

Attachment 2

**Milne Port - Camp Pad Natural Stream Diversion – Hydrology &
Hydraulic Calculations**

H353004-2100-240-030-001, Rev. 0

Project Memo

H-353004

21 June 2017

To: Matt Weaver

From: A Grobbelaar

cc: Tyler Bruce

Baffinland Iron Mines LP Mary River Project



Milne Port - Camp Pad Natural Stream Diversion- Hydrology & Hydraulic Calculations

1. Introduction

The accommodation camp pad intersects a minor seasonal stream. In order to maintain continuation of the stream, it has to be diverted around the camp pad. (See below camp pad location and streams identified)

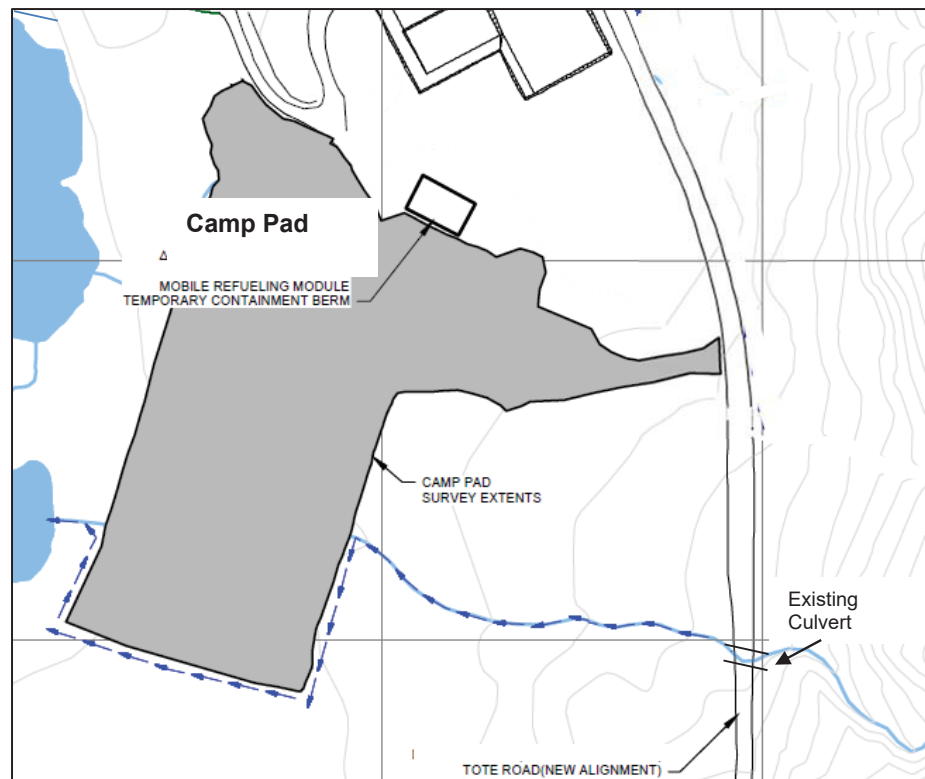


Figure 1: Accommodation Camp Pad Diversion

If you disagree with any information contained herein, please advise immediately.

H353004-2100-240-030-001, Rev. 0

Page 1

The catchment area for the seasonal stream is depicted below:

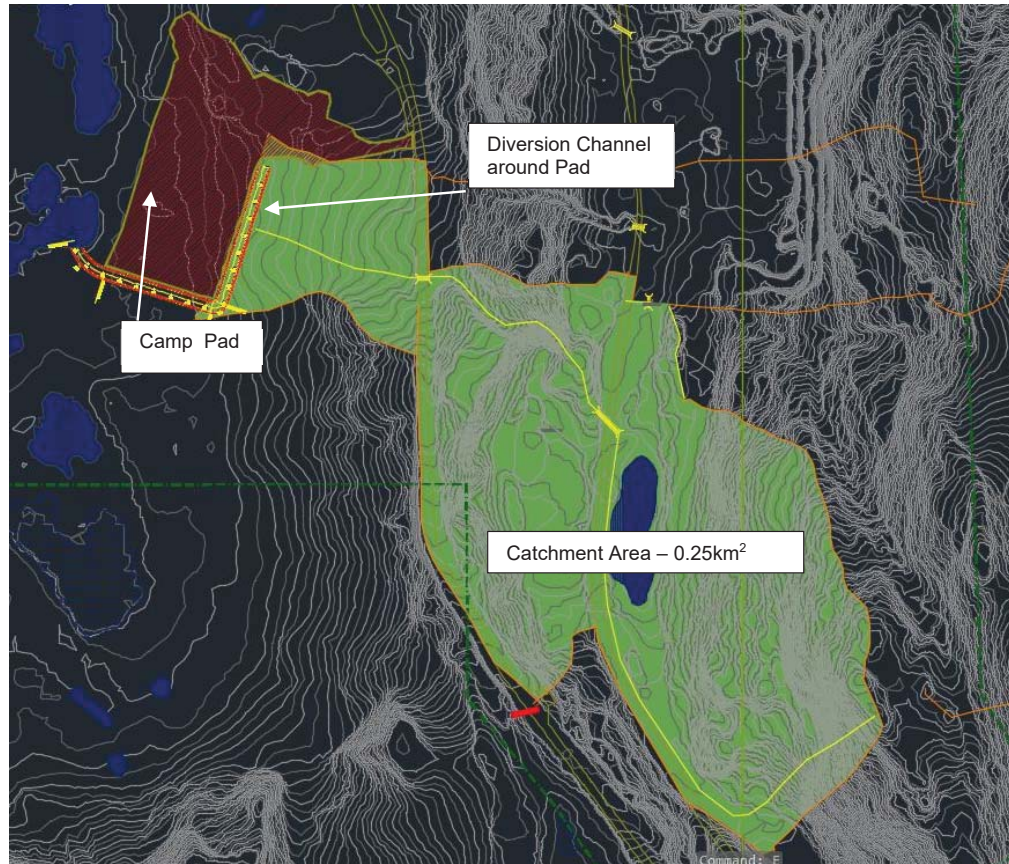


Figure 2: Seasonal Stream Catchment

A suitable sized culvert under the existing quarry access road will have to be installed in order to reduce the catchment size for the seasonal stream to 0.25km². Details, including elevations near the quarry access road, will need to be confirmed by onsite survey prior to finalizing culvert design and associated geotechnical engineering.

1.1 Design Calculations

1.1.1 *Diversion Channel Catchment Runoff Calculation*

In order to design the stream diversion, the expected storm water flow needs to be calculated (For the diversion design, Hatch used a 1:100 year return period storm in line with the previously approved design philosophy for external streams & stream diversions).

Rainfall intensities were obtained from a previous phase approved report by Hatch titled “Civil Design Criteria” – H-349000-1000-10-122-001 (Rev 1). In the report reference is made to the Knight Piesold calculated rainfall intensities for various return periods – See table 1-1 below:

Table 1-1: Rainfall Intensities for Various Return Periods

Duration	2 yrs	5 yrs	10 yrs	15 yrs	20 yrs	25 yrs	50 yrs	100 yrs	200 yrs
5 min	9.5	12.0	14.0	15.1	15.9	16.5	18.3	20.1	22.0
10 min	7.2	9.0	10.5	11.3	11.9	12.4	13.7	15.1	16.5
15 min	6.0	7.5	8.7	9.4	9.9	10.3	11.4	12.6	13.7
30 min	5.0	6.3	7.3	7.9	8.3	8.6	9.5	10.5	11.4
1 hr	4.0	5.2	6.1	6.6	7.0	7.3	8.1	9.0	9.9
2 hr	3.0	3.9	4.6	5.0	5.2	5.5	6.1	6.8	7.4
6 hr	2.0	2.7	3.3	3.6	3.9	4.0	4.6	5.1	5.7
12 hr	1.3	1.8	2.2	2.4	2.6	2.7	3.1	3.4	3.8
24 hr	1.0	1.4	1.7	1.9	2.0	2.1	2.4	2.7	3.0

The catchment area is 0.25km².

The Table 1-2 below indicates the calculation to determine the peak runoff from the 1:100 storm event:

Table 1-2: Peak Flow Calculation

Q = 0.28 C I A		Tc = 0.06628(L ^{0.77} /S ^{0.385})		Unit	
Q= 0.78	m ³ /s	Tc= 0.25		hr	15.1 min
C= 0.9		L= 1.177		km	
I= 12.6	mm/hr	S= 0.04317		m/m	
A= 0.25	km ²				

The diversion channel was sized based on a peak catchment flow of **0.78m³/s** for the 1:100year return period storm.

1.1.2 Diversion Channel Hydraulic Calculation

Based on the previous phase approved report by Hatch titled “Civil Design Criteria” – **H-349000-1000-10-122-001 (Rev 1)**, the channel properties were compiled. The side slopes of 2H:1V was used together with the rip rap and the Manning flow friction factor (n) value of 0.04 applied. Using the Flow Master software by Bentley Systems Inc, the flow depth was determined using the natural ground level slope along the accommodations camp pad. A minimum slope of 1:500 was applied where the natural ground was flatter.

Hatch Drawings No **H353004-4000-228-272-0001-0001 & H353004-4000-228-271-0001-0001** indicates the layout of the diversion channel and longitudinal profile respectively (see attached).

The seasonal minor stream is re-directed into the diversion channel through a long radius intercept channel, transitioning from the natural stream shape into the trapezoidal channel. This detail is apparent in the drawings referenced above. Some dimensional data will have to be determined on site and adjusted after consultation with the Engineer.

At the south east corner of the pad where the diversion channel turns through 90 degrees, the channel was sized and detailed to contain the specific energy calculated for the stream flow, thus ensuring that no spillage will occur during the storm event.

A general freeboard of 300 mm was applied throughout the channel design.

At the discharge end of the channel, a hydraulic flow dispersion structure is detailed to allow the energy of the $0.78^3/s$ flow to dissipate and not cause any erosion damage. The actual invert level of the natural water body that the diversion channel will drain into shall be confirmed on site and conveyed to the Engineer. This invert level cannot be above the diversion channel invert so as not to allow any capacity reduction of the channel. The Engineer must be consulted in the event that the invert of the natural water body is higher than the diversion channel to allow for adjustment in the details to be constructed.

In order to obtain the flow properties for the channel at various sections (change in gradient) the software by DEVOTECH was used. The EPA storm water management model - version 5.1 (build 5.1.006) calculates the flow properties at set sections and generates the long sections data as reflected on the drawing.



A Grobbelaar

AG:AG

Attachment(s)/Enclosure:

- Diversion Channel hydraulic calculation – Attachment 1
- Diversion Channel steady uniform flow calculation- Attachment 2
- H353004-4000-228-272-0001-0001- Attachment 3
- H353004-4000-228-271-0001-0001- Attachment 4

Attachment 1:

Diversion Channel Hydraulic Calculation

Project Description

Friction Method	Manning Formula
Solve For	Bottom Width

Input Data

Roughness Coefficient	0.040
Channel Slope	0.20 %
Normal Depth	0.40 m
Left Side Slope	2.00 m/m (H:V)
Right Side Slope	2.00 m/m (H:V)
Discharge	0.78 m ³ /s

Results

Bottom Width	2.95 m
Flow Area	1.50 m ²
Wetted Perimeter	4.74 m
Hydraulic Radius	0.32 m
Top Width	4.55 m
Critical Depth	0.18 m
Critical Slope	0.02947 m/m
Velocity	0.52 m/s
Velocity Head	0.01 m
Specific Energy	0.41 m
Froude Number	0.29
Flow Type	Subcritical

Attachment 2: Diversion Channel Steady Uniform Flow Calculation

PA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.006)

About: File generated by iDAS (www.devotech.co.za)

NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.

Analysis Options

Flow Units CMS

Process Models:

Rainfall/Runoff NO

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed NO

Water Quality NO

Flow Routing Method STEADY

Starting Date JUN-08-2017 00:00:00

Ending Date JUN-09-2017 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:01:00

Routing Time Step 10.00 sec

*****	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*****	*****	*****
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.000	0.000
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	6.739	67.389
External Outflow	6.739	67.389
Internal Outflow	0.000	0.000
Evaporation Loss	0.000	0.000
Seepage Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.000	0.000
Continuity Error (%)	0.000	

Highest Flow Instability Indexes

All links are stable.

Routing Time Step Summary

Minimum Time Step : 10.00 sec
 Average Time Step : 10.00 sec
 Maximum Time Step : 10.00 sec
 Percent in Steady State : 0.00
 Average Iterations per Step : 1.00
 Percent Not Converging : 0.00

Node Depth Summary

Node	Type	Average Maximum Maximum Time of Max			
		Depth	Depth	HGL	Occurrence
		Meters	Meters	Meters	days hr:min
CN1	JUNCTION	0.40	0.40	13.68	0 00:00
CN4	JUNCTION	0.40	0.40	13.62	0 00:00
CN5	JUNCTION	0.39	0.39	13.06	0 00:00
CN6	JUNCTION	0.39	0.39	12.91	0 00:00
CN7	JUNCTION	0.20	0.20	11.76	0 00:00
CN8	JUNCTION	0.19	0.19	11.43	0 00:00
CN9	JUNCTION	0.31	0.31	10.94	0 00:00
CN10	JUNCTION	0.40	0.40	10.85	0 00:00
CN11	JUNCTION	0.40	0.40	10.78	0 00:00
CN12	JUNCTION	0.52	0.52	10.82	0 00:00
CN13	JUNCTION	0.52	0.52	10.82	0 00:00
CN14	JUNCTION	0.40	0.40	10.64	0 00:00
CN15	JUNCTION	0.40	0.40	10.63	0 00:00
MH70	OUTFALL	0.39	0.39	10.62	0 00:00

Node Inflow Summary

Node	Type	Maximum Maximum		Time of Max	Lateral Inflow Volume	Total Inflow Volume	Flow Balance Error
		Lateral Inflow	Total Inflow				
		CMS	CMS	days hr:min	10^6 ltr	10^6 ltr	Percent
CN1	JUNCTION	0.780	0.780	0 00:00	67.4	67.4	0.000
CN4	JUNCTION	0.000	0.780	0 00:00	0	67.4	0.000
CN5	JUNCTION	0.000	0.780	0 00:00	0	67.4	0.000
CN6	JUNCTION	0.000	0.780	0 00:00	0	67.4	0.000
CN7	JUNCTION	0.000	0.780	0 00:00	0	67.4	0.000
CN8	JUNCTION	0.000	0.780	0 00:00	0	67.4	0.000
CN9	JUNCTION	0.000	0.780	0 00:00	0	67.4	0.000
CN10	JUNCTION	0.000	0.780	0 00:00	0	67.4	0.000
CN11	JUNCTION	0.000	0.780	0 00:00	0	67.4	0.000
CN12	JUNCTION	0.000	0.780	0 00:00	0	67.4	0.000
CN13	JUNCTION	0.000	0.780	0 00:00	0	67.4	0.000
CN14	JUNCTION	0.000	0.780	0 00:00	0	67.4	0.000
CN15	JUNCTION	0.000	0.780	0 00:00	0	67.4	0.000
MH70	OUTFALL	0.000	0.780	0 00:00	0	67.4	0.000

Node Surcharge Summary

No nodes were surcharged.

Node Flooding Summary

No nodes were flooded.

Outfall Loading Summary

Flow	Avg	Max	Total
Freq	Flow	Flow	Volume

Outfall Node	Pcnt	CMS	CMS	10^6 ltr
MH70	100.00	0.780	0.780	67.389
System	100.00	0.780	0.780	67.389

Link Flow Summary

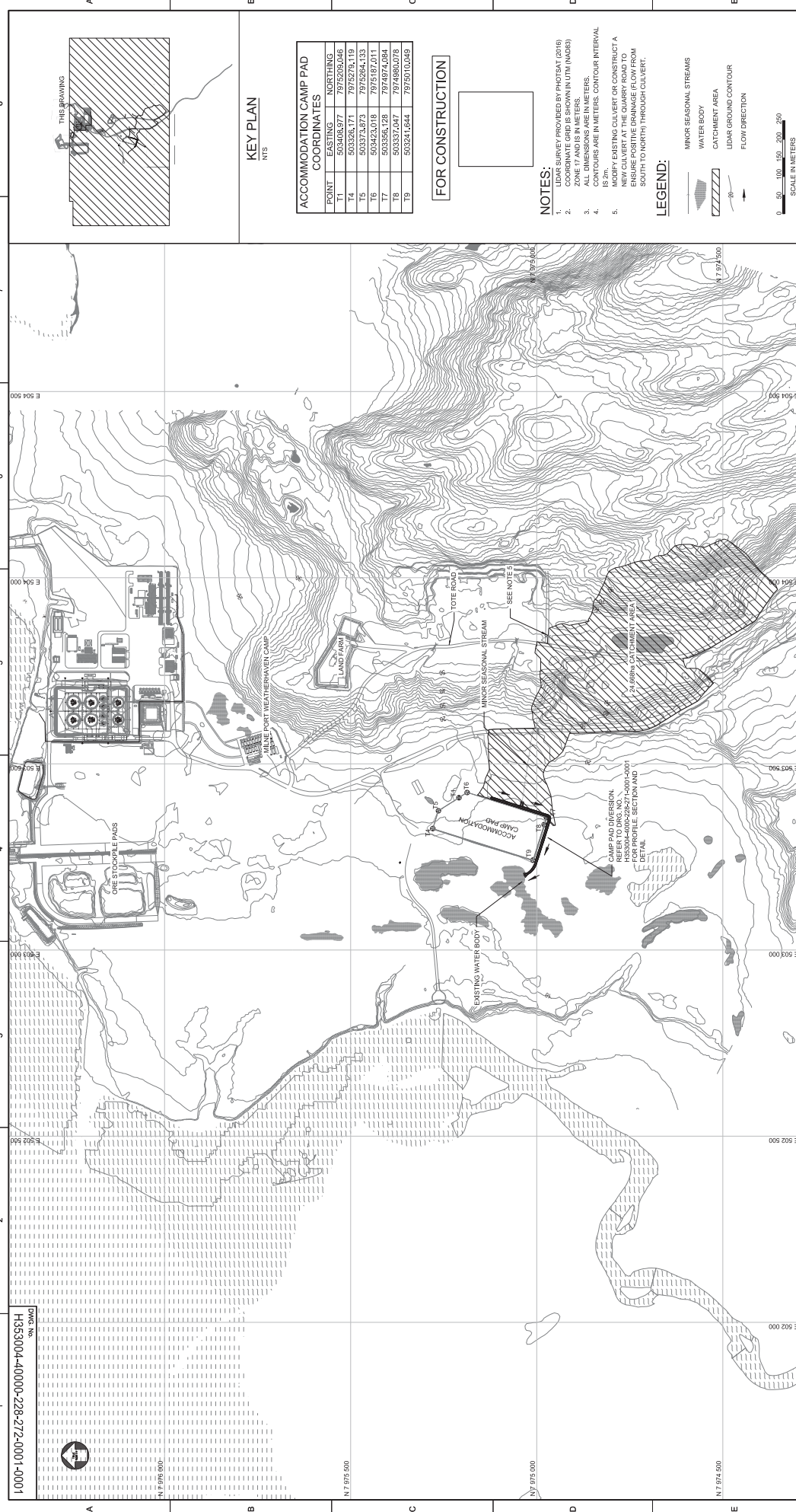
Link	Type	Maximum Flow CMS	Time of Max Occurrence days hr:min	Max Veloc m/sec	Maximum Full Flow	Max/ Full Depth
CH21	CONDUIT	0.780	0 00:00	0.37	0.57	0.74
CH24	CONDUIT	0.780	0 00:00	0.52	0.35	0.56
CH1	CONDUIT	0.780	0 00:00	0.51	0.36	0.57
CH17	CONDUIT	0.780	0 00:00	1.24	0.10	0.27
CH11	CONDUIT	0.780	0 00:00	1.20	0.10	0.27
CH8	CONDUIT	0.780	0 00:00	1.35	0.08	0.25
CH9	CONDUIT	0.780	0 00:00	0.52	0.35	0.56
CH10	CONDUIT	0.780	0 00:00	1.17	0.11	0.28
CH18	CONDUIT	0.780	0 00:00	0.68	0.24	0.45
CH19	CONDUIT	0.780	0 00:00	0.52	0.36	0.57
CH20	CONDUIT	0.780	0 00:00	0.52	0.36	0.57
CH22	CONDUIT	0.780	0 00:00	0.52	0.35	0.56
CH23	CONDUIT	0.780	0 00:00	0.51	0.36	0.57

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Tue Jun 20 16:00:38 2017
 Analysis ended on: Tue Jun 20 16:00:38 2017
 Total elapsed time: < 1 sec

Attachment 3

[illegible]

Attachment 4

