

DWG. NO. H349000-4133-10-035-0001

SETOUT POINTS FOR PLATEAU				
POINT	No.	NORTHING	EASTING	EL.
FG 01	N 7 913	158.77	E 561 678.97	200.
FG 02	N 7 913	162.68	E 561 693.65	201.
FG 03	N 7 913	174.75	E 561 738.87	201.
FG 04	N 7 913	178.80	E 561 753.50	201.
FG 05	N 7 913	143.18	E 561 702.29	199.
FG 06	N 7 913	143.64	E 561 703.24	199.
FG 07	N 7 913	161.98	E 561 744.33	200.
FG 08	N 7 913	162.04	E 561 744.51	200.
FG 09	N 7 913	029.48	E 561 500.52	193.
FG 10	N 7 913	036.00	E 561 514.03	193.
FG 11	N 7 913	039.70	E 561 522.46	193.
FG 12	N 7 913	096.89	E 561 655.49	196.
FG 13	N 7 913	109.10	E 561 700.97	197.
FG 14	N 7 913	115.18	E 561 714.72	197.
FG 15	N 7 913	118.87	E 561 716.19	197.
FG 16	N 7 913	121.47	E 561 728.93	197.
FG 17	N 7 913	135.47	E 561 754.69	199.
FG 18	N 7 913	133.90	E 561 757.01	198.
FG 19	N 7 913	139.96	E 561 770.69	199.
FG 20	N 7 913	025.80	E 561 502.14	193.
FG 21	N 7 913	022.16	E 561 503.74	193.
FG 22	N 7 913	028.68	E 561 517.24	193.
FG 23	N 7 913	037.91	E 561 523.24	193.
FG 24	N 7 913	018.25	E 561 515.91	193.
FG 25	N 7 913	020.44	E 561 520.85	193.
FG 26	N 7 913	030.25	E 561 543.03	194.
FG 27	N 7 913	061.05	E 561 612.61	195.
FG 28	N 7 913	074.15	E 561 642.20	196.
FG 29	N 7 913	082.79	E 561 661.73	196.
FG 30	N 7 912	988.65	E 561 529.01	194.
FG 31	N 7 913	044.54	E 561 655.30	194.
FG 32	N 7 912	952.23	E 561 545.10	194.
FG 33	N 7 913	008.14	E 561 671.41	196.
FG 34	N 7 913	061.83	E 561 805.26	199.
FG 35	N 7 913	060.82	E 561 805.18	199.
FG 36	N 7 913	060.78	E 561 805.73	198.
FG 37	N 7 913	050.82	E 561 804.92	199.
FG 38	N 7 912	939.32	E 561 550.82	194.
FG 39	N 7 912	955.31	E 561 632.07	194.
FG 40	N 7 912	965.42	E 561 654.91	195.
FG 41	N 7 912	978.53	E 561 684.52	196.
FG 42	N 7 913	018.38	E 561 774.55	197.
FG 43	N 7 913	030.83	E 561 802.75	198.
FG 44	N 7 913	031.05	E 561 803.32	198.

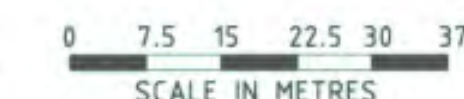
SETOUT POINTS FOR TOP OF BERM			
POINT No.	NORTHING	EASTING	ELEV.
TOB 01	N 7 913 161.17	E 561 698.57	200.
TOB 02	N 7 913 152.36	E 561 679.42	199.
TOB 03	N 7 913 113.70	E 561 697.18	197.
TOB 04	N 7 913 116.91	E 561 693.17	199.
TOB 05	N 7 913 112.20	E 561 682.34	198.
TOB 06	N 7 913 106.28	E 561 668.57	198.
TOB 07	N 7 913 101.95	E 561 659.48	198.
TOB 08	N 7 913 099.55	E 561 654.30	198.
TOB 09	N 7 913 095.77	E 561 652.85	198.
TOB 10	N 7 913 091.83	E 561 654.54	198.
TOB 11	N 7 913 087.08	E 561 657.02	198.
TOB 12	N 7 913 086.67	E 561 656.27	198.
TOB 13	N 7 913 083.08	E 561 649.51	197.
TOB 14	N 7 913 078.66	E 561 640.54	197.
TOB 15	N 7 913 074.47	E 561 631.45	197.
TOB 16	N 7 913 070.28	E 561 622.37	196.
TOB 17	N 7 913 066.09	E 561 613.29	196.
TOB 18	N 7 913 062.26	E 561 604.05	196.
TOB 19	N 7 913 057.78	E 561 595.10	196.
TOB 20	N 7 913 053.15	E 561 586.21	195.
TOB 21	N 7 913 049.00	E 561 577.11	195.
TOB 22	N 7 913 045.92	E 561 567.76	194.
TOB 23	N 7 913 043.34	E 561 558.08	194.
TOB 24	N 7 913 040.70	E 561 548.41	194.
TOB 25	N 7 913 036.07	E 561 539.23	194.
TOB 26	N 7 913 031.31	E 561 528.92	193.
TOB 27	N 7 913 022.19	E 561 504.42	193.
TOB 28	N 7 913 014.99	E 561 507.71	193.
TOB 29	N 7 912 986.17	E 561 523.77	193.
TOB 30	N 7 912 937.10	E 561 546.36	193.
TOB 31	N 7 912 934.58	E 561 551.82	193.
TOB 32	N 7 912 936.75	E 561 558.54	194.
TOB 33	N 7 912 943.88	E 561 591.32	194.
TOB 34	N 7 912 952.12	E 561 633.07	195.
TOB 35	N 7 912 962.36	E 561 656.26	195.
TOB 36	N 7 912 975.47	E 561 685.88	196.
TOB 37	N 7 912 997.90	E 561 736.56	197.
TOB 38	N 7 912 997.13	E 561 738.54	198.
TOB 39	N 7 913 013.74	E 561 776.06	199.
TOB 40	N 7 913 026.34	E 561 804.58	200.
TOB 41	N 7 913 030.70	E 561 802.48	198.

SETOUT POINTS FOR BOTTOM OF DITCH			
POINT No.	NORTHING	EASTING	EL.
BOD 01	N 7 913 083.55	E 561 660.24	195.93
BOD 02	N 7 913 075.34	E 561 641.68	195.57
BOD 03	N 7 913 062.24	E 561 612.08	194.74
BOD 04	N 7 913 046.51	E 561 576.55	194.05
BOD 05	N 7 913 034.99	E 561 545.34	192.62
BOD 06	N 7 913 019.21	E 561 509.67	192.50
BOD 07	N 7 913 016.36	E 561 510.66	192.50
BOD 08	N 7 913 009.98	E 561 513.65	192.47
BOD 09	N 7 912 987.40	E 561 526.23	192.39
BOD 10	N 7 912 952.31	E 561 541.56	192.28
BOD 11	N 7 912 949.56	E 561 542.81	192.27
BOD 12	N 7 912 938.24	E 561 548.87	192.72
BOD 13	N 7 912 937.25	E 561 551.16	192.80
BOD 14	N 7 912 945.89	E 561 590.91	193.80
BOD 15	N 7 912 954.07	E 561 632.43	194.28
BOD 16	N 7 912 964.23	E 561 655.43	194.66
BOD 17	N 7 912 977.34	E 561 685.05	195.63
BOD 18	N 7 913 017.19	E 561 775.07	197.10
BOD 19	N 7 913 028.86	E 561 801.50	197.97
BOD 20	N 7 913 185.80	E 561 764.30	200.81
BOD 21	N 7 913 177.30	E 561 756.92	199.75
BOD 22	N 7 913 174.61	E 561 760.66	200.05
BOD 23	N 7 913 167.19	E 561 760.85	199.53
BOD 24	N 7 913 157.40	E 561 765.39	198.84
BOD 25	N 7 913 140.67	E 561 772.29	198.19
BOD 26	N 7 913 079.83	E 561 800.56	197.35
BOD 27	N 7 913 074.25	E 561 803.87	197.72

ORE CRUSHING & SCREENING
SEDIMENTATION POND REFER. TO
DRAWINGS H349000-4385-10-035-0001
AND H349000-4385-10-035-0002

CULVERT ID	FISH BEARING (Y/N)	NUMBER OF PIPES (n)	D (mm)	W (mm)	TYPE	CULVERT C AT UPSTREAM		U/S INV. ELV. (m)	RIP RAP REQUIRED (Y/N)	CULVERT C AT DOWNSTREAM		D/S INV. ELV. (m)	RIP RAP REQUIRED (Y/N)	C (mm)	L (m)	S (%)	SKEW DEGREE	LENGT (m)
						NORTHING	EASTING			NORTHING	EASTING							
MS CV15	N	1	800	800	CSP	7 913 031.78	561 538.07	192.60	Y	7 913 020.85	561 513.38	192.52	Y	300	3.2	0.3	90.0	27

CULVERT SCHEDULE
REFER TO DRAWING H349000-1000-10-041-0003 FOR DETAILS


HATCH

DESIGNED BY: <u>M. McDOUGALD</u>	DRAWN BY: <u>M. McDOUGALD</u>
M. McDOUGALD	M. McDOUGALD
DATE 2013-05-28	DATE 2013-05-28
CHECKED BY: <u>A. MOHIBRAHIM</u>	DISCIP. ENGR. <u>S. HASSAN</u>
A. MOHIBRAHIM	S. HASSAN
DATE 2013-08-29	DATE 2013-08-29
PROJ. DES. COORD. <u>T. THEVENAZ</u>	PROJ. ENGR. <u>J. CLELAND</u>
T. THEVENAZ	J. CLELAND
DATE 2013-08-29	DATE 2013-08-29
PROJ. MGR. <u>S. PERRY</u>	
S. PERRY	
DATE 2013-08-29	

FOR CONSTRUCTION

†Baffinland

MARY RIVER PROJECT

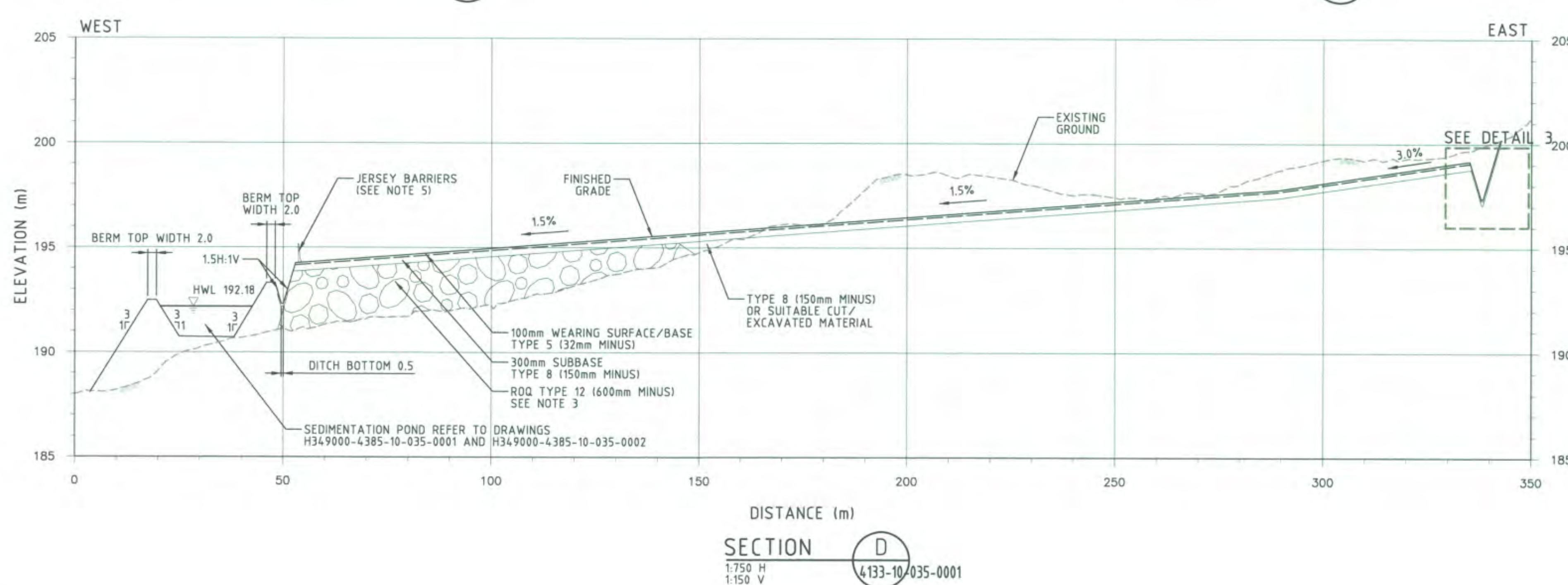
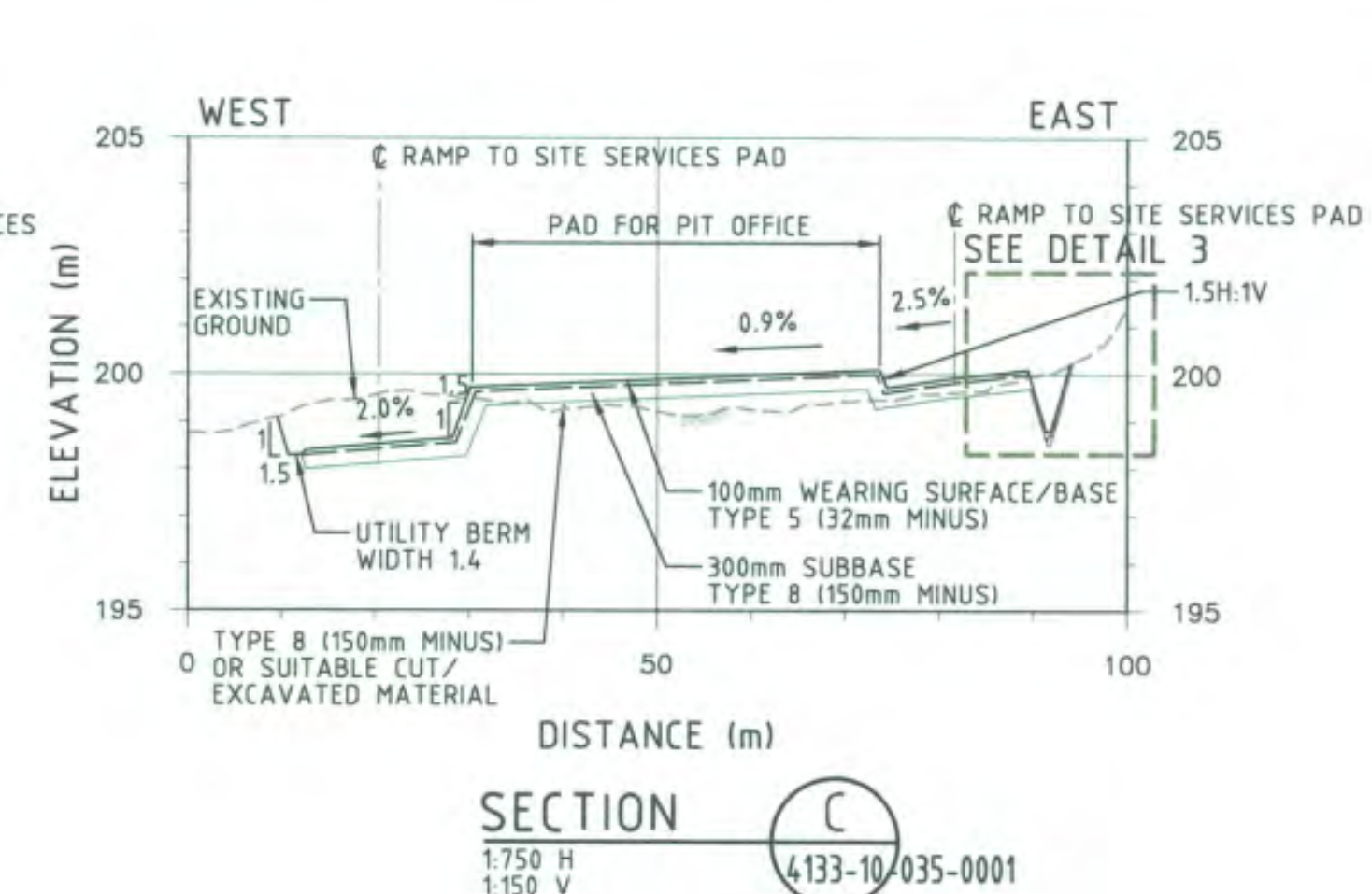
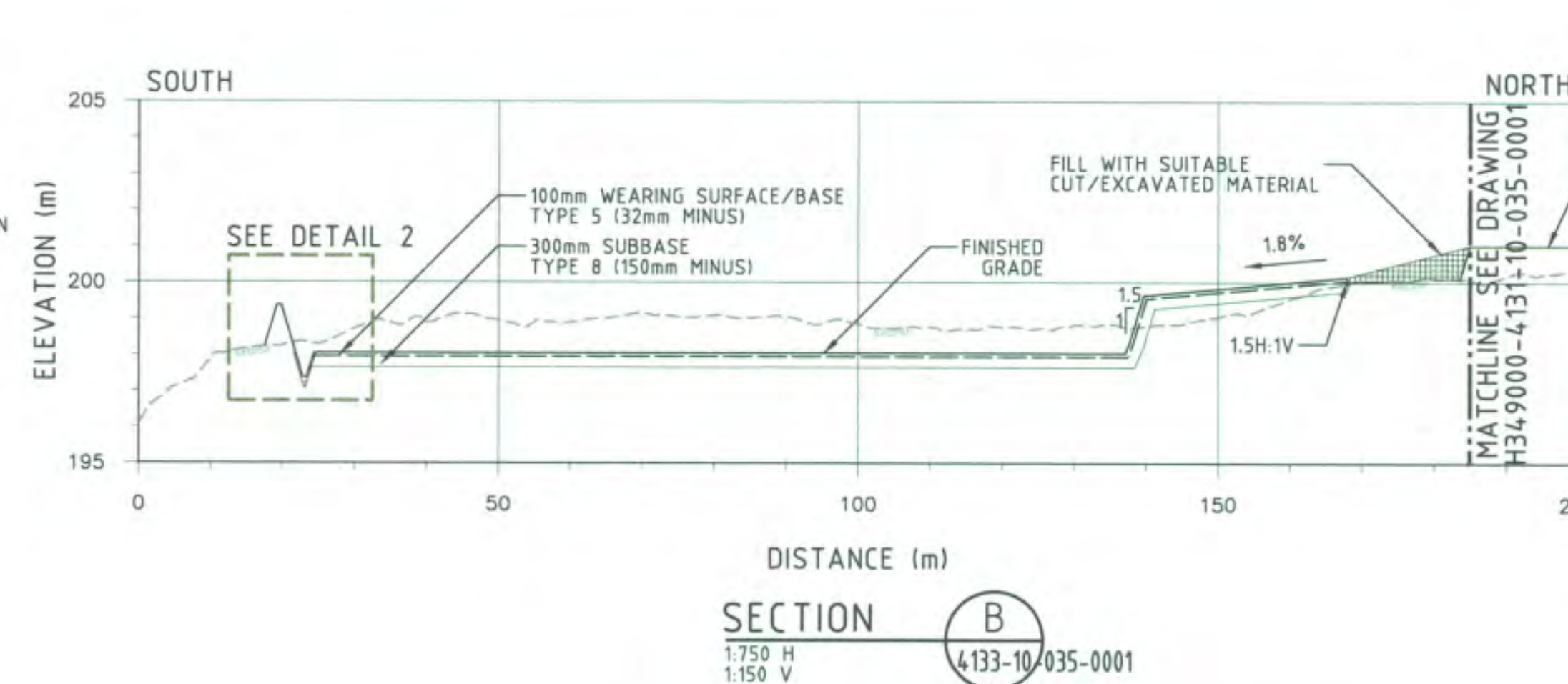
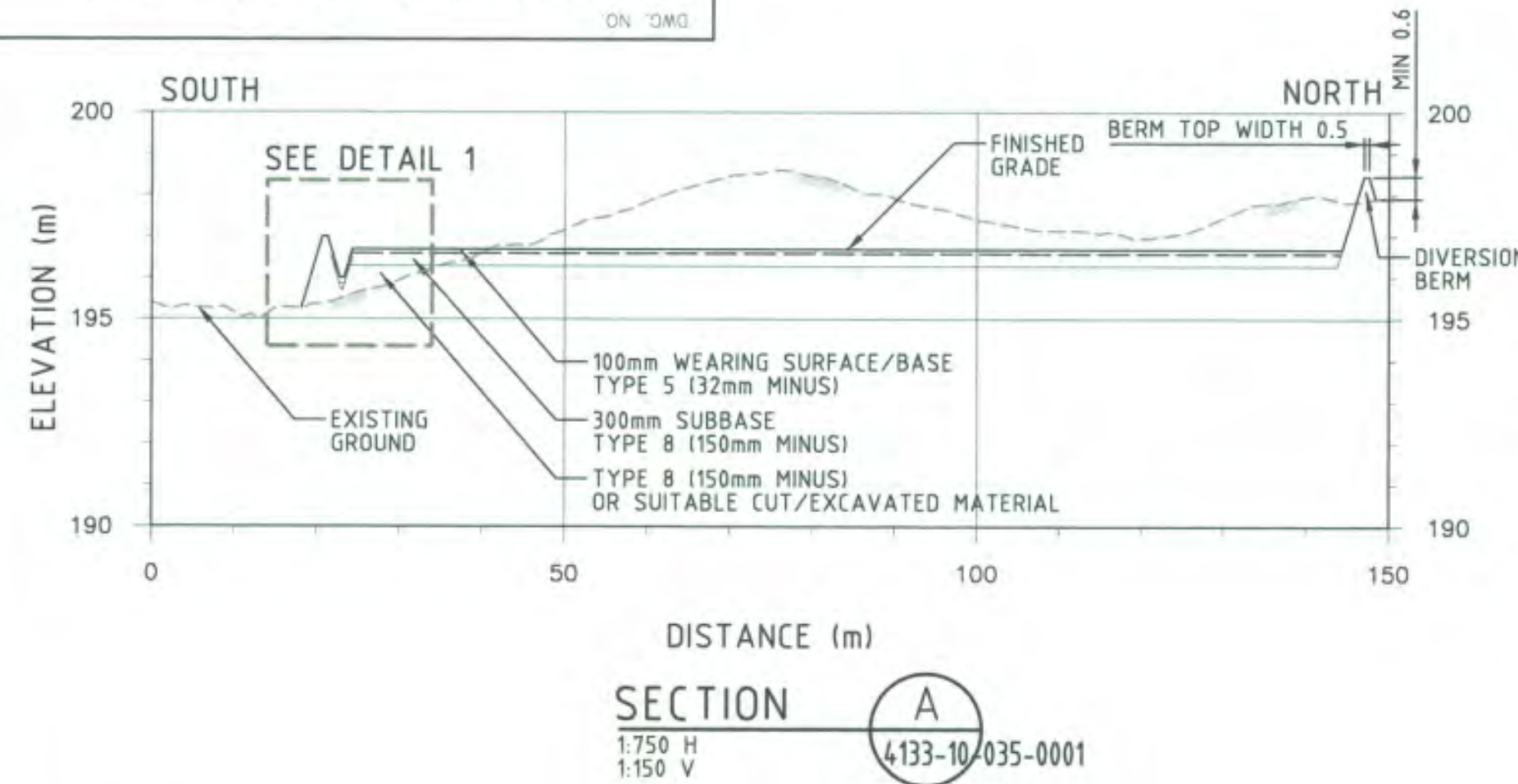
MINE SITE
ORE CRUSHING & SCREENING
EARTHWORKS & DRAINAGE - PLAN

SCALE 1:750	DWG. NO. H349000-4133-10-035-0001
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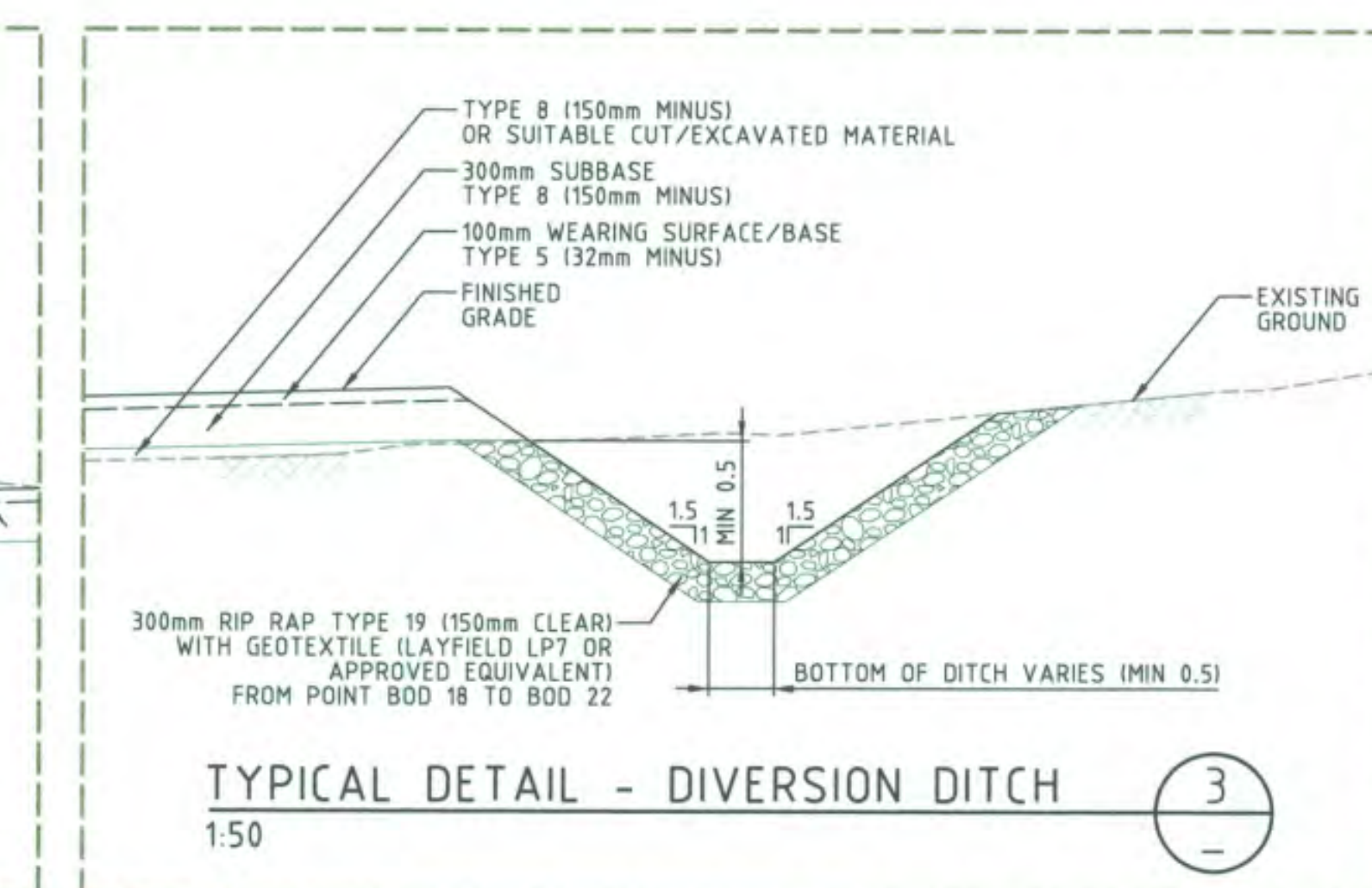
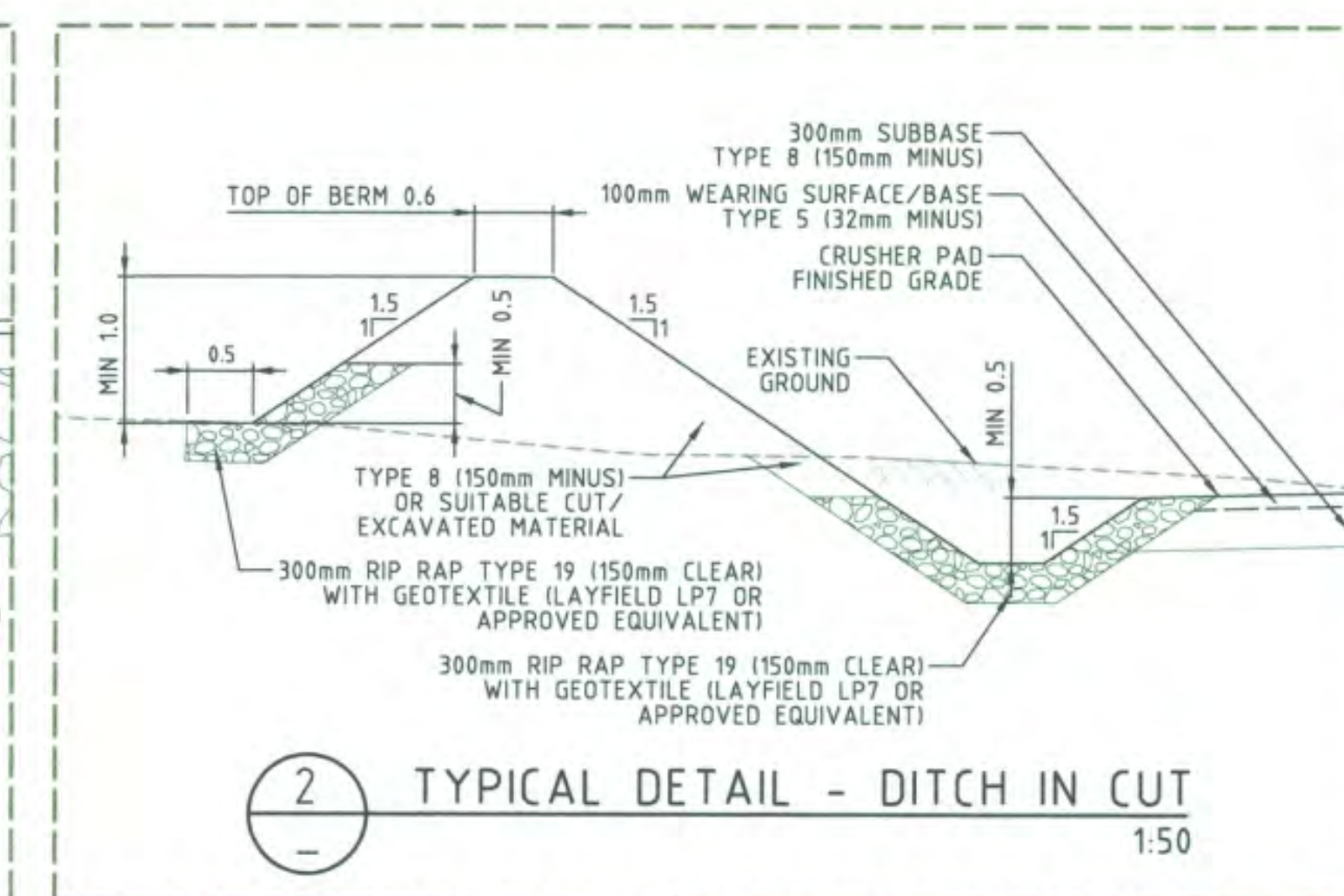
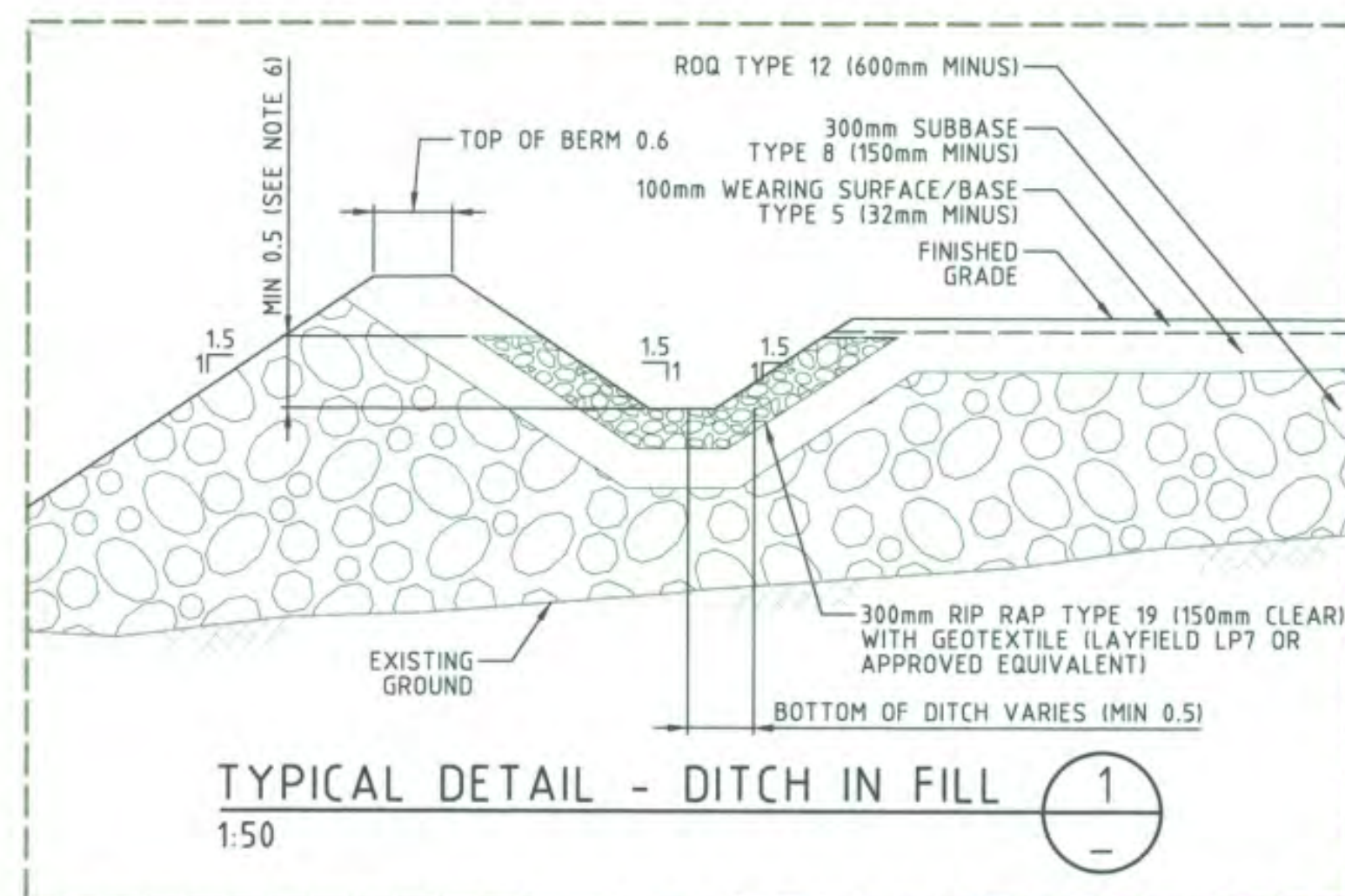
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2000-10-035-0002



- LEGEND:**
- HWL HIGH WATER LEVEL
 - ROQ RUN OF QUARRY
 - RUN OF QUARRY MATERIAL TYPE 12 (600mm MINUS) (FOR TOTAL FILL DEPTH > 1.0m)
 - RIP RAP TYPE 19 (150mm CLEAR)
 - LOCALIZED FILL

- NOTES:**
- TOPOGRAPHY PROVIDED BY TERRAPOINT CANADA INC.
 - ALL DIMENSIONS AND ELEVATIONS SHOWN ARE IN METRES UNLESS NOTED OTHERWISE.
 - FOR STANDARD EARTHWORK DETAILS REFER TO DRAWINGS H349000-1000-10-041-0001 AND H349000-1000-10-041-0002.
 - FOR RIP RAP DETAIL REFER TO DETAIL 8 ON DRAWING H349000-1000-10-041-0002.
 - JERSEY BARRIER: HY-GRADE PRECAST CONCRETE J-J HOOK CONCRETE BARRIER, LENGTH 4.000m x HEIGHT 0.900m, OR EQUIVALENT.
 - DEPTH VARIES ALONG DITCH. FOR TOP OF BERM ELEVATION SEE TABLE "SETOUT POINTS FOR TOP OF BERM" ON DRAWING H349000-4133-10-035-0001.
 - POND MAXIMUM CAPACITY IS 2730m³ WITH 0.3m FREEBOARD AND HIGH WATER LEVEL (HWL) EL. 192.18m.



FOR CONSTRUCTION

PERMIT TO PRACTICE
HATCH LTD.
Signature: *[Signature]*
Date: 29 Aug 13
PERMIT NUMBER: P 512
The Association of Professional Engineers,
Geologists and Geophysicists of NWT/NU

REGISTERED PROFESSIONAL ENGINEER
M. M. S. HASSAN
LICENSEE
29 Aug 13
NTNU

HATCH

DESIGNED BY: M. MCDUGALD
DRAWN BY: M. MCDUGALD
DATE 2013-05-28
CHECKED BY: S. HASSAN
DATE 2013-08-29
PROJECT: MARY RIVER PROJECT
PROJECT ENGINEER: J. CLELAND
DATE 2013-08-29
PROJECT MANAGER: S. PERRY
DATE 2013-08-29

Baffinland

MARY RIVER PROJECT

MINE SITE
ORE CRUSHING & SCREENING
EARTHWORKS & DRAINAGE - SECTIONS

SCALE: 1:750
DWG. NO.: H349000-4133-10-035-0002
REV. 0

DRAWING NO. REFERENCE DRAWINGS

NO. DESCRIPTION BY: CHK'D APP'D DATE

0 CONSTRUCTION
REV. ISSUE FOR AUTH. BY DATE

ISSUE AUTHORIZATION

mcdougald322
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H349000-2133-10-035-0001

ON DWG

SETOUT POINTS FOR DRAINAGE BERM

POINT No.	NORTHING	EASTING	EL.
TOB 01	N 7 976 351.70	E 503 235.44	9.60
TOB 02	N 7 976 350.57	E 503 177.64	9.60
TOB 03	N 7 976 349.89	E 503 159.01	9.60
TOB 04	N 7 976 315.76	E 503 092.68	9.60
TOB 05	N 7 976 304.19	E 503 083.75	9.60
TOB 06	N 7 976 300.65	E 503 078.77	9.06
TOB 07	N 7 976 287.60	E 503 057.68	7.50
TOB 08	N 7 976 273.38	E 503 056.47	8.65
TOB 09	N 7 976 238.86	E 503 056.81	9.26
TOB 10	N 7 976 213.85	E 503 057.30	9.54
TOB 11	N 7 976 173.85	E 503 058.45	9.74
TOB 12	N 7 976 143.78	E 503 059.84	9.81
TOB 13	N 7 976 079.27	E 503 063.73	9.84
TOB 14	N 7 976 359.12	E 503 296.62	9.97
TOB 15	N 7 976 360.13	E 503 327.75	9.89
TOB 16	N 7 976 362.41	E 503 375.99	9.75
TOB 17	N 7 976 293.01	E 503 446.70	12.10
TOB 18	N 7 976 277.42	E 503 448.06	12.64
TOB 19	N 7 976 198.59	E 503 450.28	12.15
TOB 20	N 7 976 120.19	E 503 452.44	12.50
TOB 21	N 7 976 078.40	E 503 452.81	12.50

SETOUT POINTS FOR DRAINAGE DITCH

POINT No.	NORTHING	EASTING	EL.
BOD 01	N 7 976 349.58	E 503 233.91	8.54
BOD 02	N 7 976 348.23	E 503 177.70	8.37
BOD 03	N 7 976 347.47	E 503 159.11	8.32
BOD 04	N 7 976 314.08	E 503 094.84	8.11
BOD 05	N 7 976 302.46	E 503 085.95	8.07
BOD 06	N 7 976 298.63	E 503 079.05	8.05
BOD 07	N 7 976 287.63	E 503 059.61	6.55
BOD 08	N 7 976 268.70	E 503 060.21	6.60
BOD 09	N 7 976 160.42	E 503 063.66	6.93
BOD 10	N 7 976 075.04	E 503 068.47	7.19
BOD 11	N 7 976 357.07	E 503 296.70	8.97
BOD 12	N 7 976 358.08	E 503 327.83	8.89
BOD 13	N 7 976 362.15	E 503 414.06	8.63
BOD 14	N 7 976 349.82	E 503 436.53	6.97
BOD 15	N 7 976 326.93	E 503 437.43	7.04
BOD 16	N 7 976 284.96	E 503 439.07	7.16
BOD 17	N 7 976 277.10	E 503 439.38	7.19
BOD 18	N 7 976 165.56	E 503 444.07	7.52
BOD 19	N 7 976 078.40	E 503 445.23	7.78

KEY PLAN

LEGEND

- EXISTING GROUND CONTOURS
- EXISTING WATERBODY
- BAFFINLAND'S COMMERCIAL LEASE ON INUIT OWNED LAND
- PROJECT DEVELOPMENT AREA (PDA)
- FILL SLOPE
- CUT SLOPE
- TOE OF SLOPE
- SLOPE BREAKLINE
- GRADING SLOPE
- CENTERLINE OF DITCH
- CULVERT
- FG EL. AT 50m x 50m GRID
- HIGH POINT
- SETOUT POINT NUMBER
- CORRUGATED STEEL PIPE
- CROSS SECTION DISTANCE

NOTES:

- TOPOGRAPHY PROVIDED BY TERRAPOINT CANADA INC.
- COORDINATE GRID IS SHOWN IN UTM (NAD83) ZONE 17 AND IS IN METRES.
- CONTOURS ARE IN METRES. CONTOUR INTERVAL IS 0.5m.
- ALL DIMENSIONS AND ELEVATIONS SHOWN ARE IN METRES UNLESS NOTED OTHERWISE.
- FOR SEDIMENTATION PONDS PLAN AND DETAIL REFER TO DRAWING H349000-2345-10-035-0001.
- FOR UTILITY BERM TYPICAL DETAILS REFER TO DRAWINGS H349000-1000-10-041-0006, -0007 AND -0009.

FOR CONSTRUCTION

POINT No.	NORTHING	EASTING	EL.
001	N 7 976 443.58	E 503 232.75	7.55
002	N 7 976 445.32	E 503 280.96	7.55
003	N 7 976 427.12	E 503 275.61	7.60
004	N 7 976 427.34	E 503 281.61	7.60
005	N 7 976 390.55	E 503 234.66	7.71
006	N 7 976 391.97	E 503 274.50	7.71
007	N 7 976 387.23	E 503 234.78	9.93
008	N 7 976 388.75	E 503 277.00	9.90
009	N 7 976 388.97	E 503 283.00	9.89
010	N 7 976 381.84	E 503 251.73	10.76
011	N 7 976 345.24	E 503 161.98	9.74
012	N 7 976 345.81	E 503 177.78	9.81
013	N 7 976 347.84	E 503 235.90	9.53
014	N 7 976 342.49	E 503 162.09	10.25
015	N 7 976 343.06	E 503 177.88	10.32
016	N 7 976 345.17	E 503 236.30	10.03
017	N 7 976 351.02	E 503 285.84	9.03
018	N 7 976 349.25	E 503 285.92	9.03
019	N 7 976 349.32	E 503 287.62	9.03
020	N 7 976 347.69	E 503 284.48	10.03
021	N 7 976 349.27	E 503 328.15	10.25
022	N 7 976 350.04	E 503 349.68	10.14
023	N 7 976 327.50	E 503 162.63	10.32
024	N 7 976 328.15	E 503 178.42	10.40
025	N 7 976 329.85	E 503 225.58	10.16
026	N 7 976 332.36	E 503 281.19	10.09
027	N 7 976 334.07	E 503 328.7	10.33
028	N 7 976 334.85	E 503 350.24	10.22
029	N 7 976 319.51	E 503 162.97	10.14
030	N 7 976 320.22	E 503 178.71	10.24
031	N 7 976 321.59	E 503 216.77	10.05
032	N 7 976 325.14	E 503 288.95	9.98
033	N 7 976 326.15	E 503 328.98	10.16
034	N 7 976 326.92	E 503 350.48	10.06
035	N 7 976 310.32	E 503 095.05	9.56
036	N 7 976 308.81	E 503 097.35	10.07
037	N 7 976 314.81	E 503 418.90	9.99
038	N 7 976 314.81	E 503 441.25	10.22
039	N 7 976 293.75	E 503 082.57	9.58
040	N 7 976 295.03	E 503 086.93	10.09
041	N 7 976 299.77	E 503 109.32	10.18
042	N 7 976 294.92	E 503 115.68	10.02
043	N 7 976 296.84	E 503 441.25	9.86
044	N 7 976 285.99	E 503 098.90	10.19
045	N 7 976 281.20	E 503 105.30	10.03
046	N 7 976 240.24	E 503 065.95	9.75
047	N 7 976 240.70	E 503 069.79	10.26
048	N 7 976 241.24	E 503 084.78	10.33
049	N 7 976 241.45	E 503 092.77	10.17
050	N 7 976 271.90	E 503 409.61	10.06
051	N 7 976 272.23	E 503 417.54	10.22
052	N 7 976 275.04	E 503 432.41	10.13
053	N 7 976 276.96	E 503 435.54	9.58
054	N 7 976 160.64	E 503 068.72	10.14
055	N 7 976 160.78	E 503 072.67	10.66
056	N 7 976 161.32	E 503 087.66	10.73
057	N 7 976 161.61	E 503 095.55	10.57
058	N 7 976 164.81	E 503 184.31	11.01
059	N 7 976 166.24	E 503 223.78	10.82
060	N 7 976 166.52	E 503 231.48	10.98
061	N 7 976 167.40	E 503 255.90	10.87
062	N 7 976 158.99	E 503 263.43	10.85
063	N 7 976 159.85	E 503 287.41	10.95
064	N 7 976 160.14	E 503 295.34	10.79
065	N 7 976 161.57	E 503 334.92	10.99
066	N 7 976 164.40	E 503 413.57	10.59
067	N 7 976 164.69	E 503 421.42	10.76
068	N 7 976 165.23	E 503 436.40	10.68
069	N 7 976 165.44	E 503 439.85	10.17
070	N 7 976 075.22	E 503 072.51	9.72
071	N 7 976 075.33	E 503 075.75	10.23
072	N 7 976 075.88	E 503 090.74	10.23
073	N 7 976 077.51	E 503 095.14	10.14
074	N 7 976 078.44	E 503 422.34	10.03
075	N 7 976 077.66	E 503 424.55	10.08
076	N 7 976 078.20	E 503 439.54	10.08
077	N 7 976 078.30	E 503 442.29	9.57

SETOUT POINTS FOR UTILITY BERM

POINT No.	NORTHING	EASTING	EL.
UB 01	N 7 976 437.03	E 503 284.76	8.57
UB 02	N 7 976 427.46	E 503 285.11	8.60
UB 03	N 7 976 389.33	E 503 286.48	10.87
UB 04	N 7 976 359.37	E 503 287.73	11.10
UB 05	N 7 976 351.62	E 503 295.95	11.10
UB 06	N 7 976 352.54	E 503 328.03	11.11
UB 07	N 7 976 353.48	E 503 349.56	11.11
UB 08	N 7 976 318.42	E 503 420.86	11.10
UB 09	N 7 976 317.70	E 503 441.39	11.21

MATCHLINE REFER TO DRAWING H349000-2133-10-035-0002

PERMIT TO PRACTICE

HATCH LTD.

Signature: [Signature]

Date: 30 Aug 13

PERMIT NUMBER: P 512

The Association of Professional Engineers, Geologists and Geophysicists of NWT/NTNU



HATCH

Baffinland

MARY RIVER PROJECT

MILNE PORT
ORE STOCKPILES NO. 1 & 2
EARTHWORKS & DRAINAGE - PLAN

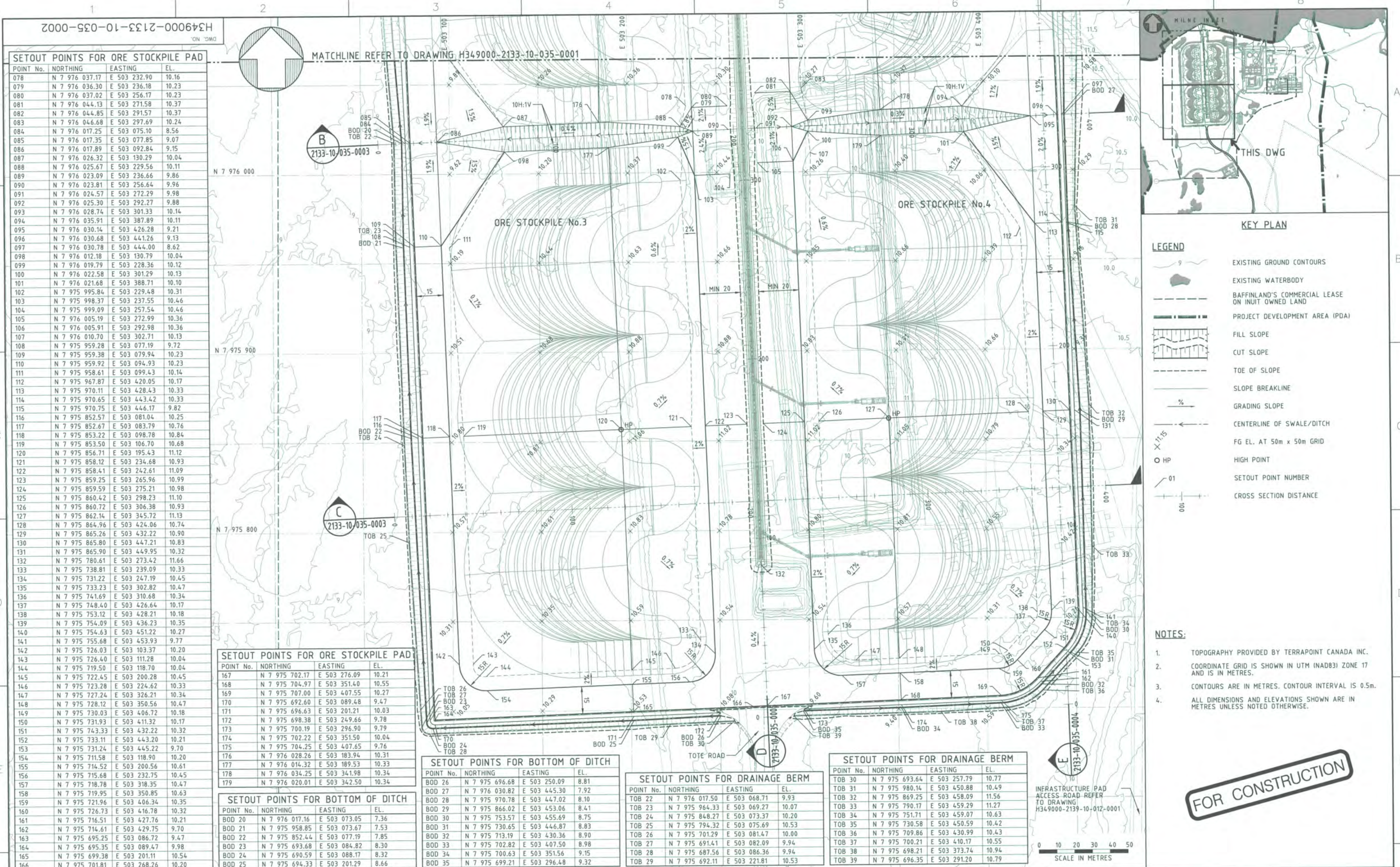
H349000-2133-10-035-0001

SCALE
1:1000
OR AS NOTED

REV. 0

ORIGINAL SHEET SIZE: ISO A1 (841 x 594)

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KEY PLAN

- LEGEND**
- EXISTING GROUND CONTOURS
 - EXISTING WATERBODY
 - BAFFINLAND'S COMMERCIAL LEASE ON INUIT OWNED LAND
 - PROJECT DEVELOPMENT AREA (PDA)
 - FILL SLOPE
 - CUT SLOPE
 - TOE OF SLOPE
 - SLOPE BREAKLINE
 - GRADING SLOPE
 - CENTERLINE OF SWALE/DITCH
 - FG EL. AT 50m x 50m GRID
 - HIGH POINT
 - SETOUT POINT NUMBER
 - CROSS SECTION DISTANCE

- NOTES:**
- TOPOGRAPHY PROVIDED BY TERRAPOINT CANADA INC.
 - COORDINATE GRID IS SHOWN IN UTM (NAD83) ZONE 17 AND IS IN METRES.
 - CONTOURS ARE IN METRES. CONTOUR INTERVAL IS 0.5m.
 - ALL DIMENSIONS AND ELEVATIONS SHOWN ARE IN METRES UNLESS NOTED OTHERWISE.

FOR CONSTRUCTION

HATCH

DESIGNED BY: *[Signature]* DRAWN BY: *[Signature]*
 K. FALLAH M. MCDOUGALD
 DATE 2013-08-23 DATE 2013-08-23
 CHECKED BY: *[Signature]* DISCIPL. ENGR.
 A. MOHLEKANI S. HASSAN
 DATE 2013-08-30 DATE 2013-08-30
 PROJ. DES. COORD. PROJ. ENGR.
 T. THERTELL S. PERRY
 DATE 2013-08-30 DATE 2013-08-30
 PROJ. MGR.
 J. CLELAND
 DATE 2013-08-30

Baffinland

MARY RIVER PROJECT

MILNE PORT
ORE STOCKPILES NO. 3 & 4
EARTHWORKS & DRAINAGE - PLAN

SCALE 1:1000
DWG. NO. H349000-2133-10-035-0002
ORIGINAL SHEET SIZE: ISO A1 (841 x 594)

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Date: 30 Aug 13
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NO. DESCRIPTION BY CHK'D APP'D DATE

REVISIONS

0 CONSTRUCTION SH MM 2013-08-30

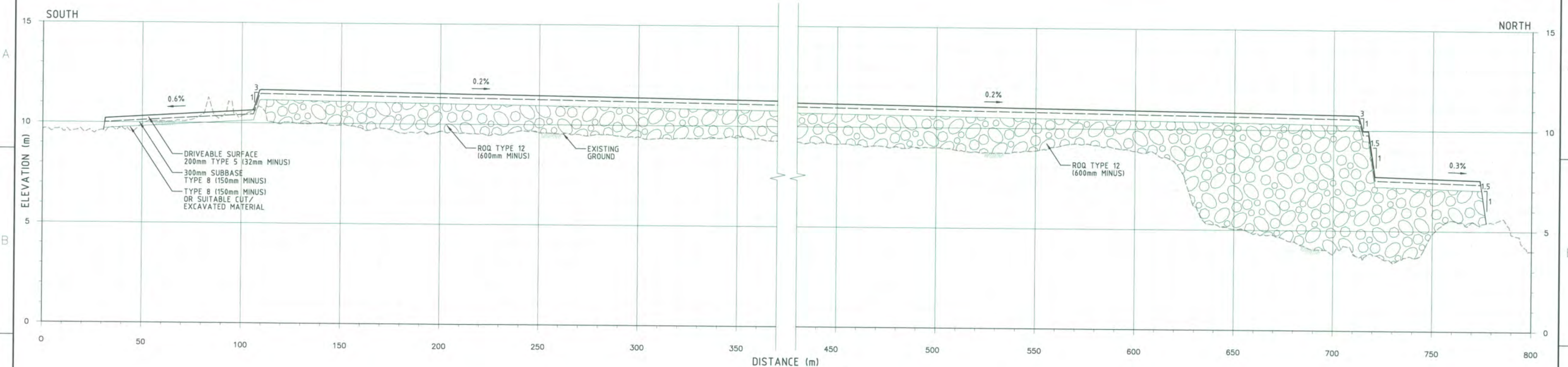
ISSUE AUTHORIZATION

REFERENCE DRAWINGS

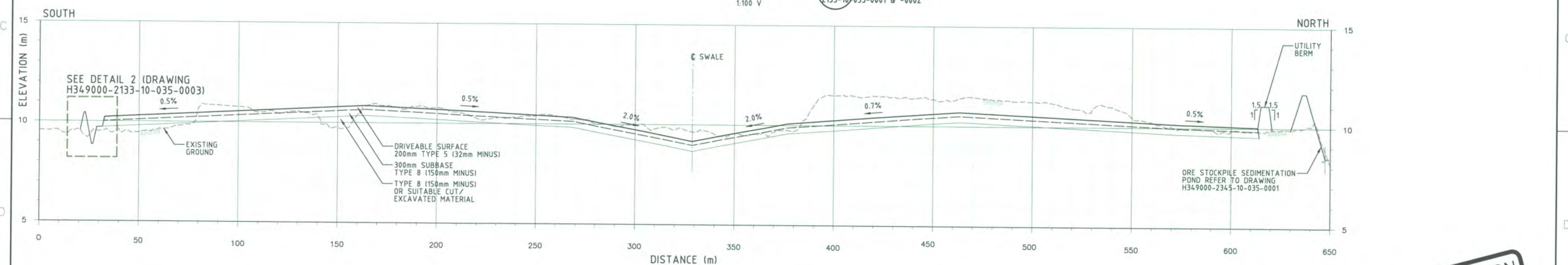
H349000-3000-10-012-0001 TOTE ROAD - PLAN AND PROFILE
 H349000-2000-10-014-0001 MILNE PORT - SITE LAYOUT

H349000-2131-10-035-0004

ON DWG



SECTION D

1:1000 H
1:100 V
2133-10-035-0001 & -0002

SECTION E

1:1000 H
1:100 V
2133-10-035-0001 & -0002

FOR CONSTRUCTION

CULVERT ID	FISH BEARING (P/Y/N)	NUMBER OF PIPES (n)	D (mm)	W (mm)	TYPE	CULVERT @ AT UPSTREAM		U/S INV. ELV. (m)	RIP RAP REQUIRED (Y/N)	CULVERT @ AT DOWNSTREAM		D/S INV. ELV. (m)	RIP RAP REQUIRED (Y/N)	C (mm)	L (m)	S (%)	SKEW DEGREE	LENGTH (m)
						NORTHING	EASTING			NORTHING	EASTING							
MP CV7	N	1	1000	1000	CSP	7 976 284.96	503 439.07	7.16	Y	7 976 326.93	503 437.43	7.04	Y	500	4.2	0.3	92.3	42
MP CV8	N	1	500	500	CSP	7 976 349.79	503 286.98	9.03	Y	7 976 357.01	503 296.57	8.97	Y	300	2.0	.5	-	12

CULVERT SCHEDULE

REFER TO DRAWING H349000-1000-10-041-0003 FOR DETAIL.

LEGEND:

HWL	HIGH WATER LEVEL
ROQ	RUN OF QUARRY
CSP	CORRUGATED STEEL PIPE
FISH BEARING	(P=POTENTIAL, Y=YES, N=NO)
	RUN OF QUARRY MATERIAL TYPE 12 (600mm MINUS) (FOR TOTAL FILL DEPTH > 1.0m)

NOTES:

- TOPOGRAPHY PROVIDED BY TERRAPOINT CANADA INC.
- ALL DIMENSIONS AND ELEVATIONS SHOWN ARE IN METRES UNLESS NOTED OTHERWISE.

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T. FORTIN
DATE: 2013-08-29
PROJ. MGR.
S. PERRY
DATE: 2013-08-29

DRAWN BY: M. MCDUGALD
DATE: 2013-08-23
DISCIP. ENGR.
S. HASSAN
DATE: 2013-08-29
PROJ. ENGR.
J. CLELAND
DATE: 2013-08-29

Baffinland

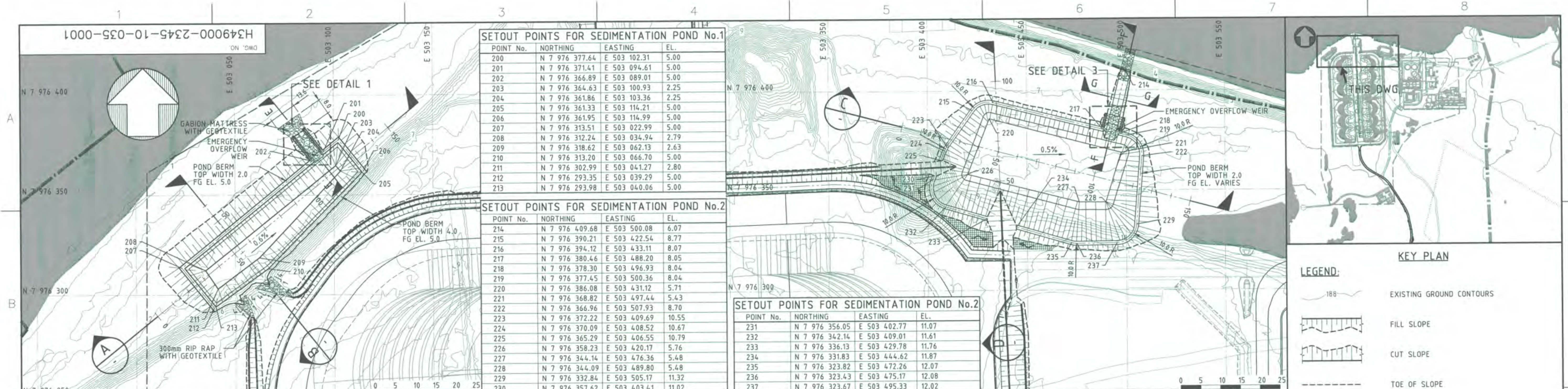
MARY RIVER PROJECT

MILNE PORT
ORE STOCKPILES
EARTHWORKS & DRAINAGE-SECTIONS SHEET 2 OF 2

SCALE: 1:1000
OR AS NOTED

DWG. NO.
H349000-2133-10-035-0004

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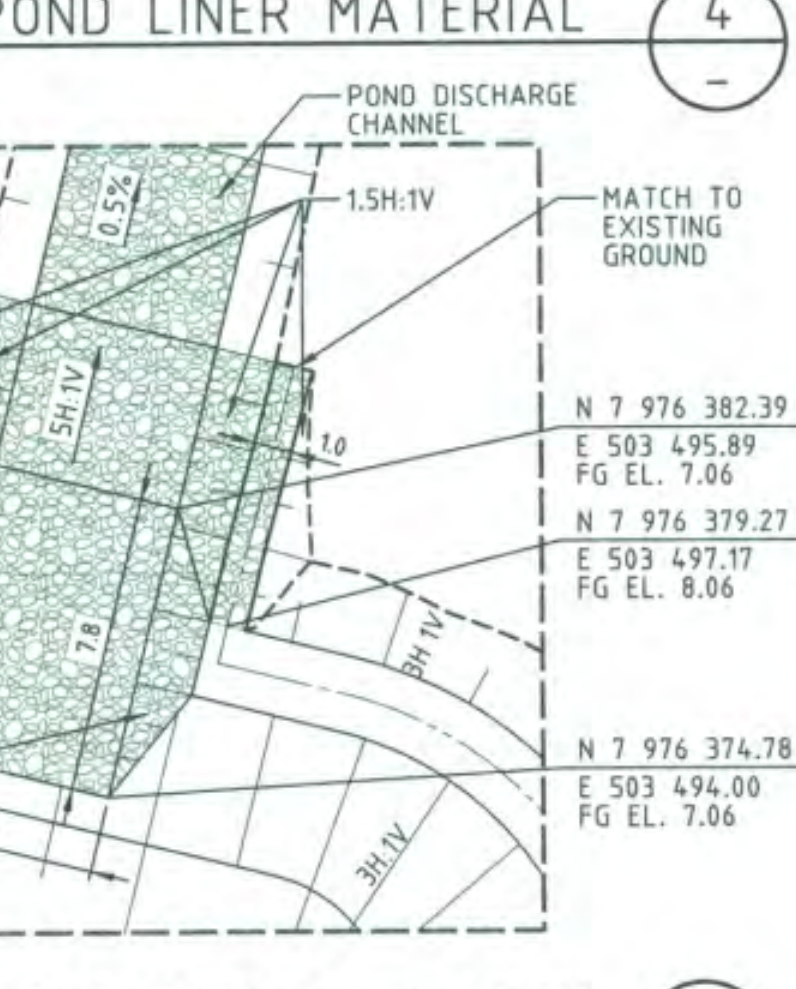
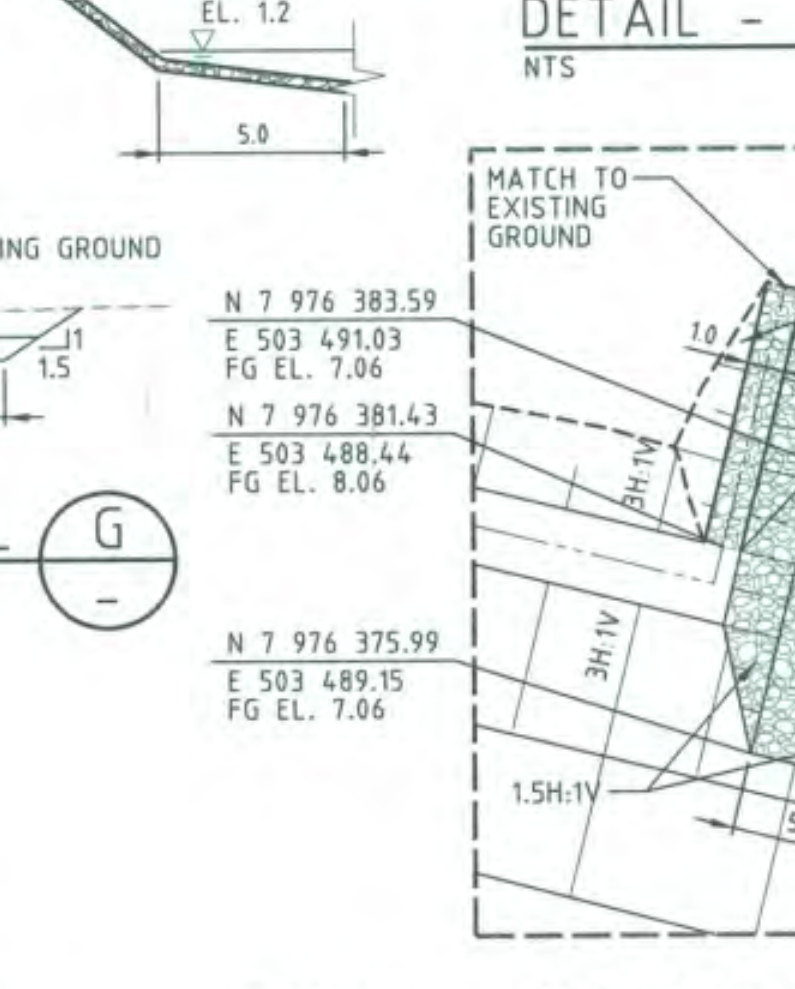
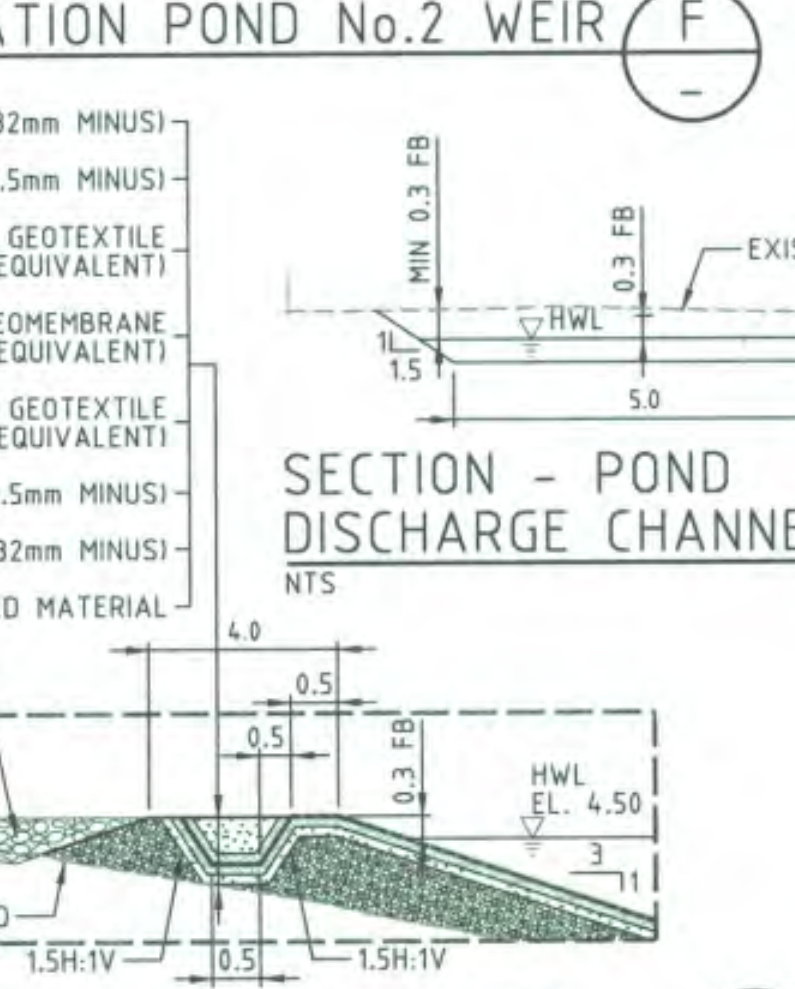
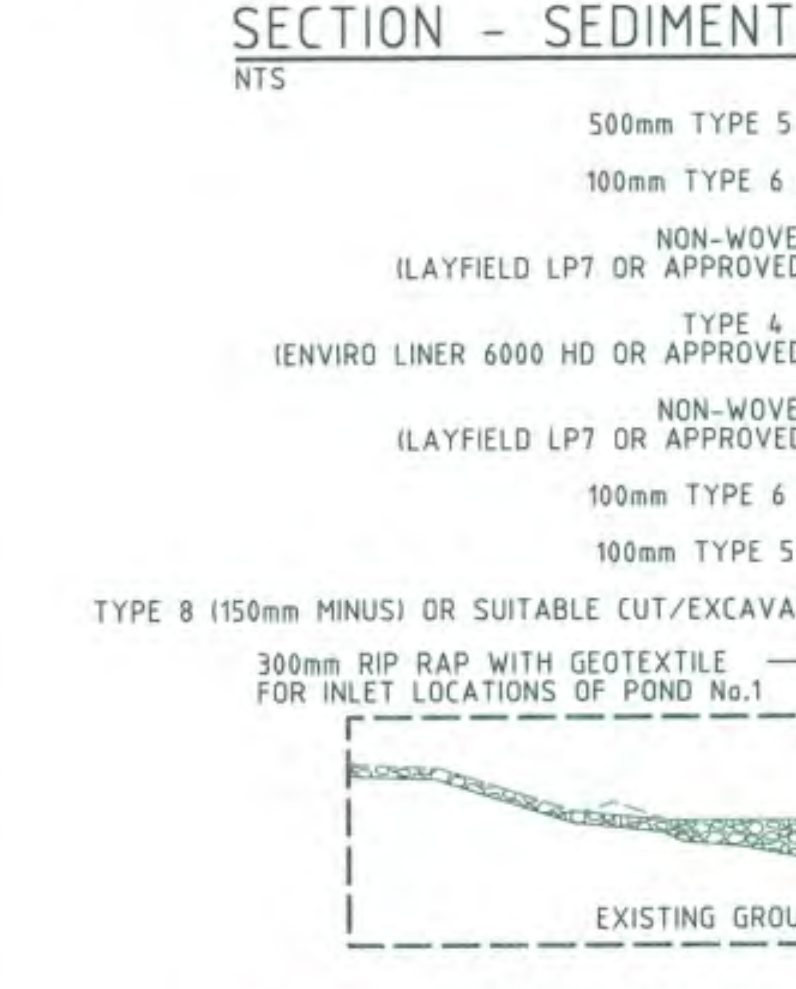
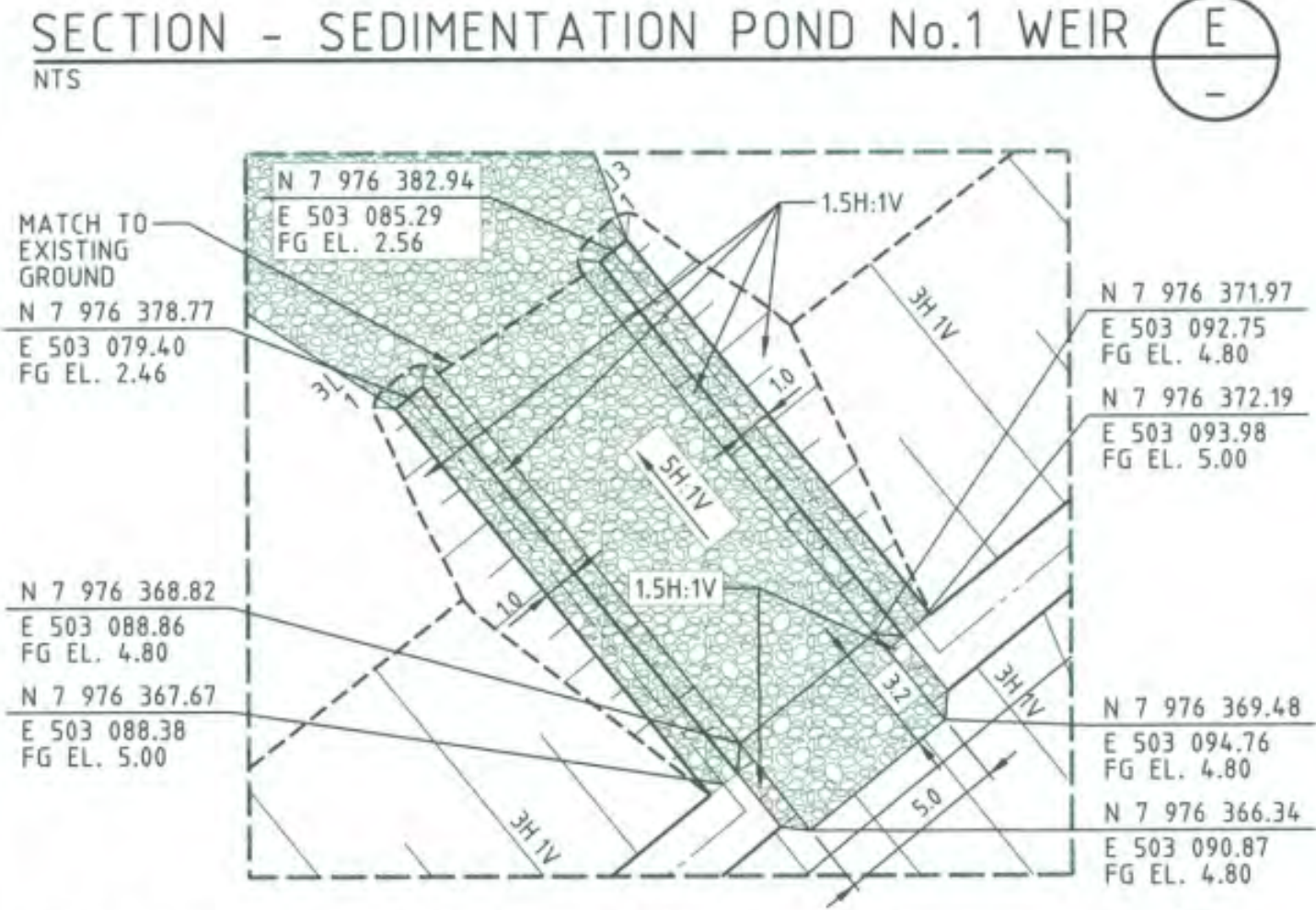
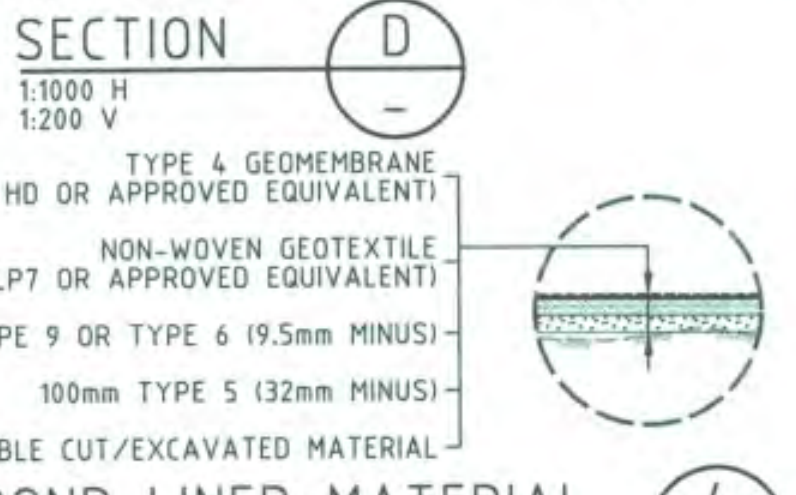
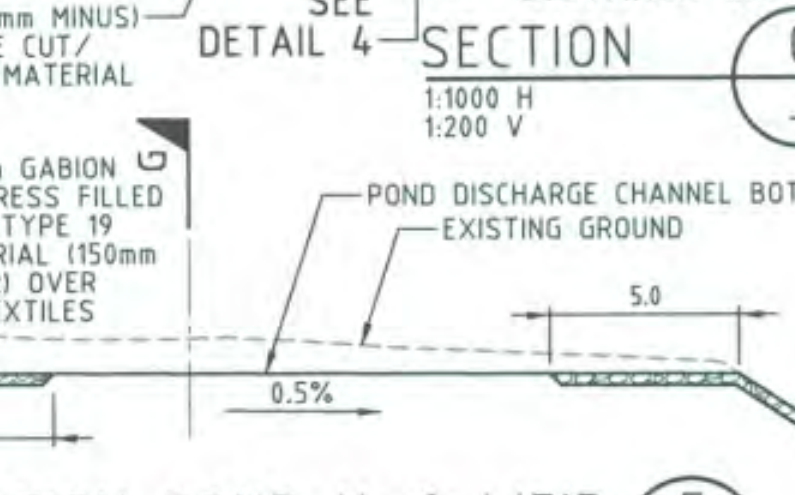
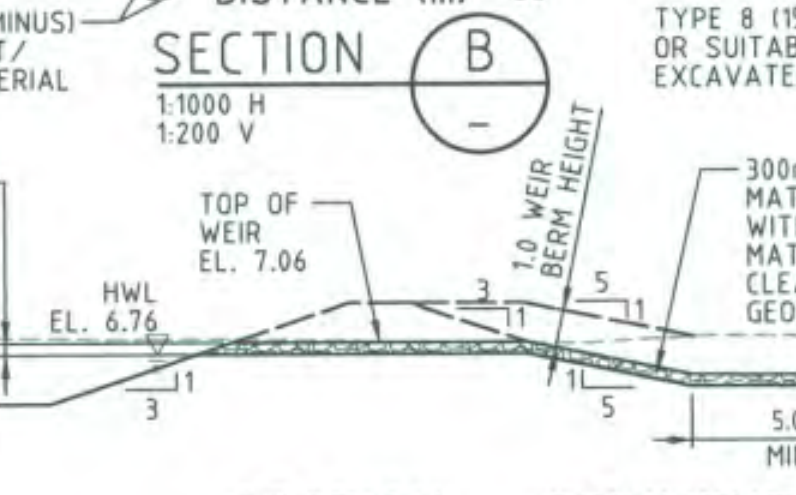
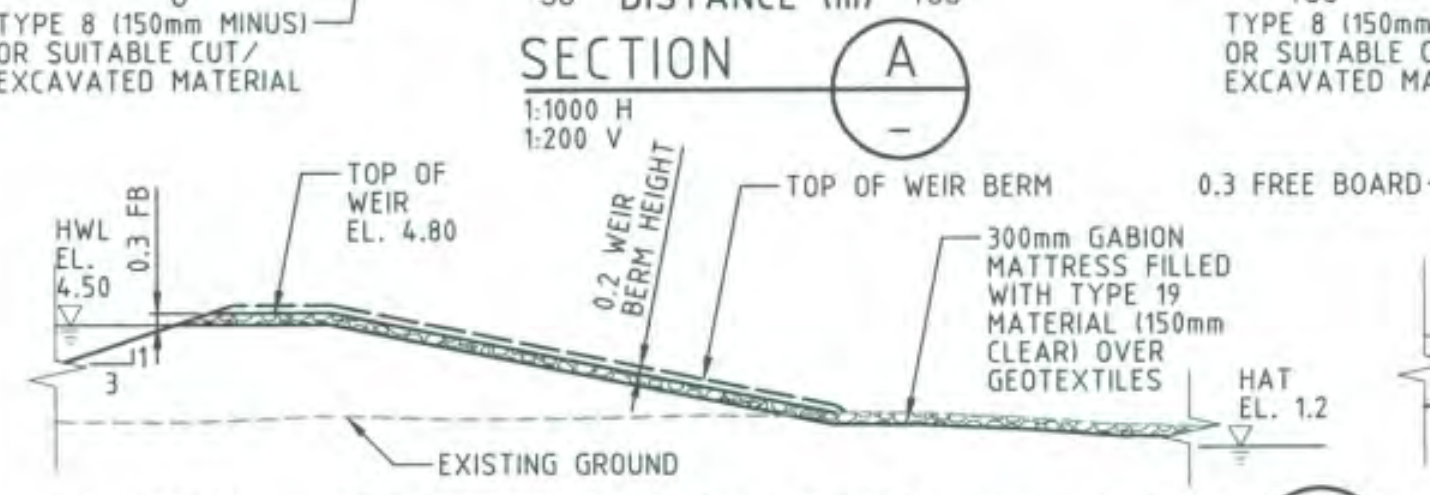
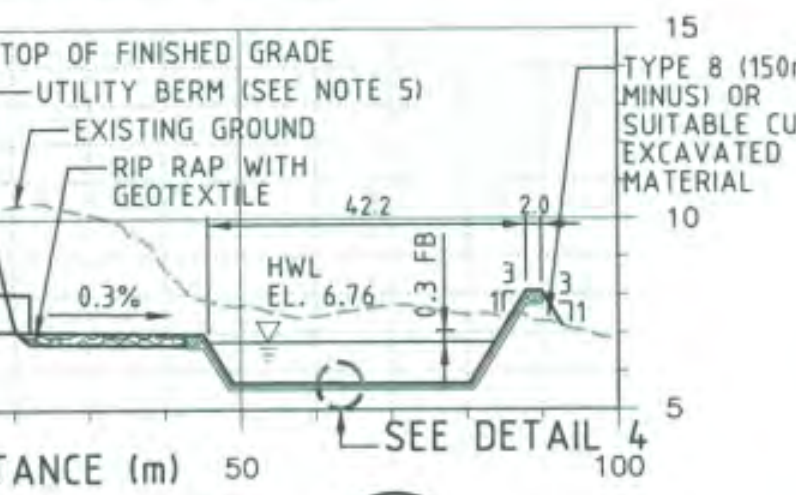
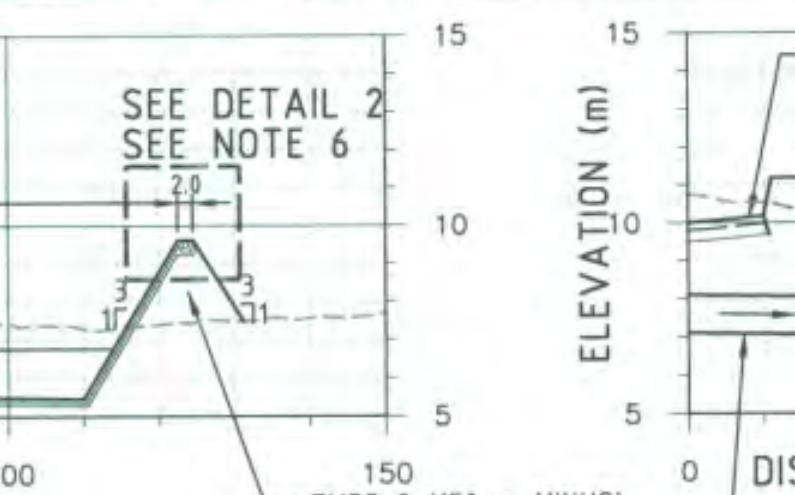
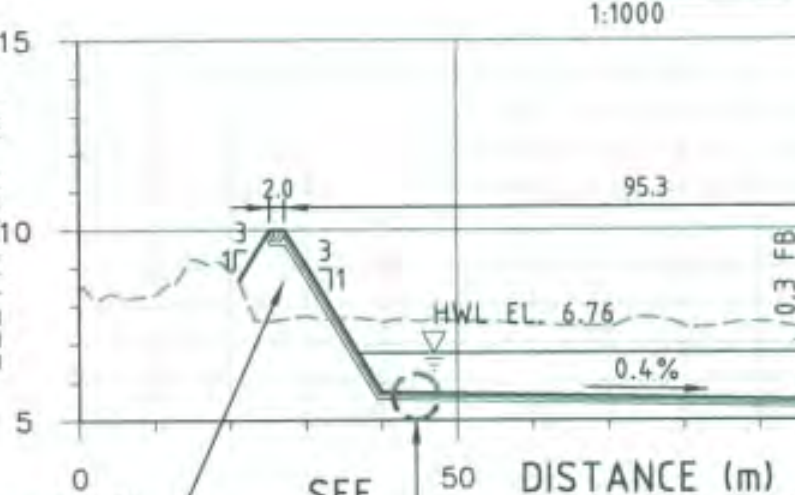
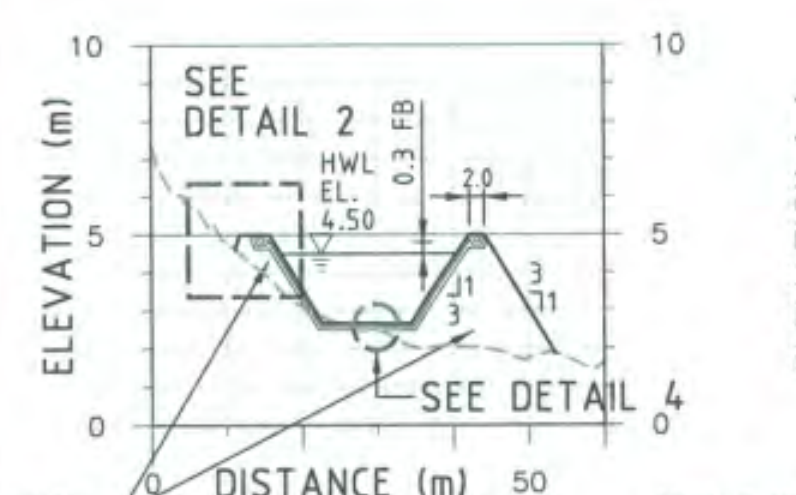
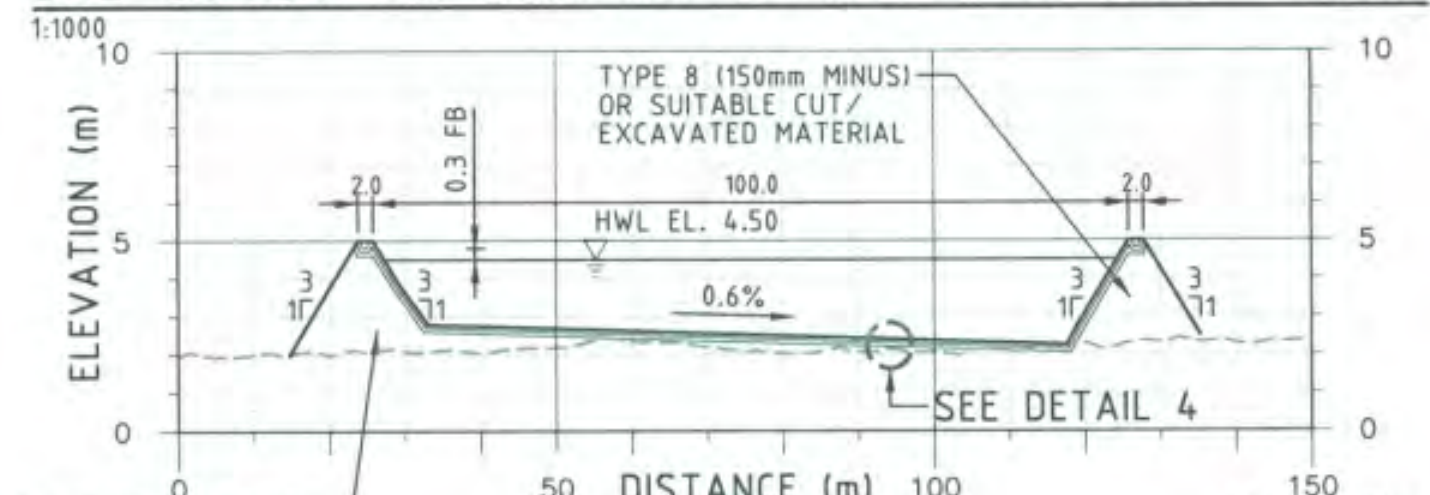
SETOUT POINTS FOR SEDIMENTATION POND No.1			
POINT No.	NORTHING	EASTING	EL.
200	N 7 976 377.64	E 503 102.31	5.00
201	N 7 976 371.41	E 503 094.61	5.00
202	N 7 976 366.89	E 503 089.01	5.00
203	N 7 976 364.63	E 503 100.93	2.25
204	N 7 976 361.86	E 503 103.36	2.25
205	N 7 976 361.33	E 503 114.21	5.00
206	N 7 976 361.95	E 503 114.99	5.00
207	N 7 976 313.51	E 503 022.99	5.00
208	N 7 976 312.24	E 503 034.94	2.79
209	N 7 976 318.62	E 503 062.13	2.63
210	N 7 976 313.20	E 503 066.70	5.00
211	N 7 976 302.99	E 503 041.27	2.80
212	N 7 976 293.35	E 503 039.29	5.00
213	N 7 976 293.98	E 503 040.06	5.00

SETOUT POINTS FOR SEDIMENTATION POND No.2			
POINT No.	NORTHING	EASTING	EL.
214	N 7 976 409.68	E 503 500.08	6.07
215	N 7 976 390.21	E 503 422.54	8.77
216	N 7 976 394.12	E 503 433.11	8.07
217	N 7 976 380.46	E 503 488.20	8.05
218	N 7 976 378.30	E 503 496.93	8.04
219	N 7 976 377.45	E 503 500.36	8.04
220	N 7 976 386.08	E 503 431.12	5.71
221	N 7 976 368.82	E 503 497.44	5.43
222	N 7 976 366.96	E 503 507.93	8.70
223	N 7 976 372.22	E 503 409.69	10.55
224	N 7 976 370.09	E 503 408.52	10.67
225	N 7 976 365.29	E 503 406.55	10.79
226	N 7 976 358.23	E 503 420.17	5.76
227	N 7 976 344.14	E 503 476.36	5.48
228	N 7 976 344.09	E 503 489.80	5.48
229	N 7 976 332.84	E 503 505.17	11.32
230	N 7 976 357.62	E 503 403.41	11.02

SETOUT POINTS FOR SEDIMENTATION POND No.2			
POINT No.	NORTHING	EASTING	EL.
231	N 7 976 356.05	E 503 402.77	11.07
232	N 7 976 342.14	E 503 409.01	11.61
233	N 7 976 336.13	E 503 429.78	11.76
234	N 7 976 331.83	E 503 444.62	11.87
235	N 7 976 323.82	E 503 472.26	12.07
236	N 7 976 323.43	E 503 475.17	12.08
237	N 7 976 323.67	E 503 495.33	12.02

ORE STOCKPILE SEDIMENTATION POND No.1 - PLAN

ORE STOCKPILE SEDIMENTATION POND No.2 - PLAN



KEY PLAN

LEGEND:

- 188 EXISTING GROUND CONTOURS
- FILL SLOPE
- CUT SLOPE
- TOE OF SLOPE
- % GRADING SLOPE
- CROSS SECTION DISTANCE
- FG EL. FINISHED GRADE ELEVATION
- HWL HIGH WATER LEVEL
- HAT HIGHEST ASTRONOMICAL TIDE
- FB FREEBOARD
- GRADE TO FLOW TOWARDS DITCH TO AVOID LOCAL PONDING

NOTES:

- TOPOGRAPHY PROVIDED BY TERRAPoint CANADA INC.
- COORDINATE GRID IS SHOWN IN UTM (NAD83) ZONE 17 AND IS IN METRES.
- CONTOURS ARE IN METRES. CONTOUR INTERVAL IS 2.0m.
- ALL DIMENSIONS AND ELEVATIONS SHOWN ARE IN METRES UNLESS NOTED OTHERWISE.
- FOR UTILITY BERM TYPICAL DETAILS REFER TO DRAWINGS H349000-1000-10-041-0006, -0007 AND -0009.
- APPLY SAME LINER DETAIL AT ALL LOCATIONS.
- POND No.1 MAXIMUM CAPACITY IS 2,660m³ WITH 0.3m FREEBOARD AND HIGH WATER LEVEL (HWL) EL. 4.50m.
- POND No.2 MAXIMUM CAPACITY IS 2,800m³ WITH 0.3m FREEBOARD AND HIGH WATER LEVEL (HWL) EL. 6.76m.

FOR CONSTRUCTION

HATCH

DESIGNED BY: K. FALLAH
DATE: 2013-08-27
CHECKED BY: A. MOHEBKHANI
DATE: 2013-08-30
PROJ. DES. COORD: T. THERTEL
DATE: 2013-08-30
PROJ. MGR: S. PERRY
DATE: 2013-08-30

DRAWN BY: M. MCDUGALD
DATE: 2013-08-27
DISCIP. ENGR: S. HASSAN
DATE: 2013-08-30
PROJ. ENGR: J. CLELAND
DATE: 2013-08-30

Baffinland

MARY RIVER PROJECT

MILNE PORT
ORE STOCKPILE SEDIMENTATION PONDS
EARTHWORKS & DRAINAGE-PLAN & SECTIONS

SCALE: 1:1000
DWG. NO.: H349000-2345-10-035-0001
ORIGINAL SHEET SIZE: ISO A1 (841 x 594)

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REVISIONS

0 CONSTRUCTION SH MM 2013-08-30

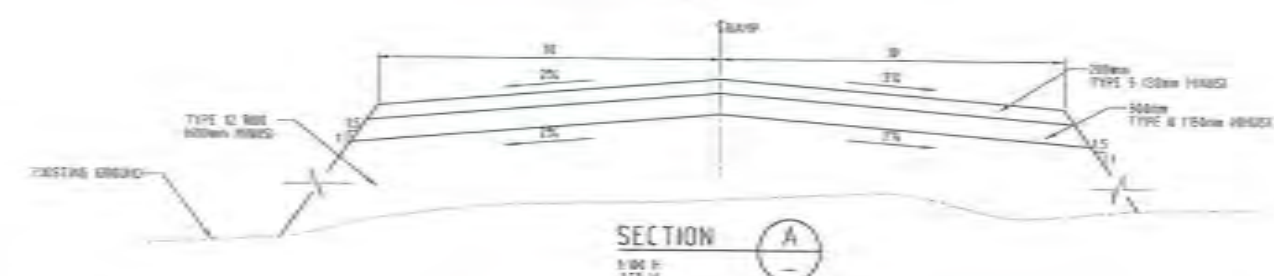
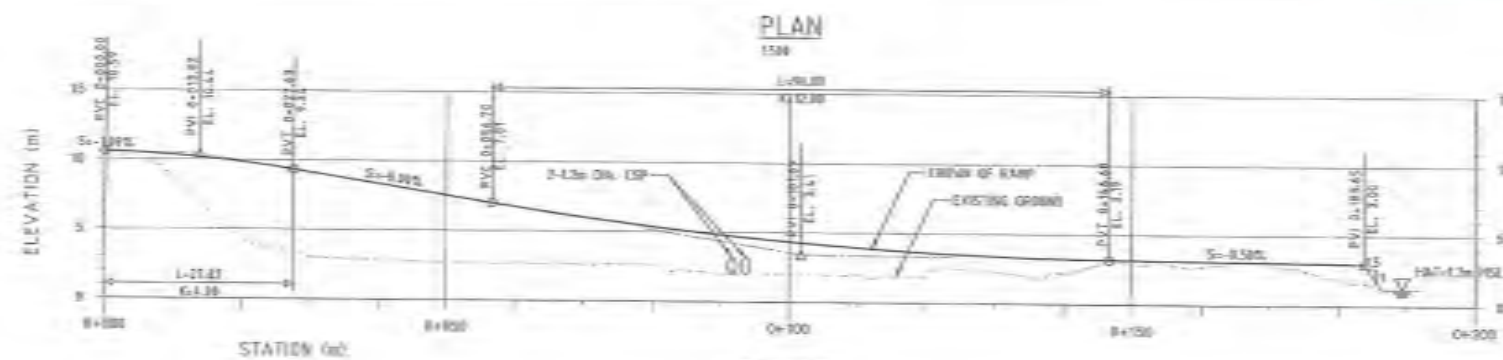
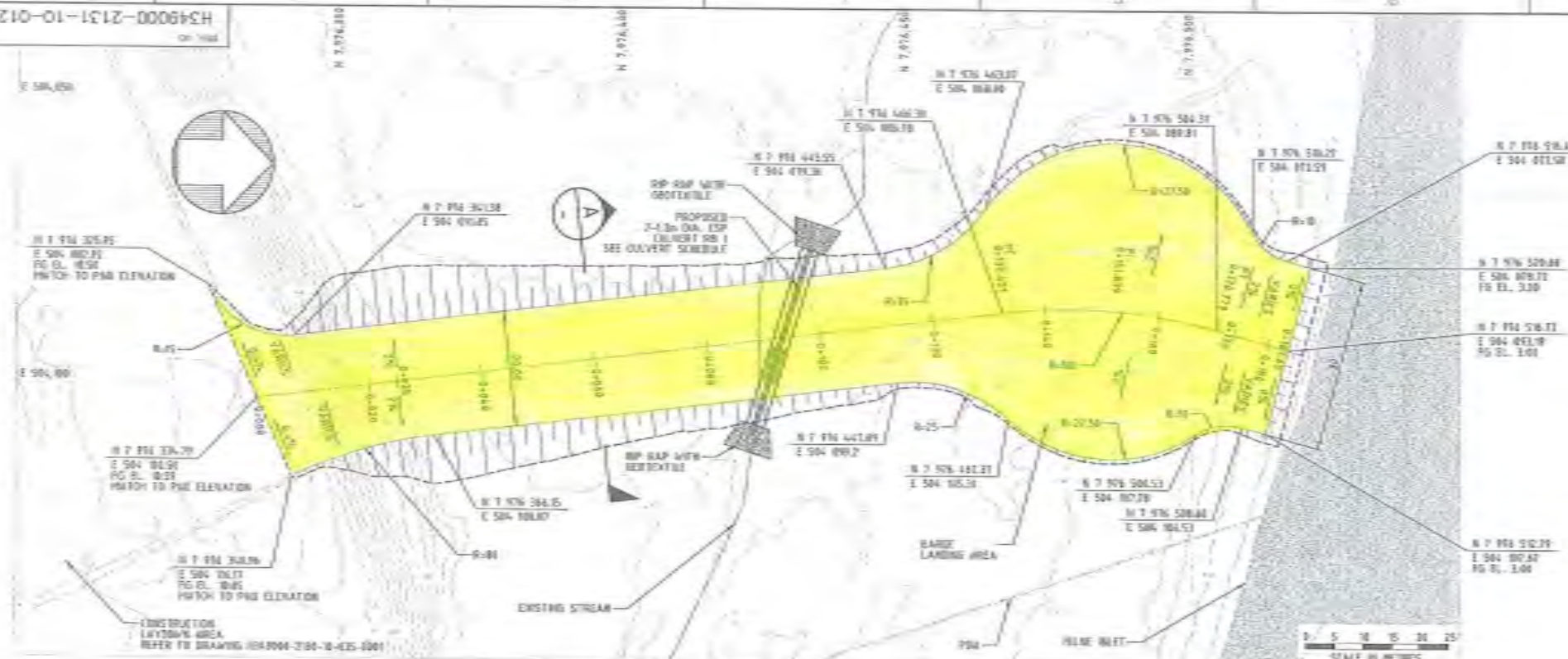
REV. ISSUE FOR AUTH. BY DATE

ISSUE AUTHORIZATION

REFERENCE DRAWINGS

H349000-2133-10-035-0001	MILNE PORT-ORE STOCKPILES No.1&2-EARTHWORKS & DRAINAGE-PLAN
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H349000-2131-10-012-0001



CULVERT ID	FISH PASSING TYPE	NUMBER OF PIPES	B (mm)	M (mm)	TYPE	CULVERT AT UPSTREAM		W/S INV. (m)	CULVERT AT DOWNSTREAM		B/S INV. (mm)	C (mm)	L (mm)	S (mm)	SHW (mm)	LENGTH (m)
						WORKING	CLOSING		WORKING	CLOSING						
RS 1	N	3	1200	2000	CSP	P 114 411.38	584.86/74	220	T 174 430.21	584.86/74	1.80	500	4.0	1.00	13.25	32

CULVERT SCHEDULE

REFER TO DRAWING H349000-2131-10-012-0001 FOR DETAIL

KEY PLAN

LEGEND:

- EXISTING WATERBODY
- EXISTING STREAM
- PROJECT DEVELOPMENT BOUNDARY FROM
- FILL SLOPE
- CUT SLOPE
- TOP OF SLOPE
- GRADING SLOPE
- EXISTING BOUNDARY CONTOURS
- PT POINT OF TANGENT
- PC POINT OF CURVE
- PI POINT OF INTERSECTION
- PVI POINT OF VERTICAL CURVE
- PVI POINT OF VERTICAL INTERSECTION
- PVI POINT OF VERTICAL TANGENT
- ROB RUN OF QUARRY
- HAT HIGHEST ASTROIDEAL TIDE
- MSL MEAN SEA LEVEL
- K BASE OF VERTICAL CURVATURE

NOTES:

- ALL DIMENSIONS AND ELEVATIONS SHOWN ARE IN METRES UNLESS NOTED OTHERWISE.
- TOPOGRAPHY PROVIDED BY TERRAPONT CANADA INC.
- COORDINATE GRID IS SHOWN IN UTM UNITS (ZONE 17 AND 18) IN METRES.
- CONTOURS ARE IN METRES. CONTOUR INTERVAL IS 0.5 METRES.
- SAFETY BORDERS NEED TO BE ADDED AS PER SITE REQUIREMENTS AND REQUEST, AS APPROVED BY COMPANY'S REPRESENTATIVE.
- THE CULVERT UPSTREAM AND DOWNSTREAM LOCATIONS AND INVERT ELEVATIONS ARE BASED ON LIDAR DATA. NO STREAM CROSS-SECTION SURVEY DATA IS AVAILABLE.
- ADJUST CULVERT START AND END COORDINATES AND INVERT ELEVATIONS AT FIELD.
- FLUM DIRECTION MUST BE FROM UPSTREAM TO DOWNSTREAM. PROVIDE AVERAGE STREAM SLOPE ALONG THE CULVERT AS CULVERT SLOPE BASED ON ACTUAL FIELD CONDITIONS.

HATCH

Baffinland

MARY RIVER PROJECT

MILNE PORT RAMP TO BEACH PLAN, PROFILE & SECTION

DWS. NO. H349000-2131-10-012-0001

ORIGINAL SHEET SIZE: ISO A1 (841 x 594)

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H349000-4133-10-035-0001

SETOUT POINTS FOR PLATEAU

POINT No.	NORTHING	EASTING	EL.
PG 01	7 7 913 108.70	E 561 479.91	198.43
PG 02	7 7 913 103.68	E 561 499.45	198.78
PG 03	7 7 913 104.75	E 561 758.61	191.25
PG 04	7 7 913 108.00	E 561 753.94	191.12
PG 05	7 7 913 101.18	E 561 760.21	199.16
PG 06	7 7 913 101.64	E 561 760.34	199.25
PG 07	7 7 913 101.99	E 561 764.39	198.34
PG 08	7 7 913 102.06	E 561 764.52	198.44
PG 09	7 7 913 102.48	E 561 504.51	190.56
PG 10	7 7 913 104.00	E 561 506.03	190.59
PG 11	7 7 913 109.74	E 561 522.44	190.88
PG 12	7 7 913 104.49	E 561 481.49	196.64
PG 13	7 7 913 109.36	E 561 704.97	197.36
PG 14	7 7 913 105.16	E 561 706.72	197.57
PG 15	7 7 913 108.87	E 561 706.71	199.16
PG 16	7 7 913 107.47	E 561 708.93	197.89
PG 17	7 7 913 105.47	E 561 754.89	199.82
PG 18	7 7 913 103.49	E 561 751.61	199.27
PG 19	7 7 913 103.96	E 561 756.09	199.37
PG 20	7 7 913 105.01	E 561 501.36	195.41
PG 21	7 7 913 102.18	E 561 501.74	195.48
PG 22	7 7 913 104.08	E 561 507.24	195.71
PG 23	7 7 913 107.91	E 561 501.24	195.71
PG 24	7 7 913 109.25	E 561 505.91	195.77
PG 25	7 7 913 108.44	E 561 501.05	195.85
PG 26	7 7 913 108.25	E 561 501.03	194.21
PG 27	7 7 913 104.06	E 561 402.61	195.25
PG 28	7 7 913 104.15	E 561 401.34	194.31
PG 29	7 7 913 102.79	E 561 401.72	194.45
PG 30	7 7 913 104.05	E 561 521.89	194.25
PG 31	7 7 913 104.54	E 561 405.39	194.37
PG 32	7 7 913 102.23	E 561 545.10	194.25
PG 33	7 7 913 100.14	E 561 471.17	194.32
PG 34	7 7 913 101.83	E 561 405.26	191.17
PG 35	7 7 913 104.80	E 561 405.18	191.16
PG 36	7 7 913 104.79	E 561 405.73	198.38
PG 37	7 7 913 105.80	E 561 404.92	194.00
PG 38	7 7 913 103.30	E 561 506.02	194.04
PG 39	7 7 913 105.38	E 561 430.87	194.98
PG 40	7 7 913 105.42	E 561 454.91	195.35
PG 41	7 7 913 108.50	E 561 408.52	194.32
PG 42	7 7 913 108.34	E 561 706.95	197.00
PG 43	7 7 913 108.80	E 561 602.75	194.71
PG 44	7 7 913 107.05	E 561 603.30	194.71

SETOUT POINTS FOR TOP OF BERM

POINT No.	NORTHING	EASTING	EL.
T00 01	7 7 913 101.87	E 561 479.52	200.59
T00 02	7 7 913 101.34	E 561 479.42	199.23
T00 03	7 7 913 103.70	E 561 497.38	191.93
T00 04	7 7 913 106.91	E 561 493.07	198.10
T00 05	7 7 913 102.21	E 561 482.34	199.88
T00 06	7 7 913 104.39	E 561 609.57	190.88
T00 07	7 7 913 101.95	E 561 459.48	198.54
T00 08	7 7 913 109.20	E 561 454.39	198.39
T00 09	7 7 913 105.21	E 561 452.45	198.25
T00 10	7 7 913 109.83	E 561 454.54	198.30
T00 11	7 7 913 107.28	E 561 457.02	198.34
T00 12	7 7 913 109.21	E 561 456.21	198.48
T00 13	7 7 913 100.88	E 561 449.52	197.10
T00 14	7 7 913 107.84	E 561 449.54	197.15
T00 15	7 7 913 107.47	E 561 404.45	197.16
T00 16	7 7 913 107.28	E 561 402.21	196.80
T00 17	7 7 913 106.09	E 561 403.29	196.57
T00 18	7 7 913 102.34	E 561 404.25	196.52
T00 19	7 7 913 102.38	E 561 505.30	196.87
T00 20	7 7 913 105.05	E 561 506.21	195.38
T00 21	7 7 913 104.30	E 561 507.18	195.41
T00 22	7 7 913 105.25	E 561 504.34	194.87
T00 23	7 7 913 104.34	E 561 558.08	194.91
T00 24	7 7 913 104.30	E 561 548.87	194.90
T00 25	7 7 913 104.07	E 561 528.71	194.95
T00 26	7 7 913 103.39	E 561 528.43	193.89
T00 27	7 7 913 102.19	E 561 504.42	193.89
T00 28	7 7 913 106.99	E 561 501.71	193.85
T00 29	7 7 913 104.19	E 561 523.11	193.89
T00 30	7 7 913 101.10	E 561 544.34	193.71
T00 31	7 7 913 104.38	E 561 501.80	193.89
T00 32	7 7 913 104.75	E 561 504.94	194.70
T00 33	7 7 913 104.88	E 561 501.30	194.81
T00 34	7 7 913 101.10	E 561 481.07	195.29
T00 35	7 7 913 101.36	E 561 486.36	195.44
T00 36	7 7 913 101.47	E 561 495.88	196.44
T00 37	7 7 913 101.90	E 561 706.56	197.17
T00 38	7 7 913 101.10	E 561 706.56	196.54
T00 39	7 7 913 101.71	E 561 706.86	196.52
T00 40	7 7 913 104.36	E 561 604.58	198.04
T00 41	7 7 913 104.70	E 561 603.48	198.11

SETOUT POINTS FOR BOTTOM OF DITCH

POINT No.	NORTHING	EASTING	EL.
B00 01	7 7 913 101.55	E 561 480.34	195.89
B00 02	7 7 913 101.54	E 561 484.88	195.57
B00 03	7 7 913 102.24	E 561 483.88	194.76
B00 04	7 7 913 104.57	E 561 574.25	194.85
B00 05	7 7 913 104.99	E 561 545.34	192.62
B00 06	7 7 913 106.71	E 561 520.47	192.50
B00 07	7 7 913 104.34	E 561 506.66	192.50
B00 08	7 7 913 100.98	E 561 503.65	192.47
B00 09	7 7 913 100.48	E 561 524.23	192.39
B00 10	7 7 913 102.38	E 561 544.96	192.29
B00 11	7 7 913 104.58	E 561 542.81	192.71
B00 12	7 7 913 109.24	E 561 548.87	192.75
B00 13	7 7 913 100.25	E 561 548.56	192.88
B00 14	7 7 913 104.58	E 561 520.91	193.89
B00 15	7 7 913 107.34	E 561 405.43	194.29
B00 16	7 7 913 107.20	E 561 405.05	195.42
B00 17	7 7 913 101.10	E 561 705.47	197.31
B00 18	7 7 913 102.86	E 561 604.50	197.91
B00 19	7 7 913 105.08	E 561 704.34	198.00
B00 20	7 7 913 107.30	E 561 704.97	197.75
B00 21	7 7 913 104.61	E 561 704.44	194.05
B00 22	7 7 913 107.19	E 561 705.89	198.84
B00 23	7 7 913 107.42	E 561 705.89	198.84
B00 24	7 7 913 104.47	E 561 702.21	198.09
B00 25	7 7 913 107.83	E 561 604.56	197.25
B00 26	7 7 913 104.25	E 561 603.48	197.21

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SETOUT POINTS FOR ORE STOCKPILE PAD

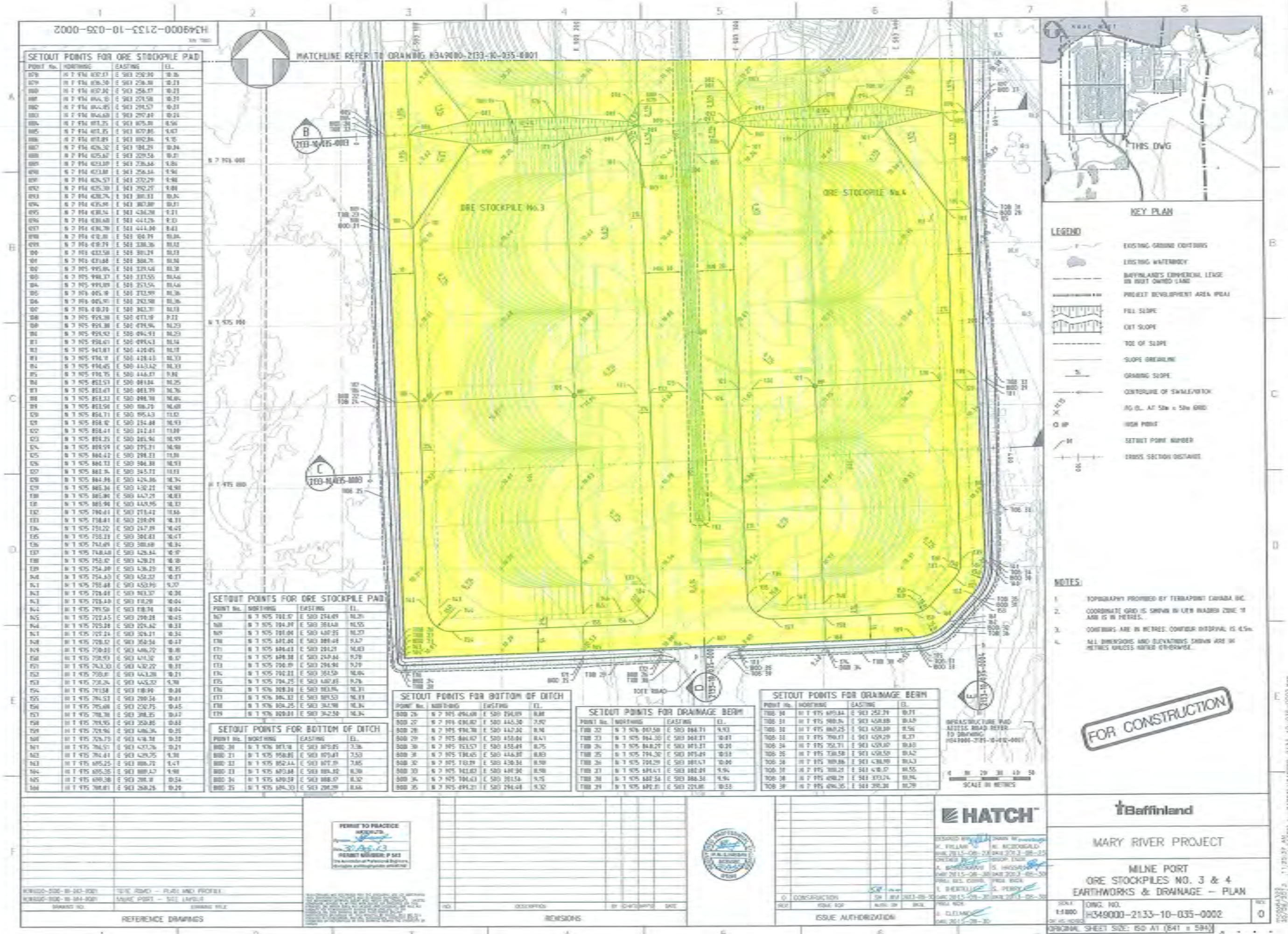
POINT No.	NORTHING	EASTING	EL.
001	6 7 976 443.84	1 943 232.75	1.23
002	6 7 976 443.81	1 943 230.76	1.23
003	6 7 976 443.78	1 943 228.77	1.23
004	6 7 976 443.75	1 943 226.78	1.23
005	6 7 976 443.72	1 943 224.79	1.23
006	6 7 976 443.69	1 943 222.80	1.23
007	6 7 976 443.66	1 943 220.81	1.23
008	6 7 976 443.63	1 943 218.82	1.23
009	6 7 976 443.60	1 943 216.83	1.23
010	6 7 976 443.57	1 943 214.84	1.23
011	6 7 976 443.54	1 943 212.85	1.23
012	6 7 976 443.51	1 943 210.86	1.23
013	6 7 976 443.48	1 943 208.87	1.23
014	6 7 976 443.45	1 943 206.88	1.23
015	6 7 976 443.42	1 943 204.89	1.23
016	6 7 976 443.39	1 943 202.90	1.23
017	6 7 976 443.36	1 943 200.91	1.23
018	6 7 976 443.33	1 943 198.92	1.23
019	6 7 976 443.30	1 943 196.93	1.23
020	6 7 976 443.27	1 943 194.94	1.23
021	6 7 976 443.24	1 943 192.95	1.23
022	6 7 976 443.21	1 943 190.96	1.23
023	6 7 976 443.18	1 943 188.97	1.23
024	6 7 976 443.15	1 943 186.98	1.23
025	6 7 976 443.12	1 943 184.99	1.23
026	6 7 976 443.09	1 943 182.99	1.23
027	6 7 976 443.06	1 943 180.99	1.23
028	6 7 976 443.03	1 943 178.99	1.23
029	6 7 976 443.00	1 943 176.99	1.23
030	6 7 976 442.97	1 943 174.99	1.23
031	6 7 976 442.94	1 943 172.99	1.23
032	6 7 976 442.91	1 943 170.99	1.23
033	6 7 976 442.88	1 943 168.99	1.23
034	6 7 976 442.85	1 943 166.99	1.23
035	6 7 976 442.82	1 943 164.99	1.23
036	6 7 976 442.79	1 943 162.99	1.23
037	6 7 976 442.76	1 943 160.99	1.23
038	6 7 976 442.73	1 943 158.99	1.23
039	6 7 976 442.70	1 943 156.99	1.23
040	6 7 976 442.67	1 943 154.99	1.23
041	6 7 976 442.64	1 943 152.99	1.23
042	6 7 976 442.61	1 943 150.99	1.23
043	6 7 976 442.58	1 943 148.99	1.23
044	6 7 976 442.55	1 943 146.99	1.23
045	6 7 976 442.52	1 943 144.99	1.23
046	6 7 976 442.49	1 943 142.99	1.23
047	6 7 976 442.46	1 943 140.99	1.23
048	6 7 976 442.43	1 943 138.99	1.23
049	6 7 976 442.40	1 943 136.99	1.23
050	6 7 976 442.37	1 943 134.99	1.23
051	6 7 976 442.34	1 943 132.99	1.23
052	6 7 976 442.31	1 943 130.99	1.23
053	6 7 976 442.28	1 943 128.99	1.23
054	6 7 976 442.25	1 943 126.99	1.23
055	6 7 976 442.22	1 943 124.99	1.23
056	6 7 976 442.19	1 943 122.99	1.23
057	6 7 976 442.16	1 943 120.99	1.23
058	6 7 976 442.13	1 943 118.99	1.23
059	6 7 976 442.10	1 943 116.99	1.23
060	6 7 976 442.07	1 943 114.99	1.23
061	6 7 976 442.04	1 943 112.99	1.23
062	6 7 976 442.01	1 943 110.99	1.23
063	6 7 976 441.98	1 943 108.99	1.23
064	6 7 976 441.95	1 943 106.99	1.23
065	6 7 976 441.92	1 943 104.99	1.23
066	6 7 976 441.89	1 943 102.99	1.23
067	6 7 976 441.86	1 943 100.99	1.23
068	6 7 976 441.83	1 943 98.99	1.23
069	6 7 976 441.80	1 943 96.99	1.23
070	6 7 976 441.77	1 943 94.99	1.23
071	6 7 976 441.74	1 943 92.99	1.23
072	6 7 976 441.71	1 943 90.99	1.23
073	6 7 976 441.68	1 943 88.99	1.23
074	6 7 976 441.65	1 943 86.99	1.23
075	6 7 976 441.62	1 943 84.99	1.23
076	6 7 976 441.59	1 943 82.99	1.23
077	6 7 976 441.56	1 943 80.99	1.23
078	6 7 976 441.53	1 943 78.99	1.23
079	6 7 976 441.50	1 943 76.99	1.23
080	6 7 976 441.47	1 943 74.99	1.23
081	6 7 976 441.44	1 943 72.99	1.23
082	6 7 976 441.41	1 943 70.99	1.23
083	6 7 976 441.38	1 943 68.99	1.23
084	6 7 976 441.35	1 943 66.99	1.23
085	6 7 976 441.32	1 943 64.99	1.23
086	6 7 976 441.29	1 943 62.99	1.23
087	6 7 976 441.26	1 943 60.99	1.23
088	6 7 976 441.23	1 943 58.99	1.23
089	6 7 976 441.20	1 943 56.99	1.23
090	6 7 976 441.17	1 943 54.99	1.23
091	6 7 976 441.14	1 943 52.99	1.23
092	6 7 976 441.11	1 943 50.99	1.23
093	6 7 976 441.08	1 943 48.99	1.23
094	6 7 976 441.05	1 943 46.99	1.23
095	6 7 976 441.02	1 943 44.99	1.23
096	6 7 976 440.99	1 943 42.99	1.23
097	6 7 976 440.96	1 943 40.99	1.23
098	6 7 976 440.93	1 943 38.99	1.23
099	6 7 976 440.90	1 943 36.99	1.23
100	6 7 976 440.87	1 943 34.99	1.23

SETOUT POINTS FOR DRAINAGE BERM

POINT No.	NORTHING	EASTING	EL.
1001	6 7 976 443.84	1 943 232.75	1.23
1002	6 7 976 443.81	1 943 230.76	1.23
1003	6 7 976 443.78	1 943 228.77	1.23
1004	6 7 976 443.75	1 943 226.78	1.23
1005	6 7 976 443.72	1 943 224.79	1.23
1006	6 7 976 443.69	1 943 222.80	1.23
1007	6 7 976 443.66	1 943 220.81	1.23
1008	6 7 976 443.63	1 943 218.82	1.23
1009	6 7 976 443.60	1 943 216.83	1.23
1010	6 7 976 443.57	1 943 214.84	1.23
1011	6 7 976 443.54	1 943 212.85	1.23
1012	6 7 976 443.51	1 943 210.86	1.23
1013	6 7 976 443.48	1 943 208.87	1.23
1014	6 7 976 443.45	1 943 206.88	1.23
1015	6 7 976 443.42	1 943 204.89	1.23
1016	6 7 976 443.39	1 943 202.90	1.23
1017	6 7 976 443.36	1 943 200.91	1.23
1018	6 7 976 443.33	1 943 198.92	1.23
1019	6 7 976 443.30	1 943 196.93	1.23
1020	6 7 976 443.27	1 943 194.94	1.23
1021	6 7 976 443.24	1 943 192.95	1.23
1022	6 7 976 443.21	1 943 190.96	1.23
1023	6 7 976 443.18	1 943 188.97	1.23
1024	6 7 976 443.15	1 943 186.98	1.23
1025	6 7 976 443.12	1 943 184.99	1.23
1026	6 7 976 443.09	1 943 182.99	1.23
1027	6 7 976 443.06	1 943 180.99	1.23
1028	6 7 976 443.03	1 943 178.99	1.23
1029	6 7 976 443.00	1 943 176.99	1.23
1030	6 7 976 442.97	1 943 174.99	1.23
1031	6 7 976 442.94	1 943 172.99	1.23
1032	6 7 976 442.91	1 943 170.99	1.23
1033	6 7 976 442.88	1 943 168.99	1.23
1034	6 7 976 442.85	1 943 166.99	1.23
1035	6 7 976 442.82	1 943 164.99	1.23
1036	6 7 976 442.79	1 943 162.99	1.23
1037	6 7 976 442.76	1 943 160.99	1.23
1038	6 7 976 442.73	1 943 158.99	1.23
1039	6 7 976 442.70	1 943 156.99	1.23
1040	6 7 976 442.67	1 943 154.99	1.23
1041	6 7 976 442.64	1 943 152.99	1.23
1042	6 7 976 442.61	1 943 150.99	1.23
1043	6 7 976 442.58	1 943 148.99	1.23
1044	6 7 976 442.55	1 943 146.99	1.23
1045	6 7 976 442.52	1 943 144.99	1.23
1046	6 7 976 442.49	1 943 142.99	1.23
1047	6 7 976 442.46	1 943 140.99	1.23
1048	6 7 976 442.43	1 943 138.99	1.23
1049	6 7 976 442.40	1 943 136.99	1.23
1050	6 7 976 442.37	1 943 134.99	1.23
1051	6 7 976 442.34	1 943 132.99	1.23
1052	6 7 976 442.31	1 943 130.99	1.23
1053	6 7 976 442.28	1 943 128.99	1.23
1054	6 7 976 442.25	1 943 126.99	1.23
1055	6 7 976 442.22	1 943 124.99	1.23
1056	6 7 976 442.19	1 943 122.99	1.23
1057	6 7 976 442.16	1 943 120.99	1.23
1058	6 7 976 442.13	1 943 118.99	1.23
1059	6 7 976 442.10	1 943 116.99	1.23
1060	6 7 976 442.07	1 943 114.99	1.23
1061	6 7 976 442.04	1 943 112.99	1.23
1062	6 7 976 442.01	1 943 110.99	1.23
1063	6 7 976 441.98	1 943 108.99	1.23
1064	6 7 976 441.95	1 943 106.99	1.23
1065	6 7 976 441.92	1 943 104.99	1.23
1066	6 7 976 441.89	1 943 102.99	1.23
1067	6 7 976 441.86	1 943 100.99	1.23
1068	6 7 976 441.83	1 943 98.99	1.23
1069	6 7 976 441.80	1 943 96.99	1.23
1070	6 7 976 441.77	1 943 94.99	1.23
1071	6 7 976 441.74	1 943 92.99	1.23
1072	6 7 976 441.71	1 943 90.99	1.23
1073	6 7 976 441.68	1 943 88.99	1.23
1074	6 7 976 441.65	1 943 86.99	1.23
1075	6 7 976 441.62	1 943 84.99	1.23
1076	6 7 976 441.59	1 943 82.99	1.23
1077	6 7 976 441.56	1 943 80.99	1.23
1078	6 7 976 441.53	1 943 78.99	1.23
1079	6 7 976 441.50	1 943 76.99	1.23
1080	6 7 976 441.47	1 943 74.99	1.23
1081	6 7 976 441.44	1 943 72.99	1.23
1082	6 7 976 441.41	1 943 70.99	1.23
1083	6 7 976 441.38	1 943 68.99	1.23
1084	6 7 976 441.35	1 943 66.99	1.23
1085	6 7 976 441.32	1 943 64.99	1.23
1086	6 7 976 441.29	1 943 62.99	1.23
1087	6 7 976 441.26	1 943 60.99	1.23
1088	6 7 976 441.23	1 943 58.99	1.23
1089	6 7 976 441.20	1 943 56.99	1.23
1090	6 7 976 441.17	1 943 54.99	1.23
1091	6 7 976 441.14	1 943 52.99	1.23
1092	6 7 976 441.11	1 943 50.99	1.23
1093	6 7 976 441.08	1 943 48.99	1.23
1094	6 7 976 441.05	1 943 46.99	1.23
1095	6 7 976 441.02	1 943 44.99	1.23
1096	6 7 976 440.99	1 943 42.99	1.23
1097	6 7 976 440.96	1 943 40.99	1.23
1098	6 7 976 440.93	1 943 38.99	1.23
1099	6 7 976 440.90	1 943 36.99	1.23
1100	6 7 976 440.87	1 943 34.99	1.23

SETOUT POINTS FOR DRAINAGE BENCH

POINT No.	NORTHING	EASTING	EL.
2001	6 7 976 443.84	1 943 232.75	1.23
2002	6 7 976 443.81	1 943 230.76	1.23
2003	6 7 976 443.78	1 943 228.77	1.23
2004	6 7 976 443.75	1 943 226.78	1.23
2005	6 7 976 443.72	1 943 224.79	1.23
2006	6 7 976 443.69	1 943 222.80	1.23



Civil

						
2013-08-28	1	Approved for Use	A. Mohebkhani	S. Hassan	S. Perry	D. Matthews
2013-03-20	0	Approved for Use	A. Mohebkhani	S. Hassan	S. Perry	D. Matthews
DATE	REV.	STATUS	PREPARED BY	CHECKED BY	APPROVED BY	APPROVED BY

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1. Introduction

- The Mary River project site is located in northern Baffin Island, in Nunavut Territory of the Canadian Arctic. The Project currently consists of activities which entail mining high grade iron ore, at a production rate of 3.5 million tonnes per annum, stockpiling it throughout the year at the Milne Port, and shipping the material during the summer months. Development of this Project includes the infrastructure construction and operational activities associated with the Milne Port and Mine Site areas along with upgrading the 100 km Tote Road connecting the two sites. All associated project infrastructure shall be based on a 5 year design life, with the exception of the laydown areas, for which a 1 year design life shall be considered.
- The purpose of this document is to provide the necessary information required for the design of infrastructure at the two project sites (Milne Port and Mine Site). The works covered by this criteria include earthworks, site grading, internal roads, stormwater drainage system and the earthworks for service utilities, to be implemented at the project sites. The design criteria proposed in this document shall be treated as minimum requirements for the intended infrastructure design. Refer to Section 2 of this document for a list of other design criteria and technical design documents from the pertinent disciplines. Where a conflict between the various design criteria occurs, the most stringent shall apply.
- This document is intended to address the key criteria required for the design of site infrastructure.



1.1 Safety

The consideration of personnel safety in all stages of the design, construction and operation is paramount. Prime consideration shall be given to safety and reliability to:

- Maximize health and safety for all personnel.
- Minimize environmental impacts.
- Maximize the security of equipment.

2. Other Project Design Criteria

2.1 This design criteria document shall be read in conjunction with other documents which may already exist or will be developed as the project proceeds. These documents include the following:

- Tote Road Design Criteria (H349000-3100-10-122-0001).
- Structural Design Criteria (H349000-1000-35-122-0001).
- ~~Foundation Design Criteria (H349000-1000-35-122-0002).~~
- Aerodrome Design Criteria (H349000-1000-00-109-0001).
- Layout Design Criteria (H349000-1000-50-122-00030).
- Foundation Design Basis (H349000-1000-30-109-0001) ☐ For Non-Process buildings.



3. Units and Coordinate System

- 3.1 The International System of Units (SI units and prefixes) shall be used for all design calculations and on all drawings.
- 3.2 The grid coordinates shall be based on: projection - Universal Transverse Mercator (UTM) Zone 17 and horizontal datum - NAD 83 Canadian Spatial Reference System (CSRS).
- 3.3 Vertical datum shall be based on the Canadian Geodetic Vertical Datum of 1928 (CGVD28).

4. References

4.1 Codes, Regulations and Standards

- 4.1.1 Unless specifically stated otherwise, civil design shall be based on the applicable sections of the latest revisions of the following codes, specifications, standards, regulations and other reference documents. In addition, the design must comply with all laws or regulations of federal and Nunavut territorial authorities.

4.2 General

- 4.2.1 All applicable federal, territorial (Nunavut) and local laws and regulations.

- OHSA Occupational Health and Safety Act
- CSA Canadian Standards Association
- MHSA Mine Health and Safety Act (Nunavut □ S.N.W.T. 1994)
- OHSR Occupational Health and Safety Regulations
- NBCC National Building Code of Canada (2010)
- ASTM American Society for Testing and Materials
- ASCE American Society of Civil Engineers
- NFPA National Fire Protection Association
- NRC Natural Resources Canada □ Explosives Safety and Security Branch



4.3 Roads

- TAC Transportation Association of Canada □ Geometric Design Guide for Canadian Roads
- AASHTO American Association of State Highway and Transportation Officials
- USBM Design of Surface Mine Haulage Roads □ A Manual (US Department of the Interior, Bureau of Mines)
- MSHA Haul Road Inspection Handbook □ MSHA Document Number PH99-I-4
- MTO Ministry of Transportation, Ontario □ Ontario Traffic Manual



4.4 Stormwater Management

- MOE Ministry of the Environment - Stormwater Management Planning and Design Manual
- MTO Ministry of Transportation, Ontario □ Drainage Manual
- CDA Canadian Dam Association □ Dam Safety Guidelines



4.5 Reference Documents

Reference will be made to/contents have been used from the following documents, articulated during the previous phases of the project, during the development of these criteria:


- H337697-0000-10-122-0001: Stormwater Management and Drainage System Design.
- H337697-6170-10-122-0001: Milne Port Drainage System and Stormwater Management Ponds.
- H337697-6170-10-122-0002: Mine Site Drainage System, Stormwater and Sediment Management.
- H337697-0000-15-124-0004: Geotechnical Data Report □ Infrastructure.
- Standard Specification S311213: □ Quarried Fill Materials.
- Standard Specification S003120: Site Conditions.
- NB 102-181/30-7: Baseline Hydrology Report, Knight Piesold, Jan 04, 2012.
- BIM - Early Revenue Phase Mine Haul Road Design Criteria.
- BIM - Early Revenue Phase Tote Road Design Criteria.
- H349000-3000-00-124-0001: NB102-00181 Bulk Sampling Program □ Road Upgrade Design Summary.
- Final Environmental Impact Statement (FEIS), Mary River Project, February 2012.
- Nunavut Impact Review Board (NIRB) Project Certificate (No.:005), Dec 28, 2012.
- H349000-4221-10-220-0001: Number of Runaway Truck Arresting Provisions for the Mine Haul Road, Project Memo.
- H349000-2133-10-220-0001: Runoff Coefficient for the Milne Port Ore Stockpile Pad, Project Memo.
- H349000-1000-15-122-0001: Geotechnical Design Criteria
- H349000-1000-10-220-0001: Stormwater Sedimentation Pond Design Criteria, Project Memo.
- E349000-1000-00-124-0005: Design Brief □ Milne Inlet Landfarm, November 2012, EBA File E14101174.





5. Site Development

Site development refers to construction of civil infrastructure to support construction and operation of facilities. The following sections list the site development activities and establish criteria that shall be adhered to when carrying out site development design works.

5.1 Site Preparation

- 5.1.1 Construction areas shall be cleared of vegetation, and temporary drainage systems shall be provided prior to construction activities taking place within the proposed areas for the new site facilities.
- 5.1.2 Topsoil and/or existing roots shall be removed to a minimum depth of 150 mm, if required, from all areas where buildings, roads, yards and services are to be constructed, and shall be stockpiled in designated areas. Disposal options shall include on-site reuse, development of a designated stockpile area for disposal, or removal by truck to off-site areas, as instructed by the Company.
- 5.1.3 During the summer months, wetlands or areas with standing water shall be drained and the drying of such shall be promoted prior to construction. Watercourses shall be re-routed with the use of cut-off ditches, or re-aligned engineered channels.
- 5.1.4 Waste material shall be stockpiled in designated areas with the appropriate erosion and sedimentation control measures in place. 

5.2 Earthworks

- 5.2.1 Earthworks is defined as the activity of moving soil and/or rock. Earth-moving activities are required in order to obtain the required design elevations of the ground surface. Earthworks includes cut (if required) and fill for roads, buildings and equipment pads, utility berms, foundation excavation, and construction of ditches, diversion channels and berms, dikes, etc. Earthworks shall be carried out in accordance with the following general guidelines:
- Existing unsuitable soils shall be removed and replaced with suitable material.
 - Fill materials shall be placed and compacted over the proof-rolled subgrade in order to achieve adequate bearing capacities, as required for specific construction activities.
 - Rocks/boulders and similar objects adjacent to areas which shall undergo excavation must be removed or secured, if they potentially endanger workers/machinery.
 - The following criteria shall be used to determine the suitability of the soil for fill:
 - ◆ Satisfactory soil: ASTM D 2487 Soil Classification Groups GW, GP, GM, SW, SP, and, SM, or a combination of these groups; non ice-rich, free of debris, waste, vegetation and other deleterious matter. 
 - ◆ Unsatisfactory soil: According to ASTM D 2487 Soil Classification Groups GC, SC, CL, ML, OL, CH, MH, OH and PT; according to AASHTO M145 Soil Classification Groups A-2-6, A-2-7, A-4, A-5, A-6 and A-7 or a combination of these groups. Also, ice-rich soils or soils containing traces of contamination and/or organic materials. 
 - ◆ Water shall be diverted away from excavations, so it does not saturate the side slopes.

- ♦ If pipes are located in the vicinity of the slopes, erosion control measures shall be in place as mitigation for eventual leaks.
- ♦ No loads, including excavated material, traffic of vehicles or heavy machinery shall be allowed near the crest of the slopes (at a distance equal to the height of the excavation) if the slope-support solutions did not take such loads into account.
- ♦ Dust control measures shall be in place.
- ♦ For delineation of the project development boundaries, the minimum setback from freshwater aquatic environments, including fish-bearing streams and water bodies shall be as per NIRB Project Certification No.005. In general, a minimum 5 m set back shall be provided for non fish-bearing water bodies and streams, due to the potential risks of erosion and slope stability.
- ♦ Culvert installation in fish-bearing streams shall follow DFO guidelines.

5.2.2 Table 5-1 provides the minimum slope ratios that shall be used in cuts/excavations or fills/embankments. It must be noted that specific studies must be carried out by geotechnical engineers, if these slopes are to be modified with the aim of lowering costs of cut and/or fill.

Table 5-1: Minimum Slope Ratios

Type of Earthworks	Layer	Ratio H:V
Permanent unsupported cuts	Overburden (ice-rich)	2:1
	Overburden (non ice-rich)	1.5:1
	Rock (less than 4m)	1:8
Permanent fills (on natural, firm ground)	Granular fill	1.5:1
	Base and Subbase	1.5:1
	Rock fill	1.5:1

Notes:

1. The maximum heights and ratios shall be determined considering slopes with typical geometry and no surcharge.
2. The above-listed parameters serve as minimum requirements, and shall be updated/modified based on confirmation/update of the site-specific conditions and/or geotechnical recommendations, or as per BIM's directions.
3. Any geometry and load condition not covered by the table above shall be reviewed by the geotechnical engineer.
4. The granular fill is assumed to be in a drained condition.
5. If the total fill height is greater than 2 m, geotechnical stability analysis and benching requirements shall be considered on a case-specific basis.
6. For overburden cut/fill heights of greater than 5 m, 1.5 m wide benching with minimum 2% cross slope shall be provided.
7. The absolute minimum fill slope for granular material is 1.5H:1V. However, the desirable slope is 2H:1V.
8. The absolute minimum fill slope for rock fill material is 1.25H:1V. However, the desirable slope is 1.5H:1V.
9. For the haul road, the fill side slopes shall be 2H:1V, depending on the site conditions and slope stability.
10. Stability assessments of some cut and fill slopes may be required.
11. For rock cut heights greater than 4 m, 1H:4V slope shall be used with 2 m wide benching and minimum 2% cross slope at every 6 m.

5.2.3 In general, cut activities in permafrost shall be avoided/minimized. However, cut may be required to reduce large fills and high embankments that may affect/endanger slope stability. In addition, within areas where the cut materials can be reused as fill, the suitability of performing cuts in the native soil shall be reviewed by BIM and the geotechnical engineer for requirements of soil treatment/improvement, including geogrids and geotextiles, prior to implementation into the final design.

5.3 Backfilling

- 5.3.1 The gradation of fill material shall be within the Type 5 (32 mm minus) gradation limit for finish grading, within the Type 8 (150 mm minus) and/or suitable earth fill material gradation limit for rough grading, and Type 12 (600 mm minus) and/or suitable earth fill material gradation limit for the rest of the mass backfill. The surface voids of each layer of Type 12 (i.e. Run-of-quarry material) shall be filled with rock fragments prior to the next layer being placed.



5.4 Site Grading

- 5.4.1 If applicable, finish grade elevations for roads and yards shall be set a minimum of 100 mm below the finish floor elevation of buildings/sheltered areas, with local ramps provided at doorways, as required.



- 5.4.2 Finish grading and yard grading shall be set to slope away from planned structures at a minimum of 0.5% to 2%, and drain to a storm drainage collection system. For very long-run and localized areas, the slope shall be reduced or increased, depending on the existing ground slope and the grading around the buildings and facilities.

- 5.4.3 Site grading shall produce a useable and easily maintainable ground surface, not subject to flooding or erosion. The rough grades and finish grades shall adhere to the following:

- Final road and site grades shall ensure suitable pedestrian and vehicular access to buildings and facilitate adequate drainage of the site.
- Building floor elevations shall be established such that the ground floor of the buildings will not be subject to flooding in the event that the storm drainage system fails.
- Elevations of buildings/sheltered areas shall be established to permit gravity connections into sanitary sewers if possible, to avoid the need for pumps.

5.5 Infrastructure Facilities, Laydown and Ore Stockpile Areas

- 5.5.1 Temporary/permanent equipment and construction material laydown areas shall be provided as per the applicable Contract Drawings. The sizes of the footprints shall be optimized to keep disturbed areas to a minimum and still provide enough room for storage of material/equipment and circulation of mobile cranes/vehicles.

- 5.5.2 The subgrades shall be prepared via cut/fill activities prior to pavement installation/placement. If the height of the subgrade fill is less than 600 mm, Type 8 (150 mm minus) fill shall be used. If the height of the subgrade fill is greater than 600 mm, Type 12 Run-of-quarry (600 mm minus) and/or suitable earth fill material shall be used. The voids of each layer of Type 12 shall be filled with rock fragments prior to placement of the next layer.





- 5.5.3 In general, following attainment of the subgrade, the pavement shall be laid on top, with the following minimum thicknesses/material types for infrastructure facility pads and other areas:


- 300 mm, Type 8 (150 mm minus) subbase.
- 100 mm, Type 5 (32 mm minus) base/wearing surface course.




5.5.4 Depending upon the area and specific requirements such as insulation for permafrost protection, the minimum pavement thicknesses and placement of wearing courses may differ from the above-listed.


5.5.5 There shall be no insulation under ☐fold-away☐and ☐fabric☐buildings constructed on non-frost susceptible ground material (typical for Milne Port). 


5.5.6 Insulation shall be provided under ☐fold-away☐and ☐fabric☐buildings constructed on frost susceptible ground material (typical for Mine Site). 


5.5.7 Frost susceptible and ice-rich soils shall be excavated to the extent required and backfilled with Type 12 Run-of-☐quarry (600 mm minus). Non-frost susceptible soils with no visible ice shall not be excavated. 

5.6 Landfarm

5.6.1 ~~Both the Milne Port and Mine Site landfarms shall be designed as per the criteria listed in Section 3.2 of Annex 5 in the FEIS, Attachment 5: Waste Management Plan for Construction Operation, and Closure; Appendix 10D-4.~~ 




5.6.2 ~~The overall geometry as well as the liner details shall be as per Figure 3, ☐Hydrocarbon Impacted Soils Storage and Landfarm Facility ☐Preliminary Design of Landfarm Facility~~ contained within Attachment 5. 


5.6.3 EBA Engineering Consultants Ltd. has already carried out the design for the Milne Port Landfarm. 


5.6.4 Milne Port and Mine Site Hazardous Waste Containment designs shall be carried out as per environmental requirements. They shall be lined, and shall contain sumps. 

5.7 Milne Port Design High Tide

5.7.1 The design High Tide levels for the Project shall be as follow: 

- The Higher High Water Level (HHWL) for large tides at the Milne Port is ☐2.3 m above Chart Datum (CD) which corresponds to ☐1.1 m above Mean Sea Level (MSL). 
- The Highest Astronomical Tide (HAT) at the Milne Port is ☐2.4m above CD which corresponds to ☐1.2 m above MSL. 
- The Lower Low Water Level (LLWL) for large tides at the Milne Port is ☐0.0 m above CD which corresponds to -1.2 m below MSL. 


5.7.2 The toe of ramp and earthworks pad leading down to the sea lift from the laydown area, including the designated turnaround area at the beach within the Milne Port shall have a design elevation greater than ☐1.2 m above MSL. 

5.7.3 Landing pad elevation at the beach shall be minimum 7☐2.15 m) above the average between the HHWL and LLWL (i.e. ☐3.3 m above CD which corresponds to ☐2.1 m above MSL). 

5.8 Retaining Walls

- 5.8.1 Retaining walls and structures shall be designed based on site-specific conditions. Lateral pressure coefficients for design of retaining walls shall be as per the geotechnical recommendation.
- 5.8.2 Retaining walls shall be avoided to the greatest extent possible. Concrete, gabion walls, crib walls, reinforced earth and/or other systems of retaining structures shall be used, if required.



5.9 Erosion and Sediment Control

- 5.9.1 Erosion and sediment control measures shall be installed as required, in and around the project sites in order to minimize sediment transport off the site.
- 5.9.2 Control measures shall be designed to:
- Minimize the size of disturbed areas.
 - Remove sediments from on-site runoffs prior to the runoff leaving the sites.
 - Prevent sediments from off-site runoffs flowing across disturbed areas.
 - Reduce runoff velocity flowing across the site.
 - Meet local requirements for erosion and sediment control plans as defined in the FEIS.
- 5.9.3 A minimum set back of 30 m from fish-bearing streams and lakes or water bodies shall be provided. Any exception to this shall be consulted with and approved by the Project's environmental team. 

5.10 Construction and Permanent Fencing

- 5.10.1 Chain link fence, where required, shall be galvanized, with a minimum height of 1.8 m.
- 5.10.2 Two strands of barbed wire shall be bracketed off the top of the fence for safety reasons, where required by the Company.
- 5.10.3 Fencing within the sites shall be provided as required and as directed by the Company.

5.11 Explosives Magazine Pads and Earth Barricades

- 5.11.1 Explosives magazine pads shall be designed as per the criteria in Section 5.5 of this document. 
- 5.11.2 Geometry of the Explosives Magazine Earth Barricades shall be designed in accordance with the  Quantity-Distance Principles Manual from the Natural Resources Canada, Explosives Safety and Security Branch.

6. Road Design

6.1 General

- 6.1.1 The access roads at the two project sites may be temporary or permanent. An access road is defined as temporary if it will be used only during the construction period, including site predevelopment or site capturing. If an access road will be used during the operational period as well, it is defined as permanent. A 100 km roadway provides access from the Mine Site to the Milne Port (Tote Road), the design criteria for which is included in a separate document. In addition, there is a mine haul road along with internal site roads at the Mine Site, and internal site roads only within the Milne Port, in order to accommodate the mining operations.
- 6.1.2 The design and construction of mine haul roads, access and internal site roads at the project sites shall provide a safe environment for construction, operations and maintenance personnel, and shall facilitate the mining operations, ore transport and port operations in an efficient manner. In addition, the design shall comply with the relevant standards, guidelines, acts, approvals, permits, and other contractual environmental requirements of Baffinland as defined in Section 2 of this document.

6.2 Road Category

- 6.2.1 For the purposes of this design criteria, the roads are classified in three categories:
- **Mine Haul Roads** - The purpose of this type of road is for the mining operation at the mine site - hauling of ore from the open pit to the crusher pad and for maintenance purposes, from the crusher pad to the maintenance building. The mine haul road shall be segregated from the other project roads for safety considerations, and shall comply with the applicable Nunavut MHSA.
 - **Permanent Access and Internal Site Roads** – These roads provide two way access to and link the various facilities/areas within each site, where B-Trains will travel in both directions.
 - **Facility Service Roads** – These roads provide two way access to various facilities/areas within each site, where light vehicles will travel in both directions.
 - **Tote Road** – 100 km road providing access from the Mine Site to the Milne Port.

6.3 Design Vehicle

- 6.3.1 The following design vehicles shall be utilized for the design of the associated project roadways:
- CAT 777G Haul Truck for the Mine Haul Road.
 - B-Train (12 axle) for Permanent Access Roads and Internal Plant Roads (150 metric tonnes payload) that need to be utilized by the Tote Road trucks.
 - CAT 740B for Waste Rock Drainage Pond/Berm.
 - Other types of design vehicles have been used for the remainder of the Project roadways and a fire truck has been considered as the minimum design vehicle for fire access routes.



6.4 Geometric Design Criteria

6.4.1 All roads shall be designed as gravel roads and shall accommodate the design vehicle specified in Section 6.3 of this document. The roads' geometric design parameters are specified below.

Table 6-1: Geometric Design Criteria

Road Type	Permanent Internal Plant Road	Infrastructure Facility Service Road	Haul Road – Open Pit to Crusher Pad	Waste Rock Dump Road	Haul Road Switchback	Truck Escape Ramps
Number of Lanes	2	2	2	1	2	1
Design Speed (km/h)	30	30	50	30	30	90
Posted Speed (km/h)	20	20	40	20	20	-
Total Road Width (m)	9.2	8 or 6	20	13	20	9
Minimum Horizontal Curve C/L Radius (m)	35	35	100	50	35	280
Minimum Intersection Inner Radius (m)	15	15	30	30	30	-
Minimum Cross Slope (%)	2	2	3	3	3	3
Maximum Grade (%)	10	10	10	10	8	20
Minimum K Value (Vertical Sag Curve)	8	8	12	8	8	3
Minimum K Value (Vertical Crest Curve)	4	4	16	4	4	-
Maximum Super-elevation (%)	4	4	4	4	4	6
Minimum Vertical Clearance	7	5	9	9	9	-

Notes:

- The road design parameters are based on the desirable design speeds. Specific parameters such as the minimum turn radii may be modified for some areas locally on a case-by-case basis, via adjustment of the design speeds.
- The Haul Road width shall be based on the Nunavut Mine Health and Safety Act which requires a minimum travel width three times the width of the widest haulage vehicle for dual lane traffic and two times the width of the widest haulage vehicle for single lane traffic.
- Shoulder barriers (safety berms or guardrails) for the Haul Road shall be based on the Nunavut Mine Health and Safety Act which requires shoulder barriers of at least the height of the largest tire of any vehicle using the road and shall be provided along the edge of the haul road wherever a drop-off greater than 3.0m exists. For CAT 777G, the shoulder barrier (safety berm or guardrail) height shall be 2.0 m based on standard tire 27.00 R49 (E4).
- Total road width includes shoulder width and snow allowance but doesn't include the safety berm width for the haul road.
- For the single lane Haul Road from the crusher pad to the maintenance building, pullouts shall be provided at every 100m.
- Widening shall be provided in roadway curves as necessary.
- Need for geotextiles or geogrids shall be considered on a case-specific basis.
- For the Tote Road design criteria, refer to H349000-3100-10-122-0001.
- Provide safety stations, emergency ramps or escape lanes in accordance with the local and mine safety requirements. Hatch will only provide two escape ramps at the most critical locations as per BIM's instruction. Escape ramp design shall be carried out as per the USBM manual.
- For cut/fill heights of greater than 5 m, provide 1.5 m wide benching with minimum 2% cross slope at every 5 m.
- The ramp leading down to the sea lift from the laydown area at the Milne Port shall have a maximum grade of 8%.
- The maximum grade for ramps to the buildings is 6%.
- Fill toe key shall be provided in areas where the existing ground is steeper than 3H:1V away from the road.
- Design speeds may be reduced locally if needed.

6.4.2 The following general rules shall apply to the geometric design of the project roads:

- Roadway grades shall not exceed the maximum grades specified in Table 6-1, except for short ramps which shall be considered on a case-specific basis.
- Signage shall be provided for speed and caution at steep horizontal and/or vertical curves, and where the design criteria cannot be met.
- Light poles, traffic signs and shoulder barriers (safety berms or guardrails), shall be placed at the outer edges of the roads, as required.

6.5 Pavement Design

6.5.1 The design of pavement structures requires information such as the expected pavement service life, design vehicle traffic volume, loads, and geotechnical information such as soil type and California Bearing Ratio (CBR).

6.6 Pavement Thickness

6.6.1 For the project internal site roads, the subgrades shall be prepared via cut/fill activities prior to pavement installation/placement. If the height of the subgrade fill is less than 600 mm, Type 8 (150 mm minus) material shall be used. If the height of the subgrade fill is greater than 600 mm, Type 12 Run-of-quarry and/or suitable earth fill material shall be used. The voids of each layer of Type 12 material shall be filled with rock fragments prior to placement of the next layer.



6.6.2 The following minimum internal site road pavement thicknesses shall be used throughout the project:

- 300 mm, Type 8 (150 mm minus) subbase.
- 100 mm, Type 5 (32 mm minus) base/surface course for low speed light vehicle traffic roads and low speed B-Train traffic roads.
- 200 mm, Type 5 (32 mm minus) base/surface course for medium to high speed B-Train traffic roads.



6.6.3 The following minimum haul road pavement thicknesses shall be used throughout the project:

- 300 mm, Type 8 (150 mm minus) subbase.
- 300 mm, Type 8 (150 mm minus) base.
- 200 mm, Type 5 (32 mm minus) base/surface course.
- ~~900 mm, Type 12 Run-of-Mine structural subgrade (varies depending on the actual site conditions).~~



6.6.4 The ramp and earthworks pad leading down to the sea lift from the laydown area, including the designated turnaround area at the beach within the Milne Port shall contain the following pavement thickness:

- 300 mm, Type 8 (150 mm minus) subbase.
- 200 mm, Type 5 (32 mm minus) base/surface course.
- ~~100 mm Type 3 (19 mm minus) wearing course.~~



6.6.5 Pavement Service Life

6.6.5.1 The service life of the site pavements, prior to any structural rehabilitation work being required, shall be 5 years, unless noted otherwise for specific items.

6.6.6 Design Vehicles, Traffic Volume and Load

6.6.6.1 Vehicle types have been selected for the project roads based on the expected usage and transportation requirements of the area (Section 6.3).

6.6.6.2 All pavement, slabs, bridges, trenches, trench covers and underground installations accessible to trucks shall be designed to withstand the load associated with an HS 20-44 wheel load or its equivalent, as defined by the American Association of State Highway and Transportation Officials (AASHTO) under Standard Specification for highway bridges. However, within areas of special equipment operation, this shall be considered as per the actual vehicle loading.

6.7 Parking

6.7.1 Parking areas shall be designed to accommodate their intended use. In general, all parking areas shall be surfaced with granular materials.

6.7.2 Vehicle parking area design shall adhere to the following:

- The area shall be graded to direct stormwater away from the parking.
- Alignment and gradients shall be coordinated with the grading plans to control drainage.
- Walking distance from parking areas shall be kept to a minimum.
- Barrier-free parking spaces as well as walkways shall be provided according to the applicable regulations.
- Designated turnaround areas shall be provided at dead ends.
- Parking lot design criteria shall be as shown in Table 6-2.

Table 6-2: Parking Lot Design Criteria


Topic	Criteria
Gradient	Maximum 5% Minimum 0.5% Optimum 2%
Cross Slope	Maximum 5% Minimum 2% Optimum 3%
Pavement Structure	300 mm Type 8 (150 mm minus) subbase 100 mm Type 5 (32 mm minus) base/wearing surface course 50mm wearing course
Parking Stall Dimensions	Driving Lane <ul style="list-style-type: none"> • Width 7.5 m Standard

Topic	Criteria
	<ul style="list-style-type: none"> • Depth 6 m • Width 2.75 m Barrier-free <ul style="list-style-type: none"> • Depth 6 m • Width 3.5 m • Access Aisle Width 1.5 m



6.8 Signage




- 6.8.1 Traffic control signs and road edge markers shall be provided as required to ensure safe movement in and about the site.
- 6.8.2 Direction and information signs for both vehicle and pedestrian traffic shall be provided for parking areas, restricted areas, shipping and receiving.
- 6.8.3 Primary identification signs shall be free-standing and sited according to the applicable standards as listed in Section 4.3.
- 6.8.4 Other signs shall be free-standing, fence-mounted or wall-mounted.
- 6.8.5 Security signs shall be provided at the sites and along the site property boundaries.
- 6.8.6 Signs for the site access roads shall be compliant with the local traffic regulations.
- 6.8.7 Signs shall be lighted, if deemed necessary.
- 6.8.8 All signs and pavement markings (if applicable) shall be well maintained during the construction and operational periods.

6.9 Bollards


- 6.9.1 Bollards, if required, shall be provided at building entrances and around hazardous areas such as tanks and transformers. Bollards shall be 1.2 m high, 150 mm diameter schedule 40 CS pipes. 
- 6.9.2 Bollards shall be filled with concrete.
- 6.9.3 Bollards shall be painted and coated such that they provide clear reflection off of vehicle headlights.

6.10 Shoulder Barriers (Safety Berms/Guardrails)

- 6.10.1 Shoulder barriers (earth safety berms or guardrails) shall be provided where a 3.0 m or more drop-off exists at the edge of roads. 
- 6.10.2 ~~Shoulder barriers shall be installed where the horizontal distance from the edge of a travelled lane to an obstruction is less than 1.0 m.~~ 


- 6.10.3 Earth/safety berms for the Mine Haul Road from the open pit to the crusher pad and from the crusher pad to the maintenance building shall have heights of 2.0 m, and side slopes of 1H:1V. 
- 6.10.4 Safety berms for the internal roads shall have heights of 1.0 m and side slopes of 1H:1V. 
- 6.10.5 Discontinuous openings shall be provided in berms at maximum 25 m spacing for drainage and snow clearance, with openings smaller than half the blade width of vehicles constructing or maintaining the berms. 
- 6.10.6 Runaway vehicle collision berms or escape lanes shall be provided in accordance with industry requirements as described in the Nunavut MHSA.

6.11 Utility Berms

- 6.11.1 Utility Berms shall travel along the project roadways to the greatest extent possible, shall be of trapezoidal cross-sections, shall be minimum 0.6 m high from the road edge or the existing ground, and shall have maximum fill side slopes of 1.5H:1V, as validated by the geotechnical engineer. They shall be constructed with the use of 300 mm of granular Type 8 (150 mm minus) and 100 mm of granular Type 5 (32 mm minus) material. If the height of the subgrade fill is less than 600 mm, Type 8 (150 mm minus) fill shall be used. If the height of the subgrade fill is greater than 600 mm, Type 12 Run-of-quarry and/or suitable earth fill material shall be used. The voids of each layer of Type 12 material shall be filled prior to placement of the next layer. The top width of utility berms will depend on the pipe and cable duct sizes. Utility berms shall cross roadway intersections through utility sleeves. After crossing the intersections, they shall resume the alignments within the utility berms. 

7. Stormwater Management System

7.1 Internal Surface Drainage

- 7.1.1 The general criteria for the site internal stormwater management system are described below.
- All interior site grading and roads shall be designed to provide continuous overland flow without erosion to a drainage ditch system.
 - All drainage ditches should be of trapezoidal cross sections, where possible. 
 - Ditches shall be designed to convey a 1 in 25 year flood event.
 - Provision must be made to ensure that there is a safe flow path for events up to the 1 in 100 year event, such that the runoff will not flood key mining areas, cause significant erosion, pick up excessive contaminants or cause other significant problems.
 - Ditch freeboard, minimum depth, minimum width, side slope, longitudinal slope and maximum permissible velocities shall be as per Table 7-2.
 - Minimum set back distance of structures from top of drainage ditch slopes shall be 3 m.
 - Roof and yard drainage shall be collected in open ditches.

- Rip rap shall be provided at locations throughout the storm drainage system which are susceptible to erosion, including ditch sections subject to high-velocities (greater than 1.5 m/s), sections of super critical flow, ditch outlets, storm sewers outfalls, and culverts inlets and outlets.
- If the ditch is in rock, no rip rap is required.
- Energy dissipaters shall be used where the flow velocities may reach values high enough to cause severe erosion or hydraulic jumps.

7.2 External Surface Drainage

Criteria for drainage of the external area are as follow:

- Runoff from undisturbed areas surrounding the mine site shall be collected in perimeter ditches and diverted around and/or through the site perimeter.
- To the extent possible, these perimeter ditches shall be designed to discharge at locations that best retain the characteristics of the existing (i.e. pre-development) natural drainage patterns.
- Diversion ditches shall be designed to convey the 1 in 100 year flood event.
- Ditch freeboard, minimum depth, minimum width, side slope, longitudinal slope and maximum permissible velocities shall be as per Table 7-2.

7.2.1 Peak Flow Estimation

- **For catchment areas greater than 0.5 km²:**

Runoff peak flow estimation shall be based on the following equations developed by Knight Piñold Consulting:

$$Q_2 = 1.1 A^{0.79}$$

$$Q_5 = 1.7 A^{0.77}$$

$$Q_{10} = 2.0 A^{0.76}$$

$$Q_{25} = 2.6 A^{0.75}$$

$$Q_{100} = 3.5 A^{0.73}$$

$$Q_{200} = 3.9 A^{0.73}$$

Where:

Q = peak flow instantaneous flow in m³/s

A = drainage area in km² (0.5 km² ≤ A ≤ 1000 km²)

- **For catchment areas less than 0.5 km²:**

The Rational Method shall be used for peak flow estimation, as follows:

$$Q = 0.28 CIA$$

Where:

Q = peak instantaneous flow in m³/s

A = drainage area in km²



C = runoff coefficient = 0.90 (for all drainage areas except the Milne Port Ore Stockpile footprint, for which C = 0.0, as per BIM's instructions).

I = rainfall intensity corresponding to the time of concentration (mm/hr), estimated using Table 7-1 below.

- Time of Concentration shall be computed with the modified Kirpich equation:

$$T_c = 0.06628 (L^{0.77}/S^{0.385})$$

Where:

T_c = time of concentration (hours)

L = main channel length (km)

S = main channel slope (m/m)

Minimum T_c = 10 min

7.3 Rainfall Intensity

- 7.3.1 Table 7-1 displays the Intensity-Duration-Frequency data which shall be used for peak flow runoff approximation, developed by Knight Piesold consulting:

Table 7-1: Rainfall Intensity (mm/h)

Duration	2 yrs	5 yrs	10 yrs	15 yrs	20 yrs	25 yrs	50 yrs	100 yrs	200 yrs
5 min	9.5	12.0	14.0	15.1	15.9	16.5	18.3	20.1	22.0
10 min	7.2	9.0	10.5	11.3	11.9	12.4	13.7	15.1	16.5
15 min	6.0	7.5	8.7	9.4	9.9	10.3	11.4	12.6	13.7
30 min	5.0	6.3	7.3	7.9	8.3	8.6	9.5	10.5	11.4
1 hr	4.0	5.2	6.1	6.6	7.0	7.3	8.1	9.0	9.9
2 hr	3.0	3.9	4.6	5.0	5.2	5.5	6.1	6.8	7.4
6 hr	2.0	2.7	3.3	3.6	3.9	4.0	4.6	5.1	5.7
12 hr	1.3	1.8	2.2	2.4	2.6	2.7	3.1	3.4	3.8
24 hr	1.0	1.4	1.7	1.9	2.0	2.1	2.4	2.7	3.0

- 7.3.2 Figure 7-1 displays the 200 year design storm distribution:

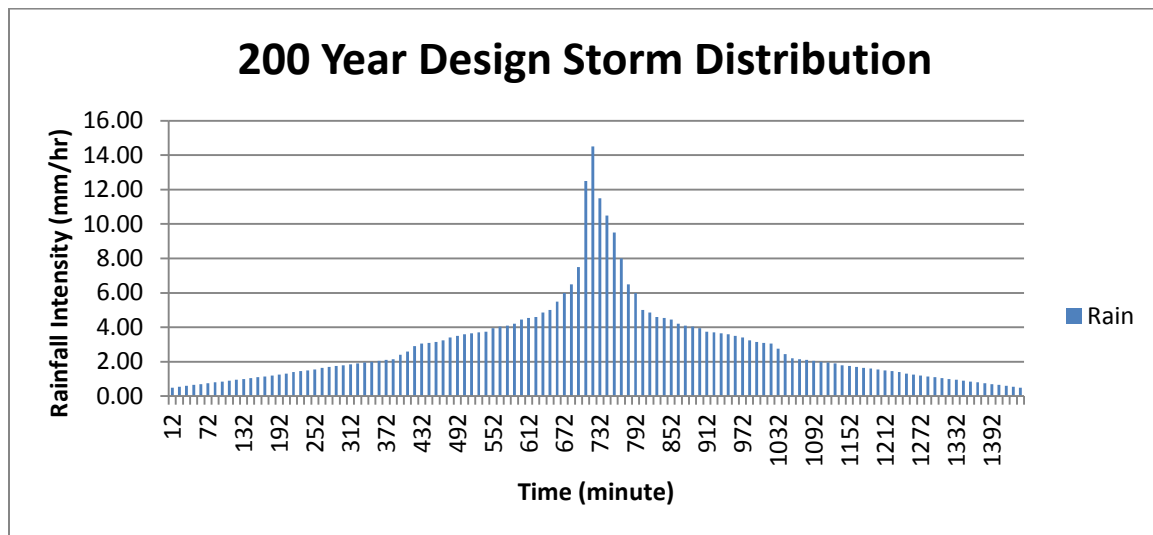


Figure 7-1: 200 Year Storm Distribution

7.3.3 The 200 year 24-hour balanced storm depth is 71 mm.

7.4 Sedimentation Ponds

7.4.1 Sedimentation ponds shall only be provided at the Milne Port Ore Stockpile area, Mine Site Crushing and Screening area and the Mine Site Waste Rock Drainage area. For all other areas, including infrastructure facility pads, laydown areas and roads, the water is considered to be clean and no sedimentation ponds shall be provided.

7.4.2 The general design criteria for the project sedimentation ponds are as follow:

- Ponds shall be sized based on 1 in 10 year, 24 hour design storm volumes.
- Runoff coefficient to estimate runoff shall be 0.9 for all drainage areas except the Milne Port Ore Stockpile footprint, for which the runoff coefficient shall be 0.0 as per BIM's instructions.
- Sedimentation shall be for Total Suspended Solids (TSS) ≤ 30 mg/l for a single sample and TSS ≤ 15 mg/l for the monthly average.
- Sedimentation ponds shall contain emergency overflow weirs of sufficient capacity to safely convey a 1 in 200 year return period storm event or the Probable Maximum Flood (PMF), maximum wind-induced waves, or unexpected operational difficulties.
- Emergency overflow weirs shall be designed to handle applicable design storms, such that the pond high water level does not increase past the set freeboard elevation.
- Emergency overflow weirs shall be designed as broad-crested weirs with rip rap.
- Gabion mattresses shall be provided at the downstream locations of emergency overflow weirs as energy dissipation measures to protect against erosion.
- The following broad-crested weir capacity flow equation shall be used for sizing the Project emergency overflow weirs:

$Q = CLH^{3/2}$ Where:

Q = Peak instantaneous flow (m^3/s)

C = Weir discharge coefficient

L = Width of weir (m)

H = Depth of flow (m), measured 2.5H upstream of the weir discharge point

- Deep sedimentation ponds shall be avoided as much as possible. Sedimentation pond depths shall be kept to less than 5 m, to avoid non-compliant TSS removal/efficiency and other safety concerns.
- Berm/embankment side slopes for the ponds shall be 3H:1V.
- Mine Site Ore Crushing and Screening and Waste Rock Drainage sedimentation ponds shall be lined and the discharge from the ponds shall be controlled.
- Milne Port Ore Stockpile pond(s) can be lined/unlined and depending on its impact to the environment and permafrost as well as geotechnical stability, the discharge from the pond(s) can be controlled/uncontrolled.
- Ponds with storage volumes greater than 30,000 m^3 and heights exceeding 2.5 m shall be classified as dams and shall meet the dam safety requirements as per the Canadian Dam Association's Dam Safety Guidelines (CDA 2007).

7.5 Off-Spec and Treated Effluent Ponds

- 7.5.1 The off-spec effluent pond at the Milne Port shall be sized based on the storage requirements specified in the event that the sewage treatment plant does not meet effluent discharge criteria and/or the system halts operations due to technical difficulties.
- 7.5.2 The treated effluent pond at the Mine Site shall be sized based on the requirements for 10 months storage of treated sewage generated at the Mine Site during the period in which the body of water receiving the discharge (i.e. Mary River) is frozen.
- 7.5.3 The ponds shall have minimum freeboards of 0.3 m.
- 7.5.4 The ponds shall have side slopes of not steeper than 3H:1V.
- 7.5.5 The effluent ponds shall be lined.

7.6 Culverts and Roadside Ditches

- 7.6.1 Drainage ditches and culverts for all internal/access roadways and vehicle access points shall be designed to convey the runoff peak flow from a 1 in 25 year return period storm, such that the inlet headwater level does not exceed the bottom of the road subbase. Their analysis and design shall consider design flow, culvert size and material, entrance structure layout, outlet structure layout and erosion protection.
- 7.6.2 Drainage ditch design shall also be subject to the criteria stated in Table 7-2.

Table 7-2: Drainage Ditch and Culvert Design Criteria

Maximum permissible flow velocity in ditch without rip rap (m/s)		1.5
Minimum ditch and culvert slope (□)		0.3
Minimum freeboard for ditch (mm)		300
Minimum ditch depth for internal roads and other areas (mm)		300
Minimum ditch bottom width for internal roads and other areas (mm)		500
Minimum rock ditch depth for haul road (mm)		500
Minimum ditch bottom width for haul road (mm)		1000
Ditch side slopes (H:V)	Rock	1:4
	Soil	2:1
Minimum culvert diameter (mm)		500

- 7.6.3 ~~All culverts shall have 50 mm diameter steam pipes welded at the top inner sides for prevention of water from freezing.~~
- 7.6.4 Loading over culverts and pipes shall be in accordance with AASHTO HS 20-44, except for areas of special equipment operation, which shall consider actual vehicle loading. The minimum cover for culverts shall be 600 mm, or as required by the differing specific design vehicle.
- 7.6.5 Fish-bearing culverts shall be minimum 1,000 mm diameter and only one pipe shall be embedded by 10□ of the pipe diameter.
- 7.6.6 All culverts shall be Corrugated Steel Pipe (CSP).
- 7.6.7 Apply Manning's n values as per the following:
- n = 0.025 for gravel ditches
 - n = 0.040 for rip rap ditches
 - n = 0.024 for all CSP pipe.

7.7 Drainage Interceptor/Collector Berms

- 7.7.1 Drainage berms diverting overland flow from the waste rock drainage area to the sedimentation ponds shall be a minimum of 1.0 m high with 1.5H:1V side slopes and 0.5 m top width.
- 7.7.2 Rip rap and other energy dissipation measures shall be provided to protect against erosion.