

Whale Tail Pit Project

MINE CONTACT WATER MODELLING COMMITMENTS

26 July 2018

AGENDA

Introduction

Modelling Results

- Whale Tail Pit Lake Hydrogeology, Arsenic Diffusion and Hydrodynamics
- Mammoth Lake Effluent Plume (near field) and Hydrodynamics (far field)
- WRSF Thermal Model

Discussion



Hydrogeological Model



HYDROGEOLOGY

Term and Condition n. 6

Objectives of the hydrogeological model:

- Evaluate groundwater flow conditions into/out of the flooded open pit post-closure
- Assess effect of hydrogeological conditions on the potential for arsenic accumulation in the pit lake from release by diffusion from submerged pit walls

HYDROGEOLOGY

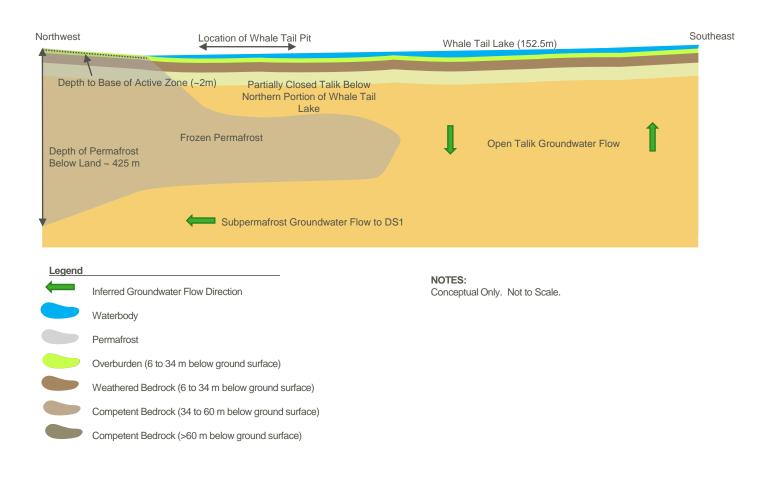
Pit Lake hydrogeological conceptual model:

- Open talik in Whale Tail Lake South Basin
- Permafrost present below the North Basin of Whale Tail Lake below the base of the pit. K of permafrost bedrock set at 1x10⁻¹²m/s; very low flow zone.
- Limited inflow of water into the open pit during operations and closure since the pit will be mostly in a closed talik above a layer of permafrost
- Post-closure gradual thaw of permafrost below pit until fully open talik in the North Basin, modelled as 300 years after closure.
- Post-closure hydraulic gradients to pit are weak to absent, flow regime into/out of pit
 may be density driven: caused by lateral variations in fluid density due to differences
 in TDS between groundwater (from 650 mg/L TDS at Year 1 post-closure to 650
 mg/L TDS 500 years post-closure) and pit Lake (TDS 77 mg/L in North Basin; 11
 mg/L South Basin at closure)



Conceptual Model of Thermal-Hydrogeological Conditions

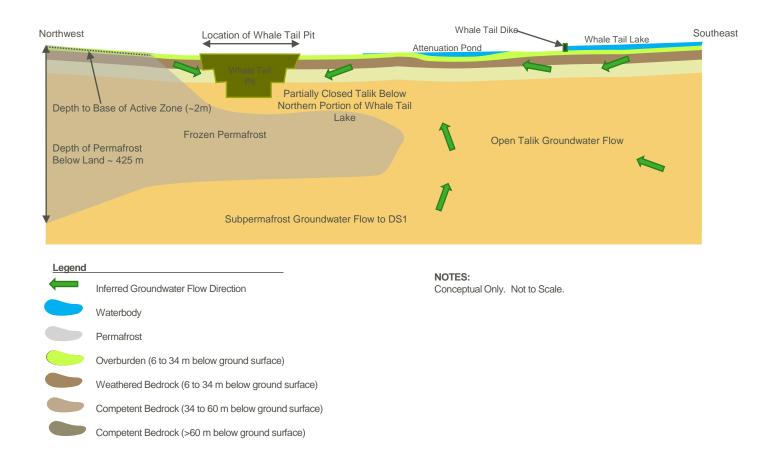
BASELINE





Conceptual Model of Thermal-Hydrogeological Conditions

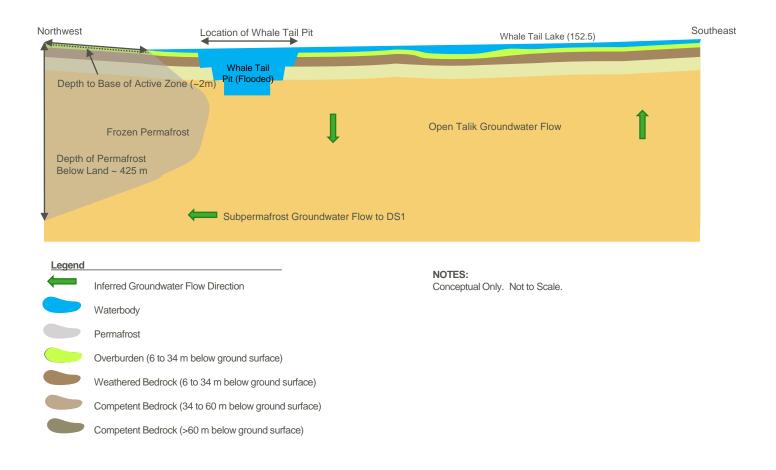
OPERATIONS





Conceptual Model of Thermal-Hydrogeological Conditions

POST CLOSURE





HYDROGEOLOGY

Simulation

- 2-dimension FEFLOW model over 500 years (300 with permafrost, 200 years for near steady-state conditions following melting
- Domain: 1,600 m NW x 2,800m SE from centre of pit
- Finite element mesh: 55,000 elements, node spacing of 5m near ground surface to 20 m near base of model

HYDROGEOLOGY - RESULTS

Pit Lake vs groundwater inflows and TDS concentrations

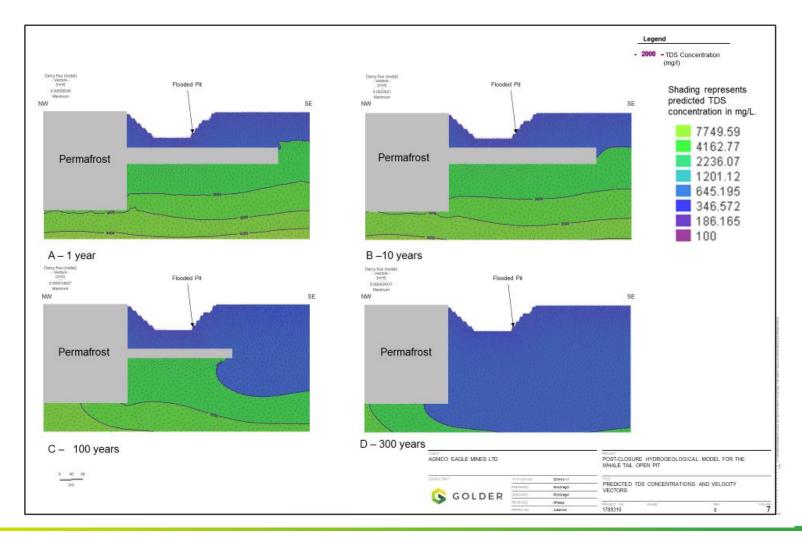
| Predicted Fluxes per 1 m Width Section | | | | | | | |
|--|--------|---|--|--|--|--|--|
| Years Following Closure Groundwater Inflow to Pit Lake (m³/day/m width) | | Average TDS Concentration into pit (mg/l) | Pit Lake Outflow to Groundwater (m³/day/m width) | | | | |
| 1 | 0.008 | 650 | 0.004 | | | | |
| 10 | 0.004 | 540 | 0.003 | | | | |
| 100 | 0.0008 | 440 | 0.003 | | | | |
| 500 | 0.0005 | 77 | 0.006 | | | | |

Predicted Fluxes Up-scaled to Whale Tail Pit Lake

| Years Following Closure | Groundwater Inflow to Pit Lake (m³/day) | Pit Lake Outflow to Groundwater (m³/day) |
|-------------------------------|---|--|
| 1 | 2.2 | 1.1 |
| 10 | 1.1 | 0.8 |
| 100 | 0.2 | 0.8 |
| 500 | 0.1 | 1.7 |



HYDROGEOLOGY - THAW OF PERMAFROST





HYDROGEOLOGY

Conclusion

Short-term post closure (to approx. 10 years)

groundwater inflow to pit > groundwater outflow to regional system

Medium and long term

Pit Lake is a groundwater recharge even before permafrost not completely thawed



Arsenic Diffusion Assessment from Submerged Pit Walls



ARSENIC DIFFUSION

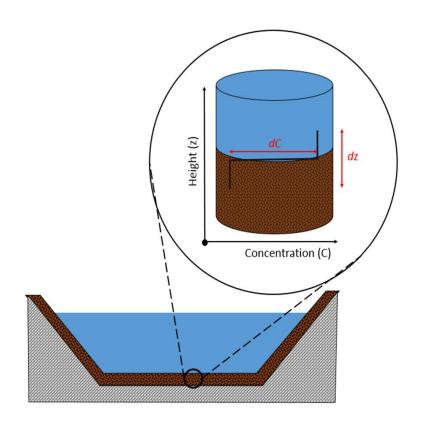
Method

Calculation of arsenic flux across the pit lake wall surface-water interface using Fick First Law of diffusion

$$J_z = \frac{D^{\circ} J}{F} \phi \frac{dC}{dz}$$

$$Jz = \frac{8.2 \times 10^{-6}}{1} \times 0.03 \times \frac{dC}{1}$$

Integration into the pit lake water quality model to evaluate additional arsenic load to pit lake from diffusion from pit walls for each lithology by proportion on the pit wall.



ARSENIC DIFFUSION

Source data

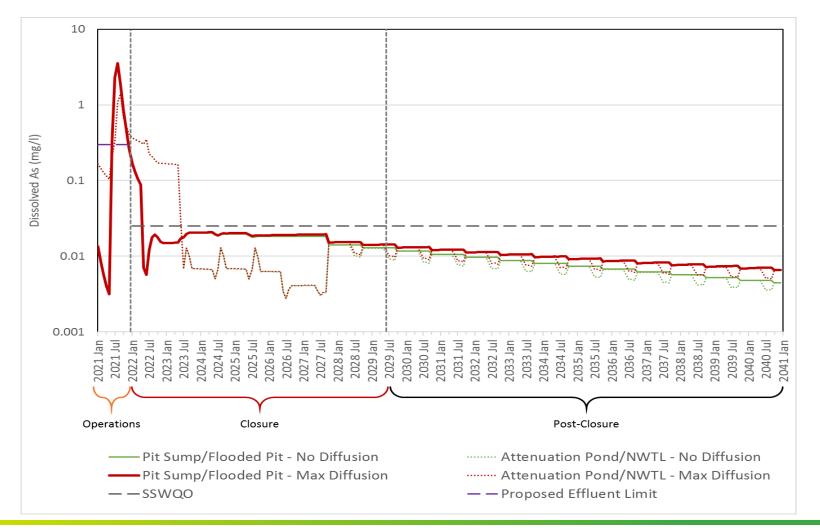
- arsenic concentrations in submerged leaching column: pore space vs above water column
- Leaching columns

Arsenic diffusive flux by lithology

| Flux (Jz) (mg cm ⁻² s ⁻¹) | Iron Formation Ultramafic Mixture (x 10 ⁻¹⁰) | Ultramafic (North and South Wall) (x 10 ⁻¹⁰) | Iron Formation (x 10 ⁻¹⁰) | South and North Greywacke (x 10 ⁻¹⁰) |
|---|--|--|---|---|
| Data Source | Submerged Column | Column Leach Tests (C1 and C5) | Column Leach Test (C2) | Column Leach Tests (C4) |
| Average | 2.42 | 5.07 | 4.64 | 0.08 |



ARSENIC DIFFUSION - RESULTS





ARSENIC DIFFUSION

Conclusion

Diffusion of arsenic from all pit walls has <u>no significant effect</u> on water quality in short and long-term.

Arsenic transfer to the open pit by diffusion from the submerged pit walls is not significantly affected by the hydrogeological regime around the flooded open pit.

Whale Tail Pit Lake Hydrodynamic Model

HYDRODYNAMICS

NIRB project certificate, Condition 16.

Objectives:

 Evaluate the potential for chemical stratification and the Pit Lake water quality profile post-closure



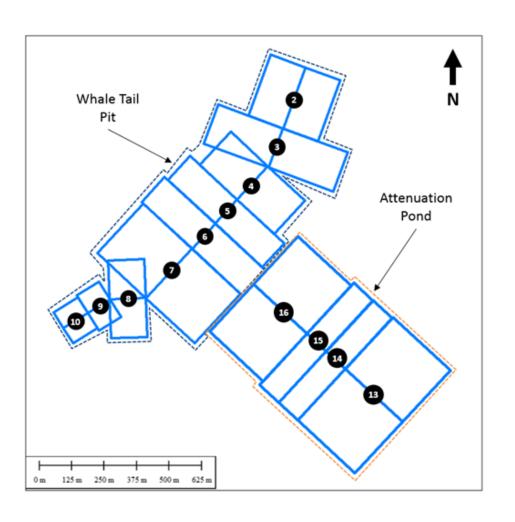
HYDRODYNAMICS - METHOD

- CE-QUAL-W2 software: fluid mechanics and water quality model to simulate distribution of heat, water momentum and mass transfer
- Model domain: 2-D grid of slices through the pit; horizontal grid spacing between 100 m and 260 m; vertical spacing.
- Model run for closure and 43 years post-closure: January 01, 2022 to December 31, 2070
- Input data: wind speed and direction, precipitation, run-off, pumped flows, groundwater flows, seepages, water temperature, outflow to Mammoth Lake



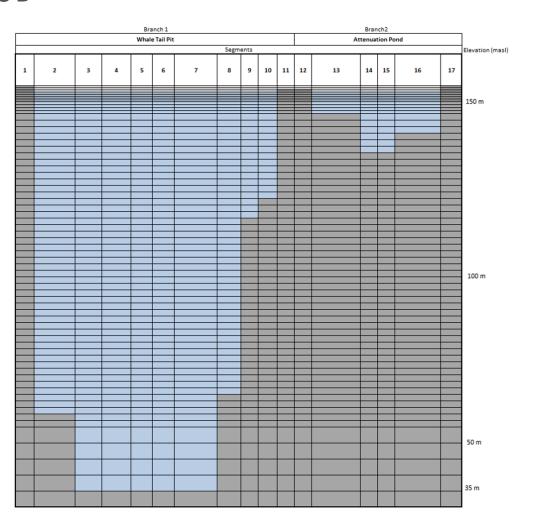
HYDRODYNAMICS - METHOD

Plan view of segments representing the pit and attenuation pond



HYDRODYNAMICS - METHOD

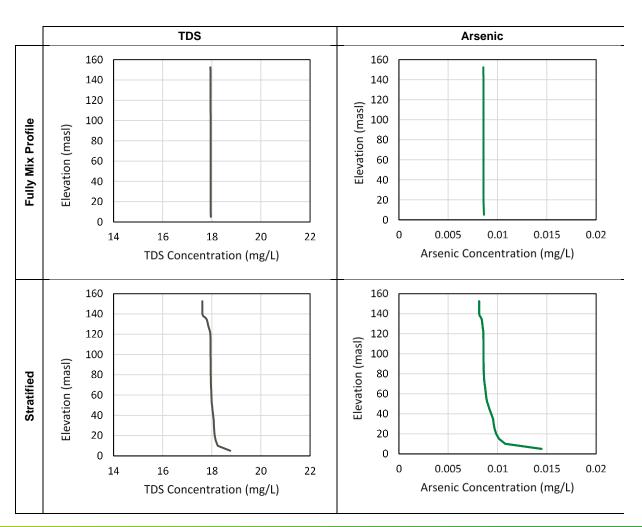
Profile of vertical layers and horizontal segmentation in the pit and attenuation pond



HYDRODYNAMICS - RESULTS

2027 – 5 years post closure:

Fully mixed in spring and fall; weak stratification in winter and summer

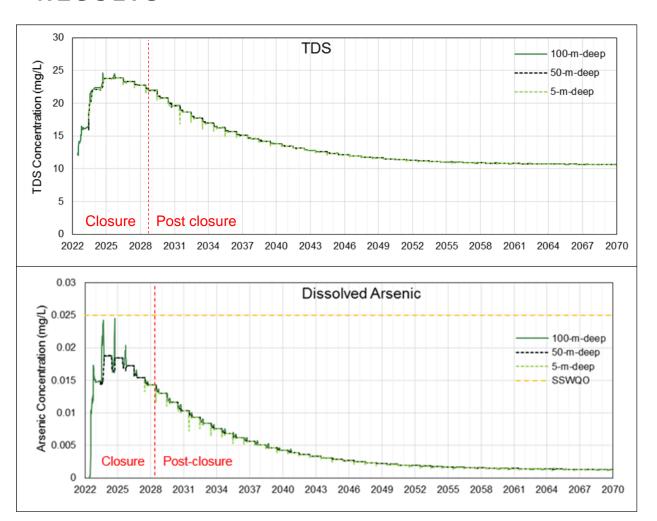




HYDRODYNAMICS - RESULTS

Evolution in time of TDS and arsenic in pit lake, fully mixed conditions

Recall: no significant effect on pit lake water quality by arsenic diffusion from submerged pit walls.

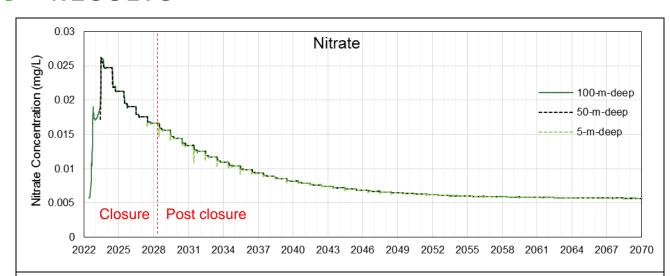


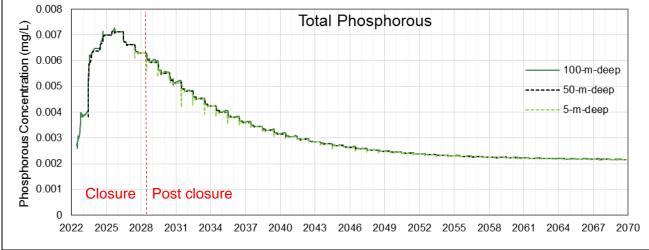


HYDRODYNAMICS - RESULTS

Evolution of nitrate and phosphorous in fully mixed pit lake

Phosphorous is lower than the 0.01 mg/L threshold between oligotrophic and mesotrophic conditions







HYDRODYNAMICS

Summary

- Pit lake to be fully flooded by 2028
- Lake water is predicted to completely mix bi-annually in spring and fall and exhibit weak chemical stratification in summer and winter.
- Pit lake water quality meets SSWQO for arsenic, oligotrophic level of 0.01 mg/L phosphorous and receiving water quality guideline for and nitrate in 2028 and post-closure, allowing breaching of dikes in 2028 to restore lake circulation

Mammoth Lake Effluent Plume Model

Mammoth Lake Model

EFFLUENT PLUME

Objective:

Mammoth Lake Near-field water quality assessment at 1) WRSF seepage outlet post-closure and 2) mine discharge effluent

CORMIX model and the following design assumptions:

- WRSF seepage: surface flow and discharge through rock-fill weir into shallow bay of Mammoth Lake
- Effluent discharge: through engineered diffusor on Mammoth Lake Bed (1-meter above lake bottom)

WRSF SEEPAGE INPUT PARAMETERS

Required Dilution

Calculated as the dilution required for the predicted maximum effluent concentration to meet receiving environment quality guideline at the edge of the mixing zone.

Minimum required dilution is 16 for Phosphorus, this will also achieve the required dilution for all other constituents modelled

| Month | Required C at edge of NFZ (mg/L) (CCME/SSWQO) | | Arsenic Concentration (mg/L) | | Phosphorus Concentration (mg/L) | | Required Dilution | |
|-----------|--|------|------------------------------------|-------|---------------------------------------|-------|-------------------|------|
| | As | P | Diss. | Total | Diss. | Total | As | P |
| June | 0.025 | 0.01 | 0.064 | 0.069 | 0.030 | 0.040 | 2.8 | 3.0 |
| July | 0.025 | 0.01 | 0.216 | 0.221 | 0.101 | 0.111 | 8.8 | 10.1 |
| August | 0.025 | 0.01 | 0.345 | 0.350 | 0.161 | 0.171 | 14.0 | 16.1 |
| September | 0.025 | 0.01 | 0.219 | 0.224 | 0.102 | 0.112 | 9.0 | 10.2 |

WRSF SEEPAGE - INPUT PARAMETERS

Design Parameters – Ambient (Mammoth Lake)

| Month | June | July | August | September | Note | |
|--|-------|------|--------|--|---|--|
| Lake water depth at discharge (m) | 0.5 | | | | Assumed | |
| Lake bed slope (°) | 10 | | | | Assumed | |
| Temperature (°C) | 2 8 | | 10 | 6 | Monthly temperature from June to September ¹ | |
| TDS concentration (mg/L) | 15 | | | Based on average of all monitoring data from 2014-2016 | | |
| Water density (kg/m³) | 999.9 | | 999.7 | 999.98 | Calculated | |
| Calm condition: Assumed current speed (m/s) | 0.001 | | | | wind velocity 0 (m/s) ² | |
| Median current condition: Assumed current speed (m/s) | 0.11 | | | | wind velocity 5.56 (m/s) ² | |
| High current condition: Assumed current speed (m/s) | 0.27 | | | | 1% exceedance; wind velocity 0.28 (m/s) ² | |

Note 1: Extracted from sheet "2013 Sample Year Temperatures" of file: "Sample year of temperature time series for Mammoth Lake inflows.xlsx"

Note 2: The hourly wind speed data were downloaded for Baker Lake A Station (2300500), Latitude of 64°17'56" and Longitude of 96°04'44"



WRSF SEEPAGE - INPUT PARAMETERS

Design Parameters - Effluent

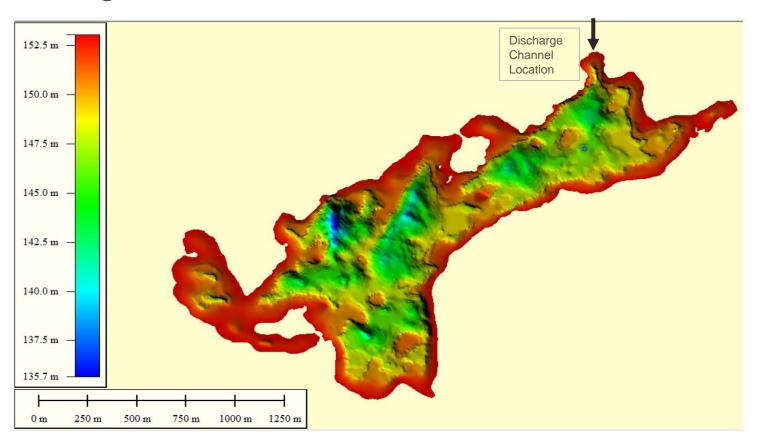
| Month | June | July | August | September | Reference |
|----------------------------------|---------|---------|---------|-----------|---|
| Discharge (m³/s) | 0.045 | 0.004 | 0.006 | 0.014 | modelled |
| Temperature (°C) | 2 | 8 | 10 | 6 | Assumed the same as Lake temperature |
| Maximum TDS concentration (mg/L) | 416 | 1382 | 2209 | 1407 | modelled |
| Density (kg/m³) | 1000.31 | 1000.97 | 1001.46 | 1001.09 | calculated |

Note 1: Extracted from sheet "2013 Sample Year Temperatures" of file: "Sample year of temperature time series for Mammoth Lake inflows.xlsx"



WRSF SEEPAGE

Discharge Channel Location





WRSF SEEPAGE - RESULTS

CORMIX simulation results

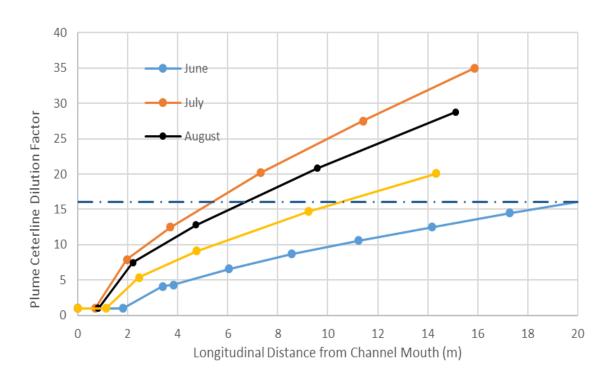
| Month | June | July | August | September | |
|----------------|--|------|--------|-----------|--|
| | Distance from Channel Mouth and along Plume Centre line (r where Dilution =16 | | | | |
| Calm condition | 20 | 5 7 | | 10 | |
| Median Current | 60 | 15 | 17 | 22 | |
| High Current | 47 | 18 | 22 | 27 | |

In all cased the minimum required dilution of 16 is provided within 60 m of the discharge location

WRSF SEEPAGE - RESULTS

Calm conditions require the shortest mixing zone distance to achieve required dilution:

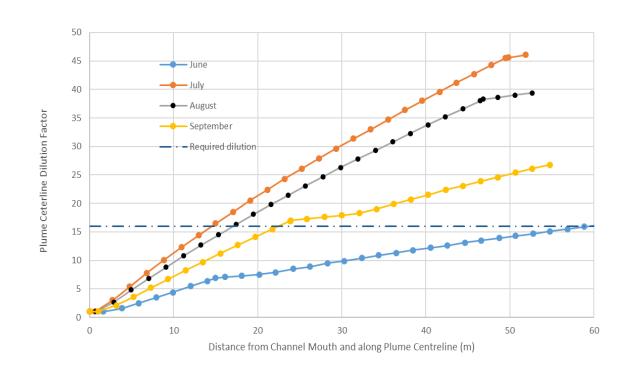
5 to 20 meters



WRSF SEEPAGE - RESULTS

In median current, required dilution is achieved at longer distances

Up to 60 meters



WRSF SEEPAGE

Conclusion

- A rock fill weir at outlet will channelize seepage outflow into Mammoth lake and facilitate dilution.
- Within Mammoth Lake, the required dilution of WRSF seepage is predicted to be met at 60 m from the discharge location in all scenarios

EFFLUENT DISCHARGE PLUME - INPUT PARAMETERS

Required Effluent Dilution

For the predicted maximum effluent concentration to meet receiving environment quality guideline at the edge of the mixing zone.

Minimum required dilution is 27 for phosphorus; this will achieve the required dilution for all other constituents

| Parameters | Units | CCME/SSWQO | Maximum Predicted Effluent Quality | Required Dilution |
|------------|-----------|------------|------------------------------------|----------------------|
| NH3 | mg/L as N | 2.9 | 0.23 | 0.1 |
| Р | mg/L | 0.01 | 0.27 | 27 |
| Al | mg/L | 0.1 | 0.32 | 3.2 |
| As | mg/L | 0.025 | 0.11 | 4.4 |
| Cd | mg/L | 0.000012 | 0.000097 | 8.1 |
| Cr | mg/L | 0.001 | 0.019 | 19 |
| Cu | mg/L | 0.002 | 0.014 | 7.1 |
| Fe | mg/L | 0.3 | 1.1 | 4 |
| Pb | mg/L | 0.001 | 0.0037 | 3.7 |
| Hg | mg/L | 0.000026 | 0.000074 | 2.9 |
| Ni | mg/L | 0.038 | 0.059 | 1.6 |
| Zn | mg/L | 0.03 | 0.019 | 0.6 |



EFFLUENT DISCHARGE PLUME - INPUT PARAMETERS

Design Parameters

Mammoth Lake

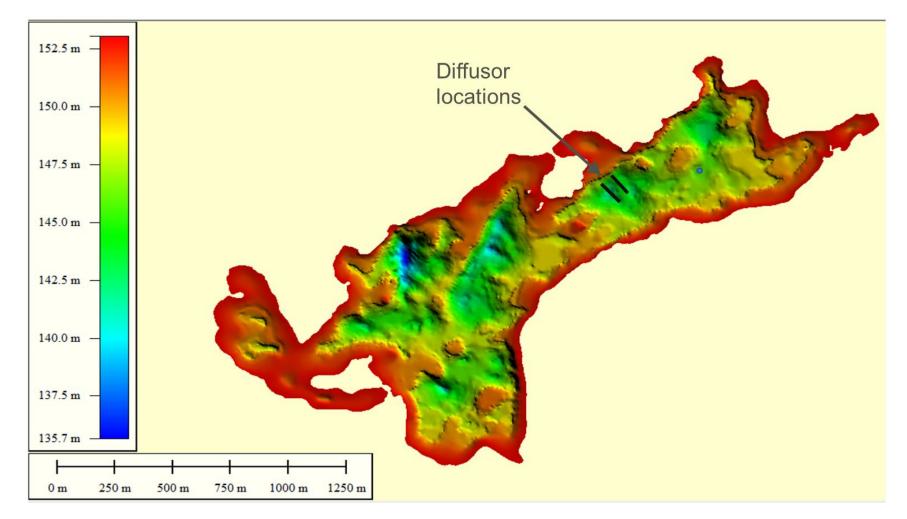
 Minimum Lake depth 7.9m; others same as for WRSF seepage analysis

Effluent

• 800 to 1600 m³/hr discharge rate in two diffusor lines. This flow represents the maximum treatment capacity for high flow events



EFFLUENT PLUME - INPUT PARAMETERS





EFFLUENT PLUME

Outputs of CORMIX Simulations for Design Scenarios

| Scenario | Open Water Season | | | |
|---|-------------------|-----|--|--|
| Discharge (m³/h) | 800 | 400 | | |
| Distance from near field mixing zone edge to diffuser (m) | 59 | 44 | | |
| Dilution factor at edge of near field zone | 27 | 31 | | |



DIFFUSOR DESIGN

Conclusions

- Proposed diffusor design: 10 ports at 12.6 m spacing and 75mm diameter diffusor ports
- Effluent mixing to receiving water quality targets are predicted to be achievable within 60 meters of the diffusor pipes. A mixing zone allowance of 100 metres is recommended.



Mammoth Lake Hydrodynamic Model

HYDRODYNAMICS

Objectives

Evaluate seasonal water circulation patterns in Mammoth Lake resulting from effluent discharge and to predict and evaluate the water quality within Mammoth lake during operations and post-closure

Use of Generalized Environmental Modelling System for Surface waters (GEMSS) 3-D modelling platform. A hydrodynamic and transport modules embedded in a geographic information and environmental data system

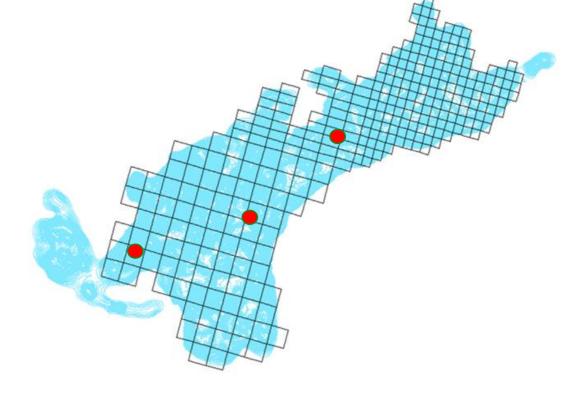
- Model domain: 3-D grid through Mammoth Lake grid size 50m² in NE part of Lake (50m x 50m x 1m depth) near the diffusor and WRSF; 100m² grid spacing in SW portion of Lake (100m x 100m x 1m).
- Model run from construction to 40 years post-closure: July 1, 2017 to January 1, 2067.
- Input data: wind speed and direction, precipitation, run-off, pumped flows, groundwater flows, seepages, water and lake bed sediment temperature, sediment heat exchange rate, outflow to Mammoth Lake
- Cryo-concentration effect from ice cover neglected given the low TDS of Mammoth Lake water quality, based on evidence in baseline water quality during ice cover and in open water season in Mammoth Lake



HYDRODYNAMICS - INPUT PARAMETERS

Model Segmentation and discharge locations

evaluated





HYDRODYNAMICS - RESULTS

Similar results obtained for all discharge locations evaluated and at each result node (away from the diffusor mixing zone) = fully mixed

conditions MAM-07 MAM-11 Near Outflow 0.070 0.060 0.060 0.060 를^{0.050} 를^{0.050} 넗0.050 ₹0.040 **2** 0.040 **\$** 0.040 2000 1000 1000 5,0.020 5 0.030 5 0.020 0.010 0.010 0.000 0.000 0.000 2017 2021 2017 2021 MAM-04 MAM-14 0.070 0.060 0.060 0.060 를 ^{0.050} 붙0.050 넗0.050 g 0.040 ₹ 0.040 **\$** 0.040 5'0.030 5'0.030 5'0.030 5_{10.020} 0.030 0.020 0.010 0.010 0.010 0.000 2021 2017 2021 2026 2021 2017 Year



HYDRODYNAMICS - RESULTS

Arsenic in effluent discharge during operation and arsenic released from cover (4-meter active thaw depth cover with low leaching waste rock).

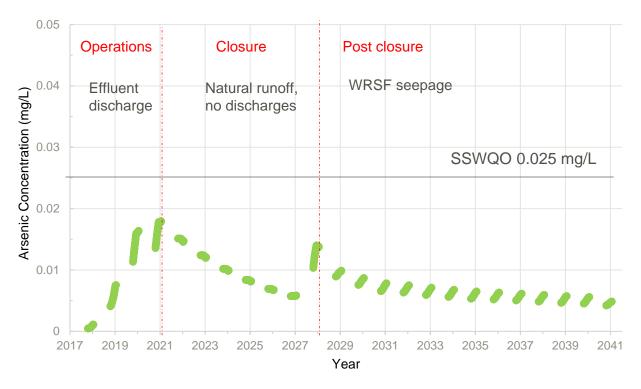




HYDRODYNAMICS - RESULTS SENSITIVITY

Arsenic in effluent discharge during operation and arsenic released from cover (4-meter active thaw depth cover with low leaching waste rock) and 50% of predicted WRSF seepage.



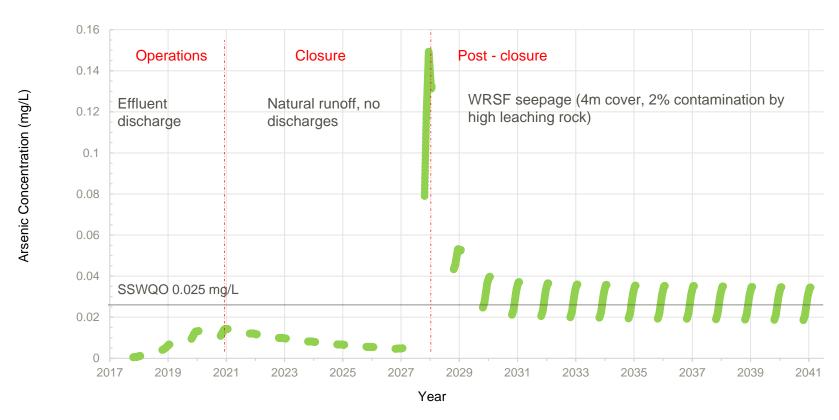




HYDRODYNAMICS - RESULTS SENSITIVITY

Arsenic release from 4-m cover with 2% contamination of high leaching waste rock

Open Water Total Arsenic



HYDRODYNAMICS - RESULTS SENSITIVITY

Arsenic release from 4-m cover with 2% contamination of high leaching waste rock, 50% of WRSF seepage.







HYDRODYNAMICS

Conclusions

- Effluent discharge into Mammoth Lake will be well mixed
- Steady-state untreated WRSF contact water released is predicted to meet SSWQO for arsenic in the Lake in the long-term, under the anticipated cover performance scenario (from the 4-meter cover of low arsenic leaching waste rock)
- Mammoth Lake is sensitive to cover material seepage quality, in turn sensitive to cover composition and WRSF pile contact water volume. Observational data of Meadowbank's WRSF suggest that WRSF contact water volumes are substantially lower than originally predicted (Portage is 20 to 40% lower, Vault WRSF contact water is minimal compared to 178,000m³ predicted at maximum footprint year) using similar modelling assumptions. Modelling results reflect a conservative chemical load estimate to Mammoth Lake in WRSF seepage that will be verified with monitoring.
- The Waste Rock Management Plan, the Water Quality and Flow Monitoring Plan and the ARD/ML Monitoring Plan are in place to verify and validate modelling assumptions and cover performance.



Downstream Lake Water Quality

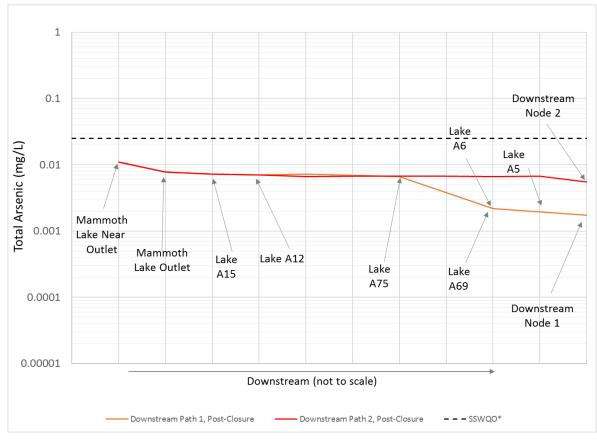


Downstream Lakes

PREDICTED WATER QUALITY

Arsenic in downstream
Lakes is predicted to
meet SSWQO during
operation and long term
post-closure

Steady-state arsenic release rate, Year 2039





Thermal Modelling of WRSF



Objectives

- Validate or update anticipated thermal conditions in the Whale Tail WRSF using Meadowbank WRSF thermal data, namely, the active thaw depth.
- Adjust cover design as needed based on modelling results

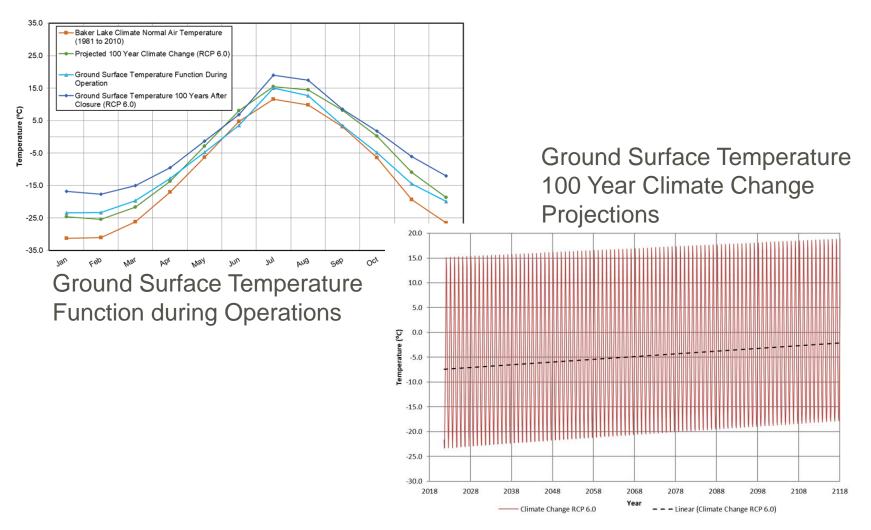
METHOD, INPUT PARAMETERS

- 1-D thermal model: TEMP/W software combined with Air/W and Seep/W
- Calibration using temperature profiles from thermistor data at Meadowbank (instrument RCP-6 which reflects the average active thaw depth of the entire pile)
- Assumed thermal properties of materials:

| Material | In-situ Vol. Water Content | (%) Conductivity (W/m-°C) | | | Volumetric Heat Capacity (MJ/m³-°C) | | Air Conductivity (m/s) | |
|-------------------------------|-------------------------------------|---------------------------|------|--------|---|--------|------------------------------|-------|
| | (m³/m³) | | | Frozen | Unfrozen | Frozen | Unfrozen | |
| NAG Waste Rock (upper 5 m) | 0.058 | 0.30 | 19.3 | 2.2 | 1.9 | 1.8 | 2.0 | 0.5 |
| Waste Rock (5 to 25 m deep) | 0.058 | 0.26 | 22.3 | 2.5 | 2.2 | 1.9 | 2.1 | 0.075 |



CLIMATE CONDITIONS CONSIDERED

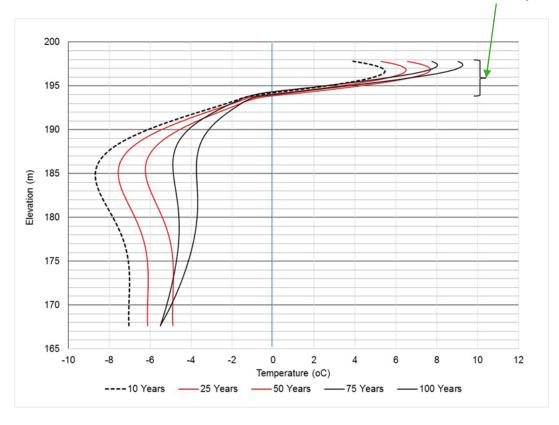




PREDICTED ACTIVE THAW DEPTH

Long-term temperature profiles computed for model scenarios

Maximum active thaw depth





Conclusions

- Based on results calibrated to the Meadowbank WRSF thermal data to date and climate change predictions, the maximum predicted thickness of the WRSF active layer is 4.24 meters ± 0.5 meters = 4.7 meter cover thickness (4.2 + 0.5 contingency).
- There is sufficient NPAG/NML material for this cover thickness if needed.
- Increased active thaw depth/rock cover from 4.0 to 4.7 is expected to have no effect on WRSF contact water quality during operations, and long-term post closure effects to water quality of a thicker active layer are expected to be within model accuracy where a clean (low leaching) waste rock cover present.
- The Thermal Monitoring Plan has measures to verify and validate the WRSF thermal model with operational data from site.



Modelling Conclusions

For the mine, water and waste management plans that describe the scenarios modelled, and per the interpretation of the modelling scenarios, no change to the overall water and waste management strategy is required for the operation and closure of the Whale Tail project since:

- Whale Tail flooded Pit Lake waters are predicted to fully mix twice per year
- Arsenic diffusion from submerged pit walls and the anticipated hydrogeological conditions around the Pit Lake post-closure are not expected to play a significant role on Pit Lake arsenic concentration
- Mammoth Lake is predicted to continue to be a fully mixed system during operation and post-closure with effluent and seepage discharge flowing into it
- Mammoth Lake water quality as well as downstream lakes are predicted to meet the project specific SSWQO for arsenic during operation and at closure according to the mine waste and water management plans proposed
- The average thickness of the WRSF active layer is within the range modelled. Should monitoring suggest the need for a thicker cover, material is available for this and the effect on contact water quality of a thicker, clean rock (NPAG and NML) cover is anticipated to fall within the model accuracy.
- The Mine Waste Management Plan, ARD/ML Monitoring Plan, Water Quality and Flow Monitoring Plan and the Thermal Monitoring Plan are in place to monitor and verify the performance of the cover material and systems and adapt as needed. Progressive covering of the WRSF and Meadowbank WRSF experience will assist in validating modelling predictions on the cover.





Open Discussion