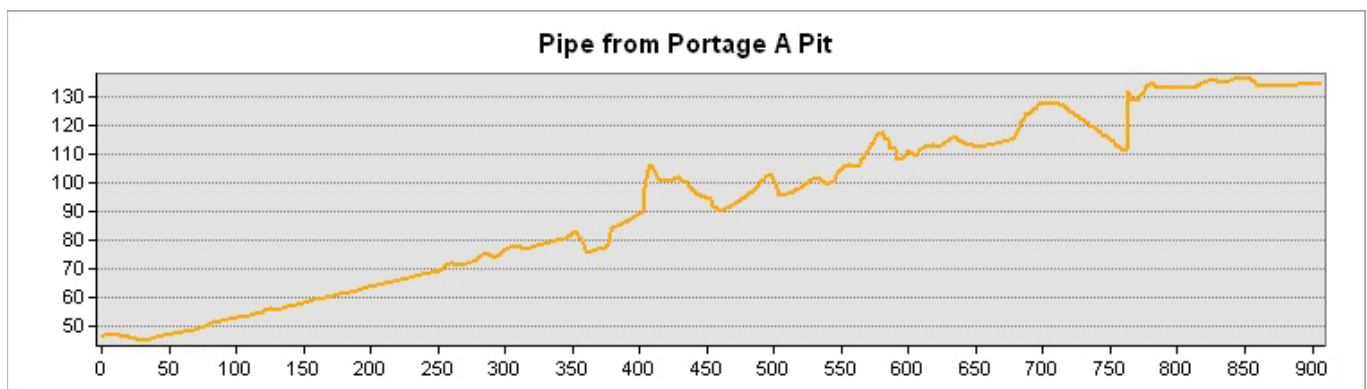
**Figure 6-2: Approximate Pipeline Profile to Goose Pit**




**Figure 6-3: Approximate Pipeline Profile to Portage Pit E**



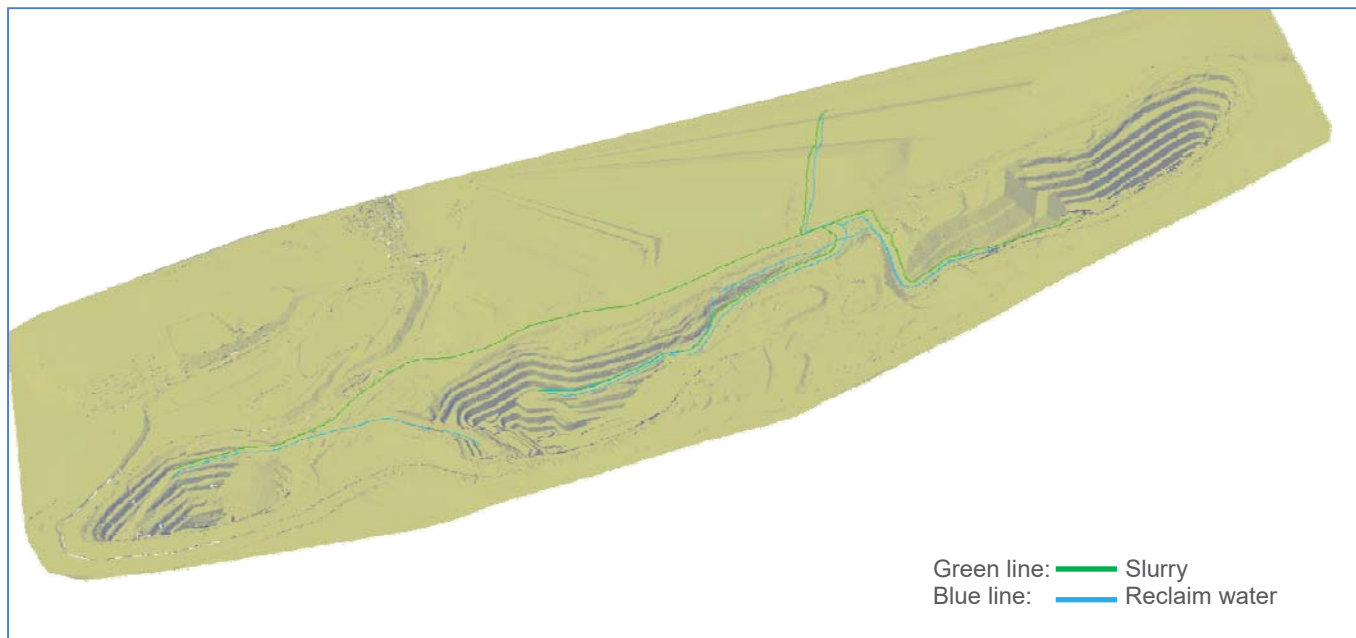
**Figure 6-4: Approximate Pipeline Profile to Portage Pit A**





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**Figure 6-5: General Overview of Slurry and Reclaim Water Pipelines for In-Pit Deposition**



## 6.3 Pumping Stations

Table 6-2 presents a summary of the estimate capacity and total dynamic head (TDH) required for the tailings pumps and reclaim water pumps.

### Tailings Pumps


Tailings will be transferred to the pits using the existing final tailings pumps no. 1 & 2 (360-PP-040 & 041) and no. 3 & 4 (360-PP-105 & 106). The pump model is an FLSmith Krebs millMAX 8x6-24 4V with a design flow of 506 m<sup>3</sup>/h with a slurry head of 57.5 m (equivalent water head 59.3 m). To achieve this operating point, the pump speed is adjusted at 931 RPM. The maximum operating speed of the pump is 1200 rpm.

The elevation of the mill floor is at 148.65 m while the pits are located below elevation 130 m. Thus, the existing tailings pumps need mainly to provide the necessary head to compensate for the friction loss in the pipeline. The pipeline friction loss will be offset by the elevation drop between the mill and the pit.

Based on the estimated tailings pump capacity and head, the existing pump have the required capacity to transfer 506 m<sup>3</sup>/h (or 12,144 m<sup>3</sup>/day) of tailings slurry to the pits. The speed of the pump will have to be adjusted to meet the required flow and slurry head requirements.

### Reclaim Water Pumps

New reclaim water pumps will be needed to transfer water from Portage Pit A or Pit E to the reclaim water tank 650-TK-036 located in the mill. The water/mass balance considers an average daily reclaim water flow of 230 m<sup>3</sup>/h (5520 m<sup>3</sup>/d). However, a design flow of 400 m<sup>3</sup>/h was selected in order to provide the required daily volume in a shorter time. The design head is based on the lowest water elevation expected during operation in Pit A and Pit E. As the water rises in the pit, the pump speed will be adjusted to account for the lower static head.

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In order to maintain the water level in Goose Pit below 130 masl during in-pit deposition, a transfer pump with a design capacity of 250 m<sup>3</sup>/h was considered. At this pump capacity, about 180,000 m<sup>3</sup> can be transferred over 30 days. During operation, once in-pit deposition is completed in Goose Pit, the water elevation is not expected to vary significantly.

The water treatment system required after deposition for pit closure is assumed to have a treatment design capacity of 500 m<sup>3</sup>/h (12,000 m<sup>3</sup>/day). For the PFS design, the water treatment system is assumed to be located at an elevation of 135 masl. The pump will be equipped with a variable speed motor to adjust the treatment capacity.

For the PFS design, each reclaim water pump will be housed inside a heated container. The container will also house the electrical motor starter or VFD panels, electrical panel, local control panel and instrumentations. The container will be design so that it can be moved easily along the pit ramp.

**Table 6-2 : Summary of Estimated Pump Capacity**

Item	Description	Nominal Flow (m <sup>3</sup> /h)	TDH approx. (m)	Notes
1	Tailings to Goose Pit	506	73 (slurry)	Variable speed (approx. 1030 rpm)
2	Tailings to Portage Pit E	506	47 (slurry)	Variable speed (approx. 840 rpm)
3	Tailings to Portage Pit A	506	50 (slurry)	Variable speed (approx. 870 rpm)
4	Reclaim water from Portage Pit A and Pit E	400	180	Variable speed
5	Goose Pit to Portage Pit E	250	35	Fixed speed
6	Reclaim water to WTP (for pit closure)	500	85	Variable speed

Note: TDH = Total Dynamic Head

## 6.4 Water Treatment System


Water treatment will be required following in-pit deposition to treat the pit water for closure, as described in Section 5.5.

The objective of this treatment system is to precipitate any dissolved metals in the pit water so that at closure, the dissolved and total metal concentrations are lower than the CCME guidelines and/or site specific closure limits.

As part of the hydrological modeling of the site, a 3D contaminant transport model was developed. The results of the modelling indicate that there could be very little diffusion of water within the pits to the environment, even if the transport simulations are considered conservative since neither contaminant retardation factor nor contaminant concentration reduction by natural degradation or treatment were considered. As an example, at post closure, the contaminant plume originating from Portage Pit A will only reach the East Dike and Second Portage Lake about 200m downgradient after more than 2500 years (SNC 2017b). Thus, the reclaim water should be contained within the pits, providing the necessary time to treat the water following in-pit deposition.

For the purpose of the PFS study, the water treatment system included in the design consists of the following:



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- > Pumping system that will pump water from the pit to the water treatment system.
- > Dosage of a proprietary chemical that allows for the precipitation of dissolved metals. The chemical to be added could be Nalco's Nalmet, SNF's Metasorb, a coagulant like ferric sulphate or other type of chelating chemicals.
- > Addition of a flocculant to assist in the settling of the metal precipitate (if required)
- > Return of the treated water to the pit to allow the precipitate metals to settle out of solution.


The treatment system is designed to pump and treat a flow of 500 m<sup>3</sup>/hr, or 12,000 m<sup>3</sup>/day. Treatment of the pit water could be implemented over the summer months or on a yearly basis.

## 6.5 Portage Central Dump Monitoring Wells

Due to concerns of migration of reclaim water into the more permeable Portage Central Dump, monitoring well(s) will be required in this area.

The monitoring well(s) will be used to sample regularly the groundwater in the Central Dump and monitor its water quality at different depths. Moreover, the monitoring well(s) will also be equipped with a piezometer which will allow monitoring the water level in the dump. With this information, hydraulic gradients between Central Dump and the underneath Portage Fault and Bay Fault could be investigated during different in-pit deposition periods, including before mine closure, to assess groundwater flow and manage reclaim water migration risks toward lakes.

If the water quality degrades due to migration of reclaim water, then a contingency solution will have to be considered. This includes a possible "pump and treat" system, similar to the system described in Section 6.4.


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## 7.0 Material Take-Off Summary


Table 7-1 presents the preliminary material take-off for the In-Pit Tailings Deposition. The quantities estimation has been estimated based on PFS engineering drawings.

**Table 7-1: Preliminary Material Take-Off for In-Pit Deposition**

Item	Description	Unit	Quantity
	<b>TAILINGS SLURRY PIPELINE</b>		
	14-in HDPE DR11 from Process Plant to Goose/Portage Pit area	m	500
	14-in HDPE DR11 to Portage Pit E	m	900
	Modifications to Road to Pit E	m.l	900
	14-in HDPE DR11 to Portage Pit A	m	900
	Modifications to Road to Pit A	m.l	900
	14-in HDPE DR11 to Goose Pit	m	1800
	Modifications to Road to Goose Pit	m.l	1800
	14-in gate valve (1 to Pit E, 1 to Pit A, 1 to Goose Pit, 1 header, 1 to SC TSF)	u	5
	14-in HDPE tee to install at connection close to SC TSF	u	1
	14-in HDPE tee to install at Portage Pit to send to Pit A or Pit E and Goose Pit	u	2
	<b>PORTAGE PIT RECLAIM WATER PIPELINE</b>		
	14-in HDPE DR11 from Portage Pit E	m	900
	14-in HDPE DR11 from Portage Pit A	m	900
	14-in HDPE DR11 from Portage Pit to existing header	m	500
	14-in HDPE DR11 suction line	m	10
	Electrical heat tracing of 14-in HDPE DR11 lines	m	2300
	14-in isolation gate valves (2 x tees)	u	4
	14-in HDPE tee to install at connection close to SC TSF	u	1
	14-in HDPE tee to install at Portage Pit to take reclaim water from Pit A or E	u	1
	Reclaim Pump Station: 1 x 400 m <sup>3</sup> /hr at 180 m TDH, c/w 450 HP motor, pump container, piping, valve and electrical container	lot	1
	High-Voltage Transformer for Reclaim Pump Station and In-Situ Water Treatment container (to be moved between Pit E and Pit A)	u	1
	Pad (foundation work along the ramp if required)	Lot	1
	<b>GOOSE PIT WATER TRANSFER TO PORTAGE PIT E</b>		
	8-in HDPE DR11 from Goose Pit to Portage Pit E	m	720
	8-in HDPE DR11 suction line	m	10

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Item	Description	Unit	Quantity
	8-in isolation gate valve (1 x on HDPE line, at discharge of pump container)	u	1
	Water Transfer Pump Station: 1 x 250 m <sup>3</sup> /hr at 35 m TDH, c/w 50 HP motor, pump container, piping, valve and electrical container	lot	1
	Pad (foundation work along the ramp if required)	lot	1
	High-Voltage Transformer for Goose Pit pump station	u	1
	<b>PORTAGE PIT WATER TREATMENT SYSTEM (FOR PIT CLOSURE)</b>		
	14-in HDPE DR11 pipeline from the pit to the water treatment system	m	850
	14-in HDPE DR11 treated water pipeline back to pit	m	850
	14-in HDPE DR11 suction line	m	10
	14-in isolation gate valve (1 x on HDPE line, at discharge of pump container)	u	1
	Pit Water Pump Station: 1 x 500 m <sup>3</sup> /hr at 85 m TDH c/w 450 HP motor, pump container, piping, valve and electrical container	lot	1
	Pad (foundation work along the ramp if required)	lot	1
	Chemical dosing container, c/w skid mounted duplex dosing system, dosing drum, drum transfer pump, containment dike.	lot	1
	Pad (foundation) for Water Treatment System	lot	1
	<b>PORTAGE CENTRAL DUMP</b>		
	Monitoring well(s)	u	1 minimum

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# Appendix 1

## Process Flow Diagram





# Appendix 2

## General Site Layout for In-pit Deposition



