

Figure 2: Interpreted georadar image showing a typical ice body

4 CONCLUSIONS

A geophysical investigation involving Georadar was carried out at the Mary River Project, Baffin Island, Nunavut.

Subsurface ice mapping was carried out at nine sites along the proposed rail alignment. Results of the survey are presented in Drawings GPR17 – MILNE INLET, GPR17 – KM19, GPR17 – KM20, GPR17 – KM39.6, GPR17 – KM49, GPR17 – KM82.2, GPR17 – KM97, GPR17 – KM100.1, GPR17 – KM109. Ice was only found in Km 49, seen in drawing GPR17-KM49.

Interpretation of the geophysical data has been performed by Mauritz van Zyl. This report has been written by Milan Situm, P.Geo.

PRACTISING MEMBER

Milan Situm, P.Geo.

Mila Stur

Manager

APPENDIX A

Drawings GPR17 – MILNE INLET,

GPR17-KM19,

GPR17-KM20,

GPR17 -KM39.6,

GPR17-KM49, Ice was only found in Km 49, seen in drawing GPR17-KM49.

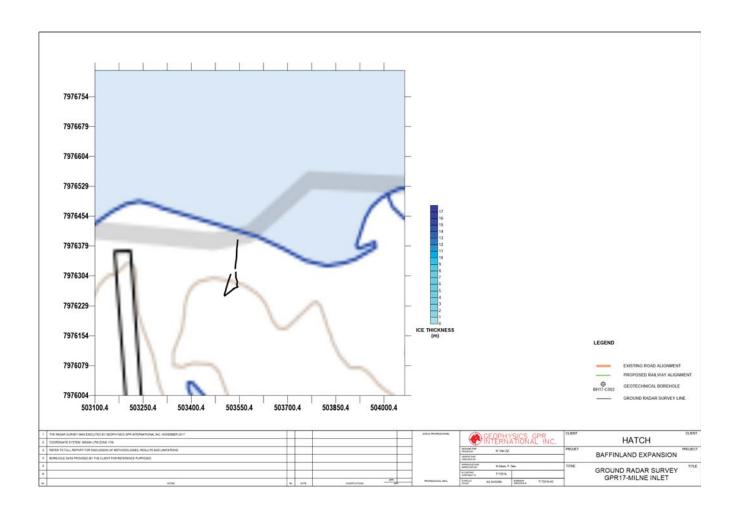
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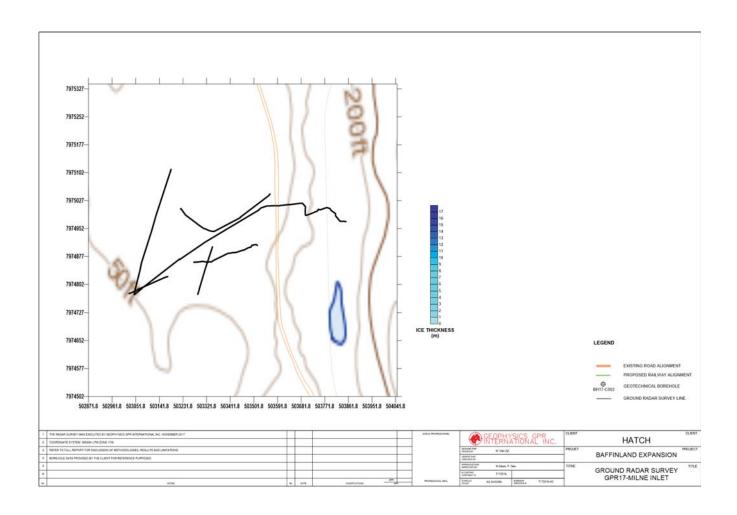
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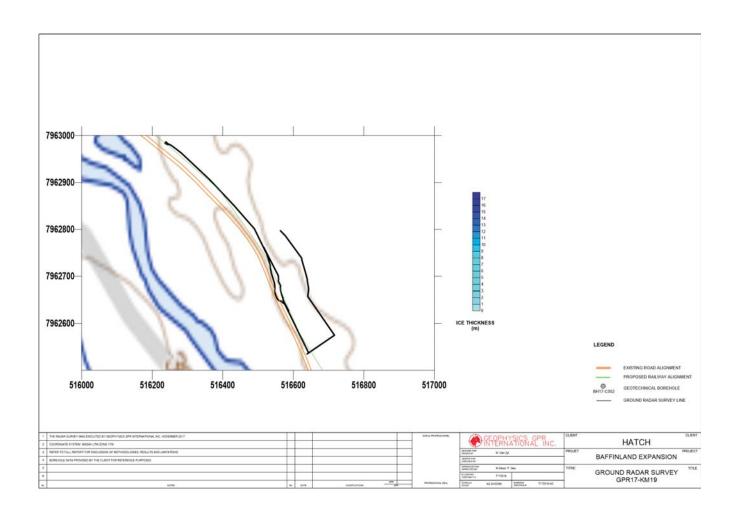
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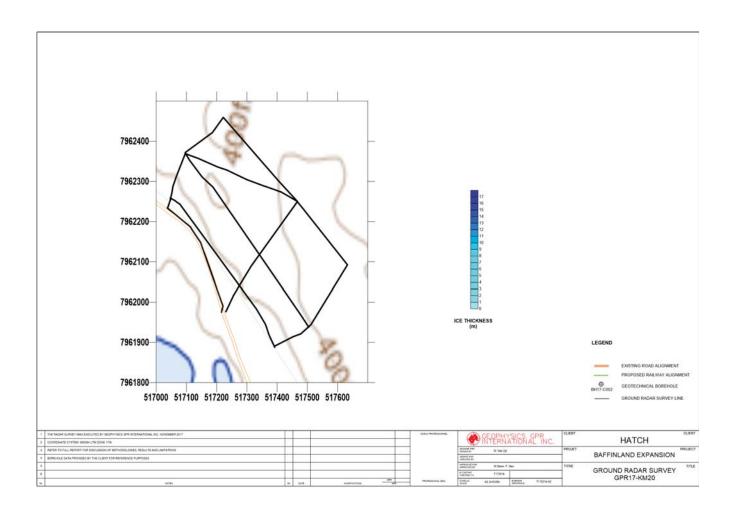
GPR17-KM109.



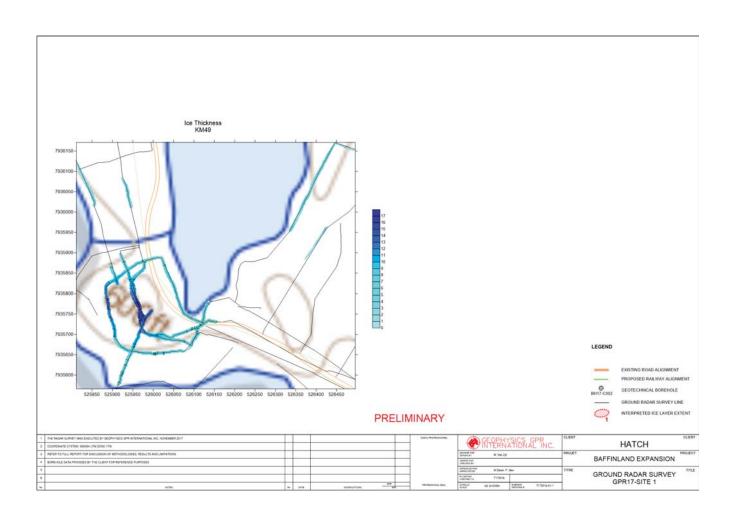


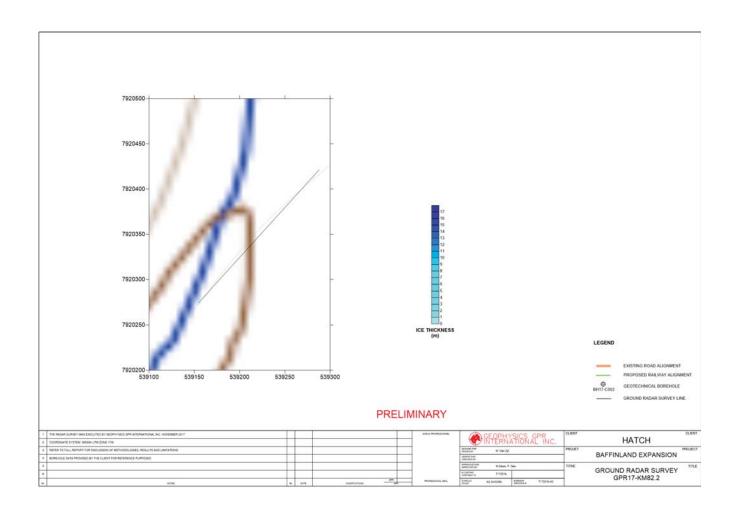


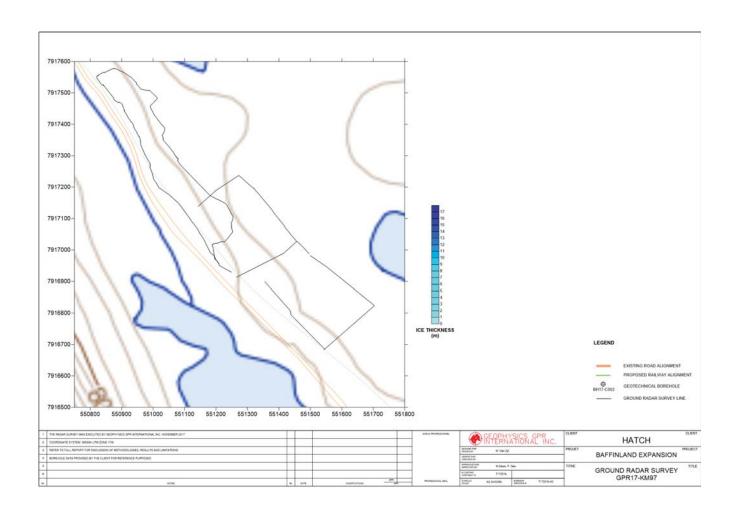


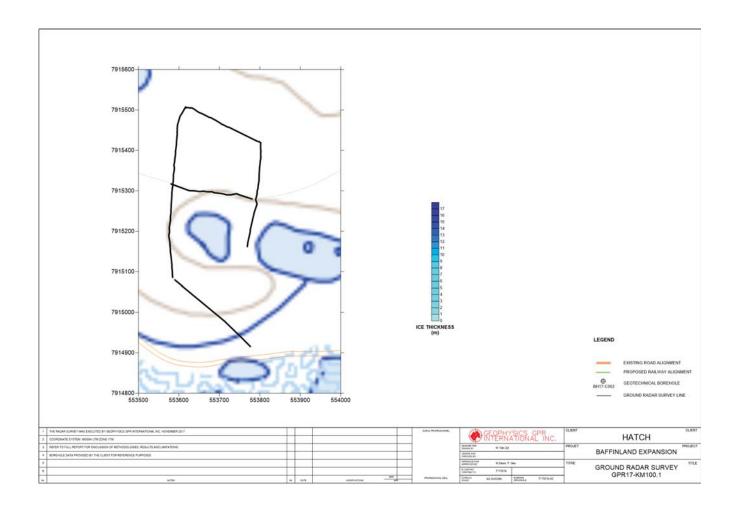


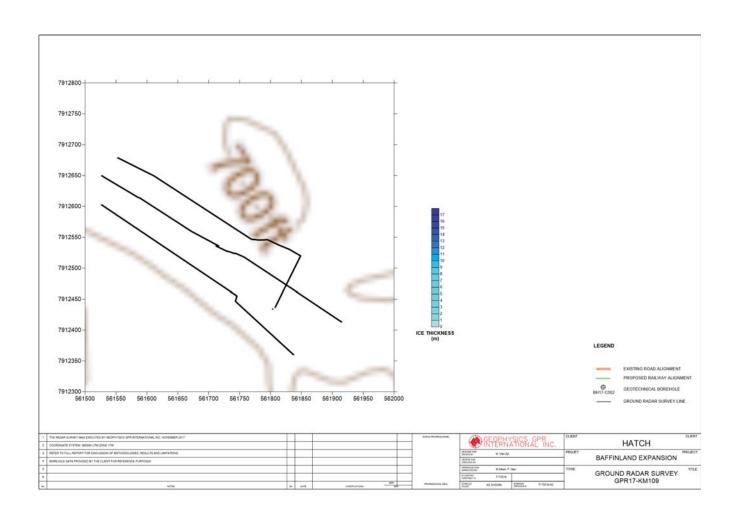










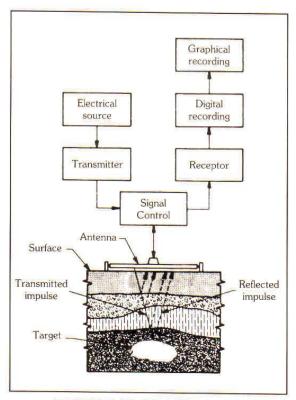


APPENDIX B

Additional Georadar information

GEORADAR

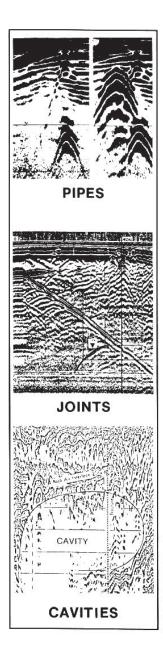
As indicated by its name, georadar combines high resolution radar with geology. The underlying principle is based on the propagation of electromagnetic wave impulses (VHF) that are reflected by anomalies in the terrain (joints, irregularities, interfaces, etc.) at different depths, and then captured by the antenna. The georadar records the time taken by each transmitted signal to complete the cycle in order to calculate the depth of the anomaly. The result is similar to a seismic reflection profile where all the reflections are displayed graphically. This technique is used to solve problems for which there had previously been no practical solution.



PRINCIPLES OF GEORADAR

FEATURES

- Penetration of more than 20 metres in certain materials (penetration being inversely proportional to conductivity).
- Surveying in continuous mode.
- Identification of objects measuring only a few centimeters.
- Light and manoeuvrable equipment.
- Detection of conductivity, open spaces and/or holes (cavities).
- Detection of breaks: faults, fractures, joints, cavities.
- Results similar to seismic reflection: continuous underground profile.
- Results available immediately.
- Can be used in land, sea or airborne surveys.



FIELDS OF APPLICATION

Civil Engineering / Mining Exploration-Exploitation / Research / Archaeology / Environment

- Geotechnology: investigation of soils and surface deposits.
- Optimal selection of anchor bolts in mines and quarries.
- Detection of buried pipes before beginning excavation.
- Detection of liquid or gas leakage in soils.
- Detection of cracks in concrete structures.
- Checking material homogeneity.
- Detection of cavities beneath road pavement.
- Determination of water saturation level.
- Detection of girders in reinforced concrete.
- Detection of pollutant leakage in water bodies.
- Inspection of buried disposal sites and or dangerous deposits.
- Continuous measurement of ice thickness.
- Archaeological research: ancient foundations, artifacts.
- Non-destructive method for measuring road pavement thickness.
- Localization and measurement of soil's thickness (swamps, peat bogs).
- Determination of rock beddings (location and thickness).
- Bathymetric studies (depth sounding).
- Calculation of the thickness of permafrost and ice.
- Geotechnical studies for the installation of aqueducts.

SPECIAL FEATURES

The equipment is practical, easy to manoeuvre, and multi-faceted. The field of application of georadar continues to expand in various sectors, particularly in geotechnology (aqueducts), civil engineering (excavation, structures) and mining (structures).





MALÅ GroundExplorer

GROUND PENETRATING RADAR

GPR with exceptional range and resolution

MALÅ GroundExplorer (GX) is an integrated GPR solution with four MALÅ GX antenna options: GX80, GX160, GX450 and GX750. Through unique hyperstacking HDR technology, MALÅ GX offers significantly faster data acquisition rates, with outstanding signal-to-noise ratio and depth penetration. An easy-to-use GPR solution on a rugged platform, with excellent detection capabilities for a wide range of applications.

MALÅ GX CONTROLLER

 Processor
 1.6 GHz Intel Atom

 Display
 1024 x 768 mm

OS Linux

Memory 8 GB compact Flash memory

Data output resolution 32 bit

Comms Ethernet, WiFi (optional), USB 3.0, RS232 (serial)

GPS Integrated support for built-in GPS, or external GPS

via USB/serial port (NMEA 0183 protocol)

Power supply Internal 12V/20.8 Ah Li-Ion battery,

or any external 10-15 V DC source

Charger Internal. Unit can also be charged from any external

12 - 15 V DC source

 Power consumption
 1.3 - 2.0 A

 Operating time
 8 - 10 h

Dimensions 326 x 216 x 92 mm including handles

326 x 216 x 52 mm excluding handles

Weight 3.2 kg

Operating temp - 20° to + 50° C or 0° to 120° F

Environmental IP 65

GX WIFI OPTION

Wireless standard: IEEE802.11 g
Power consumption: 0,3 A





MALÂ GX ANTENNAS

MALÁ GX750 HDR

Technology MALA Semi-Real- Time pat pending

 Antenna center freq.
 750 MHz

 SNR
 97 dB

 No. of bits
 16 bit

 Scans/second
 > 1290, time window 75 ns

 Survey speed
 460 [km/h] point distance 10 cm

 Bandwidth
 120%, fractional, -10 dB

Time window 75 ns

Positioning Built-in DGPS, external GPS

(NMEA 0183 protocol),

Operating time 5 h

Power supply Interchangeable 12 V

Li-Ion batt, or ext. 12 V DC source

Power consumption 1.3 A

Acq. mode Wheel, time or manual Dimensions 375 x 235 x 170 mm

Weight 3.6 kg

Operating temp. - 20° to + 50° C or 0° to 120° F

Environmental IP 65

MALA GX450 HDR

Technology MALA Semi-Real-Time pat pending

Antenna center freq. 450 MHz SNR 101 dB No. of bits > 16 bit

 Scans/second
 > 770, time window 300 ns

 Survey speed
 275 [km/h] point distance 10 cm

 Bandwidth
 >120%, fractional, -10 dB

Time window 300 ns

Positioning Inbuilt DGPS, external GPS

(NMEA 0183 protocol),

wheel encoder

Operating time 5 h
Power supply Interchangeable 12 V

Li-Ion batt, or ext. 12 V DC source

Power consumption 1.3 A

Acq. mode Wheel, time or manual Dimensions 430 x 360 x 180 mm

Weight 5.5 kg

Operating temp. - 20° to + 50° C or 0° to 120° F

Environmental IP 65

MALÂ GX160 HDR

Technology MALA Semi-Real-Time pat pending

Antenna center freq. 160 MHz SNR > 107 dB No. of bits > 17 bit

 Scans/second
 > 880, time window 625 ns

 Survey speed
 320 [km/h] point distance 10 cm

 Bandwidth
 >120 %, fractional, -10 dB

Time window 625 ns

Positioning Inbuilt DGPS, external GPS

(NMEA 0183 protocol),

wheel encoder

Operating time 5 h

Power supply Interchangeable 12 V Li-Ion batt.

or ext. 12 V DC source

Power consumption 1.3 A

Acq. mode Wheel, time or manual 720 x 480 x 190 mm

Weight 10.7 kg

Operating temp. - 20° to + 50° C or 0° to 120° F

Environmental IP 6

MALÂ GX80 HDR

Technology MALÅ Semi-Real-Time pat pending

Antenna center freq. 80 MHz

SNR > 114.4 dB

No. of bits > 19 bit

 Scans/second
 > 1200, time window 812 ns

 Survey speed
 430 [km/h] point distance 10 cm

 Bandwidth
 >120 %, fractional, -10 dB

Time window 812 ns

Positioning Built-in DGPS, external GPS

(NMEA 0183 protocol),

wheel encoder

Operating time 5 h

Power supply Interchangeable 12 V Li-lon batt.

or ext. 12 V DC source

Power consumption 1.3 A

Acq. mode Wheel, time or manual Dimensions 1010 x 780 x 220 mm

Weight 24,6 kg

Operating temp. - 20° to + 50° C or 0° to 120° F

Environmental IP 65

ABEM MALA

Guideline Geo is a world-leader in geophysics and geo-technology offering sensors, software, services and support necessary to map and visualize the subsurface. Guideline Geo operates in four international market areas: Infrastructure – examination at start-up and maintenance of infrastructure, Environment – survey of environmental risks and geological hazards, Water – mapping and survey of water supplies and Minerals – efficient exploration. Our offices and regional partners serve clients in 121 countries. The Guideline Geo AB share (GGEO) is listed on NGM Equity.





Baffinland Iron Mines Corporation - Mary River Expansion Project 2016-2017-2018 Milne Port Geotechnical Investigation Factual Data Report - October 5, 2018

Appendix J CPT Results

PRESENTATION OF SITE INVESTIGATION RESULTS

Milne Port Expansion

Prepared for:

Baffinland Iron Mines Corporation

ConeTec Job No: 17-05010

Project Start Date: 22-Mar-2017 Project End Date: 09-Apr-2017 Report Date: 13-Apr-2017 Revised Date: 21-Apr-2017



Prepared by:

ConeTec Investigations Ltd. 9033 Leslie Street, Unit 15 Richmond Hill, ON L4B 4K3

Tel: (905) 886-2663 Fax: (905) 886-2664 Toll Free: (800) 504-1116

Email: conetecON@conetec.com www.conetec.com www.conetecdataservices.com



Introduction

The enclosed report presents the results of the site investigation program conducted by ConeTec Investigations Ltd. for Baffinland Iron Mines Corporation at Milne Inlet, Baffin Island, Nunavut. The program consisted of six cone penetration tests (CPT) and two seismic cone penetration tests (SCPT) carried out under the direction of Hatch Ltd.

Project Information

Project				
Client	Baffinland Iron Mines Corporation			
Project	Milne Port Expansion			
ConeTec project number	17-05010			

A map from Google earth including the CPT and SCPT test locations is presented below.



Rig Description	Deployment System	Test Type		
Boart LS100	Portable	CPT, SCPT		

Coordinates					
Test Type	Collection Method	EPSG Number			
CPT, SCPT	ConeTec Trimble Survey (RTK)	26917			



Cone Penetration Test (CPT)				
Depth reference	Depths are referenced to the existing mudline at the time of each			
Deptimerence	test.			
Tip and sleeve data offset	0.1 meter			
Tip and sieeve data onset	This has been accounted for in the CPT data files.			
Additional plats	Advanced CPT plots with Ic, Phi, and N1(60) and SCPT plots have			
Additional plots	been included.			

Cone Penetrometers Used for this Project						
Cone Description	Cone Number	Cross Sectional Area (cm²)	Sleeve Area (cm²)	Tip Capacity (bar)	Sleeve Capacity (bar)	Pore Pressure Capacity (psi)
338:T1500F15U500	338	15	225	1500	15	500
374:T1500F15U500	374	15	225	1500	15	500
The CPT summary indicates which cone was used for each sounding.						

Interpretation Tables	
Additional information	The Soil Behaviour Type (SBT) classification chart (Robertson et al., 1986 presented by Lunne, Robertson and Powell, 1997) was used to classify the soil for this project. A detailed set of calculated CPT parameters were generated and are provided in Excel format files in the release folder. The calculated CPT parameters are based on values of corrected tip (q_t) , sleeve friction (f_s) and pore pressure (u_2) .
	Soils were classified as either drained or undrained based on the Soil Behaviour Type (SBT) classification chart (Robertson et al., 1986 presented by Lunne, Robertson and Powell, 1997). Calculations for both drained and undrained parameters were included for materials that classified as silt (zone 6).

Survey	
Tidal Fluctuations	As requested by Hatch Ltd., a survey grid was setup to monitor ice movement due to tidal fluctuation throughout the drill program. The grid was laid out around the proposed drilling area using six survey points in a 200m by 100m grid. ½ inch steel pins was installed at each point by drilling out a section of ice and freezing the rod in place. The pins were surveyed repeatedly throughout a 12-hour period to determine if the ebb and flow of the tide was moving the ice laterally. After installation they were then surveyed every couple of days.
Surveying Methodology	Due to the lack of compatibility with the onsite base station, a second base station broadcasting in the 450MHz band had to be setup to support the drill program surveying. An observed control point was surveyed in by the BIM



	surveyor onsite in datum NAD83 using an ellipsoid model. Our base station was			
	permanently setup over the surveyed point with a vertical offset of 1.32m to the			
	bottom of the R8 base. An existing control point, KM002, was surveyed for quality			
	control. A second control point, PRJCNTRL, was surveyed in to allow for easy			
	quality control when restarting the base station.			
	Significant tidal fluctuations between two and seven feet were observed on the			
	ice throughout the drill program. Constant monitoring of the elevation of the ice			
	was required while conducting the cone penetration tests (CPTs) to ensure the			
	depth was correct throughout the sounding. At the beginning of the CPT, the			
Depth Control	Northing, Easting, and Elevation of the sounding was recorded along with a dip			
	tape measurement to the sea floor. The dip tape measurement was subtracted			
	from the ice elevation to get the sea floor elevation. Throughout the CPT, the			
	elevation of ice was monitored and compared to the initial measurement to get			
	an accurate depth at the end of every meter.			
	There were large cracks in the ice near the drilling pad. They appeared to open			
Ice Cracks and	and close as the tide went up and down. The Northing and Easting coordinates of			
Survey Grid	the grid were surveyed using a continuous topo. The survey grid coordinates are			
	not presented as part of this report.			

Limitations

This report has been prepared for the exclusive use of Baffinland Iron Mines Corporation (Client) and Hatch Ltd. for the project titled "Milne Port Expansion". The report's contents may not be relied upon by any other party without the express written permission of ConeTec Investigations Ltd. (ConeTec). ConeTec has provided site investigation services, prepared the factual data reporting, and provided geotechnical parameter calculations consistent with current best practices. No other warranty, expressed or implied, is made.

The information presented in the report document and the accompanying data set pertain to the specific project, site conditions and objectives described to ConeTec by the Client and Hatch Ltd. In order to properly understand the factual data, assumptions and calculations, reference must be made to the documents provided and their accompanying data sets, in their entirety.



The cone penetration tests (CPTu) are conducted using an integrated electronic piezocone penetrometer and data acquisition system manufactured by Adara Systems Ltd. of Richmond, British Columbia, Canada.

ConeTec's piezocone penetrometers are compression type designs in which the tip and friction sleeve load cells are independent and have separate load capacities. The piezocones use strain gauged load cells for tip and sleeve friction and a strain gauged diaphragm type transducer for recording pore pressure. The piezocones also have a platinum resistive temperature device (RTD) for monitoring the temperature of the sensors, an accelerometer type dual axis inclinometer and a geophone sensor for recording seismic signals. All signals are amplified down hole within the cone body and the analog signals are sent to the surface through a shielded cable.

ConeTec penetrometers are manufactured with various tip, friction and pore pressure capacities in both 10 cm² and 15 cm² tip base area configurations in order to maximize signal resolution for various soil conditions. The specific piezocone used for each test is described in the CPT summary table presented in the first Appendix. The 15 cm² penetrometers do not require friction reducers as they have a diameter larger than the deployment rods. The 10 cm² piezocones use a friction reducer consisting of a rod adapter extension behind the main cone body with an enlarged cross sectional area (typically 44 mm diameter over a length of 32 mm with tapered leading and trailing edges) located at a distance of 585 mm above the cone tip.

The penetrometers are designed with equal end area friction sleeves, a net end area ratio of 0.8 and cone tips with a 60 degree apex angle.

All ConeTec piezocones can record pore pressure at various locations. Unless otherwise noted, the pore pressure filter is located directly behind the cone tip in the " u_2 " position (ASTM Type 2). The filter is 6 mm thick, made of porous plastic (polyethylene) having an average pore size of 125 microns (90-160 microns). The function of the filter is to allow rapid movements of extremely small volumes of water needed to activate the pressure transducer while preventing soil ingress or blockage.

The piezocone penetrometers are manufactured with dimensions, tolerances and sensor characteristics that are in general accordance with the current ASTM D5778 standard. ConeTec's calibration criteria also meets or exceeds those of the current ASTM D5778 standard. An illustration of the piezocone penetrometer is presented in Figure CPTu.



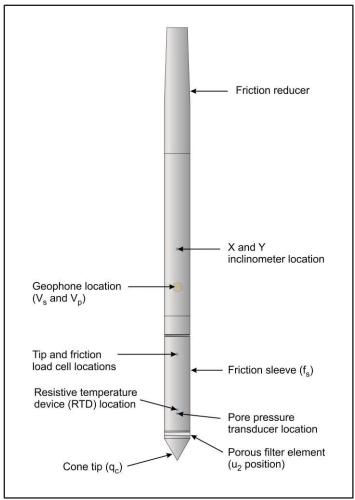


Figure CPTu. Piezocone Penetrometer (15 cm²)

The ConeTec data acquisition systems consist of a Windows based computer and a signal conditioner and power supply interface box with a 16 bit (or greater) analog to digital (A/D) converter. The data is recorded at fixed depth increments using a depth wheel attached to the push cylinders or by using a spring loaded rubber depth wheel that is held against the cone rods. The typical recording intervals are either 2.5 cm or 5.0 cm depending on project requirements; custom recording intervals are possible. The system displays the CPTu data in real time and records the following parameters to a storage media during penetration:

- Depth
- Uncorrected tip resistance (q_c)
- Sleeve friction (f_s)
- Dynamic pore pressure (u)
- Additional sensors such as resistivity, passive gamma, ultra violet induced fluorescence, if applicable

All testing is performed in accordance to ConeTec's CPT operating procedures which are in general accordance with the current ASTM D5778 standard.



Prior to the start of a CPTu sounding a suitable cone is selected, the cone and data acquisition system are powered on, the pore pressure system is saturated with either glycerine or silicone oil and the baseline readings are recorded with the cone hanging freely in a vertical position.

The CPTu is conducted at a steady rate of 2 cm/s, within acceptable tolerances. Typically one meter length rods with an outer diameter of 1.5 inches are added to advance the cone to the sounding termination depth. After cone retraction final baselines are recorded.

Additional information pertaining to ConeTec's cone penetration testing procedures:

- Each filter is saturated in silicone oil or glycerine under vacuum pressure prior to use
- Recorded baselines are checked with an independent multi-meter
- Baseline readings are compared to previous readings
- Soundings are terminated at the client's target depth or at a depth where an obstruction is encountered, excessive rod flex occurs, excessive inclination occurs, equipment damage is likely to take place, or a dangerous working environment arises
- Differences between initial and final baselines are calculated to ensure zero load offsets have not occurred and to ensure compliance with ASTM standards

The interpretation of piezocone data for this report is based on the corrected tip resistance (q_t), sleeve friction (f_s) and pore water pressure (u). The interpretation of soil type is based on the correlations developed by Robertson (1990) and Robertson (2009). It should be noted that it is not always possible to accurately identify a soil type based on these parameters. In these situations, experience, judgment and an assessment of other parameters may be used to infer soil behaviour type.

The recorded tip resistance (q_c) is the total force acting on the piezocone tip divided by its base area. The tip resistance is corrected for pore pressure effects and termed corrected tip resistance (q_t) according to the following expression presented in Robertson et al, 1986:

$$q_t = q_c + (1-a) \cdot u_2$$

where: qt is the corrected tip resistance

q_c is the recorded tip resistance

 u_2 is the recorded dynamic pore pressure behind the tip (u_2 position)

a is the Net Area Ratio for the piezocone (0.8 for ConeTec probes)

The sleeve friction (f_s) is the frictional force on the sleeve divided by its surface area. As all ConeTec piezocones have equal end area friction sleeves, pore pressure corrections to the sleeve data are not required.

The dynamic pore pressure (u) is a measure of the pore pressures generated during cone penetration. To record equilibrium pore pressure, the penetration must be stopped to allow the dynamic pore pressures to stabilize. The rate at which this occurs is predominantly a function of the permeability of the soil and the diameter of the cone.

The friction ratio (Rf) is a calculated parameter. It is defined as the ratio of sleeve friction to the tip resistance expressed as a percentage. Generally, saturated cohesive soils have low tip resistance, high



friction ratios and generate large excess pore water pressures. Cohesionless soils have higher tip resistances, lower friction ratios and do not generate significant excess pore water pressure.

A summary of the CPTu soundings along with test details and individual plots are provided in the appendices. A set of interpretation files were generated for each sounding based on published correlations and are provided in Excel format in the data release folder. Information regarding the interpretation methods used is also included in the data release folder.

For additional information on CPTu interpretations, refer to Robertson et al. (1986), Lunne et al. (1997), Robertson (2009), Mayne (2013, 2014) and Mayne and Peuchen (2012).



Shear wave velocity testing is performed in conjunction with the piezocone penetration test (SCPTu) in order to collect interval velocities. For some projects seismic compression wave (Vp) velocity is also determined.

ConeTec's piezocone penetrometers are manufactured with a horizontally active geophone (28 hertz) that is rigidly mounted in the body of the cone penetrometer, 0.2 meters behind the cone tip.

Shear waves are typically generated by using an impact hammer horizontally striking a beam that is held in place by a normal load. In some instances an auger source or an imbedded impulsive source maybe used for both shear waves and compression waves. The hammer and beam act as a contact trigger that triggers the recording of the seismic wave traces. For impulsive devices an accelerometer trigger may be used. The traces are recorded using an up-hole integrated digital oscilloscope which is part of the SCPTu data acquisition system. An illustration of the shear wave testing configuration is presented in Figure SCPTu-1.

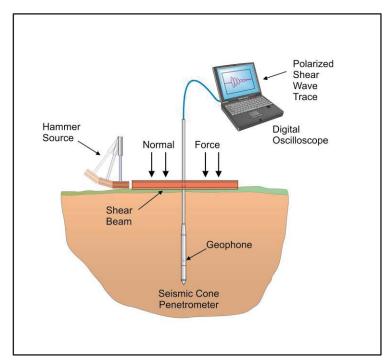


Figure SCPTu-1. Illustration of the SCPTu system

All testing is performed in accordance to ConeTec's SCPTu operating procedures.

Prior to the start of a SCPTu sounding, the procedures described in the Cone Penetration Test section are followed. In addition, the active axis of the geophone is aligned parallel to the beam (or source) and the horizontal offset between the cone and the source is measured and recorded.

Prior to recording seismic waves at each test depth, cone penetration is stopped and the rods are decoupled from the rig to avoid transmission of rig energy down the rods. Multiple wave traces are recorded for quality control purposes. After reviewing wave traces for consistency the cone is pushed to the next test depth (typically one meter intervals or as requested by the client). Figure SCPTu-2 presents an illustration of a SCPTu test.



For additional information on seismic cone penetration testing refer to Robertson et.al. (1986).

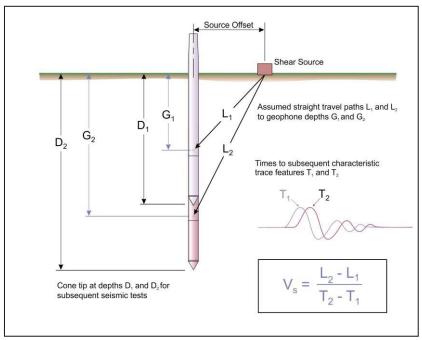


Figure SCPTu-2. Illustration of a seismic cone penetration test

Calculation of the interval velocities are performed by visually picking a common feature (e.g. the first characteristic peak, trough, or crossover) on all of the recorded wave sets and taking the difference in ray path divided by the time difference between subsequent features. Ray path is defined as the straight line distance from the seismic source to the geophone, accounting for beam offset, source depth and geophone offset from the cone tip.

The average shear wave velocity to a depth of 30 meters (V_{s30}) has been calculated and provided for all applicable soundings using an equation presented in Crow et al., 2012.

$$V_{s30} = \frac{total\ thickness\ of\ all\ layers\ (30m)}{\sum (layer\ traveltimes)}$$

The layer travel times refers to the travel times propagating in the vertical direction, not the measured travel times from an offset source.

Tabular results and SCPTu plots are presented in the relevant appendix.



The cone penetration test is halted at specific depths to carry out pore pressure dissipation (PPD) tests, shown in Figure PPD-1. For each dissipation test the cone and rods are decoupled from the rig and the data acquisition system measures and records the variation of the pore pressure (u) with time (t).

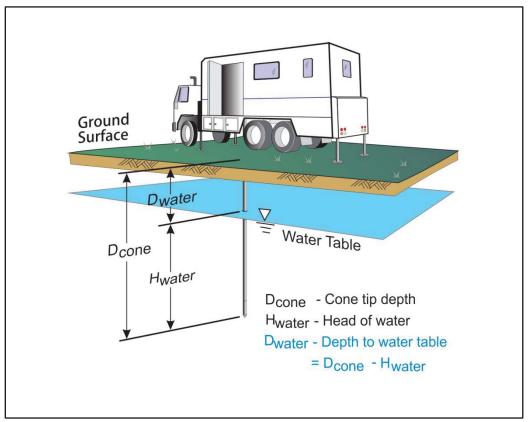


Figure PPD-1. Pore pressure dissipation test setup

Pore pressure dissipation data can be interpreted to provide estimates of ground water conditions, permeability, consolidation characteristics and soil behaviour.

The typical shapes of dissipation curves shown in Figure PPD-2 are very useful in assessing soil type, drainage, in situ pore pressure and soil properties. A flat curve that stabilizes quickly is typical of a freely draining sand. Undrained soils such as clays will typically show positive excess pore pressure and have long dissipation times. Dilative soils will often exhibit dynamic pore pressures below equilibrium that then rise over time. Overconsolidated fine-grained soils will often exhibit an initial dilatory response where there is an initial rise in pore pressure before reaching a peak and dissipating.



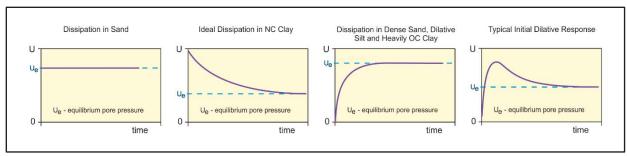


Figure PPD-2. Pore pressure dissipation curve examples

In order to interpret the equilibrium pore pressure (u_{eq}) and the apparent phreatic surface, the pore pressure should be monitored until such time as there is no variation in pore pressure with time as shown for each curve of Figure PPD-2.

In fine grained deposits the point at which 100% of the excess pore pressure has dissipated is known as t_{100} . In some cases this can take an excessive amount of time and it may be impractical to take the dissipation to t_{100} . A theoretical analysis of pore pressure dissipations by Teh and Houlsby (1991) showed that a single curve relating degree of dissipation versus theoretical time factor (T*) may be used to calculate the coefficient of consolidation (c_h) at various degrees of dissipation resulting in the expression for c_h shown below.

$$c_h = \frac{T^* \cdot a^2 \cdot \sqrt{I_r}}{t}$$

Where:

T* is the dimensionless time factor (Table Time Factor)

a is the radius of the cone I_r is the rigidity index

t is the time at the degree of consolidation

Table Time Factor. T* versus degree of dissipation (Teh and Houlsby, 1991)

						10 0110 10 17	,
Degree of Dissipation (%)	20	30	40	50	60	70	80
T* (u ₂)	0.038	0.078	0.142	0.245	0.439	0.804	1.60

The coefficient of consolidation is typically analyzed using the time (t_{50}) corresponding to a degree of dissipation of 50% (u_{50}) . In order to determine t_{50} , dissipation tests must be taken to a pressure less than u_{50} . The u_{50} value is half way between the initial maximum pore pressure and the equilibrium pore pressure value, known as u_{100} . To estimate u_{50} , both the initial maximum pore pressure and u_{100} must be known or estimated. Other degrees of dissipations may be considered, particularly for extremely long dissipations.

At any specific degree of dissipation the equilibrium pore pressure (u at t_{100}) must be estimated at the depth of interest. The equilibrium value may be determined from one or more sources such as measuring the value directly (u_{100}), estimating it from other dissipations in the same profile, estimating the phreatic surface and assuming hydrostatic conditions, from nearby soundings, from client provided information, from site observations and/or past experience, or from other site instrumentation.



For calculations of c_h (Teh and Houlsby, 1991), t_{50} values are estimated from the corresponding pore pressure dissipation curve and a rigidity index (I_r) is assumed. For curves having an initial dilatory response in which an initial rise in pore pressure occurs before reaching a peak, the relative time from the peak value is used in determining t_{50} . In cases where the time to peak is excessive, t_{50} values are not calculated.

Due to possible inherent uncertainties in estimating I_r , the equilibrium pore pressure and the effect of an initial dilatory response on calculating t_{50} , other methods should be applied to confirm the results for c_h .

Additional published methods for estimating the coefficient of consolidation from a piezocone test are described in Burns and Mayne (1998, 2002), Jones and Van Zyl (1981), Robertson et al. (1992) and Sully et al. (1999).

A summary of the pore pressure dissipation tests and dissipation plots are presented in the relevant appendix.



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Robertson, P.K., Sully, J.P., Woeller, D.J., Lunne, T., Powell, J.J.M. and Gillespie, D.G., 1992, "Estimating coefficient of consolidation from piezocone tests", Canadian Geotechnical Journal, 29(4): 551-557.

Sully, J.P., Robertson, P.K., Campanella, R.G. and Woeller, D.J., 1999, "An approach to evaluation of field CPTU dissipation data in overconsolidated fine-grained soils", Canadian Geotechnical Journal, 36(2): 369-381.



Teh, C.I., and Houlsby, G.T., 1991, "An analytical study of the cone penetration test in clay", Geotechnique, 41(1): 17-34.



The following appendices listed below are included in the report:

- Cone Penetration Test Summary and Standard Cone Penetration Test Plots
- Advanced Cone Penetration Test Plots with Ic, Phi, and N1(60)
- Seismic Cone Penetration Test Tabular Results
- Seismic Cone Penetration Test Plots
- Pore Pressure Dissipation Summary and Pore Pressure Dissipation Plots



Cone Penetration Test Summary and Standard Cone Penetration Test Plots





Client: Baffinland Iron Mines Corporation

Project: Milne Port Expansion
Start Date: 03-Apr-2017
End Date: 07-Apr-2017

CONE PENETRATION TEST SUMMARY									
Sounding ID	File Name	Date	Cone	Assumed Phreatic Surface ¹ (m)	Final Depth ² (m)	Northing ³ (m)	Easting (m)	Elevation (m)	Refer to Notation Number
CPT17-D001	17-05010_CPD001	05-Apr-2017	338:T1500F15U500	-17.6	32.750	7976717.62	503607.38	-16.97	
SCPT17-D002	17-05010_SPD002	05-Apr-2017	338:T1500F15U500	-16.9	39.475	7976728.05	503705.30	-16.12	
CPT17-D003	17-05010_CPD003	06-Apr-2017	338:T1500F15U500	-23.2	30.425	7976757.71	503785.39	-22.68	
SCPT17-D004	17-05010_SPD004	04-Apr-2017	338:T1500F15U500	-27.3	32.050	7976768.10	503646.44	-26.59	
CPT17-D005	17-05010_CPD005	03-Apr-2017	338:T1500F15U500	-26.0	25.125	7976780.84	503736.09	-24.98	
CPT17-D006	17-05010_CPD006	06-Apr-2017	374:T1500F15U500	-32.0	20.575	7976808.43	503807.55	-31.32	
CPT17-D007	17-05010_CPD007	07-Apr-2017	374:T1500F15U501	-4.7	30.200	7976683.63	503767.46	-4.23	
CPT17-D008	17-05010_CPD008	07-Apr-2017	374:T1500F15U502	-1.4	30.000	7976650.76	503635.99	-1.80	

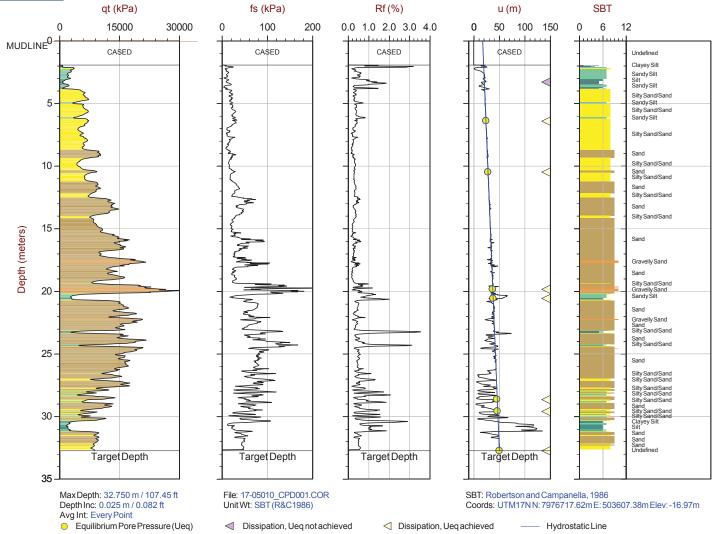
^{1.} The assumed phreatic surface was based on pore pressure dissipation tests. Hydrostatic conditions were assumed for the interpretation tables.

^{2.} Depth is referenced from the mudline at the time of testing.

^{3.} Coordinates and elevations were acquired using ConeTec Trimble Survey in datum NAD 83 / UTM Zone 17 North. Elevation is of the mudline at the time of testing.



Job No: 17-05010 Date: 2017-04-05 09:17 Site: Milne Port Expansion Sounding: CPT17-D001 Cone: 338:T1500F15U500

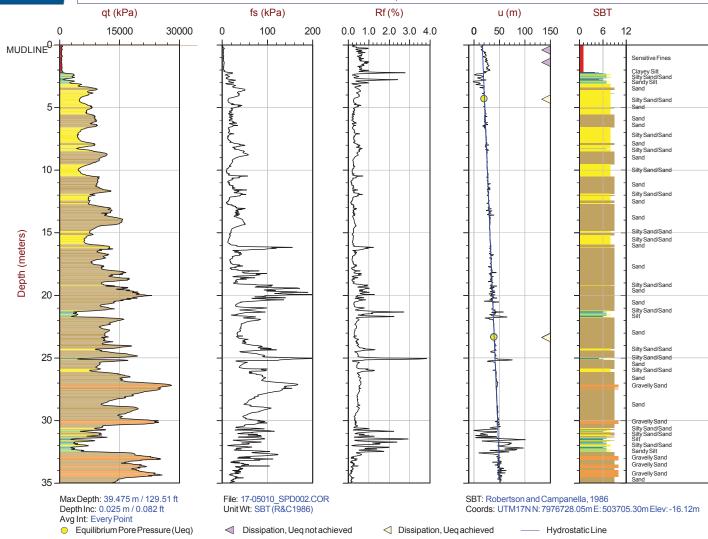




Job No: 17-05010 Date: 2017-04-05 20:44 Site: Milne Port Expansion Sounding: SCPT17-D002 Cone: 338:T1500F15U500

--- Hydrostatic Line

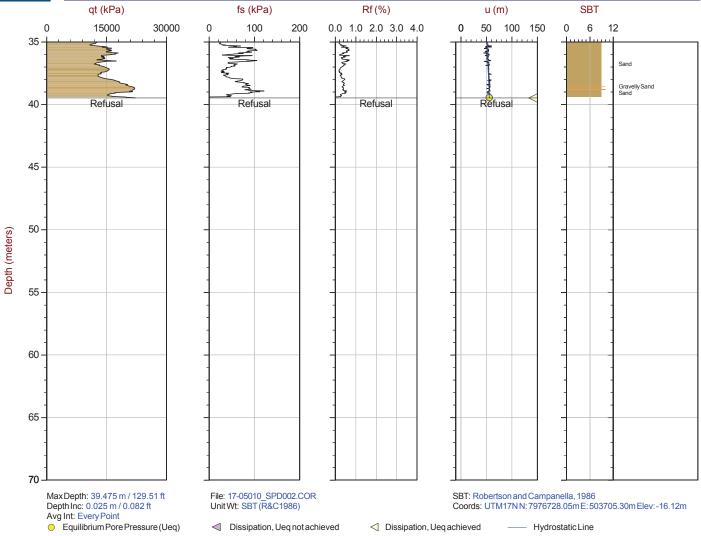
Dissipation, Ueq achieved



Dissipation, Ueq not achieved

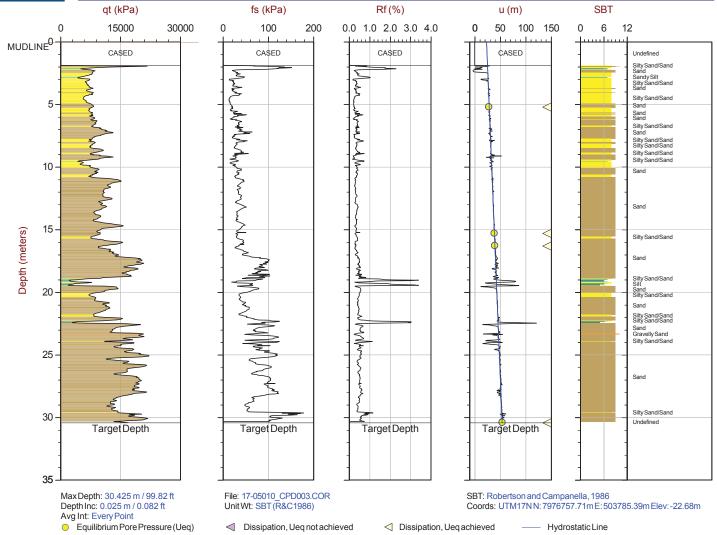


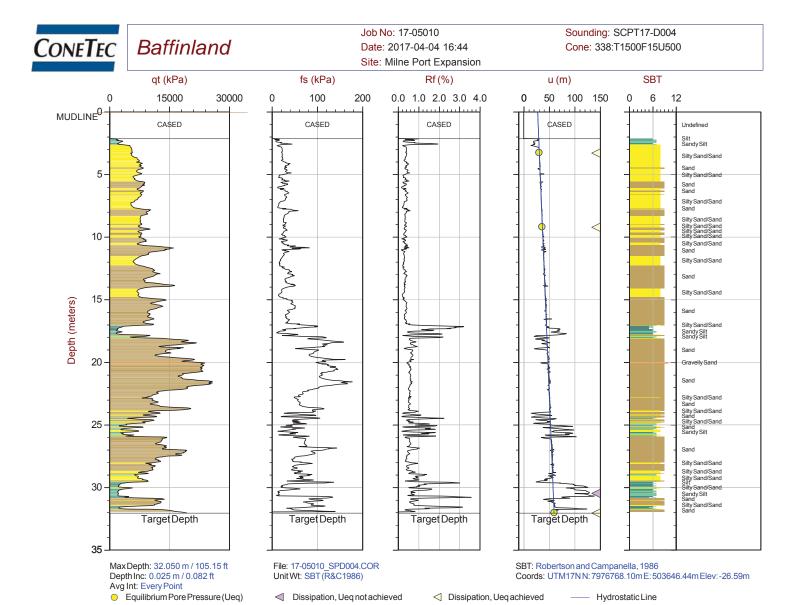
Job No: 17-05010 Date: 2017-04-05 20:44 Site: Milne Port Expansion Sounding: SCPT17-D002 Cone: 338:T1500F15U500





Job No: 17-05010 Date: 2017-04-06 13:34 Site: Milne Port Expansion Sounding: CPT17-D003 Cone: 338:T1500F15U500

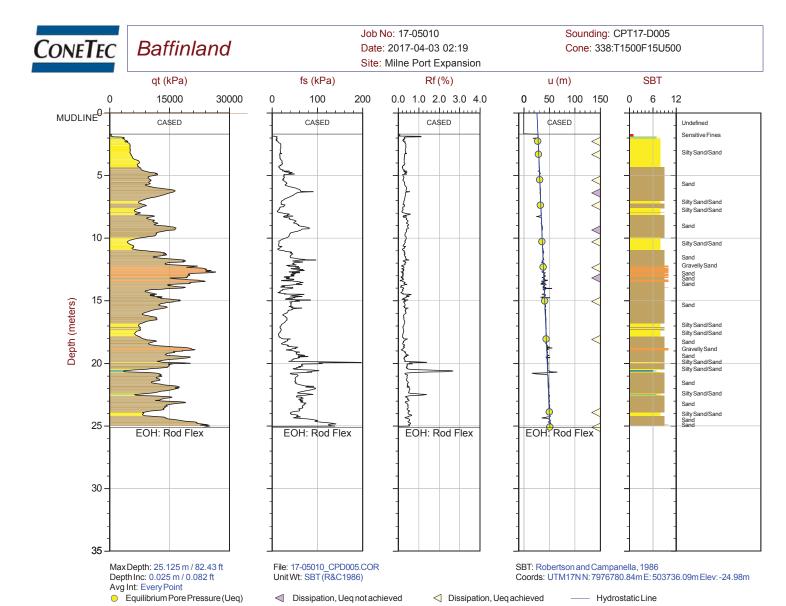




Dissipation, Ueq not achieved

Dissipation, Ueq achieved

--- Hydrostatic Line



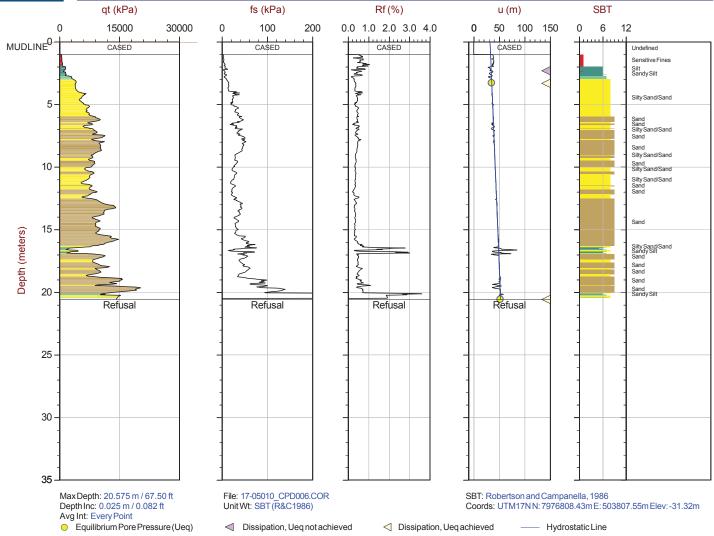
Dissipation, Ueq not achieved

--- Hydrostatic Line

Dissipation, Ueq achieved

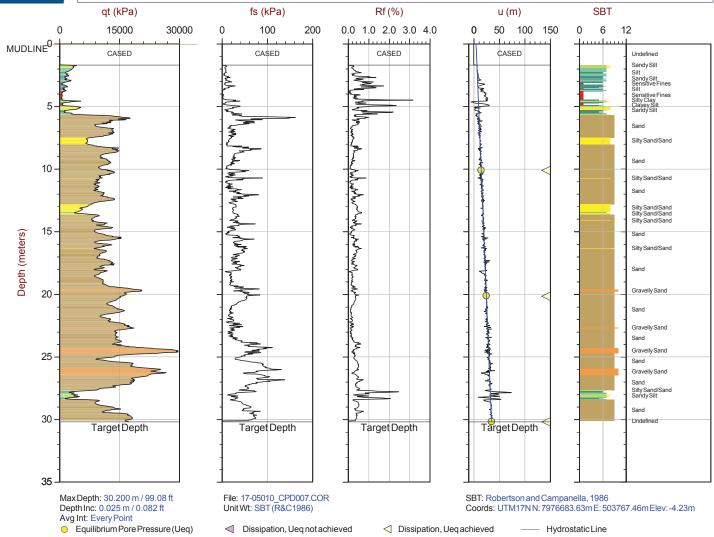


Job No: 17-05010 Date: 2017-04-06 23:59 Site: Milne Port Expansion Sounding: CPT17-D006 Cone: 374:T1500F15U500



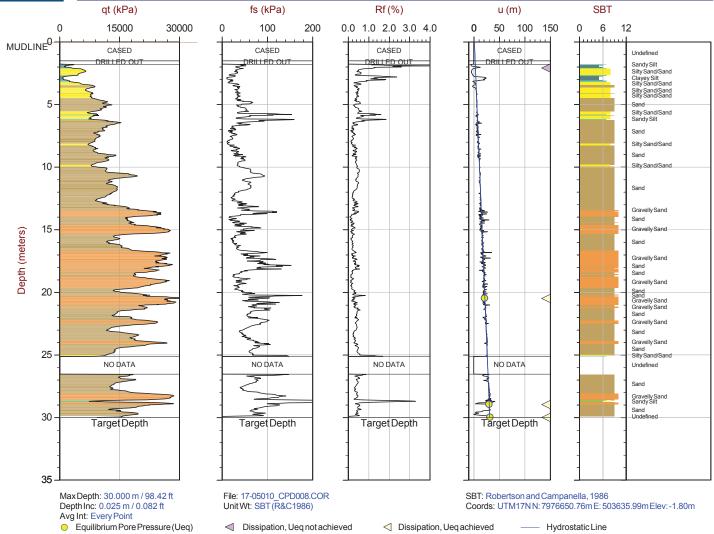


Job No: 17-05010 Date: 2017-04-07 11:27 Site: Milne Port Expansion Sounding: CPT17-D007 Cone: 374:T1500F15U500



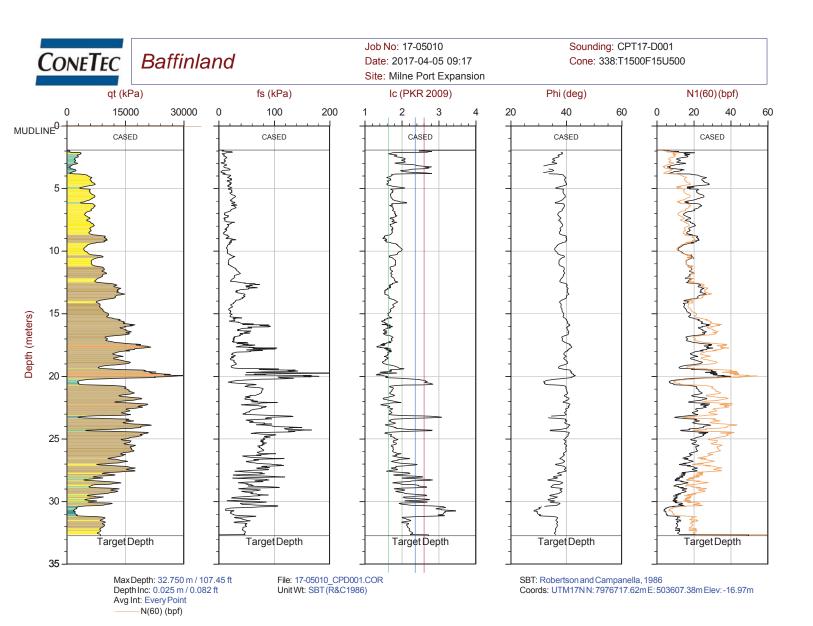


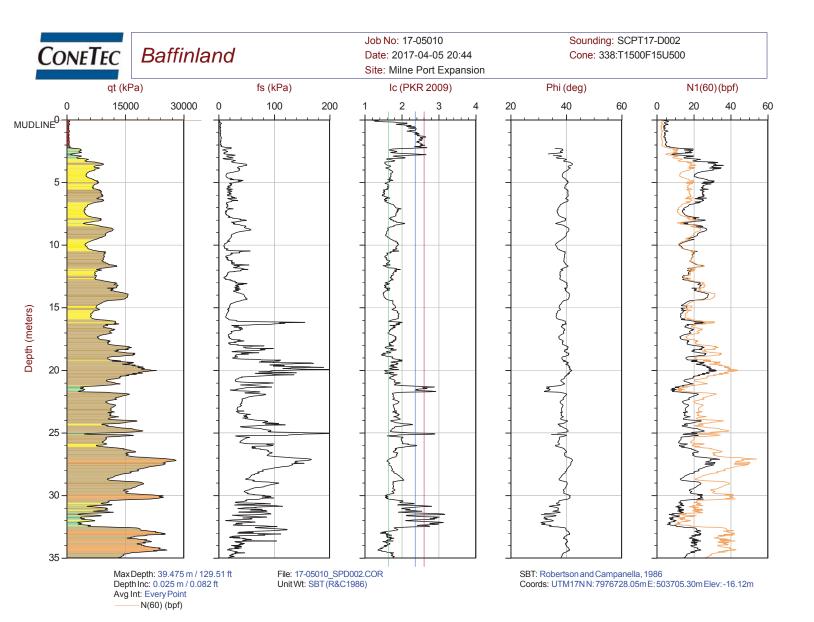
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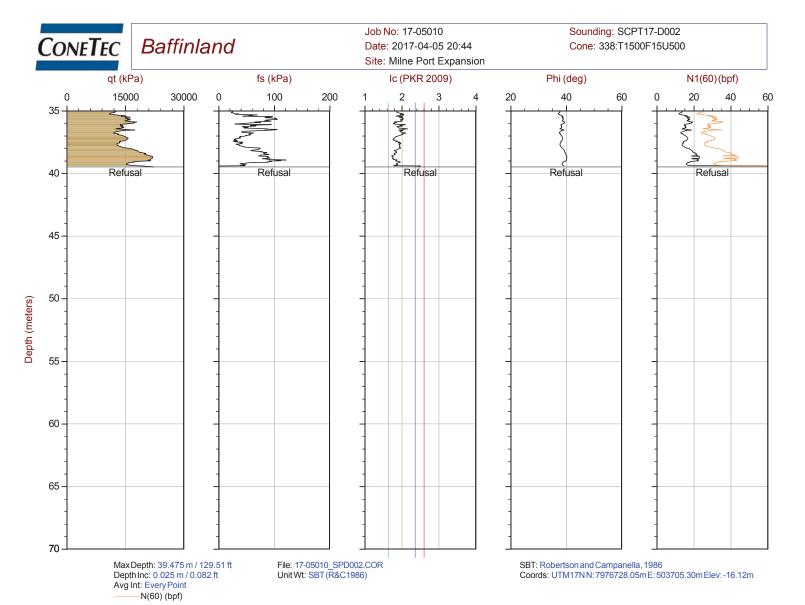


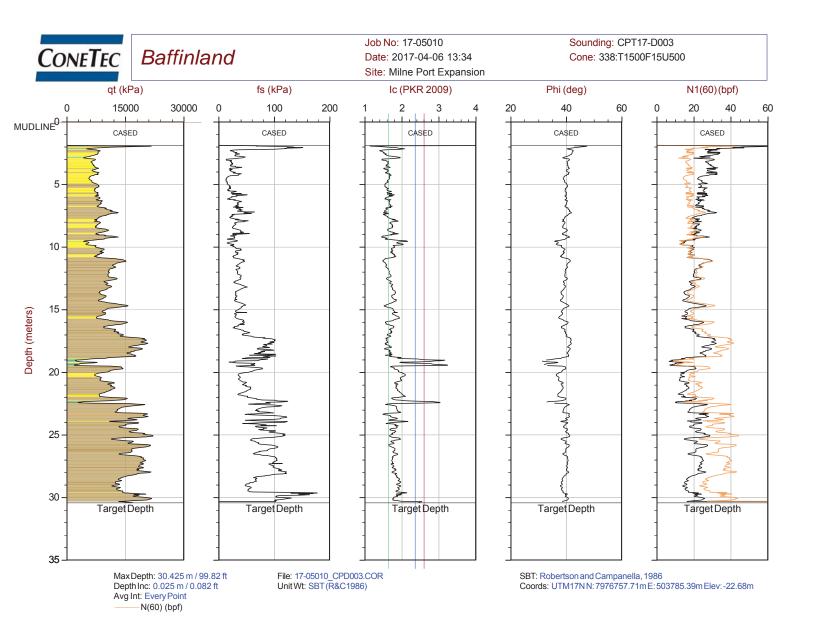
Advanced Cone Penetration Test Plots with Ic, Phi, and N1(60)

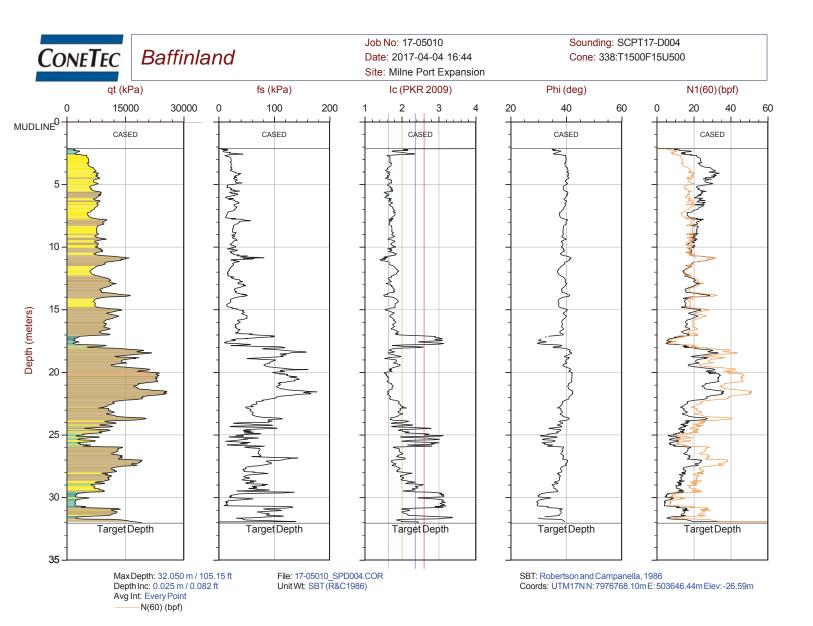


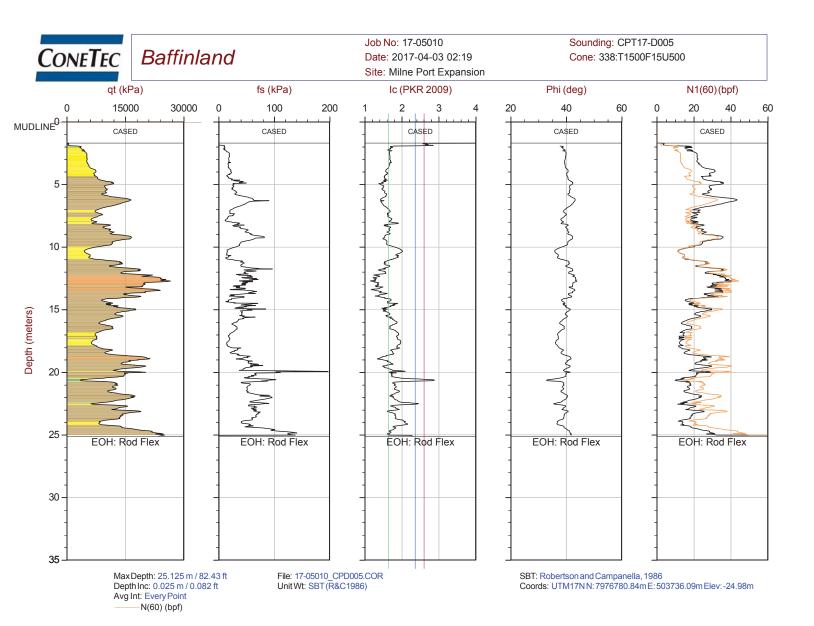


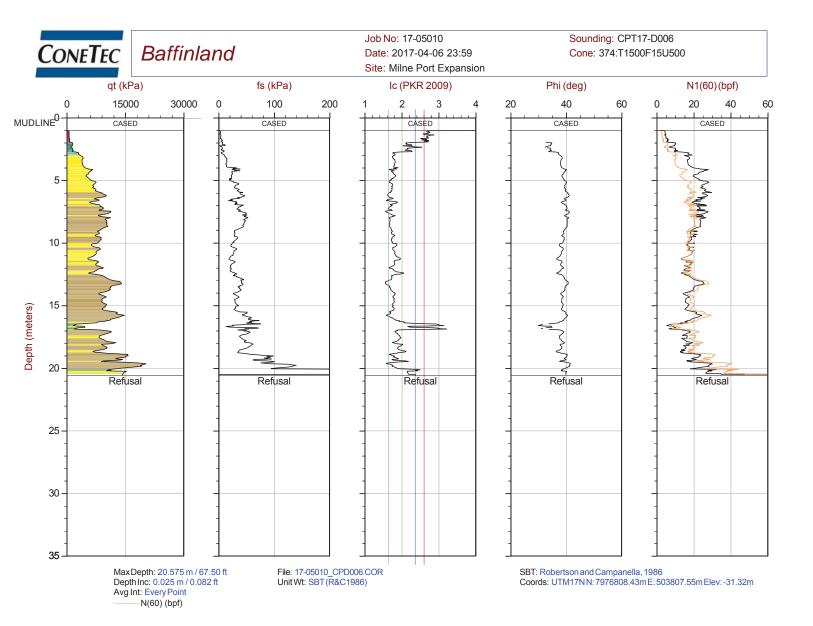


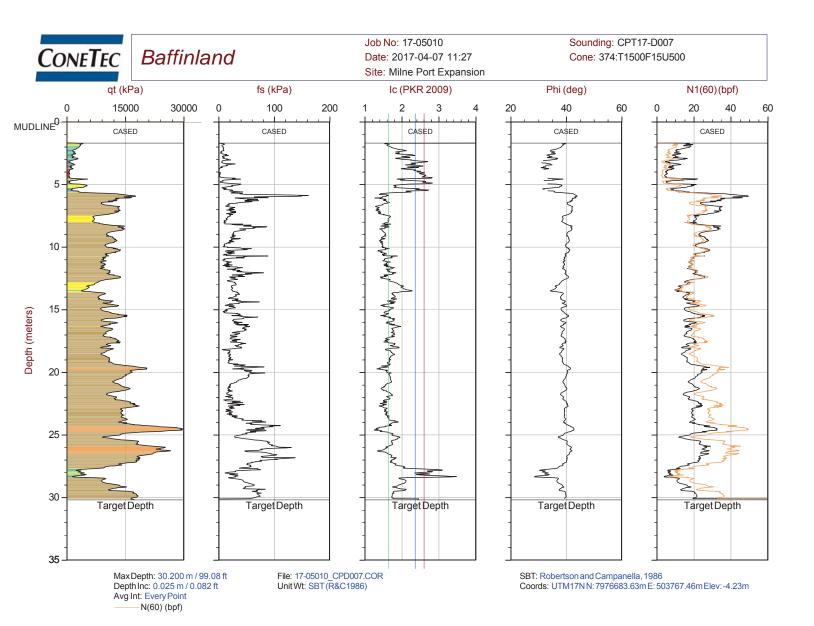


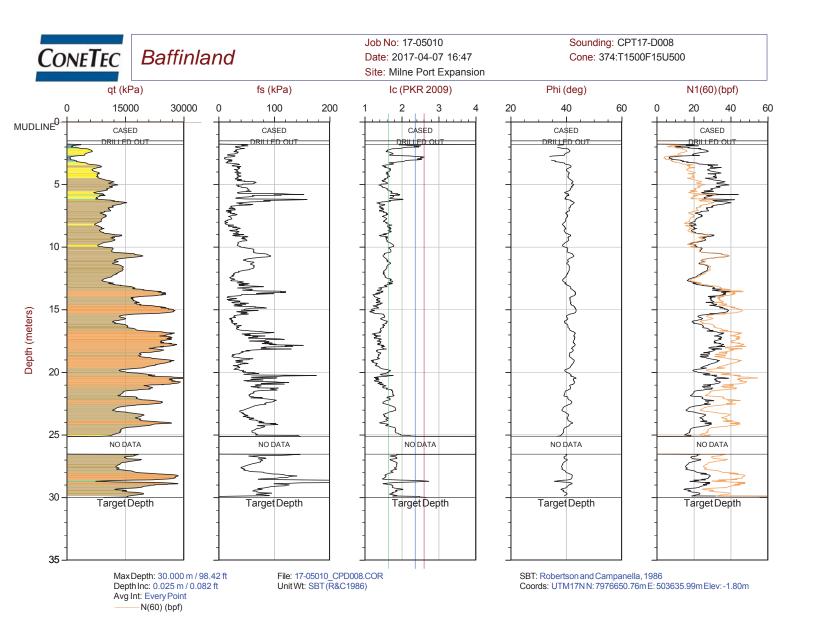












Seismic Cone Penetration Test Tabular Results





Client: Baffinland Iron Mines Corporation

Project: Milne Port Expansion

Sounding ID: SCPT17-D002 Date: 05-Apr-2017

Seismic Source: Auto-seismic

Source Offset (m): 4.30
Source Depth (m): 0.00
Geophone Offset (m): 0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs							
Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)		
3.38	3.18	5.35					
5.38	5.18	6.73	1.38	8.94	155		
6.35	6.15	7.50	0.77	4.62	167		
7.40	7.20	8.39	0.88	5.00	177		
8.38	8.18	9.24	0.86	4.38	195		
9.40	9.20	10.16	0.91	5.21	175		
10.38	10.18	11.05	0.90	4.78	187		
11.38	11.18	11.98	0.93	5.35	173		
12.40	12.20	12.94	0.96	4.82	198		
13.43	13.23	13.91	0.98	4.81	203		
14.43	14.23	14.87	0.95	4.70	203		
15.43	15.23	15.83	0.96	4.39	219		
16.43	16.23	16.79	0.96	4.40	219		
17.40	17.20	17.73	0.94	4.13	228		
18.45	18.25	18.75	1.02	4.54	225		
19.40	19.20	19.68	0.93	3.87	239		
20.35	20.15	20.60	0.93	3.91	238		
21.35	21.15	21.58	0.98	4.50	217		
22.35	22.15	22.56	0.98	4.44	221		
23.35	23.15	23.55	0.98	4.67	210		
24.27	24.07	24.45	0.91	4.13	219		
25.30	25.10	25.47	1.01	4.00	254		
26.27	26.07	26.42	0.96	3.80	252		



Client: Baffinland Iron Mines Corporation

Project: Milne Port Expansion

Sounding ID: SCPT17-D002 Date: 05-Apr-2017

Seismic Source: Auto-seismic

Source Offset (m): 4.30 Source Depth (m): 0.00 Geophone Offset (m): 0.20

5	SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs								
Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)				
27.32	27.12	27.46	1.04	4.08	254				
28.38	28.18	28.51	1.05	3.93	267				
29.43	29.23	29.54	1.04	4.08	254				
30.40	30.20	30.50	0.96	3.54	271				
31.40	31.20	31.49	0.99	3.55	279				
32.38	32.18	32.47	0.97	3.59	270				
33.38	33.18	33.46	0.99	3.56	279				
34.40	34.20	34.47	1.01	3.63	279				
35.40	35.20	35.46	0.99	3.60	276				
36.40	36.20	36.45	0.99	3.75	265				
37.40	37.20	37.45	0.99	3.87	257				
38.40	38.20	38.44	0.99	3.81	261				
39.40	39.20	39.44	0.99	3.81	261				



Client: Baffinland Iron Mines Corporation

Project: Milne Port Expansion

Sounding ID: SCPT17-D004 Date: 04-Apr-2017

Seismic Source: Auto-seismic

Source Offset (m): 3.40
Source Depth (m): 0.00
Geophone Offset (m): 0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs							
Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)		
4.30	4.10	5.33					
5.30	5.10	6.13	0.80	4.48	179		
6.20	6.00	6.90	0.77	3.86	198		
7.20	7.00	7.78	0.89	3.86	229		
8.20	8.00	8.69	0.91	4.17	218		
9.20	9.00	9.62	0.93	4.33	214		
10.95	10.75	11.27	1.65	7.11	233		
11.93	11.73	12.21	0.94	3.87	243		
12.93	12.73	13.18	0.96	4.33	223		
13.95	13.75	14.16	0.99	4.10	241		
14.88	14.68	15.07	0.90	3.75	241		
15.88	15.68	16.04	0.98	4.50	217		
16.88	16.68	17.02	0.98	4.05	242		
17.85	17.65	17.97	0.95	4.80	198		
18.85	18.65	18.96	0.98	3.75	262		
19.88	19.68	19.97	1.01	4.21	241		
20.90	20.70	20.98	1.01	3.94	255		
21.82	21.62	21.89	0.91	3.18	286		
22.82	22.62	22.87	0.99	3.63	272		
23.85	23.65	23.89	1.02	4.39	232		
24.80	24.60	24.83	0.94	3.63	259		
25.80	25.60	25.82	0.99	4.09	242		
26.80	26.60	26.82	0.99	3.63	273		



Client: Baffinland Iron Mines Corporation

Project: Milne Port Expansion

Sounding ID: SCPT17-D004 Date: 04-Apr-2017

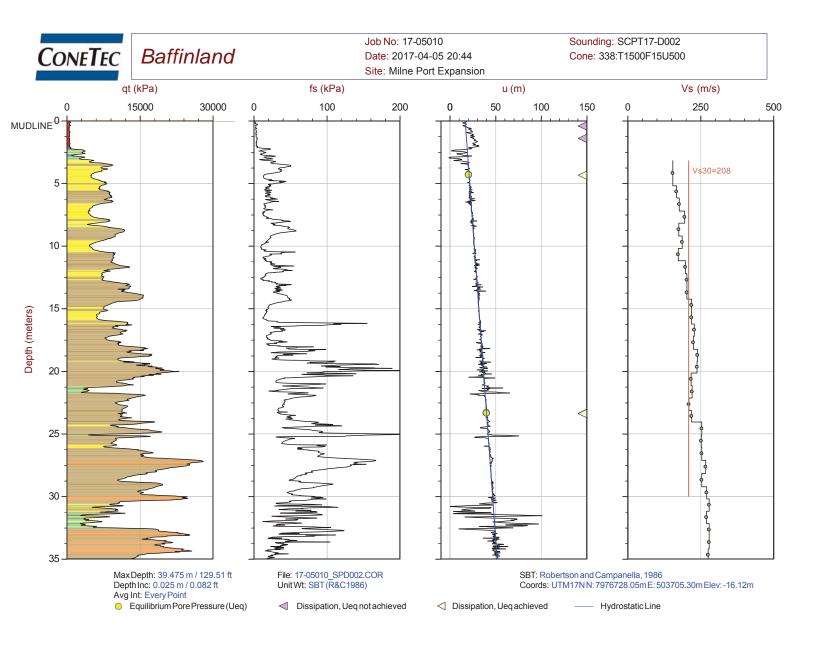
Seismic Source: Auto-seismic

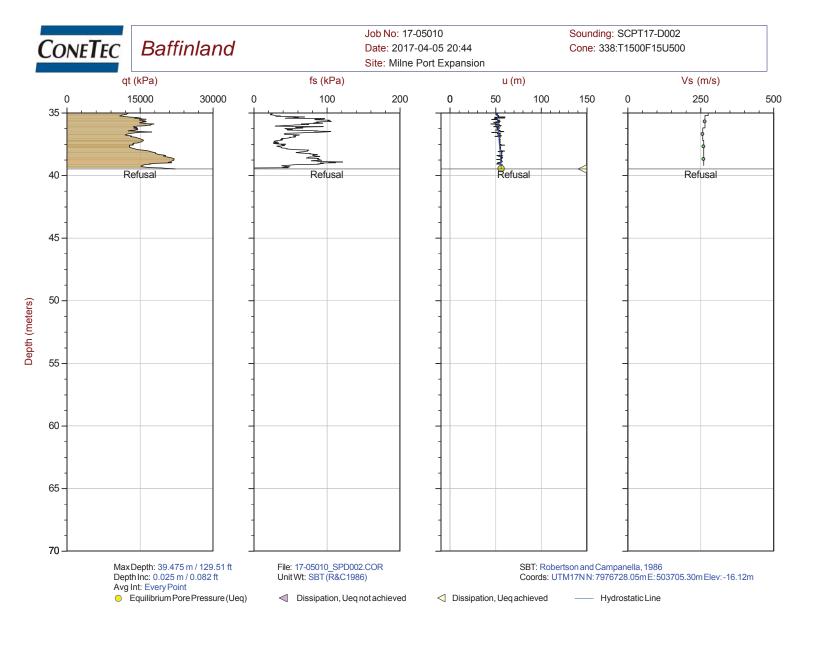
Source Offset (m):3.40Source Depth (m):0.00Geophone Offset (m):0.20

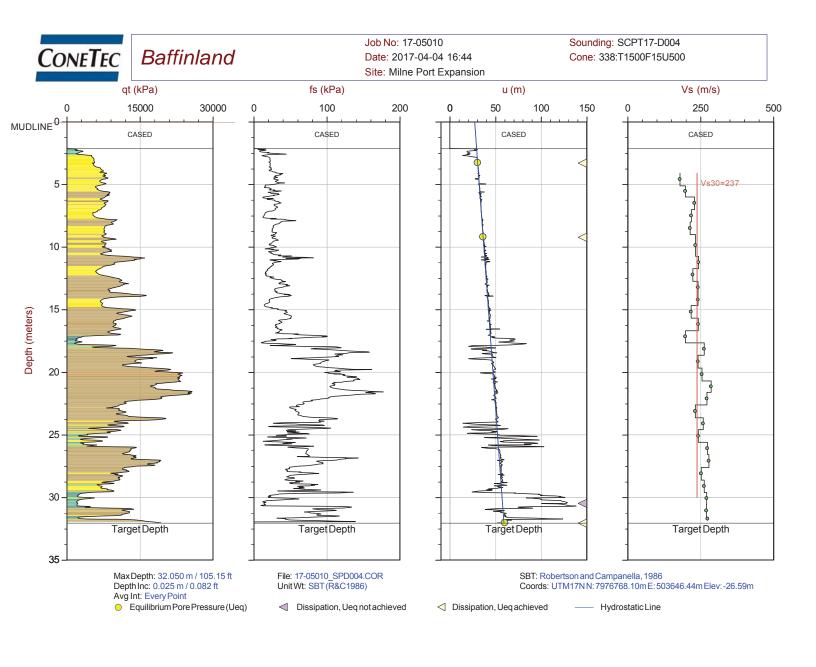
SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs							
Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)		
27.82	27.62	27.83	1.01	3.63	278		
28.82	28.62	28.82	0.99	3.94	252		
29.82	29.62	29.81	0.99	3.79	262		
30.77	30.57	30.76	0.94	3.48	271		
31.80	31.60	31.78	1.02	3.79	270		
32.05	31.85	32.03	0.25	0.91	274		

Seismic Cone Penetration Test Plots









Pore Pressure Dissipation Summary and Pore Pressure Dissipation Plots





Client: Baffinland Iron Mines Corporation

Project: Milne Port Expansion

Start Date: 03-Apr-2017 End Date: 07-Apr-2017

CPTU PORE PRESSURE DISSIPATION SUMMARY

		NESSONE DIS				
Sounding ID	File Name	Cone Area (cm²)	Duration (s)	Test Depth (m)	Estimated Equilibrium Pore Pressure U _{eq} (m)	Calculated Phreatic Surface (m)
CPT17-D001	17-05010_CPD001	15	260	3.275	Not Achieved	
CPT17-D001	17-05010_CPD001	15	95	6.400	24.0	-17.6
CPT17-D001	17-05010_CPD001	15	300	10.475	28.1	-17.6
CPT17-D001	17-05010_CPD001	15	100	19.850	37.5	-17.6
CPT17-D001	17-05010_CPD001	15	400	20.575	38.5	-17.9
CPT17-D001	17-05010_CPD001	15	95	28.650	45.6	-16.9
CPT17-D001	17-05010_CPD001	15	150	29.600	46.7	-17.1
CPT17-D001	17-05010_CPD001	15	400	32.750	50.4	-17.7
SCPT17-D002	17-05010_SPD002	15	105	0.400	Not Achieved	
SCPT17-D002	17-05010_SPD002	15	110	1.375	Not Achieved	
SCPT17-D002	17-05010_SPD002	15	150	4.325	20.7	-16.4
SCPT17-D002	17-05010_SPD002	15	600	23.350	40.2	-16.9
SCPT17-D002	17-05010_SPD002	15	275	23.375	40.4	-17.0
SCPT17-D002	17-05010_SPD002	15	200	39.475	56.6	-17.1
CPT17-D003	17-05010_CPD003	15	110	5.200	28.2	-23.0
CPT17-D003	17-05010_CPD003	15	400	15.300	38.5	-23.2
CPT17-D003	17-05010_CPD003	15	105	16.300	39.6	-23.3
CPT17-D003	17-05010_CPD003	15	1200	30.425	54.1	-23.7
SCPT17-D004	17-05010_SPD004	15	95	3.275	30.4	-27.1
SCPT17-D004	17-05010_SPD004	15	300	9.200	36.5	-27.3
SCPT17-D004	17-05010_SPD004	15	600	30.475	Not Achieved	
SCPT17-D004	17-05010_SPD004	15	300	32.050	60.3	-28.2
CPT17-D005	17-05010_CPD005	15	1340	2.275	28.3	-26.0
CPT17-D005	17-05010_CPD005	15	110	3.325	29.5	-26.2
CPT17-D005	17-05010_CPD005	15	95	5.375	31.8	-26.4
CPT17-D005	17-05010_CPD005	15	145	6.375	Not Achieved	
CPT17-D005	17-05010_CPD005	15	110	7.400	33.5	-26.1
CPT17-D005	17-05010_CPD005	15	125	9.350	Not Achieved	
CPT17-D005	17-05010_CPD005	15	300	10.300	36.5	-26.2



CPT17-D008

CPT17-D008

17-05010 CPD008

17-05010_CPD008

Job No: 17-05010

Client: Baffinland Iron Mines Corporation

Project: Milne Port Expansion

Start Date: 03-Apr-2017 End Date: 07-Apr-2017

CPTU PORE PRESSURE DISSIPATION SUMMARY Estimated Test Calculated Duration **Equilibrium Pore** Sounding ID File Name Cone Area (cm²) Depth Phreatic Surface (s) Pressure U_{eq} (m) (m) (m) CPT17-D005 17-05010_CPD005 15 1460 12.350 38.8 -26.4 CPT17-D005 17-05010_CPD005 15 275 13.175 Not Achieved CPT17-D005 17-05010_CPD005 15 305 15.050 41.7 -26.6 -26.6 CPT17-D005 17-05010_CPD005 15 165 18.100 44.7 CPT17-D005 17-05010_CPD005 15 130 23.925 50.7 -26.8 CPT17-D005 17-05010 CPD005 15 300 25.125 51.9 -26.8 CPT17-D006 17-05010 CPD006 105 2.300 Not Achieved 15 CPT17-D006 17-05010 CPD006 15 2100 3.300 35.3 -32.0 CPT17-D006 17-05010_CPD006 15 300 20.575 52.4 -31.8 CPT17-D007 17-05010 CPD007 15 200 10.100 14.8 -4.7 CPT17-D007 17-05010 CPD007 15 200 20.150 25.1 -5.0 CPT17-D007 17-05010 CPD007 15 200 30.200 35.5 -5.3 Not Achieved CPT17-D008 17-05010 CPD008 15 180 2.075 CPT17-D008 15 200 20.500 21.9 17-05010 CPD008 -1.4

15

15

120

405

28.975

30.000

30.4

32.2

-1.4

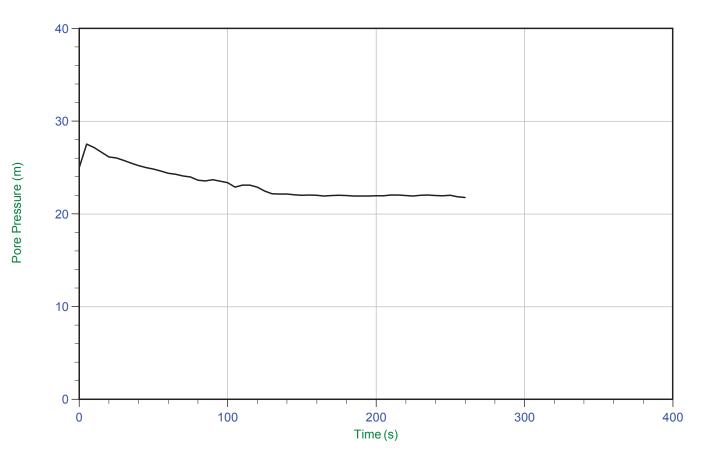
-2.2



Job No: 17-05010 Sounding: CPT17-D001

 Date:
 04/05/2017 09:17
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



 $\begin{tabular}{lll} Filename: 17-05010_CPD001.PPF & U Min: 21.8 m \\ Trace Summary: & Depth: 3.275 m / 10.745 ft & U Max: 27.5 m \\ \end{tabular}$

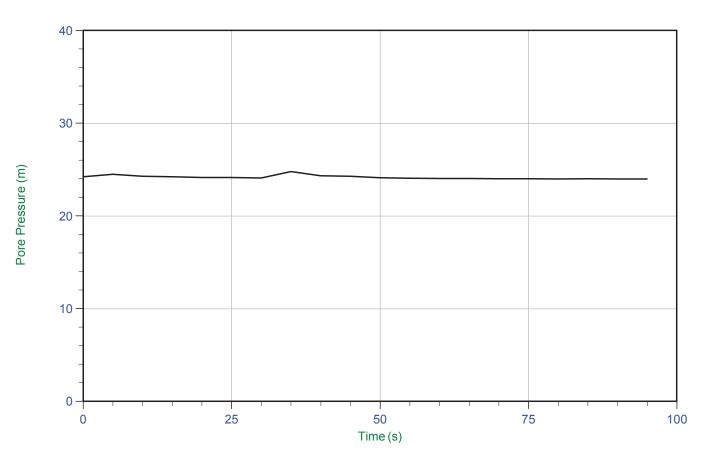
Duration: 260.0 s



Job No: 17-05010 Sounding: CPT17-D001

 Date:
 04/05/2017 09:17
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Trace Summary: Depth: 6.400 m / 20.997 ft U Max: 24.8 m Ueq: 24.0 m

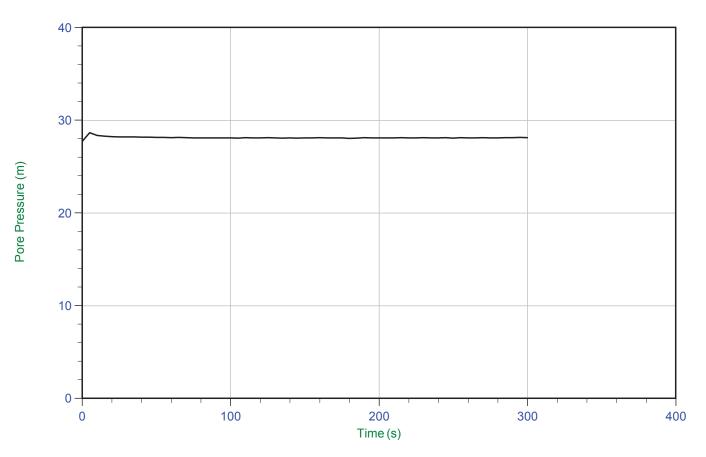
Duration: 95.0 s



Job No: 17-05010 Sounding: CPT17-D001

 Date:
 04/05/2017 09:17
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



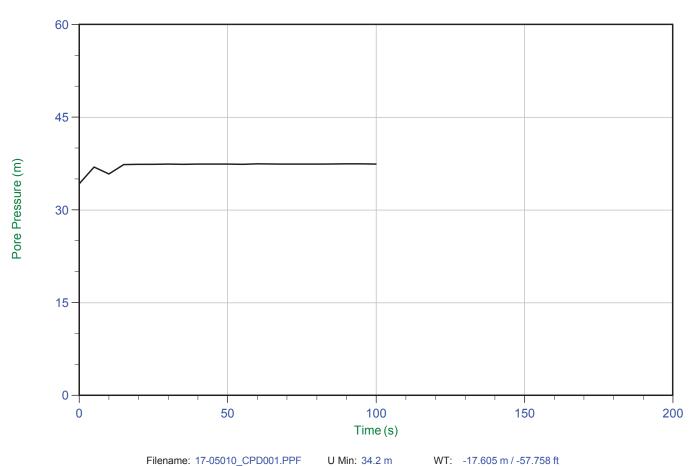
Trace Summary: Depth: 10.475 m / 34.366 ft U Max: 28.6 m Ueq: 28.1 m

Duration: 300.0 s



Sounding: CPT17-D001 Job No: 17-05010

Date: 04/05/2017 09:17 Cone: 338:T1500F15U500 Area=15 cm² Site: Milne Port Expansion



Filename: 17-05010_CPD001.PPF U Min: 34.2 m

Trace Summary: Depth: 19.850 m / 65.124 ft U Max: 37.5 m Ueq: 37.5 m

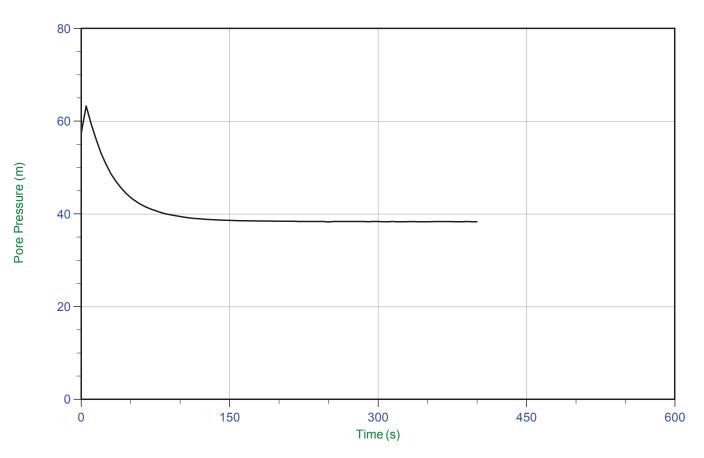
Duration: 100.0 s



Job No: 17-05010 Sounding: CPT17-D001

 Date:
 04/05/2017 09:17
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



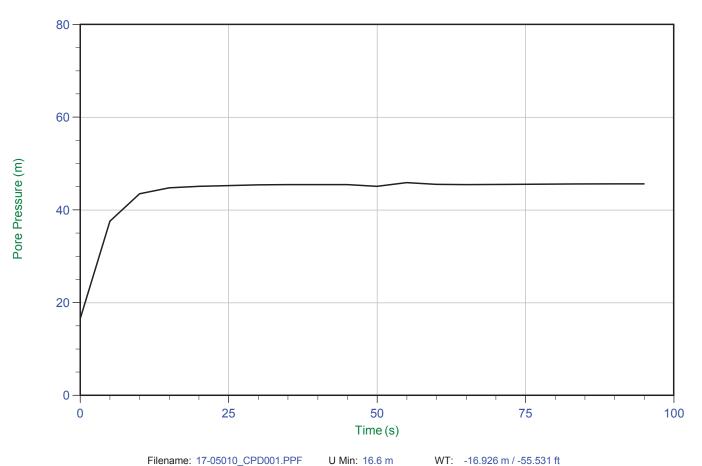
Trace Summary: Depth: 20.575 m / 67.502 ft U Max: 63.3 m Ueq: 38.5 m

Duration: 400.0 s



Sounding: CPT17-D001 Job No: 17-05010

Date: 04/05/2017 09:17 Cone: 338:T1500F15U500 Area=15 cm² Site: Milne Port Expansion



Filename: 17-05010_CPD001.PPF U Min: 16.6 m

Trace Summary: Depth: 28.650 m / 93.995 ft U Max: 45.9 m Ueq: 45.6 m

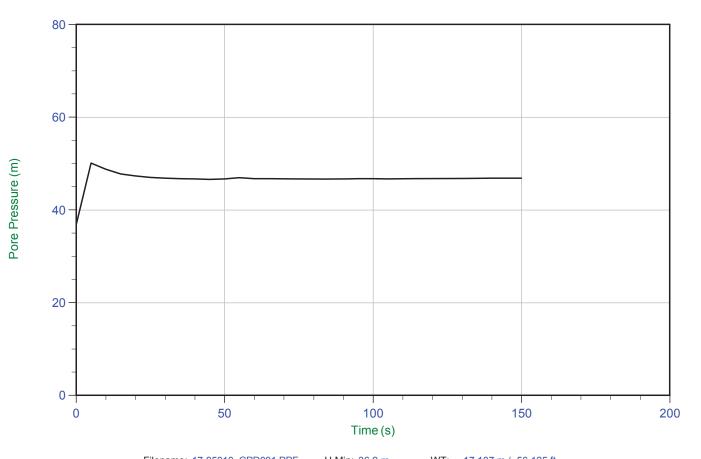
Duration: 95.0 s



Job No: 17-05010 Sounding: CPT17-D001

 Date:
 04/05/2017 09:17
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



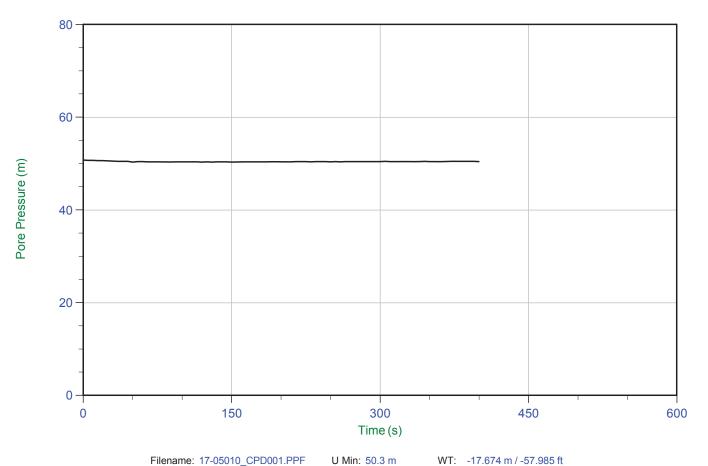
Trace Summary: Depth: 29.600 m / 97.112 ft U Max: 50.1 m Ueq: 46.7 m

Duration: 150.0 s



Sounding: CPT17-D001 Job No: 17-05010

Date: 04/05/2017 09:17 Cone: 338:T1500F15U500 Area=15 cm² Site: Milne Port Expansion



Filename: 17-05010_CPD001.PPF U Min: 50.3 m

Trace Summary: Depth: 32.750 m / 107.446 ft U Max: 50.7 m Ueq: 50.4 m

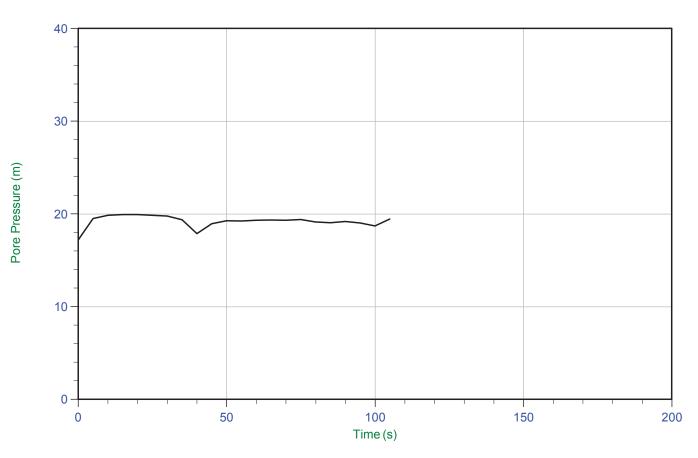
Duration: 400.0 s



Job No: 17-05010 Sounding: SCPT17-D002

 Date:
 04/05/2017 20:44
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



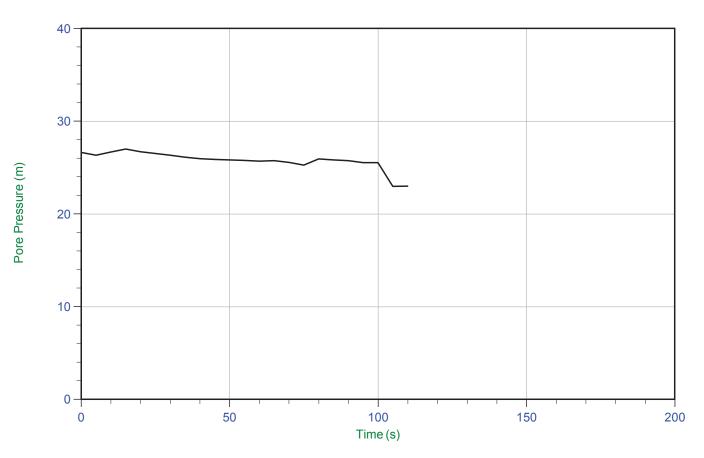
Duration: 105.0 s



Job No: 17-05010 Sounding: SCPT17-D002

 Date:
 04/05/2017 20:44
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



 $\begin{tabular}{lll} Filename: 17-05010_SPD002.PPF & U Min: 23.0 m \\ Trace Summary: & Depth: 1.375 m / 4.511 ft & U Max: 27.0 m \\ \end{tabular}$

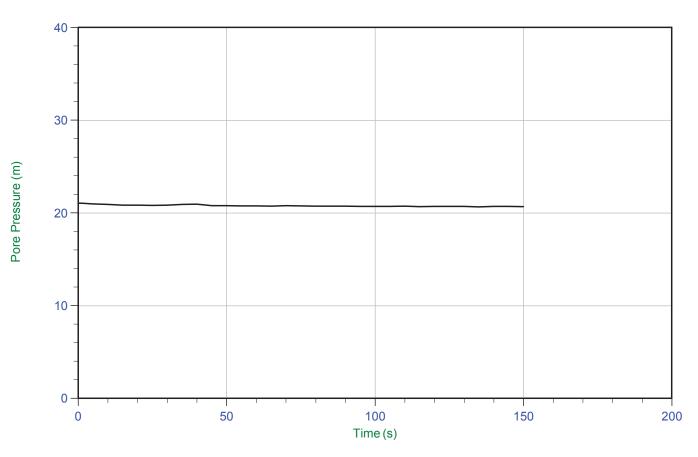
Duration: 110.0 s



Job No: 17-05010 Sounding: SCPT17-D002

 Date:
 04/05/2017 20:44
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Trace Summary: Depth: 4.325 m / 14.189 ft U Max: 21.1 m Ueq: 20.7 m

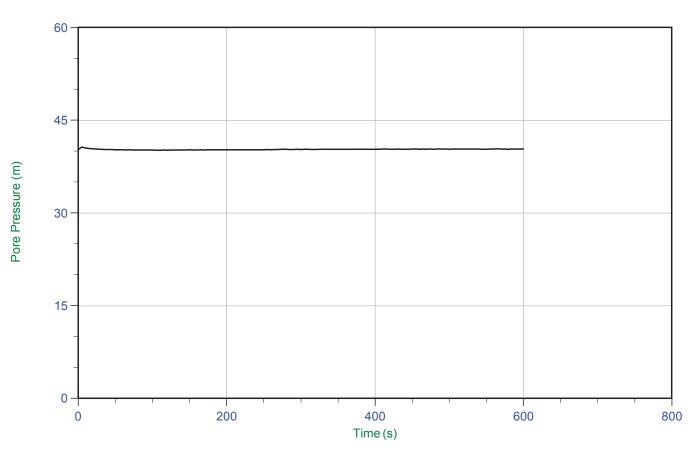
Duration: 150.0 s



 Job No: 17-05010
 Sounding: SCPT17-D002

 Date:
 04/05/2017 20:44
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



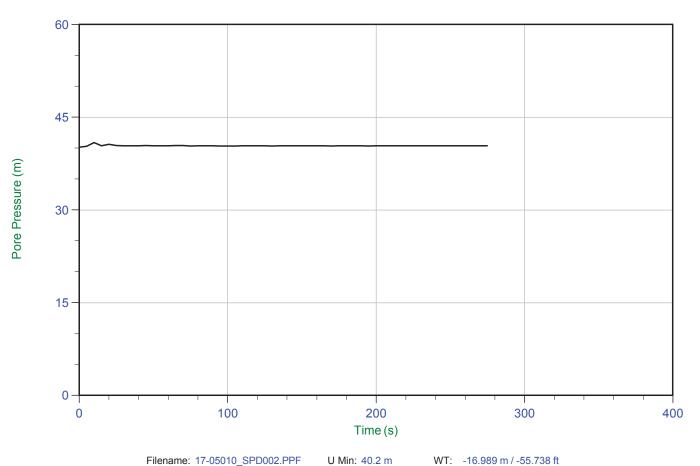
Trace Summary: Depth: 23.350 m / 76.607 ft U Max: 40.6 m Ueq: 40.2 m

Duration: 600.0 s



Sounding: SCPT17-D002 Job No: 17-05010

Date: 04/05/2017 20:44 Cone: 338:T1500F15U500 Area=15 cm² Site: Milne Port Expansion



Filename: 17-05010_SPD002.PPF U Min: 40.2 m

Trace Summary: Depth: 23.375 m / 76.689 ft U Max: 40.9 m Ueq: 40.4 m

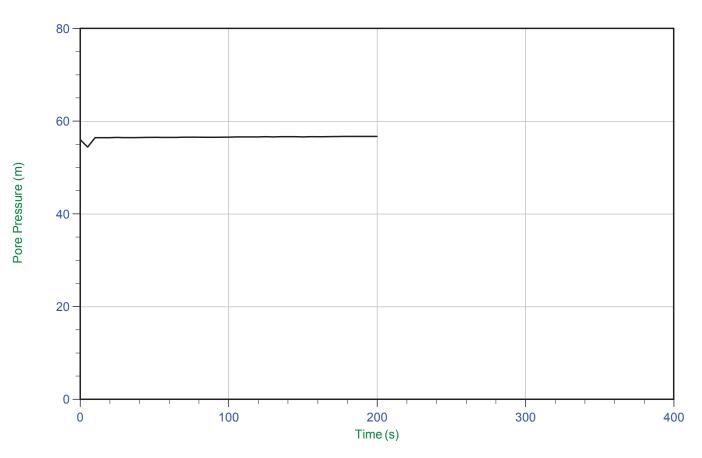
Duration: 275.0 s



Job No: 17-05010 Sounding: SCPT17-D002

 Date:
 04/05/2017 20:44
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Trace Summary: Depth: 39.475 m / 129.510 ft U Max: 56.7 m Ueq: 56.6 m

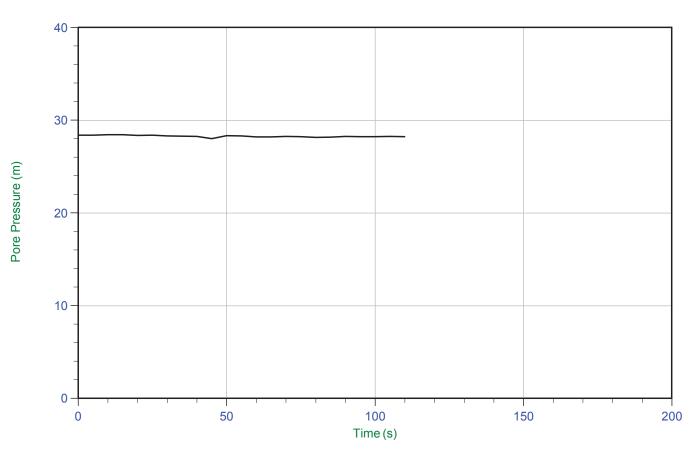
Duration: 200.0 s



Job No: 17-05010 Sounding: CPT17-D003

 Date:
 04/06/2017 13:34
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Trace Summary: Depth: 5.200 m / 17.060 ft U Max: 28.4 m Ueq: 28.2 m

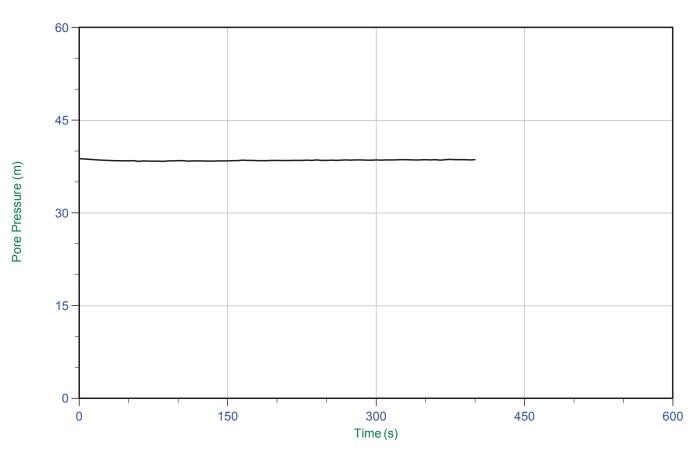
Duration: 110.0 s



Job No: 17-05010 Sounding: CPT17-D003

 Date:
 04/06/2017 13:34
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Trace Summary: Depth: 15.300 m / 50.196 ft U Max: 38.8 m Ueq: 38.5 m

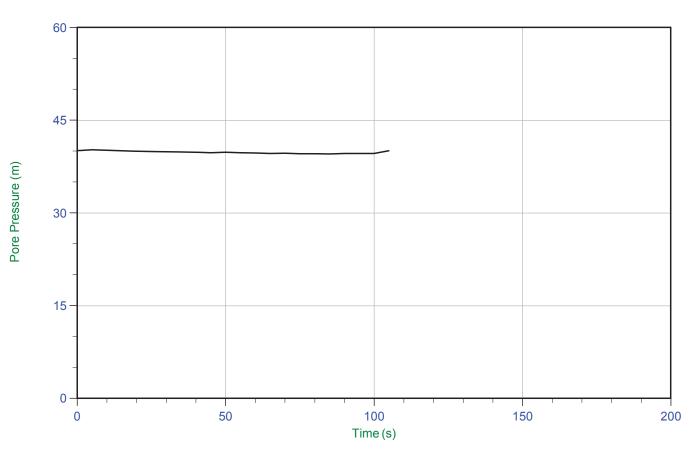
Duration: 400.0 s



 Job No: 17-05010
 Sounding: CPT17-D003

 Date:
 04/06/2017 13:34
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Trace Summary: Depth: 16.300 m / 53.477 ft U Max: 40.2 m Ueq: 39.6 m

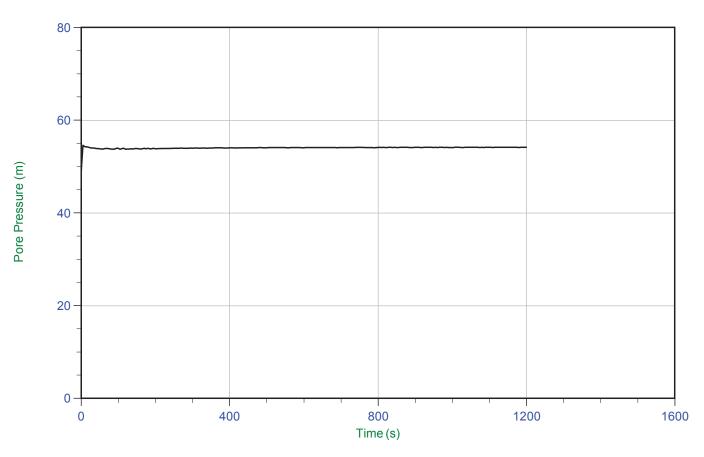
Duration: 105.0 s



 Job No: 17-05010
 Sounding: CPT17-D003

 Date:
 04/06/2017 13:34
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Trace Summary: Depth: 30.425 m / 99.818 ft U Max: 54.6 m Ueq: 54.1 m

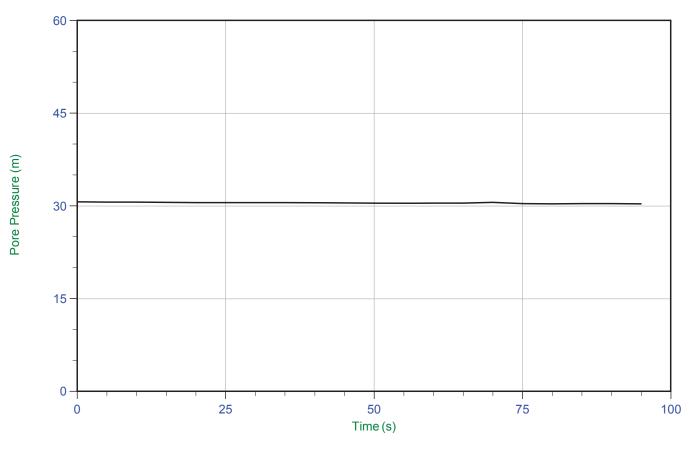
Duration: 1200.0 s



Job No: 17-05010 Sounding: SCPT17-D004

 Date:
 04/04/2017 16:44
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



 $\label{eq:TraceSummary: Depth: 3.275 m / 10.745 ft} \qquad \qquad \text{U Max: 30.7 m} \qquad \qquad \text{Ueq: 30.4 m}$

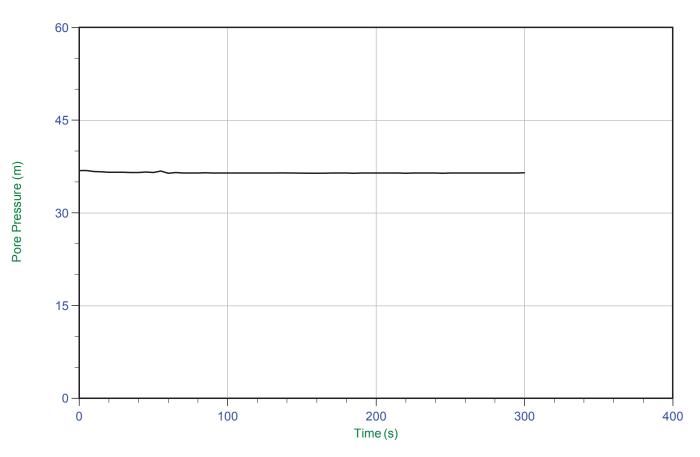
Duration: 95.0 s



Job No: 17-05010 Sounding: SCPT17-D004

 Date:
 04/04/2017 16:44
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Trace Summary: Depth: 9.200 m / 30.183 ft U Max: 36.9 m Ueq: 36.5 m

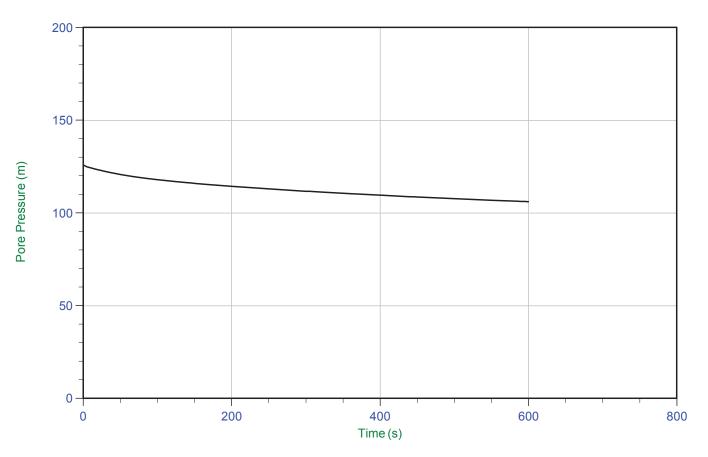
Duration: 300.0 s



Job No: 17-05010 Sounding: SCPT17-D004

 Date:
 04/04/2017 16:44
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



 $\begin{tabular}{lll} Filename: 17-05010_SPD004.PPF & U Min: 106.1 m \\ Trace Summary: & Depth: 30.475 m / 99.982 ft & U Max: 125.8 m \\ \end{tabular}$

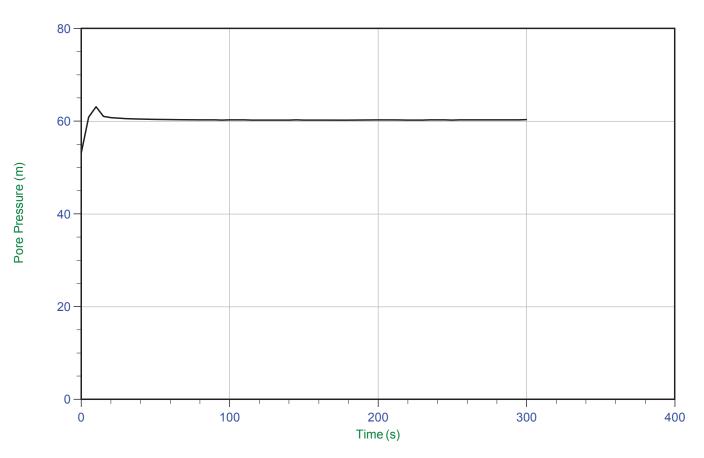
Duration: 600.0 s



Job No: 17-05010 Sounding: SCPT17-D004

 Date:
 04/04/2017 16:44
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Trace Summary: Depth: 32.050 m / 105.150 ft U Max: 63.1 m Ueq: 60.3 m

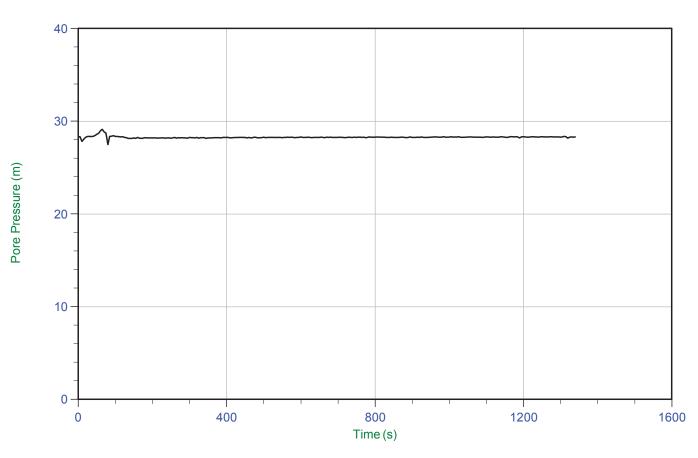
Duration: 300.0 s



Job No: 17-05010 Sounding: CPT17-D005

 Date:
 04/03/2017 02:19
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Trace Summary: Depth: 2.275 m / 7.464 ft U Max: 29.1 m Ueq: 28.3 m

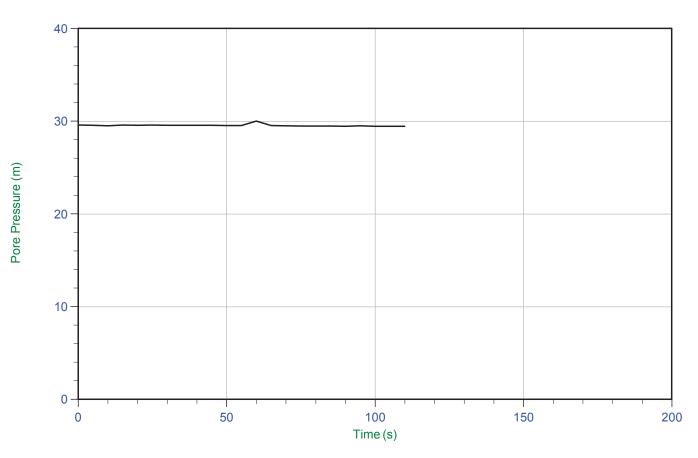
Duration: 1340.0 s



Job No: 17-05010 Sounding: CPT17-D005

 Date:
 04/03/2017 02:19
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



 $\label{eq:TraceSummary: Depth: 3.325 m / 10.909 ft} \qquad \qquad \text{U Max: 30.0 m} \qquad \qquad \text{Ueq: 29.5 m}$

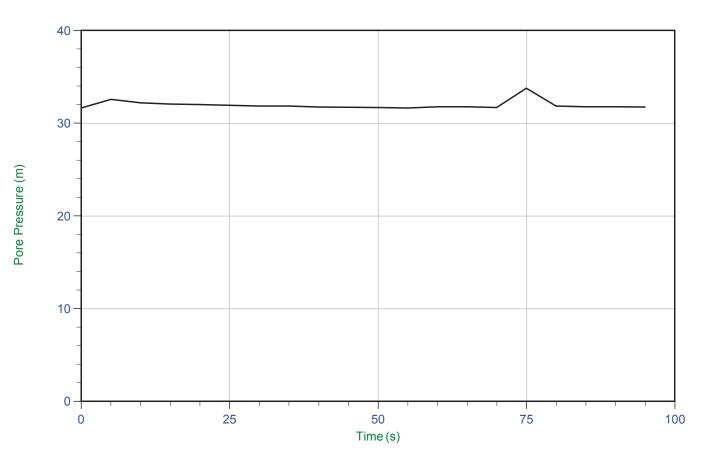
Duration: 110.0 s



Job No: 17-05010 Sounding: CPT17-D005

 Date:
 04/03/2017 02:19
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Trace Summary: Depth: 5.375 m / 17.634 ft U Max: 33.8 m Ueq: 31.8 m

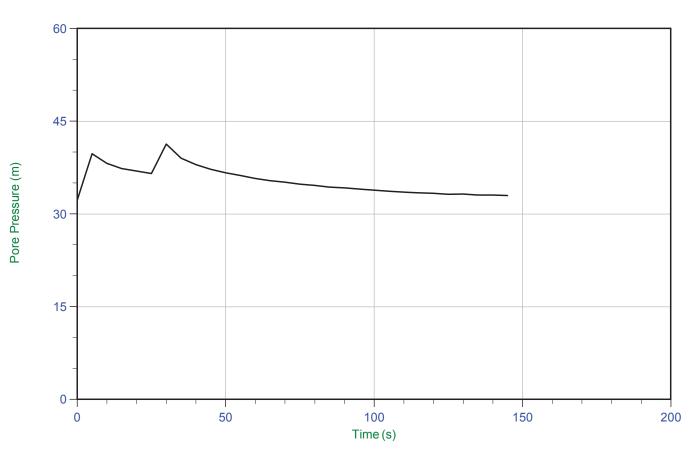
Duration: 95.0 s



Job No: 17-05010 Sounding: CPT17-D005

 Date:
 04/03/2017 02:19
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



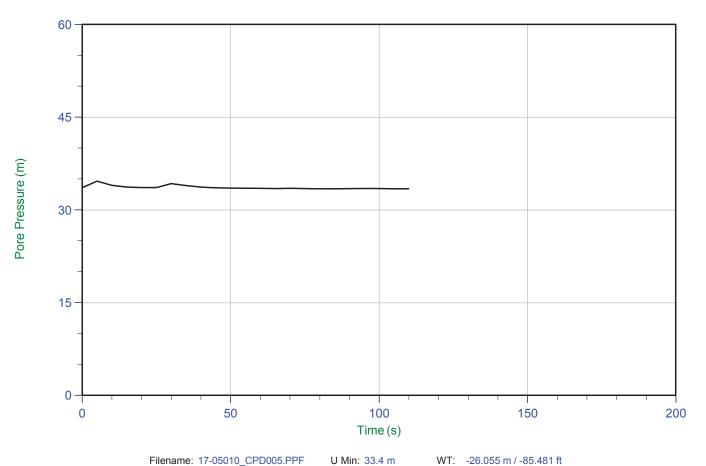
 $\begin{tabular}{lll} Filename: 17-05010_CPD005.PPF & U Min: 32.2 m \\ Trace Summary: & Depth: 6.375 m / 20.915 ft & U Max: 41.3 m \\ \end{tabular}$

Duration: 145.0 s



Sounding: CPT17-D005 Job No: 17-05010 Date: 04/03/2017 02:19

Cone: 338:T1500F15U500 Area=15 cm² Site: Milne Port Expansion



Filename: 17-05010_CPD005.PPF U Min: 33.4 m

Trace Summary: Depth: 7.400 m / 24.278 ft U Max: 34.6 m Ueq: 33.5 m

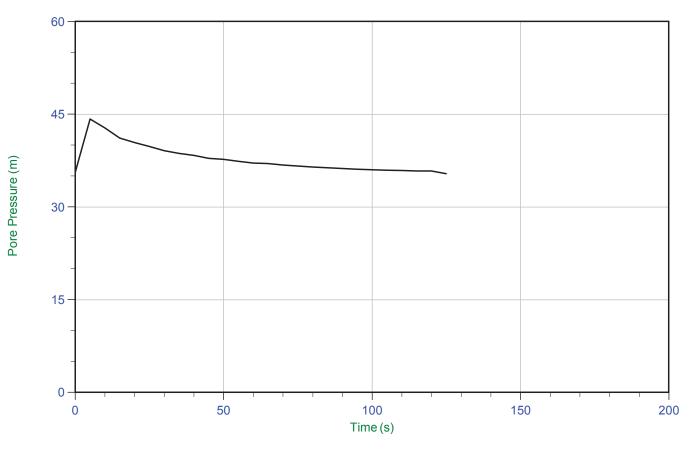
Duration: 110.0 s



Job No: 17-05010 Sounding: CPT17-D005

 Date:
 04/03/2017 02:19
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



 $\begin{tabular}{lll} Filename: 17-05010_CPD005.PPF & U Min: 35.4 m \\ Trace Summary: & Depth: 9.350 m / 30.675 ft & U Max: 44.2 m \\ \end{tabular}$

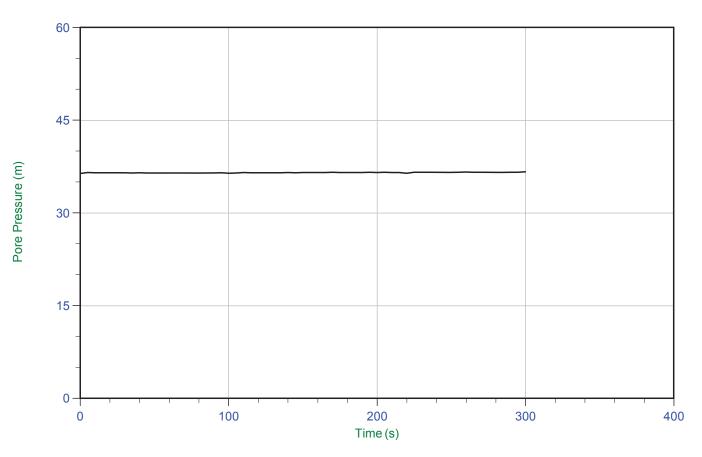
Duration: 125.0 s



Job No: 17-05010 Sounding: CPT17-D005

 Date:
 04/03/2017 02:19
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Trace Summary: Depth: 10.300 m / 33.792 ft U Max: 36.6 m Ueq: 36.5 m

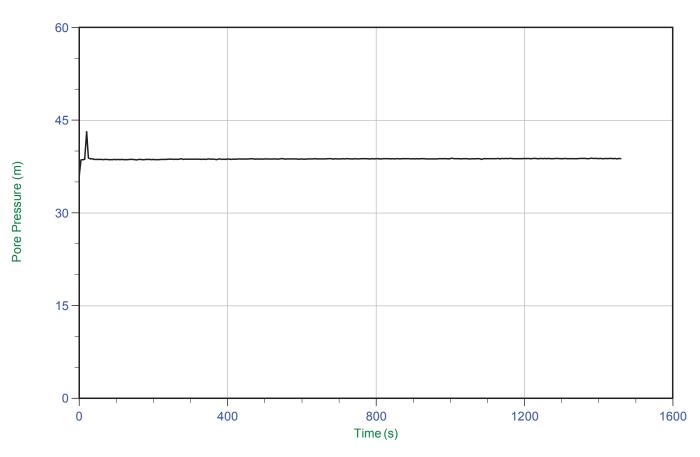
Duration: 300.0 s



 Job No: 17-05010
 Sounding: CPT17-D005

 Date:
 04/03/2017 02:19
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Trace Summary: Depth: 12.350 m / 40.518 ft U Max: 43.1 m Ueq: 38.8 m

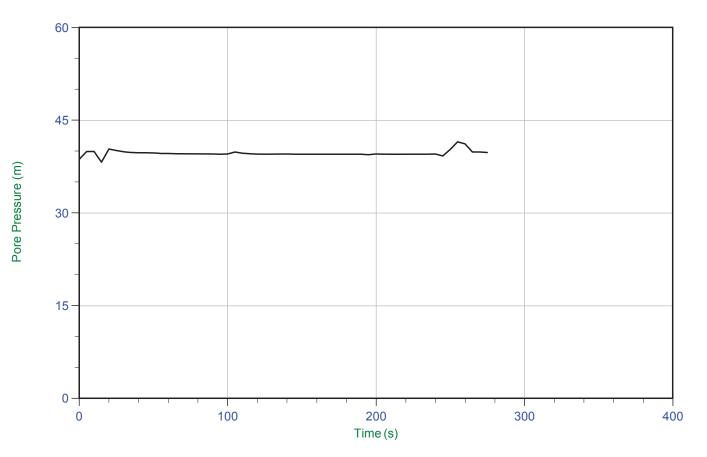
Duration: 1460.0 s



 Job No: 17-05010
 Sounding: CPT17-D005

 Date:
 04/03/2017 02:19
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



 $\begin{tabular}{lll} Filename: 17-05010_CPD005.PPF & U Min: 38.2 m \\ Trace Summary: & Depth: 13.175 m / 43.225 ft & U Max: 41.5 m \\ \end{tabular}$

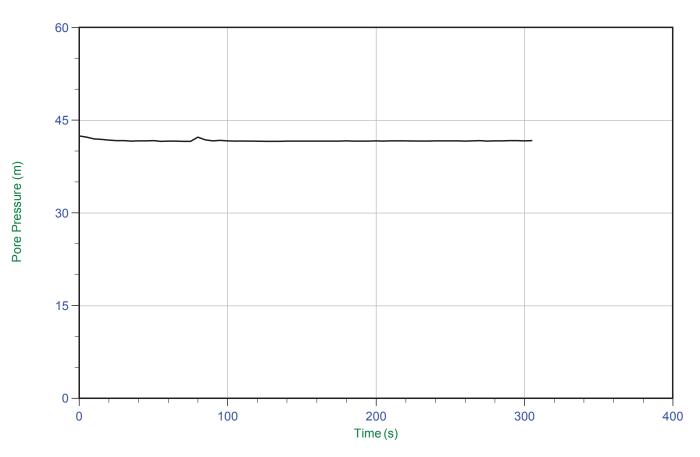
Duration: 275.0 s



 Job No: 17-05010
 Sounding: CPT17-D005

 Date:
 04/03/2017 02:19
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



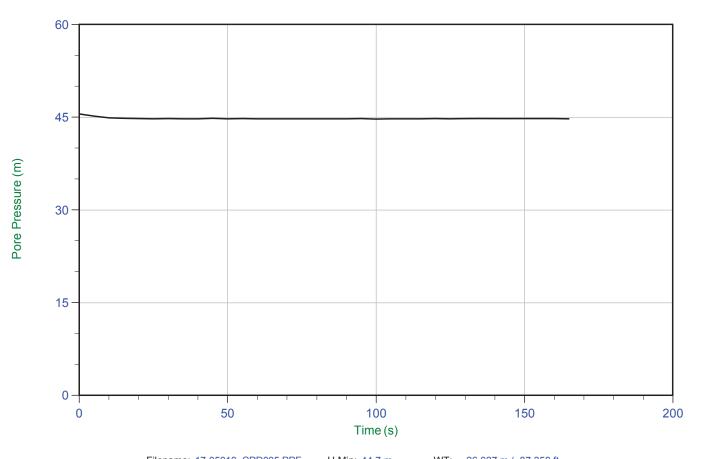
Trace Summary: Depth: 15.050 m / 49.376 ft U Max: 42.4 m Ueq: 41.7 m

Duration: 305.0 s



Job No: 17-05010 Sounding: CPT17-D005
Date: 04/03/2017 02:19 Cone: 338:T1500F15U500 Area=15 cm²

Site: Milne Port Expansion



Trace Summary: Depth: 18.100 m / 59.382 ft U Max: 45.5 m Ueq: 44.7 m

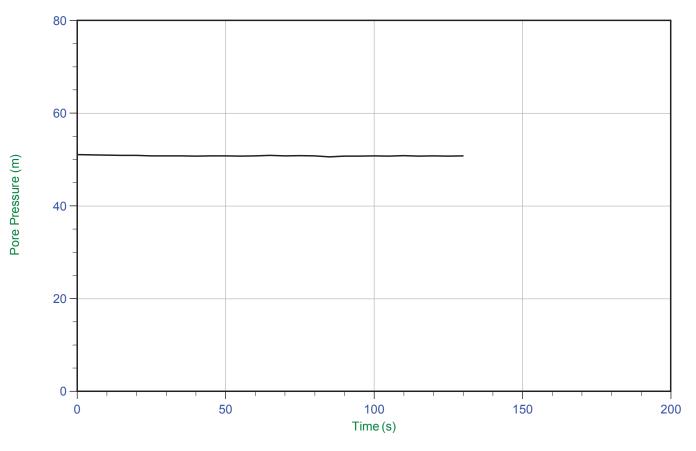
Duration: 165.0 s



 Job No: 17-05010
 Sounding: CPT17-D005

 Date:
 04/03/2017 02:19
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Trace Summary: Depth: 23.925 m / 78.493 ft U Max: 51.1 m Ueq: 50.7 m

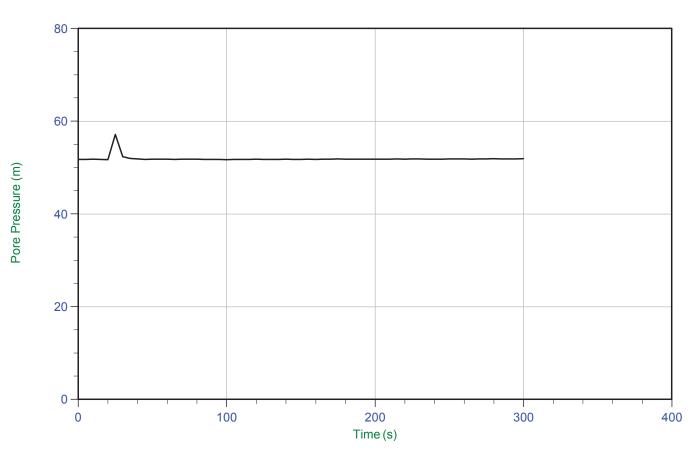
Duration: 130.0 s



Job No: 17-05010 Sounding: CPT17-D005

 Date:
 04/03/2017 02:19
 Cone:
 338:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion

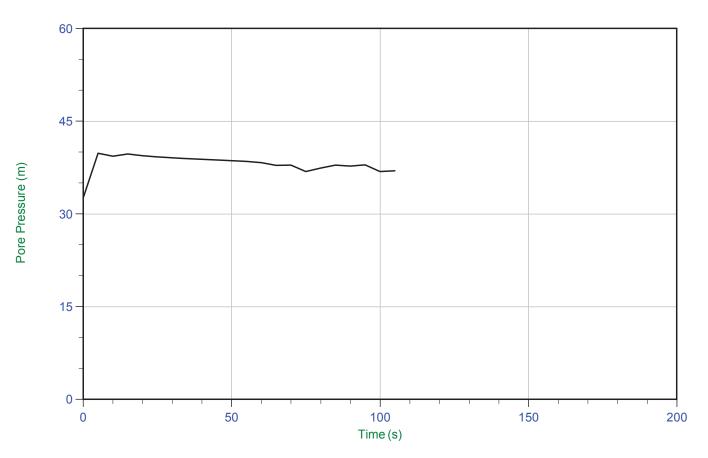


Trace Summary: Depth: 25.125 m / 82.430 ft U Max: 57.2 m Ueq: 51.9 m

Duration: 300.0 s



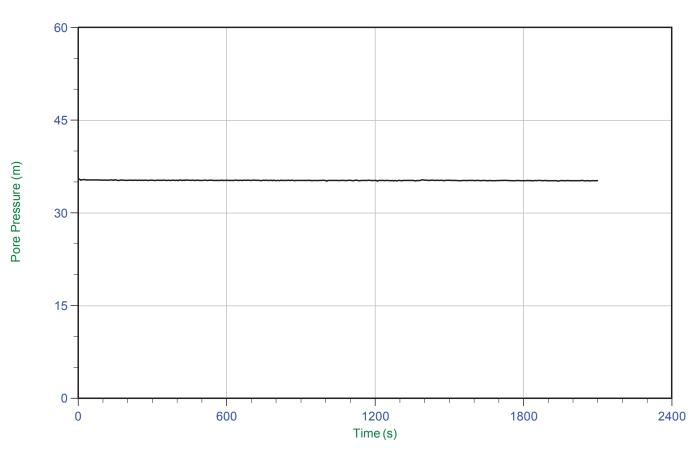
Job No: 17-05010 Sounding: CPT17-D006



Duration: 105.0 s



Job No: 17-05010 Sounding: CPT17-D006

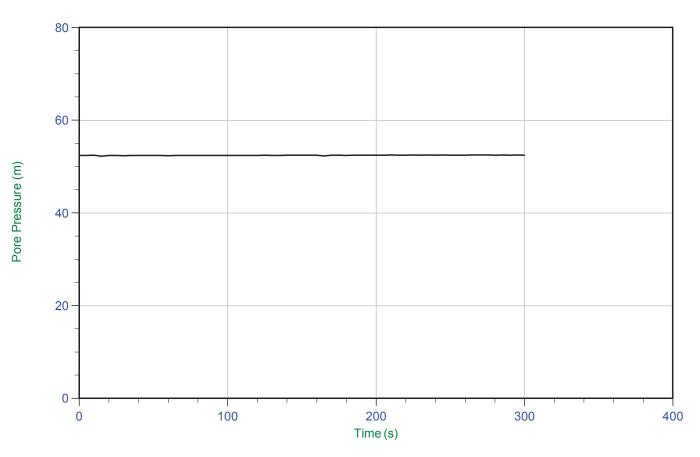


Trace Summary: Depth: 3.300 m / 10.827 ft U Max: 35.4 m Ueq: 35.3 m

Duration: 2100.0 s



Job No: 17-05010 Sounding: CPT17-D006

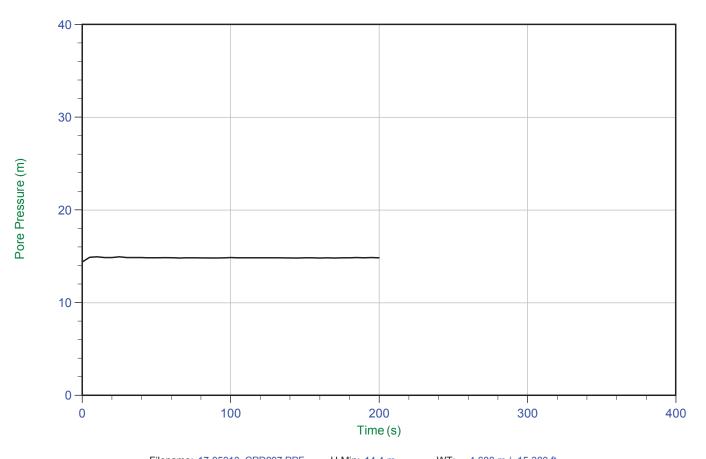


Trace Summary: Depth: 20.575 m / 67.502 ft U Max: 52.5 m Ueq: 52.4 m

Duration: 300.0 s



Job No: 17-05010 Sounding: CPT17-D007

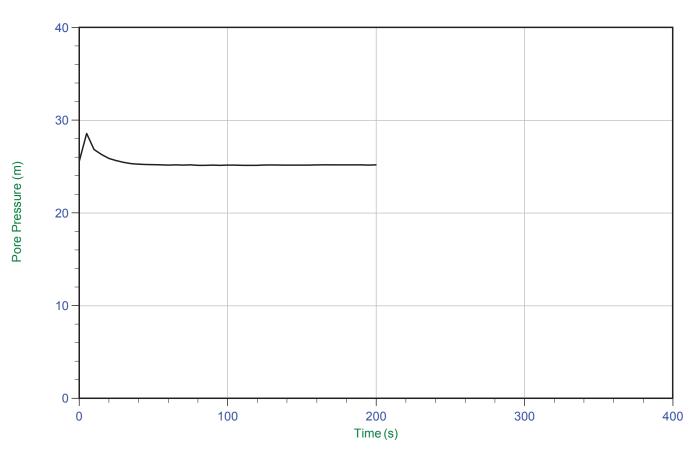


Trace Summary: Depth: 10.100 m / 33.136 ft U Max: 15.0 m Ueq: 14.8 m

Duration: 200.0 s



Job No: 17-05010 Sounding: CPT17-D007



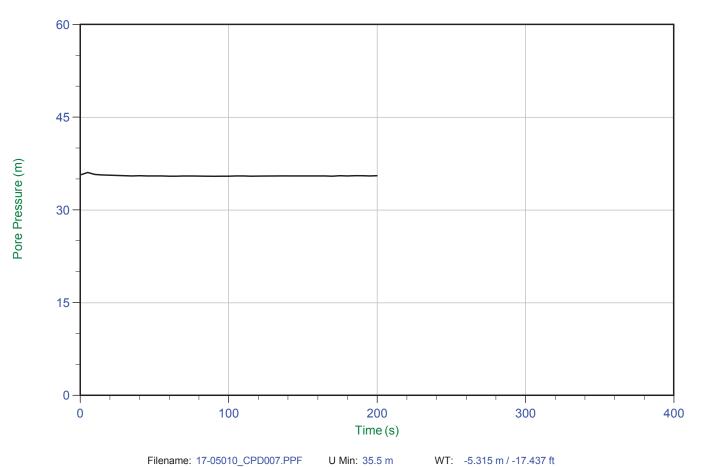
Trace Summary: Depth: 20.150 m / 66.108 ft U Max: 28.6 m Ueq: 25.1 m

Duration: 200.0 s



Sounding: CPT17-D007 Job No: 17-05010

Date: 04/07/2017 11:27 Cone: 374:T1500F15U500 Area=15 cm² Site: Milne Port Expansion



Filename: 17-05010_CPD007.PPF

Trace Summary: Depth: 30.200 m / 99.080 ft

Duration: 200.0 s

U Max: 36.0 m

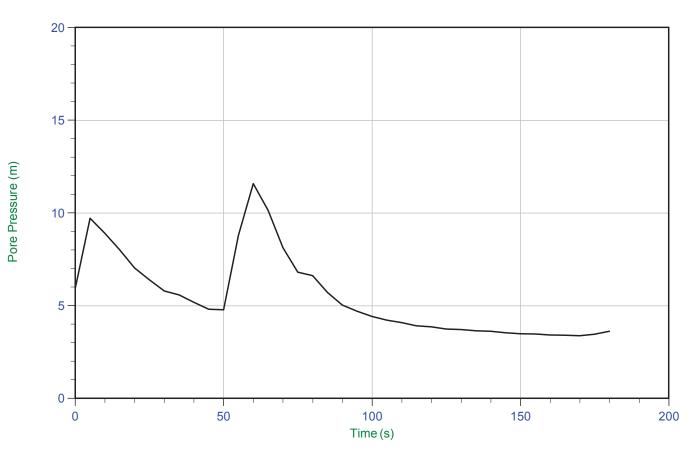
Ueq: 35.5 m



Job No: 17-05010 Sounding: CPT17-D008

 Date:
 04/07/2017 16:47
 Cone:
 374:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



 $\begin{tabular}{lll} Filename: 17-05010_CPD008.PPF & U Min: 3.4 m \\ Trace Summary: & Depth: 2.075 m / 6.808 ft & U Max: 11.6 m \\ \end{tabular}$

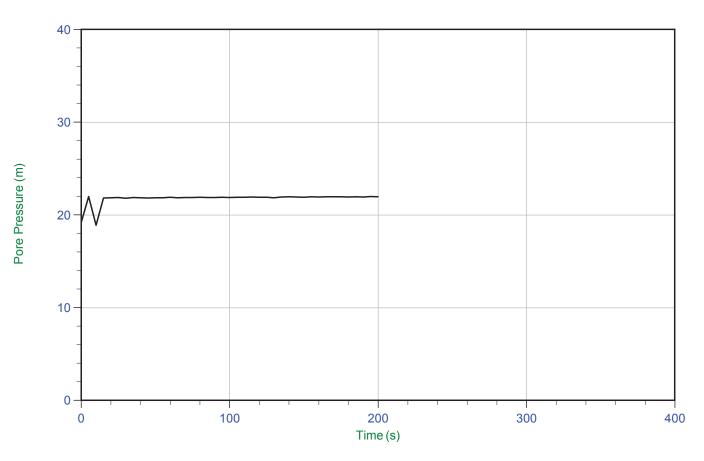
Duration: 180.0 s



Job No: 17-05010 Sounding: CPT17-D008

 Date:
 04/07/2017 16:47
 Cone:
 374:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Trace Summary: Depth: 20.500 m / 67.256 ft U Max: 22.0 m Ueq: 21.9 m

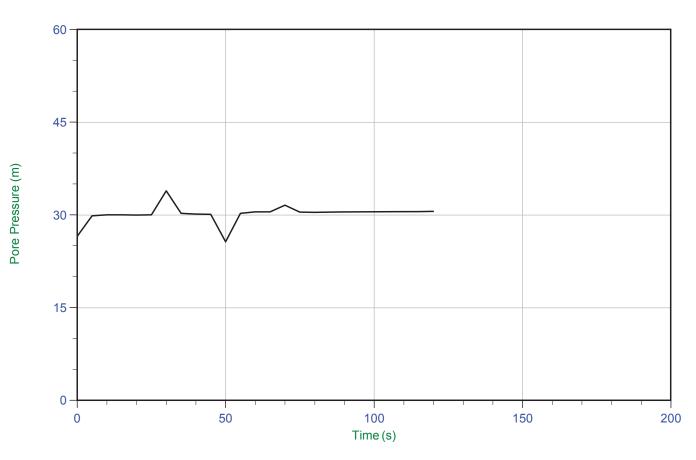
Duration: 200.0 s



Job No: 17-05010 Sounding: CPT17-D008

 Date:
 04/07/2017 16:47
 Cone:
 374:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Trace Summary: Depth: 28.975 m / 95.061 ft U Max: 33.9 m Ueq: 30.4 m

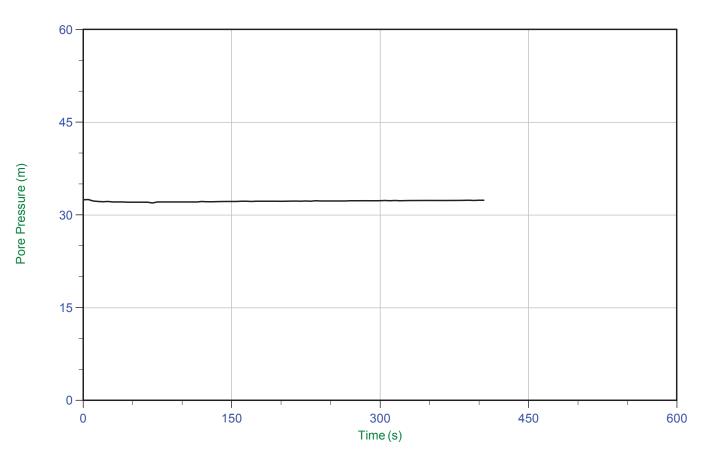
Duration: 120.0 s



Job No: 17-05010 Sounding: CPT17-D008

 Date:
 04/07/2017 16:47
 Cone:
 374:T1500F15U500
 Area=15 cm²

 Site:
 Milne Port Expansion



Duration: 405.0 s

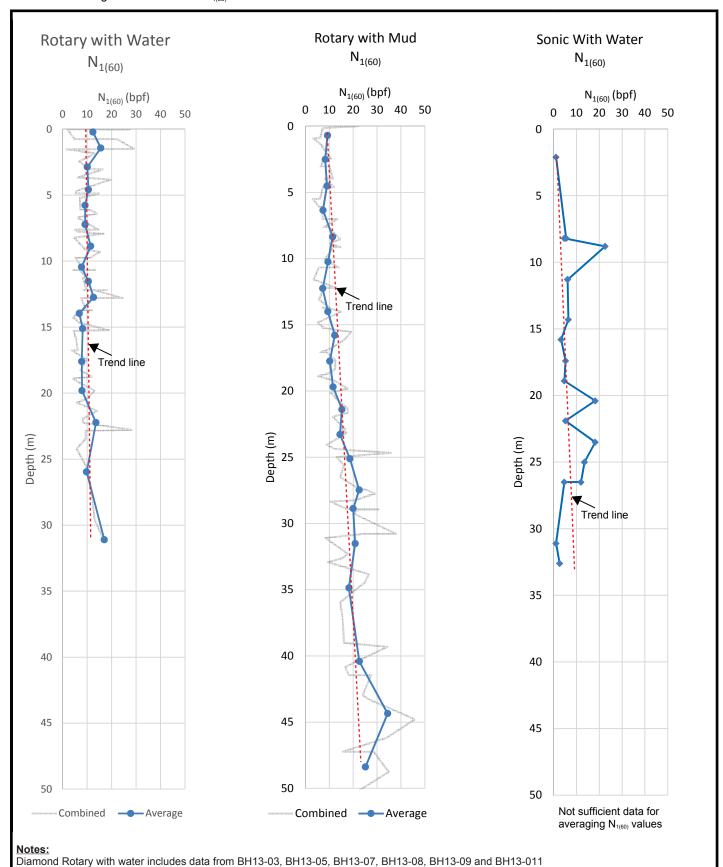




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Appendix K Influence of Drilling Methods on SPT

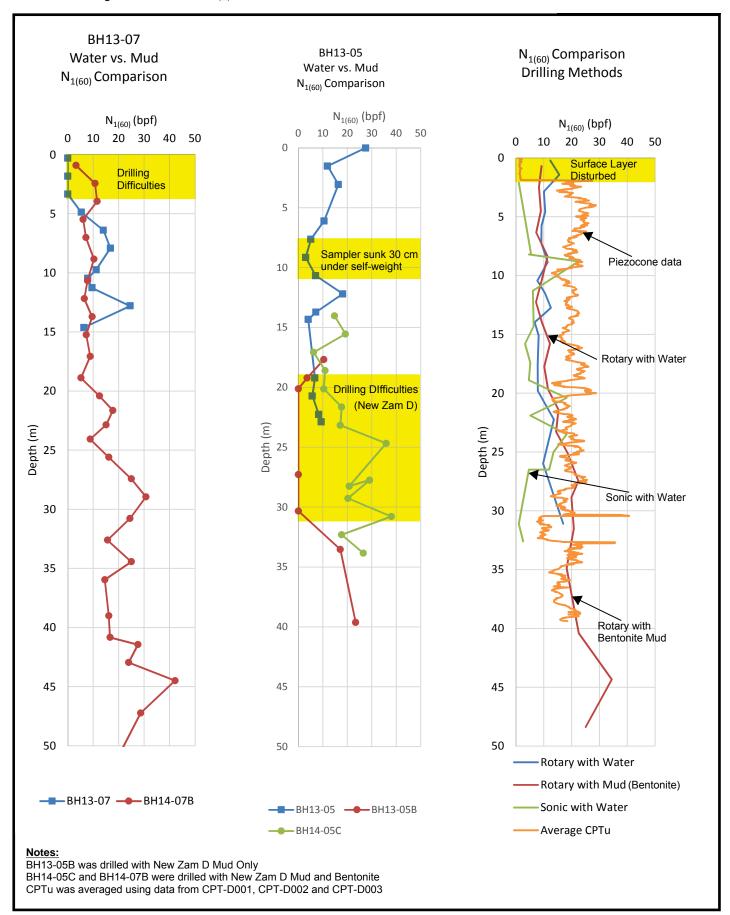




Diamond Rotary with Mud includes data from BH14-05C, BH14-06, BH14-07B, BH14-12 and BH14-13

Sonic with Water includes data from BH17-D001, BH17-D002, BH17-D003, BH17-D004, BH17-D005 and BH17-D006.









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Appendix L
Ice Thickness Tests

