

2010 Annual Geotechnical Inspection, Boston Advanced Exploration Project

Hope Bay, Nunavut



Hope Bay Mining Ltd. 300 – 889 Harbourside Drive North Vancouver, BC V7P 3S1 Canada



Prepared by:





Project Reference Number SRK 1CH008.032

February 2011

2010 Annual Geotechnical Inspection, Boston Advanced Exploration Project, Hope Bay, Nunavut

Hope Bay Mining Ltd.

300, 889 Harbourside Drive North Vancouver, BC V7P 3S1

SRK Consulting (Canada) Inc. Suite 2200, 1066 West Hastings Street Vancouver, B.C. V6E 3X2

Tel: 604.681.4196 Fax: 604.687.5532 E-mail: vancouver@srk.com Web site: www.srk.com

SRK Project Number 1CH008.032

February 2011

Author Maritz Rykaart, Ph.D., P.Eng.

Reviewed by Peter Healey, P.Eng.

Executive Summary

The Boston Advanced Exploration Project (Boston Camp) is a wholly owned exploration camp of Hope Bay Mining Ltd. (HBML), which is a wholly owned subsidiary of Newmont Mining Company (NMC). The camp is located about 170 km southwest of Cambridge Bay within the western Kitikmeot Region, Nunavut (with general coordinates of latitude 67°39'N and longitude 106°22'W). Boston Camp is used on a seasonal basis from which to carry out prospecting and exploration, various forms of exploration drilling, core splitting and logging. In addition, the site has historically been subjected to bulk underground sampling and processing. The camp was temporarily closed between mid 2009 and mid 2010, pending improvements to the camp sewage treatment plant (STP). At the time of this inspection these improvements continued; however, the camp was open and in use.

Site operations are currently conducted under Nunavut Water Board (NWB) License 2BB-BOS0712, dated July 6, 2007, which entitles HBML to use water and dispose of waste associated with their operations. HBML contracted SRK Consulting (Canada) Inc. (SRK) to conduct the annual geotechnical site inspection of Boston Camp in accordance with stipulated License conditions. This investigation was carried out during the week of July 12 - 16, 2010.

Table A below provides a summary of the inspection components and the primary recommendations stemming from the inspection. These recommendations are compared with those listed in the 2009 annual geotechnical report (SRK 2009f). There are no issues that require urgent and immediate action. SRK understands that HBML have already initiated projects to address many of the recommendations and concerns raised in this report.

Table A: Summary of Inspection Items and Associated Inspection Recommendations

Inspection Item	2009 Recommendations	2010 Recommendations
	Locate appropriate readout device for older thermistors and confirm functionality of strings	Locate appropriate readout device for older thermistors and confirm functionality of strings
Thermistors	Splice broken string	Splice broken string
	Continue formal monitoring of new (and)	Confirm status of string in 08SBD381A
	older) strings	Continue formal monitoring of new (and older) strings
Primary Tank Farm Settlement Monitoring	Continue quarterly monitoring	Continue quarterly monitoring
	Recognize foundation settlement risk in spill response plan	Recognize foundation settlement risk in spill response plan
Primary Tank	Monitor the surficial slip surfaces on the tank farm berms	Monitor the surficial slip surfaces on the tank farm berms
Farm	Continue settlement monitoring as described above	Continue settlement monitoring as described above
Power Plant Fuel Containment	No action required	No action required

Inspection Item	2009 Recommendations	2010 Recommendations		
Central Pad Fuel Containment	No action required	No action required Confirm whether secondary containment is required for two new tanks and implement if necessary		
Jet Fuel Containment	Conduct regular inspections of the portable containment berms	Conduct regular inspections of the portable containment berms		
Solid Waste Disposal Site	 Confirm that waste containment is not required through an appropriate waste inventory Clean out burn pit and dispose wood waste 	Confirm that waste containment is not required through an appropriate waste inventory Clean out burn pit and dispose wood waste		
(including burn pit)	as appropriate Remediate burn pit, or reclassify for other	as appropriate Remediate burn pit, or reclassify for other		
	functional use	functional use		
Ore Stockpiles	Implement the 2009 water and ore/waste rock management plan developed for the site	Implement the 2009 water and ore/waste rock management plan developed for the site		
		Clear out debris in pond that could damage liner		
	 Clear out debris in pond that could damage liner Implement the 2009 water and ore/waste 	Implement the 2009 water and ore/waste rock management plan developed for the site		
Settling Pond	rock management plan developed for the site Construct suitable barrier around the pond	Construct suitable barrier around the pond to prevent inadvertent human and/or animal access		
	to prevent inadvertent human and/or animal access	Confirm through water quality sampling whether the pond is leaking, and implement mitigation measures as appropriate		
Soil Containment Berm (Landfarm)	Implement action items arising from landfarm study currently underway	Implement action items arising from landfarm study recently completed		
Diamond Drill	Develop appropriate remediation plan for the pond	Develop appropriate remediation plan for the pond		
Cuttings and Settling Pond	Develop appropriate management plan for storage of drill cuttings, including possible use as remediation method for permafrost degradation zones	Develop appropriate management plan for storage of drill cuttings, including possible use as remediation method for permafrost degradation zones		
	Replace the faded notices at the portal entrance advising of the dangers associated with unauthorized access to the area	Replace the faded notices at the portal entrance advising of the dangers associated with unauthorized access to the area		
Portal	Develop site specific hazard assessment for people entering the portal area to address the rockfall hazard	Develop site specific hazard assessment for people entering the portal area to address the rockfall hazard		
	Consider installing a small diameter wire mesh over the exposed section of the portal roof to address the rockfall hazard	Consider installing a small diameter wire mesh over the exposed section of the portal roof to address the rockfall hazard		
Vent Paise	Replace weathered protective tarps covering the shelter erected over the vent raise	Replace weathered protective tarps covering the shelter erected over the vent raise		
Vent Raise	Install notices at the vent raise advising of the dangers associated with unauthorized access to the area	Install notices at the vent raise advising of the dangers associated with unauthorized access to the area		

Inspection Item	2009 Recommendations	2010 Recommendations
Road to Dock	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source
	Implement speed control measures	Implement speed control measures
Camp Complex Foundation Pad	Re-survey the pad and develop an action plan to fill in and re-grade the pad to re- establish constant pad drainage	Re-survey the pad and develop an action plan to fill in and re-grade the pad to re- establish constant pad drainage
Road to Airstrip	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source
	Implement speed control measures	Implement speed control measures
Airstrip	Maintain current maintenance practices, but do not use crushed ore material for	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source
	repairs; find an alternate clean source	Conduct frequent walk-over surveys to inspect for tension cracks along the airstrip shoulder
Drill Road	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source
	Implement speed control measures	Implement speed control measures
Core Storage	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source
Road	Monitor the pipe culvert for progressive permafrost degradation	Monitor the pipe culvert for progressive permafrost degradation
	Implement speed control measures	Implement speed control measures
Wooden Walkway to Boat Dock	Consider raising the walkway above the tundra to prevent vegetation dieback and possible onset of permafrost degradation	Consider raising the walkway above the tundra to prevent vegetation dieback and possible onset of permafrost degradation
	If boat dock is to be decommissioned consider removing the walkway altogether	If boat dock is to be decommissioned consider removing the walkway altogether
Radio Tower and Shack	No action required	No action required
Water Intake Pump Shack	Consider installing thermal pad or other appropriate foundation system	Consider installing thermal pad or other appropriate foundation system
Existing STP Foundation Pad	No action required	No action required
New STP	Monitor the areas where tundra vegetation damage has occurred	Monitor the areas where tundra vegetation damage has occurred
Foundation Pad	Develop long-term re-vegetation plan: involve a tundra vegetation expert	Develop long-term re-vegetation plan: involve a tundra vegetation expert
Core Storage Area(s)	Consolidate core box storage and ensure that no boxes are inadvertently stored on the tundra	Consolidate core box storage and ensure that no boxes are inadvertently stored on the tundra
	Develop a long-term core storage plan	Develop a long-term core storage plan
Grey Water Discharge	Implement the new sewage management plan developed for the site when the new STP is commissioned	Implement the new sewage management plan developed for the site when the new STP is commissioned
Drill Sites	Develop remediation strategy to prevent further permafrost degradation	Develop remediation strategy to prevent further permafrost degradation

Inspection Item	2009 Recommendations	2010 Recommendations
Vegetation	Initiate study to determine why dieback continues; involve a tundra vegetation expert	Initiate study to determine why dieback continues; involve a tundra vegetation expert
Dieback Zone	Develop remediation strategy to prevent further dieback and permafrost degradation	Develop remediation strategy to prevent further dieback and permafrost degradation
V-Notch Weir	Conduct complete inspection of the weir during 2010 geotechnical inspection	Conduct complete inspection of the weir during 2011 geotechnical inspection
	Develop appropriate remediation plan for the weir	Develop appropriate remediation plan for the weir

Table of Contents

	Exe	cutive Summary	i
1	Intr	oduction	
	1.1	Inspection Requirement	
	1.2	Report Structure	
	1.3	Disclaimer	
2		Conditions	
	2.1	Site History	
	2.2	Site Infrastructure	4
	2.3	Climate	5
	2.4	Regional Geology	5
	2.5	Permafrost and Geotechnical Conditions	6
3	lnor	pection Conditions	0
၁		Instrumentation/Data	
	3.1	3.1.1 Thermistors	
		3.1.2 Primary Tank Farm Settlement Monitoring	
	3.2	Containment Structures	
	3.2	3.2.1 Primary Tank Farm	
		3.2.2 Power Plant Fuel Containment	
		3.2.3 Central Pad Fuel Containment	
		3.2.4 Jet Fuel Containment	
		3.2.5 Solid Waste Disposal Site (Including Burn Pit)	
		3.2.6 Ore Stockpiles	
		3.2.7 Settling Pond	
		3.2.8 Soil Containment Berm (Landfarm)	
		3.2.9 Diamond Drill Cuttings and Settling Pond	
	3.3	Mine Openings	
		3.3.1 Portal	
		3.3.2 Vent Raise	18
	3.4	Infrastructure	18
		3.4.1 Road to Dock	18
		3.4.2 Camp Complex Foundation Pad	
		3.4.3 Road to Airstrip	
		3.4.4 Airstrip	
		3.4.5 Drill Road	
		3.4.6 Core Storage Road	
		3.4.7 Wooden Walkway to Boat Dock	
		3.4.8 Radio Tower and Shack	
		3.4.9 Water Intake Pump Shack	
		3.4.10 Existing STP Foundation Pad	
	۰.	3.4.11 New STP Foundation Pad	
	3.5	Other Areas	
		3.5.1 Core Storage Area(s)	
		3.5.2 Grey Water Discharge	
		3.5.3 Drill Sites	
		3.5.4 Vegetation Dieback Zones	
		J.J.J V-INOLOTI VVCII	∠0
4	Sun	nmarv of Recommendations	27

5 References	32
List of Tables	
Table 1: List of Individual Inspection Items	2
Table 2: Summary of Pertinent Site Ownership History	
Table 3: Summary of Permafrost Drillholes and Thermistor Installations	
Table 4: Summary of Survey Control Points Established for the Primary Tank Farm	gust
Table 6: Summary of Inspection Items and Associated Recommendations	
List of Figures	
Figure 1: Location Map	
Figure 2: Overall Site Layout	
Figure 3: Detailed Site Layout Looking South-West	
Figure 4: Detailed Site Layout Looking West	
Figure 5: Boston Thermistor Conditions	
Figure 6: Ground Temperature Profiles EBA Drillhole 12259-03	
Figure 7: Ground Temperature Profiles EBA Drillhole 12259-05	
Figure 8: Ground Temperature Profiles EBA Drillhole 12259-06	
Figure 9: Ground Temperature Profiles EBA Deep Drillhole (97NOD176)	
Figure 10: Thermistor Readings Drillhole 08SBD380	
Figure 11: Thermistor Readings Drillhole 08SBD381A	
Figure 12: Thermistor Readings Drillhole 08SBD382	
Figure 13: Thermistor Readings Drillhole 10WBW004	
Figure 14: Primary Tank Farm	
Figure 15: Workshop and Crusher Area	
Figure 16: Jet Fuel Storage	
Figure 17: Sedimentation Pond and Burn Pit	
Figure 18: Ore Stockpiles	
Figure 19: Land Farm and Bone Yard	
Figure 20: Portal and Incinerator Area	
Figure 21: Camp Area	
Figure 22: Airstrip	
Figure 23: Radio Tower and Vent Raise Area	
Figure 24: Core Storage Areas	
Figure 25: Existing and New STP	
Figure 26: Vegetation Dieback Areas	

List of Appendices

Appendix A: Primary Tank Farm Settlement Data

1 Introduction

1.1 Inspection Requirement

The Boston Advanced Exploration Project (Boston Camp) is an exploration camp of Hope Bay Mining Limited (HBML), a wholly owned subsidiary of Newmont Mining Company (NMC). The camp is located about 170 km southwest of Cambridge Bay within the western Kitikmeot Region, Nunavut (with general coordinates of latitude 67°39'N and longitude 106°22'W, as shown in Figure 1).

The Boston Camp is currently used on a seasonal basis from which to carry out prospecting and exploration, various forms of exploration drilling, core splitting and logging. In addition, the site has historically been subjected to bulk underground sampling and processing.

Site operations are currently conducted under Nunavut Water Board (NWB) License 2BB-BOS0712 (the License), dated July 6, 2007, which entitles HBML (the Licensee) to use water and dispose of waste associated with their operations. Part D, Item 20 of the License (NWB 2007) states the following:

"An inspection of the earthworks, geological regime, and the hydrological regime of the Project is to be carried out annually during the summer by a Geotechnical Engineer. The Geotechnical Engineer's report shall be submitted to the Board within sixty (60) days of the inspection, with a covering letter from the Licensee outlining an implementation plan to respond to the Engineer's recommendations."

Additionally, Part D, Item 10 states:

"The Licensee shall ensure that Containment Ponds are designed and bermed in such a way to ensure there is no seepage. A report on seepage shall be included as part of the Geotechnical Engineer's annual report required by Part D, Item 20."

In fulfillment of these regulatory requirements, Mr. Chris Hanks, Director for Environment and Social Responsibility from HBML, requested that SRK Consulting (Canada) Inc. (SRK) conduct the 2010 geotechnical site inspection. This report provides a summary of the conditions observed and the resulting mitigation recommendations. Table 1 provides a summary of the inspection components.

Table 1: List of Individual Inspection Items

Facility/Data Type	Inspection Item	
In attrium a retation /Data	Thermistors	
Instrumentation/Data	Primary Tank Farm Settlement Surveys	
	Primary Tank Farm	
	Power Plant Fuel Containment	
	Central Pad Fuel Containment	
	Jet Fuel Containment	
Containment Structures	Solid Waste Disposal Site (including Burn Pit)	
	Ore/Waste Rock Stockpiles	
	Settling Pond	
	Soil Containment Berm (Landfarm)	
	Diamond Drill Cuttings and Settling Pond	
Mina Openinga	Portal	
Mine Openings	Vent Raise	
	Road to Dock	
	Camp Complex Foundation Pad	
	Road to Airstrip	
	Airstrip	
	Drill Road	
Infrastructure	Core Storage Road	
	Wooden Walkway to Boat Dock	
	Radio Tower and Shack	
	Water Intake Pump Shack	
	Existing STP Foundation Pad	
	New STP Foundation Pad	
	Core Storage Area(s)	
	Grey Water Discharge	
Other Areas	Drill Sites	
	Vegetation Dieback Zones	
	V-Notch Weir	

Three previous formal geotechnical inspections in fulfillment of the Water Licence Condition have been carried out. The first was in October 2007 (SRK 2008), the second in July 2008 (SRK 2009a) and the last in July 2009 (SRK 2009f). This report describes the fourth formal annual geotechnical inspection.

1.2 Report Structure

Section 2 of this report provides a brief summary of the site history and physical conditions to provide context for the report content. The inspection conditions are described in Section 3 and an overall summary of recommendations is provided in Section 4. Photos representing the inspection

conditions are included as Figures and supporting settlement monitoring data is included as Appendix A.

1.3 Disclaimer

This report and the opinions and conclusions contained herein ("Report") contains the expression of the professional opinion of SRK Consulting (Canada) Inc. ("SRK") as to the matters set out herein, subject to the terms and conditions of the agreement dated September 2008, HBML Professional Services Agreement (HBML.BOC-CM.PSA.003) (the "Agreement") between SRK and Hope Bay Mining Ltd. ("Hope Bay Mining"), the methodology, procedures and sampling techniques used, SRK's assumptions, and the circumstances and constraints under which Services under the Agreement were performed by SRK. This Report is written solely for the purpose stated in the Agreement, and for the sole and exclusive benefit of Hope Bay Mining, whose remedies are limited to those set out in the Agreement. This Report is meant to be read as a whole, and sections or parts thereof should thus not be read or relied upon out of context. In addition, this Report is based in part on information not within the control of SRK. Accordingly, use of such Report shall be at the user's sole risk. Such use by users other than Hope Bay Mining and its corporate affiliates shall constitute a release and agreement to defend and indemnify SRK from and against any liability (including but not limited to liability for special, indirect or consequential damages) in connection with such use. Such release from and indemnification against liability shall apply in contract, tort (including negligence of SRK whether active, passive, joint or concurrent), strict liability, or other theory of legal liability; provided, however, such release, limitation and indemnity provisions shall be effective to, and only to, the maximum extent, scope or amount allowable by law.

2 Site Conditions

2.1 Site History

A brief summary of the site history is listed in Table 2.

Table 2: Summary of Pertinent Site Ownership History

Period	Comment
1964	Sporadic exploration in the Hope Bay area begins, resulting in several gold and silver showings including Ida Point, Ida Bay and Roberts Lake.
1970	Roberts Bay Mining explores the area for about a decade up to 1980.
1977	Noranda begins exploring for volcanogenic massive sulphide deposits. They leave the belt in 1990. Prior to 1980, Roberts Bay Mining also explored the area.
1987	Abermin Corporation stake claims in the vicinity of Spyder- and Doris Lakes. After completing some exploration they allow their claims to expire.
1988	BHP Minerals Canada Inc. (BHP) explores the southern portion of Hope Bay Volcanic Belt.
1991	BHP acquires a contiguous block of claims covering about 1,106 square kilometres.
1992	BHP commences exploration drilling at the Boston property.
1993	The first camp is constructed on the southwest shores of Spyder Lake by BHP.
1994	Construction of 35 person camp at Stickleback Lake. The Spyder Lake camp is dismantled and moved to this site.
1996 and 1997	BHP complete 2,300 m of underground development, underground exploration (drilling and sampling) and bulk sampling of the Boston deposit.
1999	BHP sells all its interests in the Hope Bay Belt to Hope Bay Joint Venture (HBJV), a 50:50 joint venture between Hope Bay Gold Corporation Inc. (formerly Cambiex Exploration Inc.), and Miramar Hope Bay Limited (MHBL), a wholly owned subsidiary of Miramar Mining Corporation (MMC).
2002	Hope Bay Gold Corporation Inc. formerly merges with MMC, and the Hope Bay site is operated under MHBL.
2008	Hope Bay Mining Limited (HBML), a wholly owned subsidiary of Newmont Mining Corporation (NMC) buys out all interests in the Hope Bay Belt from MMC. HBML assumes responsibility of the camp and Water Licence for Boston.
2009 to 2010	The camp is temporarily closed pending upgrades to the sewage treatment plant.

2.2 Site Infrastructure

The Boston Camp is situated on a ridge and is comprised of a peninsula extending northwards into Spyder Lake, as illustrated on Figure 2. The main camp footprint spans about 325 m from north to south, and 150 m east to west. The bulk of the camp facilities are located on a crushed rock pad,

ranging in thickness from 0.6 m to 3 m. The pad was designed to slope generally north at a gradient of about 1%.

The camp consists of a series of joined trailers to provide accommodations and office space for about 50 people. One trailer houses the water treatment plant and another, off the main pad, the original sewage treatment plant (STP). A new STP is currently under construction, and will ultimately replace the existing facility. There are six tents that act as additional office space and core logging shacks. A "Weatherhaven" type building, that used to contain the bulk sampling crushing plant, is now used as a workshop and a general equipment storage shed. The last remaining buildings consist of a maintenance shop and the power generator shed. Generator fuel (diesel) is supplied from two aboveground storage tanks, adjacent to the power house. Eight additional bulk fuel tanks are housed in an engineered containment facility.

An overall site layout plan is presented in Figure 2, and a more detailed illustration of the main camp complex is presented in Figures 3 and 4. In addition to the main camp complex, these figures illustrate the relative locations of all the main infrastructure components, containment structures and mine openings.

2.3 Climate

Site specific climate data at Boston Camp is limited to a few years of data collected by BHP in the late 1990s. Comparison of this data, with regional weather stations operated by Environment Canada, suggests that the mean annual site temperature is about -13.5°C. The extrapolated mean annual precipitation is about 208 mm, with 108 mm of that falling as rain and the remainder as snow. The area is classified as arctic desert (EBA 1997).

2.4 Regional Geology

During the Quaternary period, the region was subjected to multiple glaciations. The north-western sector of the vast Laurentide Ice Sheet covered the area during each glaciation, and the present day landscape provides clear evidence of the most recent (Late Wisconsin) glaciation. Striations, orientation of eskers, grooves and drumlins indicate that the predominant glacial ice movement was north-northwest (EBA 1996).

The ice disappeared about 8,800 years ago leaving a blanket of basal till. The sea level was about 200 m higher than present immediately following de-glaciation. At that time, the project area was submerged and the edge of the ice sheet abutted the open sea. Melt water streams from the ice carried fine grained sediments towards the sea, resulting in the accumulation of marine sediments on top of the till, with the greatest accumulation in deeper water zones, which now form the valley bottoms (EBA 1996).

Isostatic rebound after de-glaciation resulted in emergent landforms, and during this process all parts of the land were washed by waves. The easily erodible marine sediments, till and glacio-fluvial sands and gravels were subsequently reworked by waves, currents and sea ice. This has resulted in

the present day outcrops where thin soil veneers were washed off the uplands and deposited in the valley bottoms. Since emergence, the natural effects of slope processes, frost action and permafrost have transformed the landscape to its present day shape (EBA 1996).

2.5 Permafrost and Geotechnical Conditions

Surficial geotechnical investigations at the Boston project area are limited to a series of seven drill holes and a subsequent terrain analysis carried out by EBA Engineering Consultants Ltd. (EBA) in 1996 (EBA 1996, 1997). There is also a series of thermistors that have been installed at the site including three shallow strings in 1996 (EBA 1996), one deep string in 1997 (EBA 1997; Golder 2000a, b), and three deep strings in 2008 (SRK 2009e). A Westbay well was installed in 2010 (SRK 2011), which allows recording of down hole water temperature during pumping. The location of all surficial geology drill holes and thermistor string locations are presented in Figure 2, and summarized in Table 3.

Table 3: Summary of Permafrost Drillholes and Thermistor Installations

	UTM Coordinates		Surface	Completion Depth	Thermistor		
Drill Hole ID	Northing	Easting	Elevation (m)	(m)	Installed (Serial #)	Source	
12259-01 (BH1)	7,504,261*	441,482*	68.6*	10.9 (below lake)	No		
12259-02 (BH2)	7,504,141	441,213	71.7	4.1	No		
12259-03 (BH3)	7,504,380	441,113	77.6	16.1	Yes (#1049)	ED 4	
12259-04 (BH4)	7,503,905*	442,323*	73.9	13.9	No	EBA (1996,	
12259-05 (BH5)	7,504,778	441,172	80.8	15.6	Yes (#1050)	1997)	
12259-06 (BH6)	7,505,683	441,327	69.7	15.8	Yes (#1051)		
12259-07 (BH7)	7,506,153*	441,830*	Unknown	Unknown	No		
97NOD176	7,504,962	441,481	78.3	367 @ -60° (298 true)	Yes	Golder (2000a)	
08SBD380	7,504,780	441,080	77.3	402 @-60° (334 true)	Yes		
08SBD381A	7,504,814	441,070	69.6	401 @ -55° (298 true)	Yes	SRK	
08SBD382	7,505,141	441,026	72.8	404 @-60° (323 true)	Yes	(2009e)	
10WBW004	7,505,665	441,018	Unknown	470 @-55° (250 true)	No (Westbay)	SRK (2011)	

^{*} Approximate information as interpolated from source drawings by SRK. Exact information is not available. Locations not marked with asterisk are surveyed coordinates.

Figures 6 through 13 summarize all available thermistor string data. It is not known if any other data from the 1996 and 1997 installations has been recorded since their installation and reporting in 1997 (EBA 1997). Golder (2000a, b) documents the findings of a site inspection, including revisiting some of the thermistors; however, no additional data was added. With assistance from the HBML surveyors, the historic thermistors were located as part of the 2009 geotechnical inspection, to

determine their status. One string was severed completely (drill hole 12259-03, see Figure 5), but the remaining three appear to be intact. A readout device compatible with the military connectors on the strings was not available to test the functionality of these strings. An appropriate readout device should be obtained from EBA Engineering (the original thermistor supplier) and the string functionality should be tested during the 2011 geotechnical inspection. If the three in-tact strings are functional, the fourth string should be spliced and tested as well.

The available information confirms that the Boston Camp is located well within the region of cold, continuous permafrost. Permafrost temperatures are below about -8°C and the active layer is generally less than 1 m thick, with the depth of zero annual amplitude about 10 m. Based on data from the deep thermistor installed in 1997, the permafrost depth is estimated to be about 520 m (Golder 2000a).

Laboratory testing (moisture contents, Atterberg Limits, grain size distribution and pore water salinity) on intact samples collected during the drilling campaign in 1996 confirms that overburden soils are comprised mainly of marine silt and morainal till ranging in thickness from 1.5 to 8 m. The silt contains up to 50% (by volume of soil) ground ice, while the till contains low to moderate ice contents (5 to 25%) (EBA 1997).

3 Inspection Conditions

Mr. Maritz Rykaart, P.Eng., Ph.D., a Principal Geotechnical Engineer with SRK, conducted the geotechnical inspection during the week of July 12-16, 2010. The detailed site inspection was carried out on foot, after travelling to site via helicopter from the Doris North camp. No-one accompanied SRK during the inspection. Ms. Jill Turk, the HBML Environmental site representative did not accompany SRK on the site inspection, but was available for questioning.

Weather conditions during the inspection were cool but sunny with light winds and no precipitation. Photos detailing the inspection conditions are included in Figures 14 through 26.

3.1 Instrumentation/Data

3.1.1 Thermistors

A summary of the available site thermistors are discussed in Section 2.5 and all available data are presented graphically in Figures 6 through 13. With the help of HBML surveyors, the 1996 and 1997 thermistor strings were located in 2009. Three of the four strings were still intact, although they are generally in poor condition, having fallen over from their support struts. Figure 5 illustrate their current state. The fourth cable has been completely severed, most likely by an animal. The section of cable to which the readout connector is attached, is still at the site, and it should be possible to reattach the cable through splicing.

A readout device compatible with the military connectors of these older strings was not available during the inspection. SRK understands that there is an appropriate readout device on site, but at the time of the inspection, it could not be located. These older strings were supplied by EBA Engineering (EBA), and if the on-site readout device cannot be found, a new device could be rented from EBA. It is recommended that during the 2011 geotechnical inspection that this is carried out, such that the functionality of these strings can be confirmed. Installation of thermistor strings represents a considerable investment, and therefore re-instating these strings would be valuable, although not a necessity.

Data collected from the three strings installed in 2008 (SRK 2009e), as well as the Westbay well installed in 2010 (SRK 2011) are presented in Figures 10 through 13. An attempt was made in July 2010 to collect data from the string in 08SBD381A; however, it was unsuccessful. Follow-up readings should be taken in 2011 to confirm if the string is active.

Recommendations:

1. A compatible readout device for the older thermistor strings should be obtained from EBA, the supplier (if the on-site device cannot be located), and the functionality of the three intact thermistors should be checked. If these strings are operational, the severed string should be

spliced and tested as well. Any strings that are found to be functional should be included in the formal thermistor monitoring program for the site.

- 2. Additional attempts must be made to read the string in 08SBD381A to confirm if it remains active.
- 3. Formal monitoring of the on-site thermistor strings should continue. This program should consist of quarterly readings (or as close to this schedule as the camp operating window allows). This data should be reported as part of all subsequent annual geotechnical inspections.

3.1.2 Primary Tank Farm Settlement Monitoring

The 2007 annual geotechnical report recommended that a series of settlement beacons be installed on the primary tank farm containment berm to allow quarterly settlement surveys to provide early warning signs of undue tank settlement as a result of foundation settlement due to permafrost degradation. HBML opted not to install the recommended beacons, but rather initiated a survey program based on three control points on each of the eight tanks in the containment area. This is an appropriate monitoring program, in the opinion of SRK. The control points were established by the site surveyor, Mr. Jay Hallman, on April 21, 2008. The control point co-ordinates and elevations are listed in Table 4.

Table 4: Summary of Survey Control Points Established for the Primary Tank Farm

Tank	Control Point	Northing (m)*	Easting (m)*	Elevation (m)
	A	5,325.879	1,305.901	80.674
1	В	5,326.428	1,308.581	80.989
	С	5,328.263	1,306.711	80.992
	A	5,327.678	1,315.749	80.877
2	В	5,326.866	1,318.217	81.190
	С	5,329.353	1,318.048	81.114
	А	5,331.618	1,306.850	81.057
3	В	5,331.612	1,309.744	81.062
	С	5,335.467	1,307.263	81.090
	А	5,331.166	1,318.159	81.128
4	В	5,334.739	1,317.563	81.092
	С	5,334.220	1,314.710	81.128
	А	5,337.355	1,307.654	80.896
5	В	5,337.490	1,310.713	81.075
	С	5,341.035	1,307.826	81.089
	А	5,337.092	1,317.422	80.991
6	В	5,340.813	1,317.436	81.031
	С	5,340.311	1,314.183	81.061

Tank	Control Point	Northing (m)*	Easting (m)*	Elevation (m)
	Α	5,343.001	1,307.814	80.875
7	В	5,343.343	1,310.862	81.005
	С	5,346.505	1,307.626	81.060
	Α	5,342.700	1,317.450	80.956
8	В	5,345.860	1,317.826	80.962
	С	5,345.604	1,313.962	81.033

^{*} This is a local grid for settlement surveying only.

Two subsequent settlement surveys were carried out in 2008 (August 7 and October 17), two in 2009 (July 25 and September 19), and one in 2010 (August 2). These surveys were completed by HBML survey staff using a TOTAL Station and prisms. The survey accuracy is not stated; however, it should be within ± 10 mm. The complete results are presented in Appendix A and the overall summary data is presented in Table 5.

A review of the data suggest a slow but consistent trend of the tanks settling; however, this settlement is very small and since there is no trend of movement in the horizontal plane there is no indication that differential settlement is taking place which may cause the tanks to topple.

Table 5: Summary of Overall Settlement Data for the Primary Tank Farm (April 2008 to August 2010)

Taul	Average Survey Differences (mm)				
Tank	Northing ¹	Easting ¹	Elevation ²		
#1	3.4	-0.4	-7.5		
#2	3.5	-1.4	-6.1		
#3	0.9	1.0	-6.3		
#4	2.9	-1.2	-5.4		
#5	-0.2	0.0	-8.9		
#6	3.2	-2.7	-7.1		
#7	-5.6	1.4	-9.9		
#8	3.2	-2.5	-6.3		

^{1.} A negative value implies tank has moved to the south (Northing) or the west (Easting).

Recommendations

- 1. Quarterly monitoring (or as close to this schedule as the camp operating window allows) of tank settlement should continue. This data should be reviewed and reported on as part of the annual geotechnical inspection, and should there be any signs of undue movement, appropriate mitigation plans can be put in motion.
- 2. The foundation settlement risk should be recognized in the spill response plan for the tank farm.

^{2.} A negative value implies tank has moved down.

3.2 Containment Structures

3.2.1 Primary Tank Farm

The primary tank farm, housing eight large fuel tanks is located in an engineered secondary containment facility constructed in 2001 (Figure 14). SRK understands that there is no formal asbuilt documentation for the facility. Based on interviews, SRK concluded that the facility was designed by EBA and subsequently constructed by MHBL with engineering supervision by EBA.

It is understood that secondary containment is provided by a PVC liner (type unspecified) placed on a prepared rockfill pad with constructed containment berms of rockfill providing the necessary containment capacity. The liner has a top cover of gravel (crushed ore stockpile material) as a protection layer. The eight tanks are placed directly onto the protection layer and are interconnected with permanent steel piping. Fuel transfer from these main tanks into equipment, fuel drums and Tidy Tanks are done in a contained fuel transfer area, using an electric pump. The entire facility is constructed directly on permafrost overburden soils, as described in Section 2.5.

Visual inspection of the secondary containment facility showed several signs of surficial slip surfaces on the containment side slopes. In 2008 a few small tension cracks were observed along the berm crest. These were not noticed during the 2009 inspection, but were again observed as part of the 2010 inspection. The slip surfaces could be an early indication of settlement, or may simply be relaxation due to the over steepened nature of the gravel berm. The liner is not exposed anywhere, and the containment berms for both the main containment facility and the fuel transfer areas are intact. There were no visible signs of fuel spills outside of the respective containment areas. HBML has rigorous protocols in place for fuel transfer, and provided those are followed, the facility design appears adequate to provide environmental protection.

Settlement could occur as a result of permafrost thaw due to the foundation conditions under the tank. A settlement monitoring program was put in place in April 2008 as described in Section 3.1.2. Data to date suggest that the tanks may be undergoing some settlement; however, the rate appears to be very slow and since there is no significant horizontal movement, there are no signs of differential settlement. This situation should continue to be monitored and an acknowledgement of the settlement risk should remain.

During the inspection it was noted that there was no ponded water in the containment area. The facility is equipped with a sump, and at the time of the inspection there was a trash pump installed in the sump, with a pipeline leading out from it. The practice of keeping the containment area free of ponded water is appropriate and should be maintained.

Recommendations:

 The appearance of surficial slip surfaces and tension cracks on the containment berms should be monitored. Remedial measures should be implemented if there are any signs of these progressing. Should excessive deformation of these berms occur (the probability of which is likely low), the tank integrity is not at risk. It is simply the effectiveness of the secondary containment that will be compromised.

2. The tank settlement monitoring program that has been put in place is reasonable. Quarterly monitoring (or as close to this schedule as the camp operating window allows) of tank settlement should continue. This data should be reviewed and reported on as part of the annual geotechnical inspection and, should there be any signs of undue movement appropriate mitigation plans should be put in motion.

3.2.2 Power Plant Fuel Containment

Two small double-wall fuel tanks servicing the power plant are located in a secondary containment facility (rockfill berm) immediately west of the maintenance shop (Figure 15). Construction details for this secondary containment are not available; however, repairs to this containment system were completed in 2008, including installation of a liner (SRK 2009a). There are no concerns with this facility.

Recommendations:

1. No action required.

3.2.3 Central Pad Fuel Containment

A small double-wall fuel tank was installed since the last annual geotechnical inspection was carried out in July 2008. This tank, illustrated in Figure 15, is located approximately in the center of the camp pad, immediately east of the geology offices. The fuel tank was installed in a purpose built secondary containment facility using a liner (type unspecified) and the stockpiled crushed ore. The facility was founded directly on the camp pad. Construction details (design or as-built drawings) of this facility are not available. There are no apparent concerns with this facility.

Two new fuel tanks were observed during the 2010 inspection within the confines of the camp (Figure 15). These are elevated double-walled tanks. Neither of the tanks were however placed within secondary containment as per the normal HBML protocol.

Recommendations:

 Confirm whether secondary containment is required for the two new tanks, and if so install secondary containment as required.

3.2.4 Jet Fuel Containment

Jet fuel is stored in drums, which are grouped together on wooden pallets, stacked two high, in an area of the rockfill pad northeast of the primary fuel tank farm. Three portable pollution control berms are used to provide secondary containment as illustrated in Figure 16.

One of the secondary containment facilities were compromised at the time of the inspection due to the fact that at least one wall of the containment structure was collapsed. Contrary to observations, during the 2009 inspection, none of the facilities contained appreciable amounts of ponded water.

Recommendations:

1. The secondary containment berms should be regularly inspected and repaired as needed.

3.2.5 Solid Waste Disposal Site (Including Burn Pit)

Combustible domestic waste is incinerated on site. Other non-hazardous and hazardous waste is stockpiled, packaged and seasonally removed from site to Yellowknife or Hay River as backhaul opportunities arise. HBML has substantially cleaned up the site and the backlog of material that still has to be hauled away has been significantly reduced since the 2008 annual geotechnical inspection was completed. The waste material that remain on site is not stored within designated containment facilities; however, the waste is neatly organized and due to the nature of the waste (as described by site staff), environmental containment does not appear to be necessary. This should be confirmed through an appropriate inventory.

At one time, all wood waste was burned in a burn pit (a converted sedimentation pond) located immediately south of the active sedimentation pond (Figure 17); however, this practice has been discontinued and all non-combustible materials was removed from the pit. The burn pit itself is still used to contain unburned wood waste and ash, until such time as HBML backhauls these materials, or adopts an alternate strategy to dispose of these elements.

Recommendations:

- 1. Confirm through an appropriate waste inventory that there are no wastes that require environmental containment. *This may have already been conducted; however, SRK is not aware of the study.*
- 2. Since the burn pit no longer serves its original design intent, it should be cleaned out by removing all of the wood waste and ash and relocating it to an appropriate disposal site.
- 3. If the burn pit could be used to perform another functional use, it should be so designated, otherwise HBML should prepare a plan to completely decommission this facility.

3.2.6 Ore Stockpiles

A large number of crushed ore stockpiles are located on the north-western portion of the camp complex foundation pad (Figure 18). This ore comes from the 27,000 ton bulk sampling program carried out between 1996 and 1997. These stockpiles are individual un-compacted end-dump piles. Surface water drainage from this part of the foundation pile is not specifically separated from the rest of the foundation fill pad, and is not contained, but allowed to flow directly onto the tundra.

The 2007 inspection report recommended that HBML compile a detailed database of all the seep sampling tests carried out over the life of the facility and have that data reviewed by an appropriately qualified professional with the specific objective of determining whether there is any poor quality seepage emanating from the exposed ore stockpiles. HBML contracted a specialist geochemical study with SRK to complete an inspection and sampling program to assess the geochemical performance of historic waste rock and ore at Boston. The objectives of this work were twofold: (1) to fulfill the conditions of Water License No. 2BB-BOS0112 Part E, Item 8 and, (2) to assess the geochemical performance of the weathered materials as a part of the geochemical characterization currently in progress to support future permitting activities.

The program included sampling of waste rock and ore from the ore stockpiles, roads and airstrip, as well as a seep survey around the perimeter of the site. This work was done in July 2008. Testing of the waste rock included field contact tests, acid-base accounting, metal analyses, and leach extraction tests. There is also historical seepage available for this area that was analyzed as part of this program. The results of this study were presented in a technical report (SRK 2009b) which was submitted to the Nunavut Water Board in 2009.

SRK also completed a water and ore/waste rock management plan (Plan) for the Boston site, based on the results of the geochemical assessment completed (SRK 2009d). This Plan was also submitted to the Nunavut Water Board in 2009 and stipulates appropriate management protocols for this material.

Recommendations:

1. The procedures, protocols and monitoring plan stipulated in the 2009 water and ore/waste rock management plan for the Boston site should be implemented.

3.2.7 Settling Pond

One lined settling pond (Figure 17) has been constructed along the eastern perimeter of the camp foundation pad (immediately north of the burn pit). As-built records for the construction of this pond are not available. It is understood that this pond was used to contain wash water during the screening and crushing of ore as part of the bulk sampling program.

The pond was in poor shape in 2007; however, substantial repairs were carried out on the liner in 2008 (SRK 2009a). The condition of the pond during the 2010 inspection showed signs of deterioration, most notably due to the liner no longer being supported at the crest through sand bags, probably as a result of strong winds. The pond contained various amounts of gravel (crushed ore) and wood debris which could compromise the liner integrity.

Currently the pond is used as an emergency holding pond for possible fuel spills, disposal of water from fuel containment berms, or when the sewage treatment plant experiences upset conditions. SRK is of the opinion that, if this pond is to be used for anything where there would be solids collected in the pond, its design would make it extremely difficult to remove these solids to retain

pond capacity due to its depth and the fact that the liner is not protected. Furthermore, since the pond does not have a designed overflow facility (i.e. spillway), it would experience uncontrolled overflow when its capacity is exceeded. HBML has stipulated that an overflow is not required as the management practice is to pump out snowmelt and rainwater as required, after testing for contaminants.

The pond has no instrumentation of any nature and, as such nothing can be said about its historic performance. A reconnaissance survey of the pond did identify a clear zone of water seeping from the downstream toe of the pond embankment. Although it cannot be definitively confirmed that this seepage is emanating from the pond, there are no other likely sources.

Recommendations:

- 1. Water quality sampling should be undertaken to confirm whether the wet zone downstream of the pond is in fact seepage emanating from the pond. If the flow is confirmed as seepage, an appropriate mitigation plan must be implemented to have the liner repaired.
- 2. The debris in the pond should be cleared out as it poses a potential puncture risk to the liner.
- 3. A management plan must be implemented to ensure sediment (i.e. hydrocarbon contaminated soil, sewage treatment plant sludge, etc.) can be removed without damaging the liner.
- 4. If the pond is to be used to retain water for any length of time, a suitable leak detection monitoring system should be implemented. As a minimum, a protocol involving frequent visual inspections would have to be put in place for the pond. Excessive and prolonged leaking will lead to permafrost degradation, which in turn will result in differential settlement that may cause the liner in the pond to fail.
- 5. The pond should have a suitable barricade around it to prevent human and animal access. Due to the current design, it would be extremely difficult to get out of the pond unassisted if a human or animal were to inadvertently enter or fall in.

3.2.8 Soil Containment Berm (Landfarm)

As a result of a historic fuel spill, HBML constructed a lined soil containment facility (Figure 19) within which all excavated contaminated soils have been stored (EBA 2004). SRK reviewed the asbuilt records for this facility (EBA 2004) and, supported by visual inspection, confirms that it consists of a bermed and lined area in which contaminated soil is placed. In addition to soils spread about 1 m thick over the entire surface of the facility, there are also a large number of old fuel drums filled with contaminated soils contained within the confines of the facility.

From discussions with HBML site staff in 2007 and a review of the as-built report, it appears that the soil containment berm was designed to be used as an active hydrocarbon landfarm area. A land farming protocol was not provided in the as-built report; however, site staff confirmed that since

initial placement of the contaminated soils into the containment area, there has been no work carried out in the form of tilling or any other means of soil mixing. HBML did routinely conduct soil sampling within the confines of this facility, the results of which are reported as part of the annual Licence conditions. Based on a review of the formal operational procedure of HBML land farming practices (MHBL 2007), and comparison of that with the site staff, SRK doubts whether the soil sampling results reported by HBML would be representative. The primary reason for coming to this conclusion is that the soil in the facility is about 1 m thick, and has never been tilled or reworked in any way, as confirmed by HBML staff. Furthermore, the soil sampling to date only effectively covers the upper 10 cm of the profile.

HBML did commission a study in 2009 to test the soils contained in the landfarm in accordance with appropriate protocols, and are in the process of developing an appropriate remediation strategy for these materials.

The containment facility itself however appears to be intact; although it is filled to capacity and would not be able to contain more soil until some of it has been adequately treated and/or relocated.

Recommendations:

- 1. HBML commissioned a study to test the soils in the landfarm and developed a strategy to relocate and treat these soils. The study has been completed and HBML is currently reviewing the recommended remediation measures.
- 2. The site appears to be fully contained and therefore does not pose any immediate risk.

3.2.9 Diamond Drill Cuttings and Settling Pond

Some drill cuttings have historically been disposed of permanently in a settling pond immediately west of the airstrip (Figures 22 and 26). Site staff could not confirm if this pond was intentionally designed, but if so there are no as-built records and the timeframe for how long this practice has been in operation is not clear. Visual inspection suggests that the pond is located at a historic drill hole. Poor control of the drill fluid resulted in permafrost degradation and subsequent annual thaw created by a pool of standing water resulted in the pool increasing in size. At some stage, the pond started to overflow and silt-laden water started to flow overland towards open water bodies. At that time, drill cuttings were placed in the pond in an attempt to stop further degradation. Geotextile was also installed to control silt flowing from the pond.

Although there were signs of this pond being actively used in 2007, there was no evidence of it being used since 2008. Considering the amount of standing water present during the inspection, as well as the apparent previous random placement of drill cuttings, SRK is not convinced that the permafrost degradation has stopped, and although there was no visual evidence of silt laden water flowing from the pond, there remains a significant section of the pond downstream of the geotextile silt barrier.

Recommendations:

- 1. SRK is not convinced that the settling pond is appropriate for its current use. Should there be a need for a settling pond, it is recommended that it be re-engineered to control the permafrost degradation, and to ensure that silt traps are located in the optimal positions.
- 2. Considering the fact that HBML will continue to collect significant amounts of drill cuttings, an appropriate management plan for these cuttings will have to be developed. This may include specific placement procedures for drill cuttings into permafrost degradation areas. An operational plan should be developed for this, possibly with the assistance of an appropriately qualified Professional Engineer with permafrost experience.

3.3 Mine Openings

3.3.1 Portal

A bulk sampling program was completed by BHP in 1996 and 1997, at which time 27,000 tonnes of ore and 106,000 tonnes of waste rock were extracted. The ore was crushed on site, and stockpiled on a rockfill pad constructed from the waste rock. The waste rock was also used for other infrastructure such as the airstrip. The bulk sampling extraction was via 2,300 m of underground development (completed by Procon Mining and Tunnelling Ltd.) using a ramp that extends from ground surface at approximately 4,035 m elevation to approximately 3,850 m elevation (local mine grid). The 185 m deep ramp dimensions are approximately 5 m in wide by 3.6 m high. The orientation of the ramp is generally north-south. Five cross-cuts were established, three into the B2 Zone and the remaining two into the B3 Zone.

The portal, which is located about 25 m east of the maintenance shop as illustrated in Figure 20, was collared in altered volcanic rock, all within the permafrost. This was confirmed through installation of four underground thermistors (Golder 2000a, b). During extraction of the bulk sample, the portal was not heated but operated at an ambient temperature of about -10°C. The portal was operated under dry conditions with no groundwater inflow. After completion of the bulk sample collection, the portal was abandoned and sealed off with a locked gate.

The decline was reported to be dry and geotechnically sound during a site inspection by Golder Associates Ltd. in April 2000 (Golder 2000b). According to site personnel the last operational entrance of the portal was in 2001. An attempt to enter in 2004 was aborted, reportedly due to the presence of a frost plug, likely created due to pooled water (from rainfall and snowmelt) at the portal entrance. There are also unconfirmed reports that water has run down the ramp some distance and formed an ice dam.

During the 2010 site inspection, the bulk of the portal access was flooded. It would appear as if the condition of the portal remain unchanged from the last inspection in 2009 where it was found that the portal seal to prevent unauthorized access was intact, and the signpost that identifies the area as

potentially hazardous and warning persons against entering the area without permission was badly weathered and barely legible.

The visible exposed portion of the portal roof shows signs of minor rock spalling; however, the roof appears to be essentially structurally intact. There continues to be evidence of small fragments (less than 10 cm diameter) having broken off. The roof is armoured with 10 cm wide steel banding and rock bolts at this time. The most likely cause of spalling is freeze-thaw action.

Recommendations:

- 1. SRK recommends that HBML replace the weathered warning notices at the portal entrance advising of the dangers associated with unauthorized access to the area.
- 2. The rock spalling on the exposed section of the portal roof is likely a fall hazard. Persons entering the area should wear appropriate personal protective equipment; however, a site specific hazard assessment should be completed to make people aware of the dangers. Should there be a need for any individual to enter the area for reasons other than a brief inspection, consideration should be given to installing roof support, such as a small diameter wire mesh (50 mm mesh) to mitigate the fall hazard.

3.3.2 Vent Raise

There is a single vent raise located about 100 m south-west of the portal entrance (Figure 23). Mechanical and electrical support equipment is installed on a levelled wooden platform about 0.6 m off the tundra. The vent area and wooden platform base are sealed off with tarps and the mechanical and electrical equipment is locked in a steel shed. Overall the facility looks weathered; but there does not appear to be permafrost degradation. Site staff could not confirm when the facility was last accessed or inspected in detail.

Recommendations

- 1. The tarps are significantly weathered and their attachment points are starting to come apart. The tarps should be replaced.
- 2. Signposts warning visitors of potential dangers associated with accessing the area do not exist. It is recommended that signs be erected.

3.4 Infrastructure

3.4.1 Road to Dock

The single lane road to the dock consists of 0.3 to 0.6 m thick rockfill placed directly onto the tundra. Since the road runs down-gradient towards Stickleback Lake, small contour berms have been constructed, redirecting surface runoff from the roadway. Minor signs of surface water erosion are evident along the road, but this damage would be considered quite normal for a road of this nature.

Likewise, minor undulations (deformation) in the road suggest there may be isolated small pockets where permafrost degradation has occurred, and/or peat in the active layer has compressed. There is no thermal instrumentation or geologic data to support this observation. Considering the amount of time the road has been in operation, this deformation is likely historic; however, the undulating road could be a safety concern. Appropriate speed control should be implemented for the road.

Site staff confirmed that repairs are conducted to the road surface if and when there are any signs of surface erosion or other significant undulations. Based on descriptions from site staff, the predominant material used for maintenance purposes is crushed ore. This amount of maintenance has never been substantial.

Recommendations:

- Maintain the current level of care and maintenance on this road; but stop the use of crushed ore
 to avoid water quality problems linked to the geochemistry of the ore. A suitable alternative
 clean source of rock should be located.
- 2. Ensure that appropriate speed control is exercised on this road.

3.4.2 Camp Complex Foundation Pad

The foundation pad of crushed rock (Figure 21), which underlies most of the site infrastructure, varies in thickness from 0.6 to 3 m according to previous records. Initially the pad was constructed to ensure north-south drainage with the pad sloping about 1% towards the north. The foundation pad was designed to prevent thaw settlement and permafrost degradation within the operating footprint of the advanced exploration camp.

There is no instrumentation installed in the pad to confirm the thermal regime beneath the pad. Visual inspection suggests that localized settlement has occurred, as there are local low spots and evidence of significant ponding on the pad. There is no longer a constant drainage grade off the pad.

Differential settlement of the pad appears to be within areas where the pad is the thinnest, although there are no as-built records to corroborate this observation. The accommodation complex does not appear to be impacted structurally by differential settlement, probably since these structures can be levelled by simply adding more blocking as required. It is not known how much levelling of the camp has occurred over the years. The only significant consequence of differential settlement is localized ponding of water. This ponding is likely an inconvenience in day-to-day camp life, but more importantly, it acts as a new heat source and further increases the active layer depth leading to more settlement.

There is one large erosion gully south of the camp complex. This gully has been repaired by infilling with fine crush material, from the ore stockpiles. Whilst this appears to have been successful in preventing further erosion and permafrost degradation, this material may contribute towards poor quality leachate. This should be evaluated as part of the newly developed water and ore/waste rock

management plans. Other than this gully, there are no visual signs of concentrated flows from this pad, and there is no evidence of any erosion gullies along the edge of the pad.

There was a fuel spill at one time immediately south of the camp. The hydrocarbon contaminated soils were excavated and placed in the landfarm. Currently this area is poorly drained and at the time of inspection, there was standing water which appeared to contain algae. This ponded water will result in permafrost degradation, and should be pumped out on a seasonal basis.

Recommendations:

 HBML should have the pad surveyed and develop an action plan to fill in and re-grade the pad to re-establish constant drainage from the pad. Special attention must be given to preventing further ponding on the pad as it may promote permafrost degradation.

3.4.3 Road to Airstrip

The single lane roadway to the airstrip is constructed from crushed rock ranging in thickness from 0.3 to 0.6 m. There are local depressions along the road that are more pronounced than the immediately adjacent topography, suggesting that some permafrost degradation has occurred resulting in settlement. Site staff confirmed that on a few occasions minor infilling of low spots has been carried out; however, there does not appear to be a formal record of any such remediation works.

Visual inspection did not identify any signs of surface water erosion, and although there are no culverts through the road, there are no signs that the road is resulting in surface water ponding.

Recommendations:

- 1. Maintain the current level of care and maintenance on this road, but stop the use of crushed ore. A suitable alternative clean source of rock should be located.
- 2. Ensure that appropriate speed control is exercised on this road.

3.4.4 Airstrip

The airstrip (Figure 22) was constructed in the summer of 1997 by Procon Mining & Tunnelling Ltd. under contract to BHP. Boston development waste rock was used to construct the airstrip (BHP 1997).

The north-south all-weather airstrip is a rockfill structure similar to the roads and foundation pad. It appears to be generally thicker than the road, and although there is no as-built information available, visual inspection suggests that its thickness ranges between 0.6 and 1.2 m.

Significant settlement along the airstrip alignment reportedly occurs every year, and as a result frequent infilling and levelling has had to be carried out on the airstrip over the years to ensure safe

aircraft operation. According to HBML staff the airstrip is inspected annually by the aircraft charter company for operational suitability and, if requested, HBML carries out maintenance as needed. The latest levelling and maintenance was carried out in August 2007 by Nuna Logistics, under the direction of SNC-Lavalin Engineers and Contractors (SLEC). Material from the crushed ore stockpiles was used as infill material for the repairs, and site staff confirmed that this material was used for repairs in previous years as well.

Although there is no thermal monitoring instrumentation under the airstrip, the settlement is most likely as a result of thaw settlement in the underlying permafrost.

There are no signs of surface erosion on the airstrip. The airstrip does not have any culverts to allow water flow; however, visual inspection did not identify any pre-construction flow paths that may have been obstructed by the airstrip. There is a significant number of standing water ponds immediately adjacent to the airstrip. These ponds are permafrost degradation zones resulting from drillholes. More details about these ponds are discussed later in the report; however, the presence of these ponds threatens the integrity of the airstrip, and will lead to elevated maintenance costs.

There are small tension cracks along the crest of the airstrip shoulder, generally in areas where large ponds are situated. While these cracks do not suggest any immediate risk, they should be monitored frequently for signs of progression.

Recommendations:

- 1. The ponding immediately adjacent the airstrip, resulting from permafrost degradation at historic drill sites, should be prevented. Further details about this issue are discussed elsewhere in this report.
- 2. Conduct frequent walk-over surveys of the airstrip crest to ensure there are no progressive worsening of the tension cracks along the shoulder crests.

3.4.5 Drill Road

This road leads off from the north end of the airstrip to an old drill staging area. It has the same design as the other site roads. There are no additional issues or concerns relating to this road other than those raised previously for other roads.

Recommendations:

- 1. Maintain the current level of care and maintenance on this road, but stop the use of crushed ore. A suitable alternative and clean source of rock must be located.
- 2. Ensure that appropriate speed control is exercised on this road.

3.4.6 Core Storage Road

The core storage road leads off midway from the airstrip towards a rock outcrop area where core boxes are stored. This road, which receives relatively little traffic, is of similar design to the other site roads. There is a 200 mm steel pipe culvert at the west end of the road, apparently allowing water from the large permafrost degradation zone pond to the north to drain towards the south. The pipe culvert appears to have settled to a point where its invert level is below that of the areas to be drained. Subsequently the culvert no longer functions and ponding at either end of the pipe is contributing to additional permafrost degradation.

Recommendations:

- 1. Consideration should be given to removing the culvert and implementing appropriate remedial measures to the areas of permafrost degradation. This should not be done without developing a comprehensive permafrost degradation mitigation plan for the site, as there are many ponded areas that may have to be interconnected to resolve the problem in the long term (see also Section 3.5.3).
- 2. Ensure that appropriate speed control is exercised on this road.

3.4.7 Wooden Walkway to Boat Dock

The wooden walkway leading from the southern end of the airstrip to a boat dock in Stickleback Lake (Figure 22) has been constructed as a floating walkway directly on the tundra. The walkway has settled into the tundra hummocks and although there is no lasting permafrost damage at this time, vegetation dieback may ultimately result in the start of an erosion gulley, which in turn would lead to erosion permafrost degradation.

SRK understands that HBML is considering decommissioning the boat dock in Stickleback Lake. If this is done, SRK recommends removing the walkway altogether.

Recommendations:

- Consideration should be given to reconstructing the walkway such that it does not rest directly
 on the tundra. If this is not practical given the use the walkway gets, a monitoring program
 should be implemented during the summer months to ensure that erosion gullies do not go
 unnoticed.
- 2. If the boat dock is decommissioned, remove the walkway.

3.4.8 Radio Tower and Shack

A new radio repeater tower was installed south-east of the vent raise in 2009 (Figure 23). The tower was designed and installed by SNC Lavalin Engineers and Contractors (SLEC). The tower is supported by a concrete foundation embedded in bedrock and three wire anchors embedded in

bedrock. The radio tower equipment is installed in an un-insulated wooden shack immediately adjacent to the tower. The shack is on a timber foundation of levelling blocks directly on an outcrop area.

Recommendations:

1. No action required.

3.4.9 Water Intake Pump Shack

Potable water for the Boston Camp is supplied from Spyder Lake. A wooden pump shack houses the primary pump elements. This wooden shack is located immediately outside the ordinary high water mark on Spyder Lake, and is placed directly onto the tundra. There are no signs of permafrost damage at this time; however, vegetation dieback likely has occurred immediately beneath the shack.

Recommendations:

 It is not good practice to construct infrastructure directly onto the permafrost. HBML should consider constructing a thermal pad or other appropriate foundation to ensure preservation of the permafrost.

3.4.10 Existing STP Foundation Pad

The existing sewage treatment plant (STP) is constructed on a small levelling pad of crushed ore, some distance west of the camp pad (Figure 25). The pad is generally very thin, (less than 0.5 m thick) and therefore not sufficiently thick to act as a true thermal pad. There are however no signs of permafrost damage at this time.

Recommendations:

1. No action required.

3.4.11 New STP Foundation Pad

The new sewage treatment plant (STP) will be constructed north-west of the camp, and north of the existing STP (Figure 25). Originally this STP was to be constructed on a levelled thermal pad constructed from crushed ore; however, in accordance with the newly adopted water and ore/waste rock management plan for the site (SRK 2009d), HBML changed the design. The pads were however already constructed before the decision to change was made and therefore the ore had to be backhauled. One of the two constructed pads was however not removed. Where the pad was removed some minor damage to the tundra vegetation occurred, which could result in ongoing permafrost degradation if not monitored and repaired if and when it becomes evident.

The new STP foundation consists of levelling timbers and platforms to allow circulation of cold air, which in turn will ensure integrity of the permafrost.

Recommendations:

 The area where the ore pad was backhauled, and where minor damage to the tundra occurred, must be monitored to ensure no ponding of water, which would lead to increased vegetation dieback and subsequent permafrost damage.

3.5 Other Areas

3.5.1 Core Storage Area(s)

Core boxes are being stored at the following locations, as illustrated in Figure 24:

- East of the airstrip, scattered around sections of exposed bedrock and occasionally directly on the tundra; however, due to the location, the permafrost overburden at these locations is likely shallow. Visual inspection yielded no concerns with respect to permafrost degradation.
- At the end of the drill road north-west of the runway. Boxes are partly stored on a pad, but mostly directly on the tundra. This area has extensive permafrost and vegetation dieback damage, but this is not from storage of the core boxes (see Section 3.5.4).
- On the camp pad at various locations. There are no concerns about any of these areas.
- At two locations immediately east of Stickleback Lake. At both these sites the boxes are stored directly on the tundra. Visual inspection yielded no concerns with respect to permafrost degradation, but vegetation dieback has occurred immediately beneath the boxes.

SRK understands that HBML is reviewing their site wide core storage protocols. It is recommended that wherever possible core storage should be on rock outcrops or dedicated gravel pads. Where there are no reasonable alternative, but to store core on the tundra, the boxes should be placed on timbers, and the area must not be low-lying or poorly drained. Storage of core boxes directly on the tundra does not automatically lead to permafrost degradation; however the underlying vegetation dies, and that could lead to permafrost and erosional damage if the vegetation cannot be reestablished.

Recommendations:

- 1. HBML should re-evaluate their core storage requirements, as the random aerial spread of core boxes at these locations may not be suitable in the long term.
- 2. Consideration should also be given to relocating any core storage boxes that are not currently on exposed bedrock. This should be done as part of a long-term core storage plan.
- 3. HBML should consult the services of an expert knowledgeable with tundra vegetation to implement appropriate remediation strategies.

3.5.2 Grey Water Discharge

Grey water from the sewage treatment plant is currently being discharged at a location immediately north of the camp foundation fill pad (Figure 25). This water ultimately flows overland towards the east arm of Stickleback Lake. During the 2007 inspection it was noted that a large clearing devoid of any vegetation has developed where the water is discharged, and although there was no standing water at the time of the inspection, it is evident that at times significant ponding did exist. A well developed overland channel has also formed where the ponds overflow onto the tundra, and since the vegetation in this area no longer exists, there are signs of overland erosion.

The 2008 inspection revealed that HBML had constructed a permanent drop box for the grey water discharge. Water overflowed from this box onto an area covered with cocoa fibre matting that has been placed in the area where vegetation dieback was observed in 2007. This practice continued in 2009 and 2010. This is an improved strategy, although, a long-term management plan is still required to prevent permanent vegetation dieback and permafrost degradation.

HBML developed new management plans for disposal of grey water in 2009 (SRK 2009c), and these will be implemented as part of the commissioning of the new STP in 2011.

Recommendations:

- 1. SRK understands that HBML has developed a new sewage management plan (SRK 2009c), which will be implemented to coincide with commissioning of the new STP. Grey water discharge should be in accordance with this new plan.
- 2. The erosion protection measures currently in effect is an improvement over what was in place in 2007; however, a long-term plan is required as prolonged application of grey water in the same area will not be managed through erosion protection measures alone.
- 3. HBML should consult the services of an expert knowledgeable with tundra vegetation to implement appropriate remediation strategies.

3.5.3 Drill Sites

The bulk of exploration drilling is carried out with diamond core drills, using mud and brine as drilling fluid. Much of this drilling fluid is recycled; however, there are instances where a significant amount of this fluid ends up being discharged at the drill site (or at least this has historically been the case). Along the north and eastern perimeter of the foundation fill pad, there are a number of locations where drill fluid was allowed to discharge directly onto the tundra. At these locations vegetation dieback has occurred, which in time has resulted in minor erosion damage. Examples of this design are illustrated in Figure 26.

A number of historic drill sites are visible from the airstrip (some of which are immediately adjacent to the airstrip). In these areas the brine resulted in vegetation dieback and, because natural drainage

in the area is poor, the ponded water remained in place. This ponding causes permafrost degradation, which causes a larger pond and this process of increased degradation continues to get progressively worse over time.

HBML will, whenever practical during the early spring, pump out any standing ponds. This practice must however cease once the bird nesting season begins.

Recommendations:

- HBML has initiated remediation measures to address some of the erosion gulleys formed by drill
 fluid using cocoa matting and re-vegetation. This program appears to be successful at controlling
 erosion and although vegetation re-growth appears slow, it is likely to occur. HBML should
 consult the services of an expert knowledgeable with tundra vegetation to implement appropriate
 remediation strategies.
- 2. An action plan is needed to remediate the drill sites where significant permafrost degradation has resulted in permanent ponds of standing water. These ponds are resulting in increased permafrost degradation, which in turn results in increased ponds.

3.5.4 Vegetation Dieback Zones

In addition to the localized areas of vegetation dieback described in Section 3.5.2 and 3.5.3, there are two large areas of vegetation dieback on the property, the origin of which is not clear. The first is an area south of the core storage road and east of the airstrip. In this area the vegetation has died but the underlying soils have not yet been exposed. The second area is between the drill road and the airstrip. Figure 26 provides examples of this damage. At this location the vegetation has died and the overburden soils have been exposed. The area is wet and difficult to traffic.

Recommendations:

- 1. HBML should initiate a study to determine why vegetation dieback has occurred in these areas.
- 2. An appropriate mitigation plan should be implemented to address these areas. If left unattended to, permafrost degradation will continue to get worse.
- 3. HBML should consult the services of an expert knowledgeable with tundra vegetation to implement appropriate remediation strategies.

3.5.5 V-Notch Weir

A V-notch weir was installed at the outlet from Stickleback Lake in the early 1990's as part of baseline data gathering studies (Figure 22). The installation was done with the least amount of invasive techniques, by wedging in the measurement weir using tote bags filled with drill cuttings. In accordance with the Water Licence, this weir should be removed. A detailed inspection of the conditions at this weir was not completed during the 2010 inspection.

Recommendations:

- Complete a thorough inspection of the conditions at the V-notch weir during the 2011 annual geotechnical inspection.
- 2. Develop an appropriate remediation plan for removal of the V-notch weir.

4 Summary of Recommendations

This report provides a performance assessment of the numerous foundation pads and infrastructure at the Boston Advanced Exploration Camp. The findings are based on a site visit and walkover survey on between July 12 - 16, 2010 and subsequent consultation with site staff and contractors. This is the fourth formal annual geotechnical inspection undertaken at the site, and shows many improvements over the findings observed in previous years. HBML has initiated a number of projects which have been completed, or are currently underway, which specifically targets many of the remaining issues identified during this geotechnical inspection.

Overall there are no immediate or significant areas of concern at the Boston Camp from a geotechnical point of view. There are also no issues that require urgent and immediate action, but there are elements that should be monitored. Table 6 below provides a summary of recommendations resulting from the geotechnical inspection completed in 2010, complete with observations listed in the 2009 annual geotechnical report (SRK 2009f).

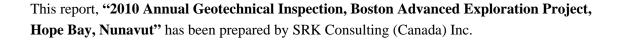
Table 6: Summary of Inspection Items and Associated Recommendations

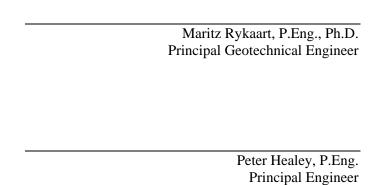
Inspection Item	2009 Recommendations	2010 Recommendations
Thermistors	 Locate appropriate readout device for older thermistors and confirm functionality of strings Splice broken string Continue formal monitoring of new (and older) strings 	 Locate appropriate readout device for older thermistors and confirm functionality of strings Splice broken string Confirm status of string in 08SBD381A Continue formal monitoring of new (and older) strings
Primary Tank Farm Settlement Monitoring	Continue quarterly monitoring Recognize foundation settlement risk in spill response plan	Continue quarterly monitoring Recognize foundation settlement risk in spill response plan
Primary Tank Farm	 Monitor the surficial slip surfaces on the tank farm berms Continue settlement monitoring as described above 	Monitor the surficial slip surfaces on the tank farm berms Continue settlement monitoring as described above
Power Plant Fuel Containment	No action required	No action required
Central Pad Fuel Containment	No action required	No action required Confirm whether secondary containment is required for two

Inspection Item	2009 Recommendations	2010 Recommendations
		new tanks and implement if necessary
Jet Fuel Containment	Conduct regular inspections of the portable containment berms	Conduct regular inspections of the portable containment berms
Solid Waste Disposal Site (including burn pit)	Confirm that waste containment is not required through an appropriate waste inventory	Confirm that waste containment is not required through an appropriate waste inventory
	Clean out burn pit and dispose wood waste as appropriate	Clean out burn pit and dispose wood waste as appropriate
	Remediate burn pit, or reclassify for other functional use	Remediate burn pit, or reclassify for other functional use
Ore Stockpiles	Implement the 2009 water and ore/waste rock management plan developed for the site	Implement the 2009 water and ore/waste rock management plan developed for the site
Settling Pond		Clear out debris in pond that could damage liner
	 Clear out debris in pond that could damage liner Implement the 2009 water and 	Implement the 2009 water and ore/waste rock management plan developed for the site
	ore/waste rock management plan developed for the site Construct suitable barrier around the	Construct suitable barrier around the pond to prevent inadvertent human and/or animal access
	pond to prevent inadvertent human and/or animal access	Confirm through water quality sampling whether the pond is leaking, and implement mitigation measures as appropriate
Soil Containment Berm (Landfarm)	Implement action items arising from landfarm study currently underway	Implement action items arising from landfarm study recently completed
Diamond Drill Cuttings and Settling Pond	Develop appropriate remediation plan for the pond	Develop appropriate remediation plan for the pond
	Develop appropriate management plan for storage of drill cuttings, including possible use as remediation method for permafrost degradation zones	Develop appropriate management plan for storage of drill cuttings, including possible use as remediation method for permafrost degradation zones
Portal	Replace the faded notices at the portal entrance advising of the dangers associated with unauthorized access to the area	Replace the faded notices at the portal entrance advising of the dangers associated with unauthorized access to the area
	Develop site specific hazard assessment for people entering the portal area to address the rockfall hazard	Develop site specific hazard assessment for people entering the portal area to address the rockfall hazard
	Consider installing a small diameter wire mesh over the exposed section of the portal roof to address the rockfall hazard	Consider installing a small diameter wire mesh over the exposed section of the portal roof to address the rockfall hazard

Inspection Item	2009 Recommendations	2010 Recommendations
Vent Raise	Replace weathered protective tarps covering the shelter erected over the vent raise Install notices at the vent raise advising of the dangers associated with unauthorized access to the area	 Replace weathered protective tarps covering the shelter erected over the vent raise Install notices at the vent raise advising of the dangers associated with unauthorized access to the area
Road to Dock	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source Implement speed control measures	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source Implement speed control measures
Camp Complex Foundation Pad	Re-survey the pad and develop an action plan to fill in and re-grade the pad to re-establish constant pad drainage	Re-survey the pad and develop an action plan to fill in and re-grade the pad to re-establish constant pad drainage
Road to Airstrip	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source
	Implement speed control measures	Implement speed control measures Maintain current maintenance practices, but do not use crushed
Airstrip	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source	ore material for repairs; find an alternate clean source Conduct frequent walk-over surveys to inspect for tension cracks along the airstrip shoulder
Drill Road	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source
	Implement speed control measures	Implement speed control measures
Core Storage Road	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source	Maintain current maintenance practices, but do not use crushed ore material for repairs; find an alternate clean source
5	 Monitor the pipe culvert for progressive permafrost degradation Implement speed control measures 	Monitor the pipe culvert for progressive permafrost degradation
	· · ·	Implement speed control measures
Wooden Walkway to Boat Dock	Consider raising the walkway above the tundra to prevent vegetation dieback and possible onset of permafrost degradation	Consider raising the walkway above the tundra to prevent vegetation dieback and possible onset of permafrost degradation
DOAL DOCK	If boat dock is to be decommissioned consider removing the walkway altogether	If boat dock is to be decommissioned consider removing the walkway altogether
Radio Tower and Shack	No action required	No action required
Water Intake Pump	Consider installing thermal pad or	Consider installing thermal pad or

Inspection Item 2009 Recommendations		2010 Recommendations
Shack	other appropriate foundation system	other appropriate foundation system
Existing STP Foundation Pad	No action required	No action required
New STP Foundation	Monitor the areas where tundra vegetation damage has occurred	Monitor the areas where tundra vegetation damage has occurred
Pad	Develop long-term re-vegetation plan: involve a tundra vegetation expert	Develop long-term re-vegetation plan: involve a tundra vegetation expert
Core Storage Area(s)	Consolidate core box storage and ensure that no boxes are inadvertently stored on the tundra	Consolidate core box storage and ensure that no boxes are inadvertently stored on the tundra
	Develop a long-term core storage plan	Develop a long-term core storage plan
Grey Water Discharge	Implement the new sewage management plan developed for the site when the new STP is commissioned	Implement the new sewage management plan developed for the site when the new STP is commissioned
Drill Sites	Develop remediation strategy to prevent further permafrost degradation	Develop remediation strategy to prevent further permafrost degradation
Vegetation Dieback	Initiate study to determine why dieback continues; involve a tundra vegetation expert	Initiate study to determine why dieback continues; involve a tundra vegetation expert
Zone	Develop remediation strategy to prevent further dieback and permafrost degradation	Develop remediation strategy to prevent further dieback and permafrost degradation
V-Notch Weir	Conduct complete inspection of the weir during 2010 geotechnical inspection	Conduct complete inspection of the weir during 2011 geotechnical inspection
	Develop appropriate remediation plan for the weir	Develop appropriate remediation plan for the weir





All data used as source material plus the text, tables, figures, and attachments of this document have been reviewed and prepared in accordance with generally accepted professional engineering and environmental practices.

5 References

BHP Minerals Canada Ltd. 1997. 1997 Report on the Construction of the Boston Camp Airstrip. Internal Report, December 17.

EBA Engineering Consultants Ltd. 1996. *Boston Gold Project, Surficial Geology and Permafrost Features*. Report prepared for Rescan Environmental Services Ltd., Report No. 0101-96-12259. December.

EBA Engineering Consultants Ltd. 1997. *Boston Gold Project, Tailings Disposal Evaluation - DRAFT*. Report prepared for BHP World Minerals, Report No. 0101-96-12259.006. December.

EBA Engineering Consultants Ltd. 2004. *Hydrocarbon Spill Assessment and Remediation, Boston Camp*, Nunavut. Report Submitted to Miramar Mining Corporation. Project Number 1740065. February.

Golder Associates Ltd. 2000a. *Data Review – Hope Bay Project*. Letter Report to Miramar Mining Corporation, ref. No. 002-1446. May 24.

Golder Associates Ltd. 2000b. *Site Visit – Hope Bay Project*. Letter Report to Miramar Mining Corporation, ref. No. 002-1446. May 24.Miramar Hope Bay Limited. 2007a. *Landfarm Management Plan, Doris North Project, Nunavut*. April.

Miramar Hope Bay Limited. 2007. Landfarm Operations & Maintenance Manual for Boston Camp Landfarm Treatment Area & Windy Lake Camp Landfarm Treatment Area. October.

Nunavut Water Board. 2007. *Licence Number 2BB-BOS0712*. Water Licence issued to Miramar Hope Bay Limited. July 6.

SRK Consulting (Canada) Inc. 2008. 2007 Annual Geotechnical Inspection, Boston Advanced Exploration Project, Hope Bay, Nunavut. Report prepared for Miramar Hope Bay Limited, Report No. 1CM014.013, February.

SRK Consulting (Canada) Inc. 2009a. 2008 Annual Geotechnical Inspection, Boston Advanced Exploration Project, Hope Bay, Nunavut. Report prepared for Hope Bay Mining Limited, Report No. 1CH008.006, March.

SRK Consulting (Canada) Inc. 2009b. *Geochemical Characterization of historic Waste Rock and Ore Stockpiles at the Boston Deposit, Hope Bay Project, Nunavut*. Report prepared for Hope Bay Mining Limited, Report No. 1CH008.005.1700, April.

SRK Consulting (Canada) Inc. 2009c. *Boston Advanced Exploration Project: Operation and Maintenance Manual for the Waste Water Treatment Facility, Hope Bay, Nunavut, Canada*. Report prepared for Hope Bay Mining Limited, Report No. 1CH008.008.200, April.

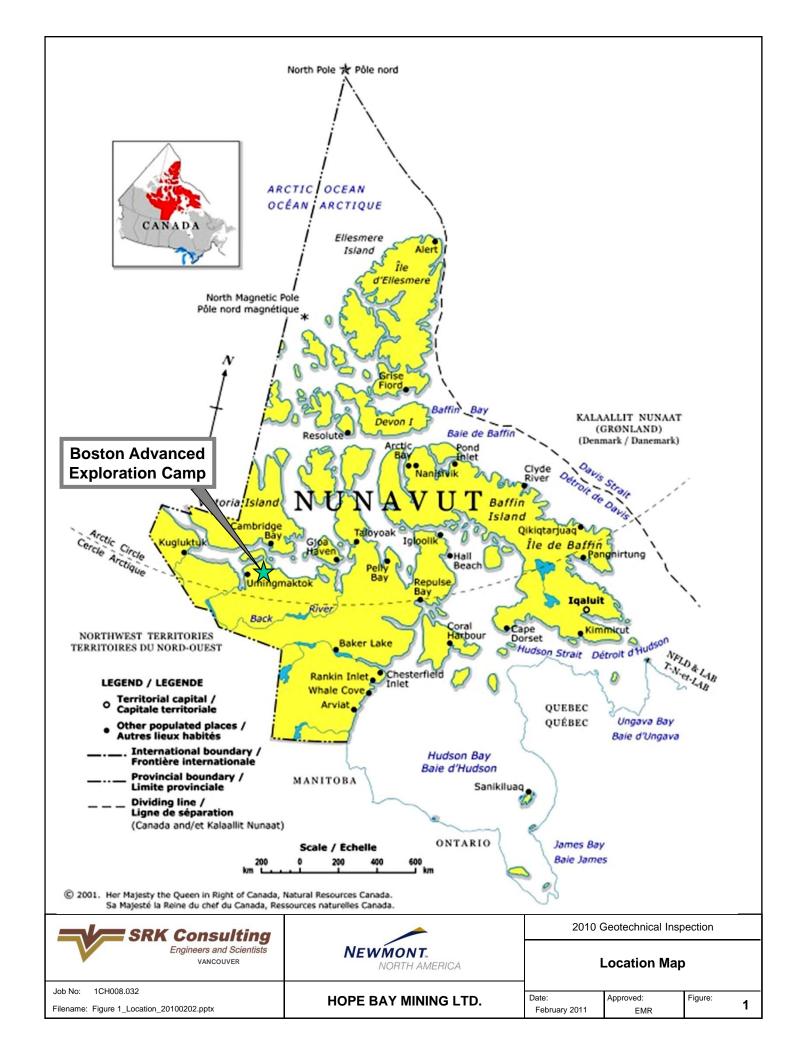
SRK Consulting (Canada) Inc. 2009d. *Water and Ore/Waste Rock Management Plan for the Boston Site, Hope Bay Project, Nunavut*. Report prepared for Hope Bay Mining Limited, Report No. 1CH008.022, July.

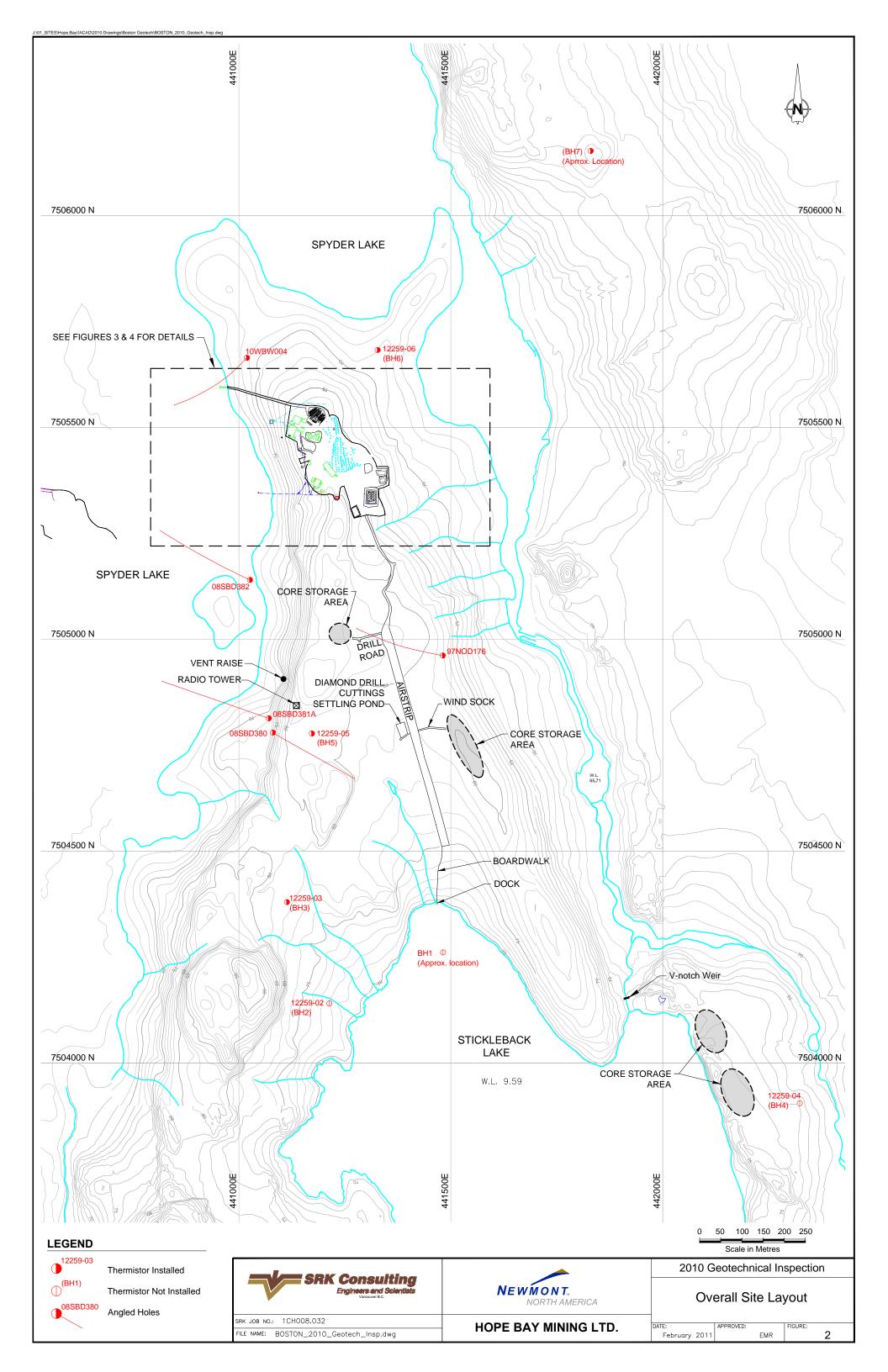
SRK Consulting (Canada) Inc. 2009e. *Hope Bay Gold Project: Stage 2 Overburden Characterization Report, Hope Bay, Nunavut, Canada*. Report prepared for Hope Bay Mining Limited, Report No. 1CH008.002, September.

SRK Consulting (Canada) Inc. 2009f. 2009 Annual Geotechnical Inspection, Boston Advanced Exploration Project, Hope Bay, Nunavut. Report prepared for Hope Bay Mining Limited, Report No. 1CH008.021, November.

SRK Consulting (Canada) Inc. 2011. *Hope Bay 2010 Westbay Program Data Report – Final Draft*. Report prepared for Hope Bay Mining limited, Report No. 1CH008.013, February











SRK JOB NO.: 1CH008.032

FILE NAME: BOSTON_2009_Geotech_Insp.dwg



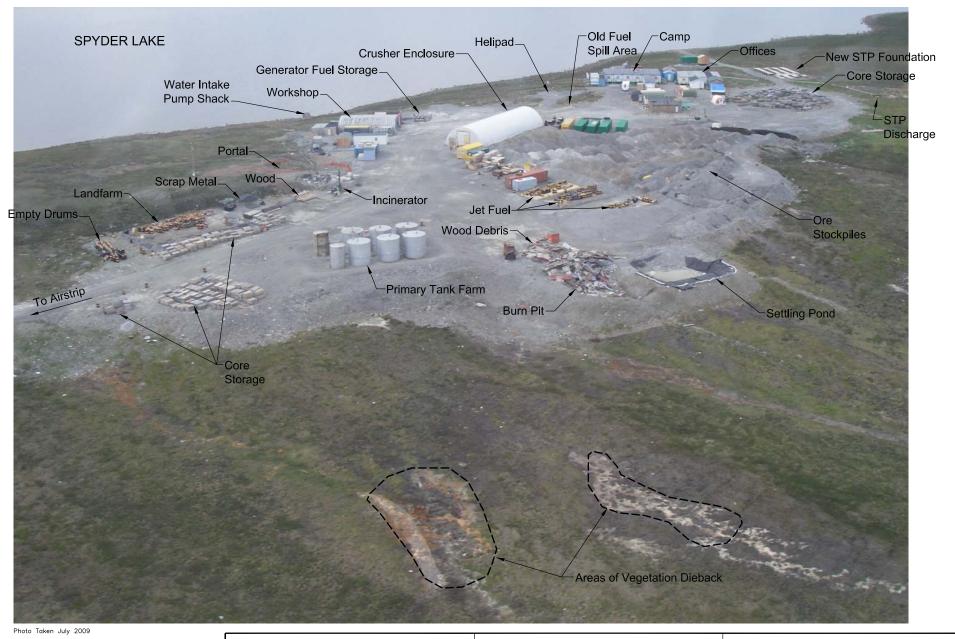
HOPE BAY MINING LTD.

2010 Geotechnical Inspection

Detailed Site Layout Looking South-West

DATE: APPROVED: February 2011 EMR

3





SRK JOB NO.: 1CH008.032

FILE NAME: BOSTON_2009_Geotech_Insp.dwg



HOPE BAY MINING LTD.

2010 Geotechnical Inspection

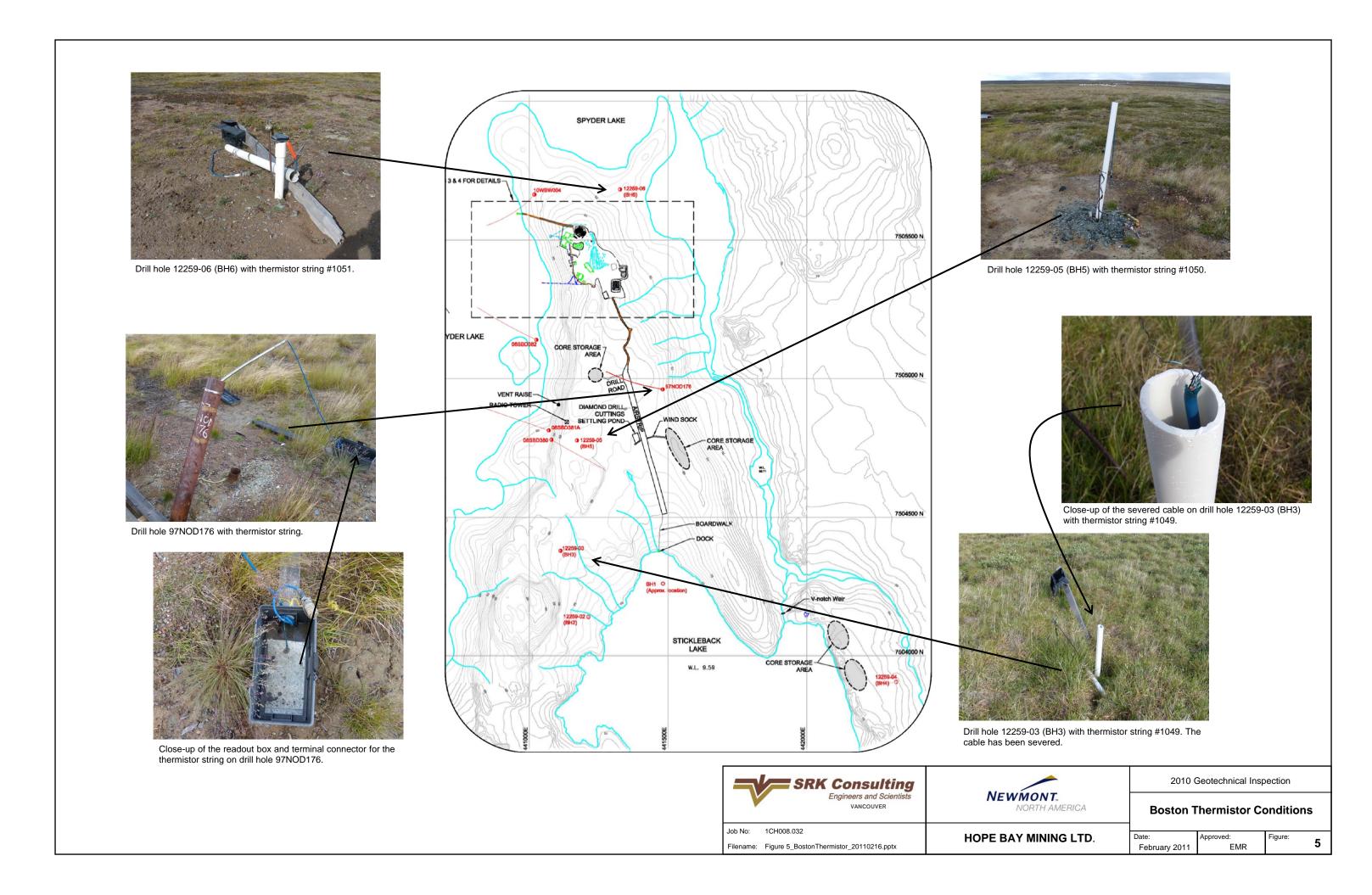
Detailed Site Layout Looking West

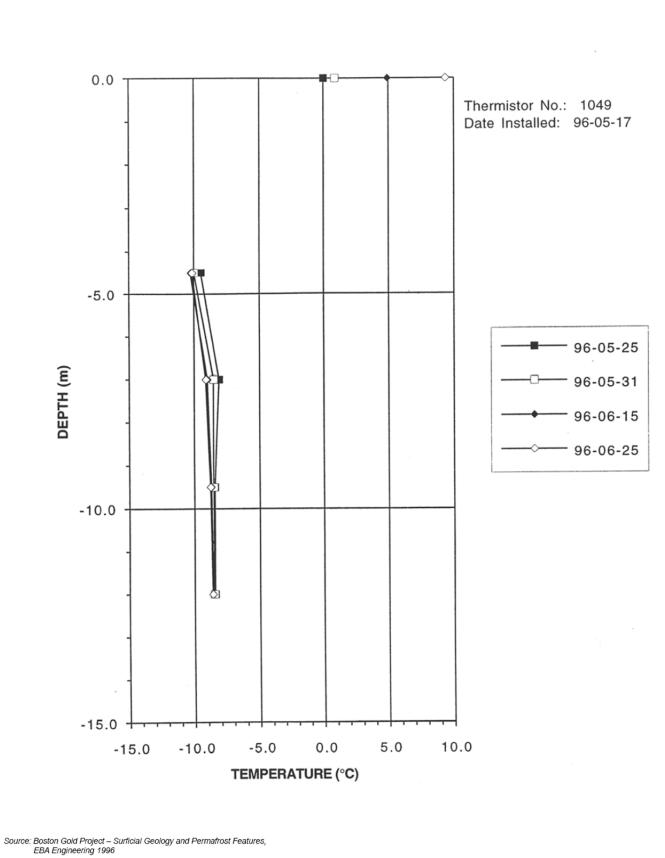
EMR

DATE: February 2011

APPROVED:

FIGURE:









2010 Geotechnical Inspection

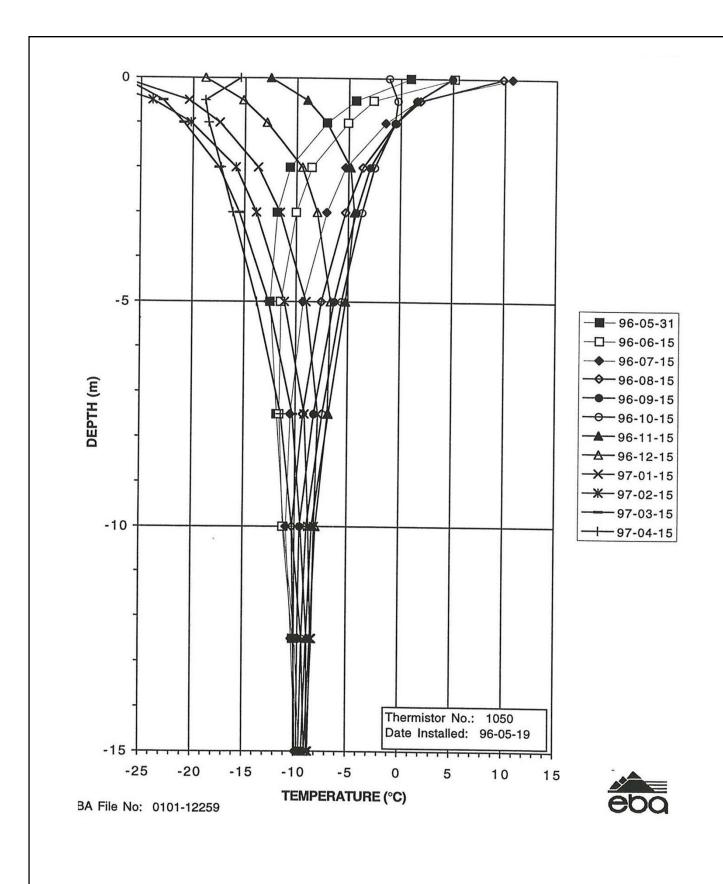
Ground Temperature Profiles EBA Drillhole 12259-03

1CH008.032 Job No:

Filename: Figure 6-9_EBA graphs_20110108.pptx

HOPE BAY MINING LTD.

Date: February 2011 Approved: EMR Figure: 6



Source: Boston Technical Reports – Environmental General, Tailings Disposal Evaluation-Draft, EBA Engineering 1997



Job No:

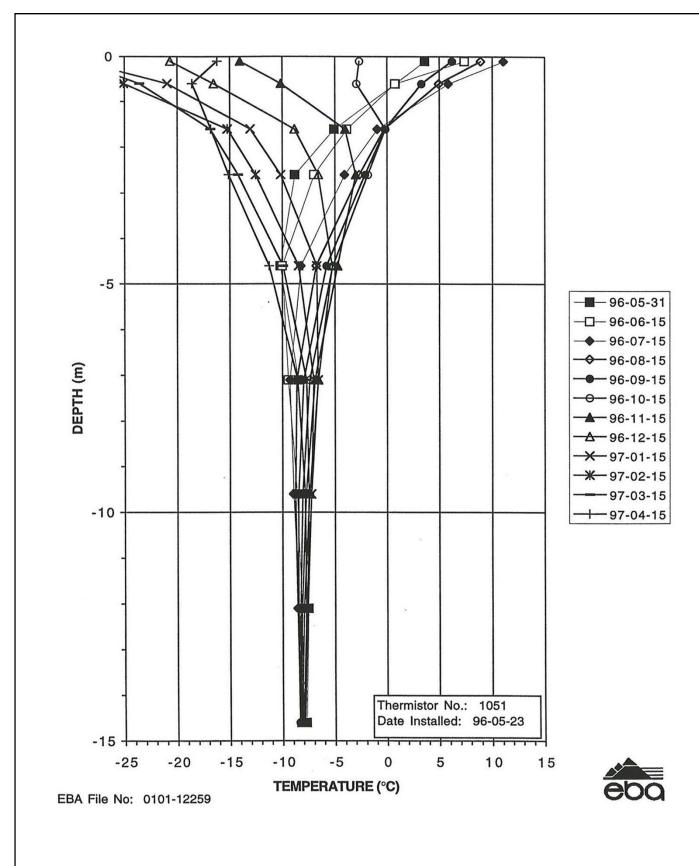
NEWMONT. NORTH AMERICA 2010 Geotechnical Inspection

Ground Temperature Profiles EBA Drillhole 12259-05

Approved:

1CH008.032 HOPE BAY MINING LTD. Filename: Figure 6-9_EBA graphs_20110108.pptx

Date: February 2011 Figure: 7



Source: Boston Technical Reports – Environmental General, Tailings Disposal Evaluation-Draft, EBA Engineering 1997



NEWMONT.

NORTH AMERICA

2010 Geotechnical Inspection

Ground Temperature Profiles EBA Drillhole 12259-06

Job No: 1CH008.032

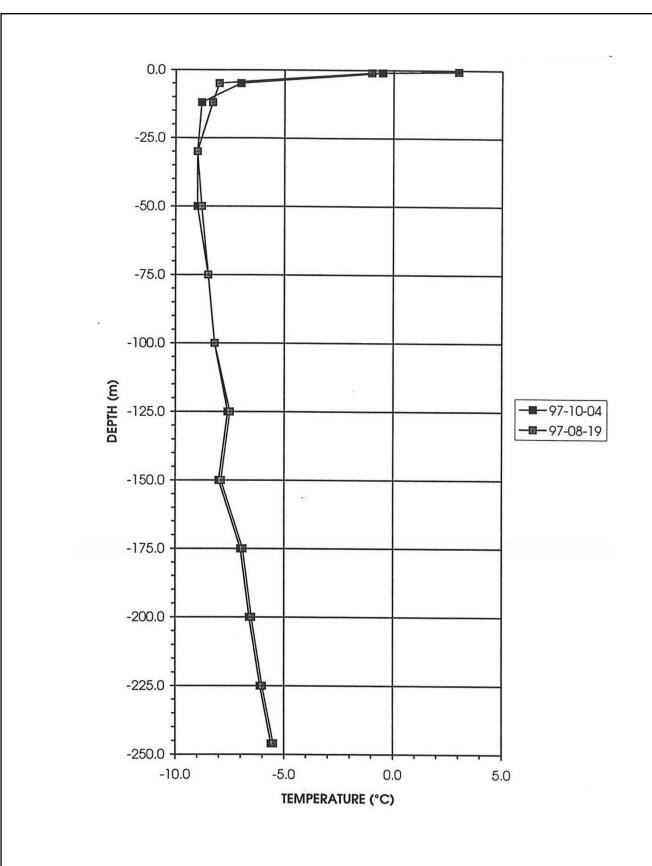
Filename: Figure 6-9_EBA graphs_20110108.pptx

HOPE BAY MINING LTD.

Date: February 2011

Approved: Figure: EMR

8



Source: Boston Technical Reports – Environmental General, Tailings Disposal Evaluation-Draft, EBA Engineering 1997



NEWMONT. NORTH AMERICA 2010 Geotechnical Inspection

Ground Temperature Profile EBA Deep Drillhole (97NOD176)

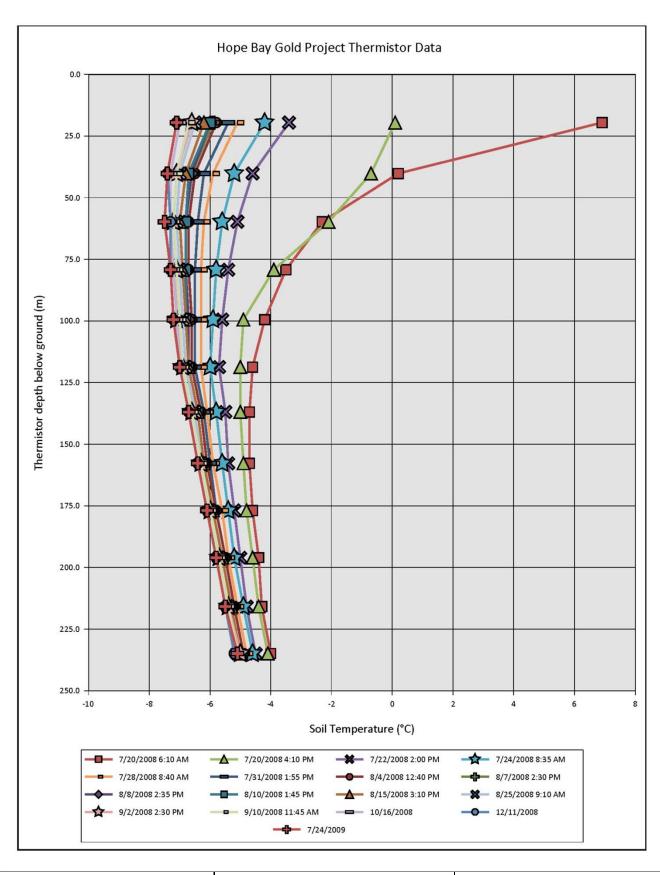
Approved:

Job No: 1CH008.032

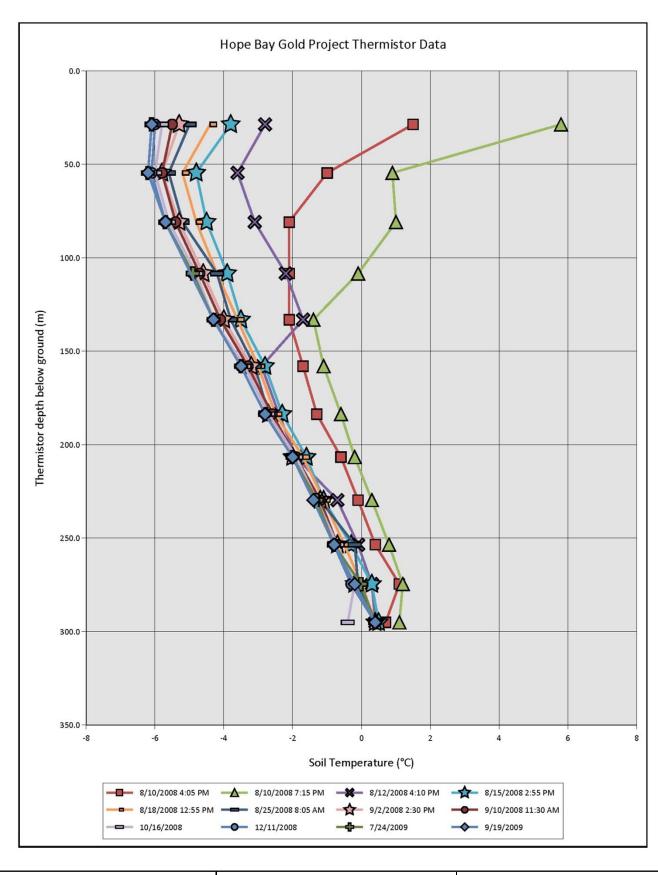
Filename: Figure 6-9_EBA graphs_20110108.pptx

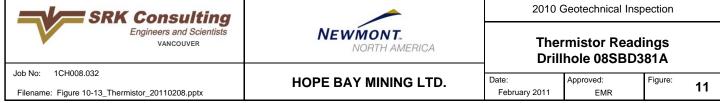
HOPE BAY MINING LTD.

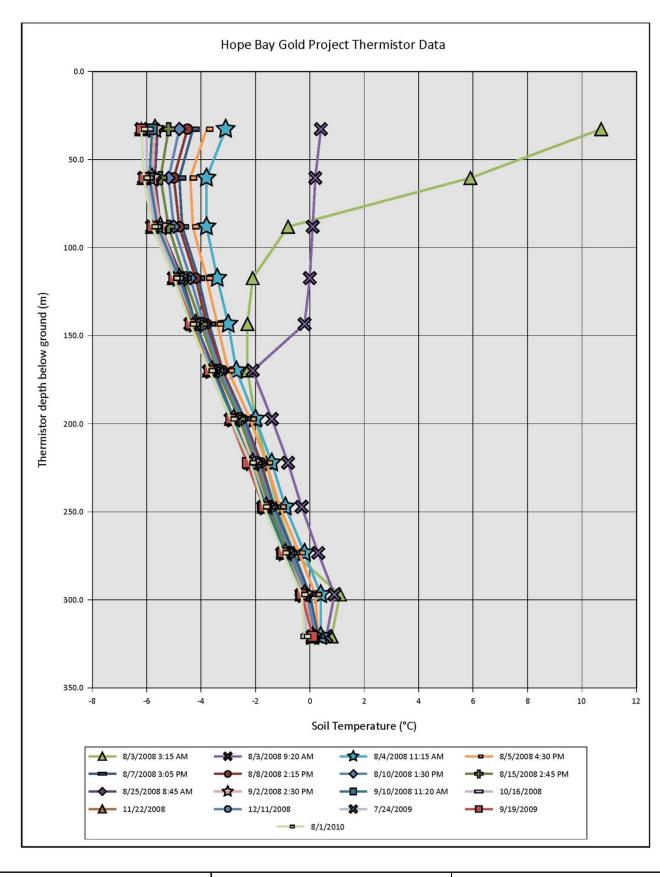
Date: February 2011 Figure: 9



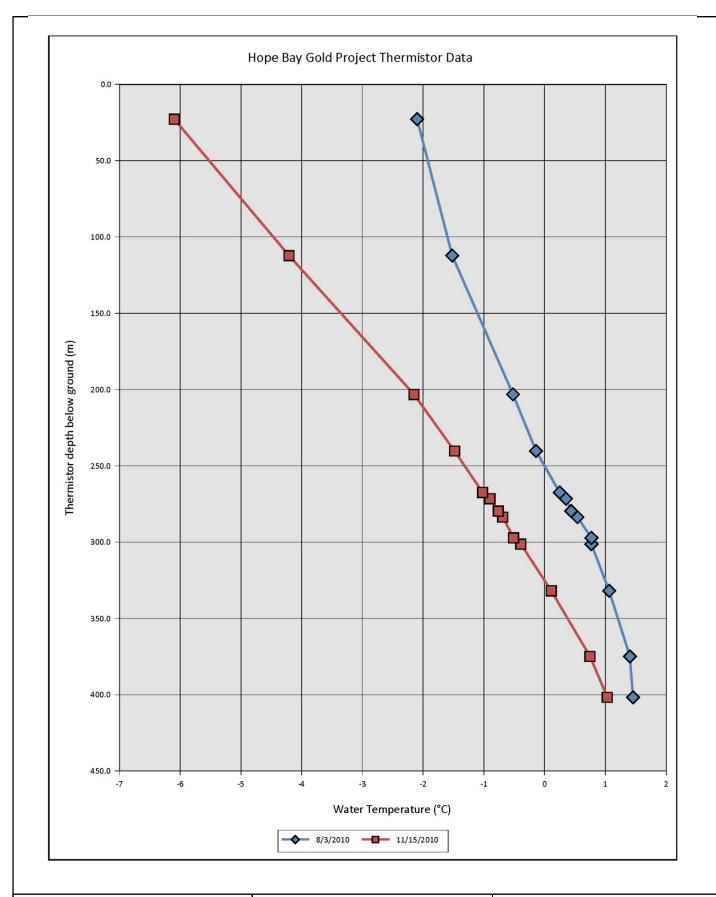


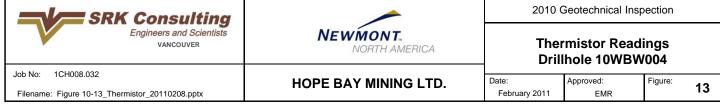














Fuel transfer pump on western containment berm.



Looking east towards the tank farm.



Tidy tank storage area west of containment area.



Western containment berm looking north.



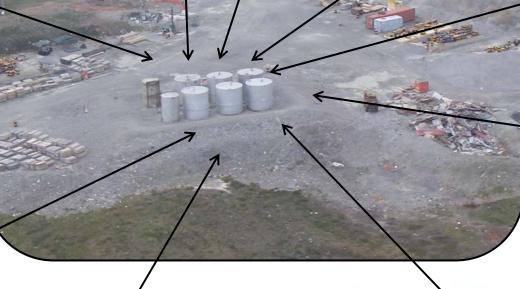
Western containment berm looking south.



Sump with submersible pump in the northwest corner of the tank farm.



Crest of eastern containment berm looking south.



Looking south towards the tank farm.



Eastern containment berm looking north.



Eastern containment berm looking south.



Erosion gulley on south outer containment berm.

Tension cracks along the crest of the containment



Job No: 1CH008.032

Filename: Figure 14_BostonTankFarm_20110216.pptx



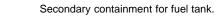
2010 Geotechnical Inspection

Primary Tank Farm

HOPE BAY MINING LTD.

Date: Approved: February 2011 E

EMR Figure: 14





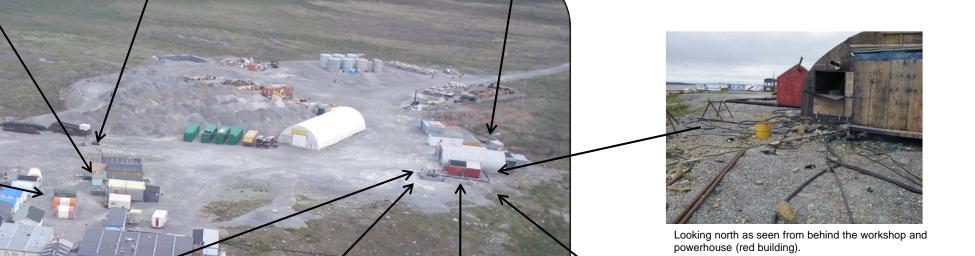




Fuel storage and pipelines behind workshop area.



Fuel tank without secondary containment.





Secondary containment for fuel tanks supplying power house and workshop.



Secondary containment for fuel tanks supplying power house and workshop looking north.



Front of powerhouse (red building).



Fuel delivery pipeline to power house and workshop.



Filename: Figure 15_WorkShop_Crusher_20110216.pptx

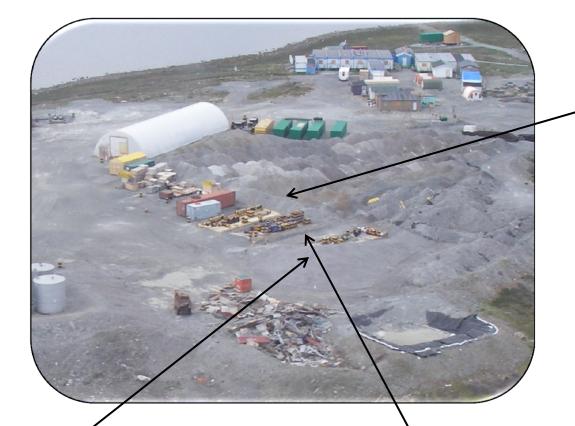


2010 Geotechnical Inspection

Workshop and Crusher Area

HOPE BAY MINING LTD.

Date: Approved: Figure: 15





Looking southeast across the three jet fuel containment areas.

Containment berm supported by timber cribbing.





Looking north towards eastern most containment area. Note access ramp leading into bermed area.



Looking west over the three jet fuel containment areas.



SRK Consulting Engineers and Scientists
VANCOUVER

Filename: Figure 16_ Jet Fuel Storage Area _ 201102116.pptx

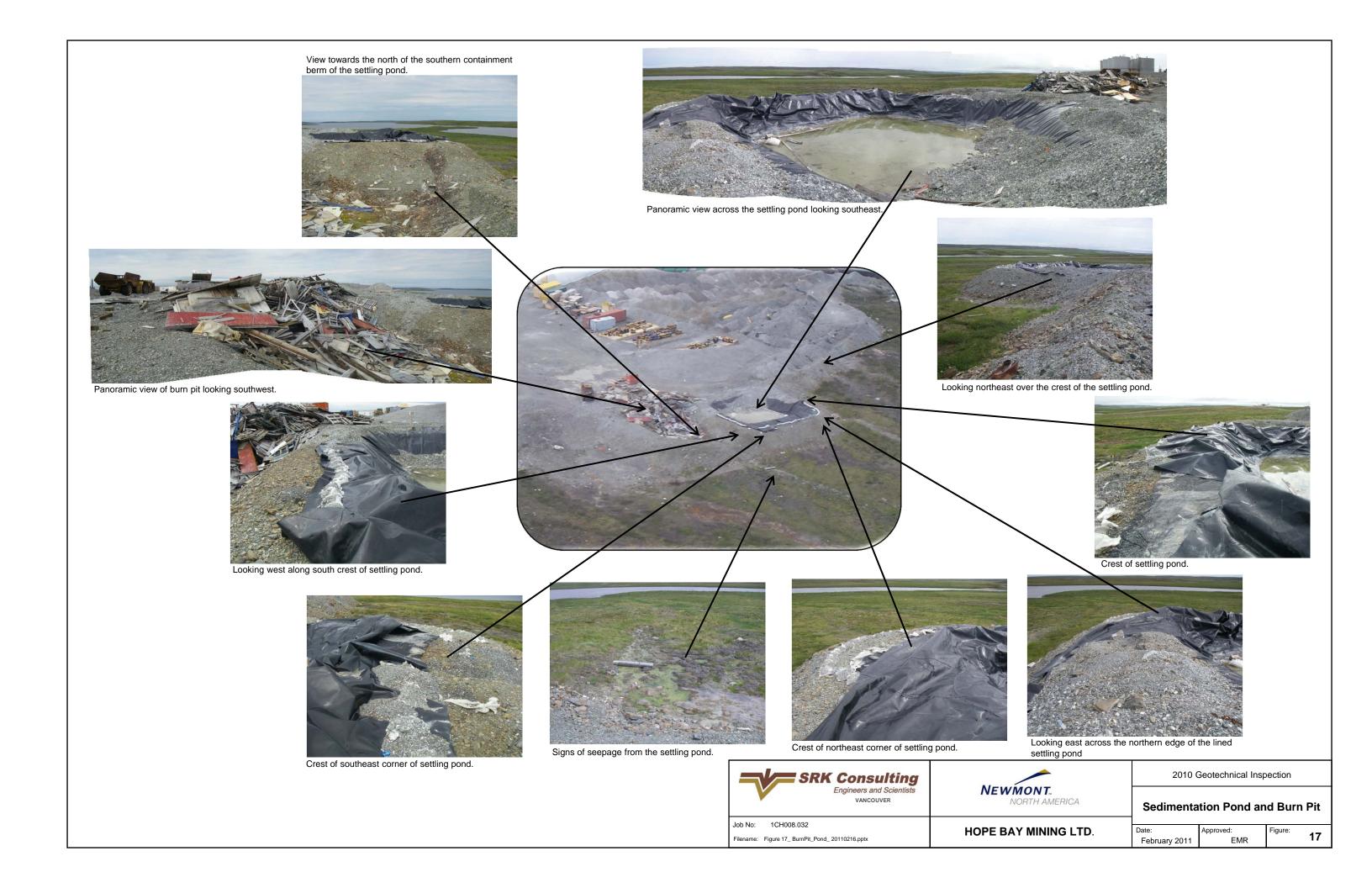


HOPE BAY MINING LTD.

2010	Geotechnica	al Insp	ection

Jet	ruei	Storage	;

Date:	Approved:	Figure:	4.0
February 2011	EMR		16





Panoramic view of the ore stockpiles looking north.



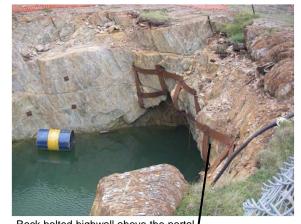
Oblique view looking northwest across the ore stockpiles.



Oblique view looking southwest across the ore stockpiles.

SRK Consulting	N	2010 (Geotechnical Insp	ection	
Engineers and Scientists VANCOUVER	NEWMONT _™ NORTH AMERICA	C	Ore Stockpile	s	
Job No: 1CH008.032	HOPE BAY MINING LTD.	Date:	Approved:	Figure:	
Filename: Figure 18_Stockpile_2011020208.pptx	= 2, = 1.2.	February 2011	EMR		18





Rock bolted highwall above the portal.



Looking south across the portal.



View across the portal from the top of the highwall.



Front of the incinerator with cash of fuel drums.



View of the protective fence along the highwall of the portal.



Entrance to the portal.



Another view of the incinerator form the back.



Filename: Figure 20_Portal_ncineratorArea _ 20110216.pptx



2010 Geotechnical Inspection

Portal and Incinerator Area

HOPE BAY MINING LTD.

20



Looking north across the core logging sheds and other office units. The depression in the foreground is the historic hydrocarbon spill area.



Looking north towards the southern camp complex consisting of skid mounted units.



Looking south towards the older camp section and main office complex.



Potable water supply pipeline to camp.



Looking east along the all-weather access road from the camp to Spyder Lake.



Looking west at an area of erosion and permafrost damage repaired by infilling with gravel



Looking northwest across the south end of the camp pad. Note power cables.



Filename: Figure 21_CampArea _ 20110216.pptx



HOPE BAY MINING LTD.

2010 Geotechnical Inspection							
Camp Area							
Date: February 2011	Approved: EMR	Figure:	21				

Permafrost degradation pond along east shoulder of airstrip



Tension cracks along crest of airstrip in areas where ponding exist,



Looking south across wooden walkway to Stickleback Lake.



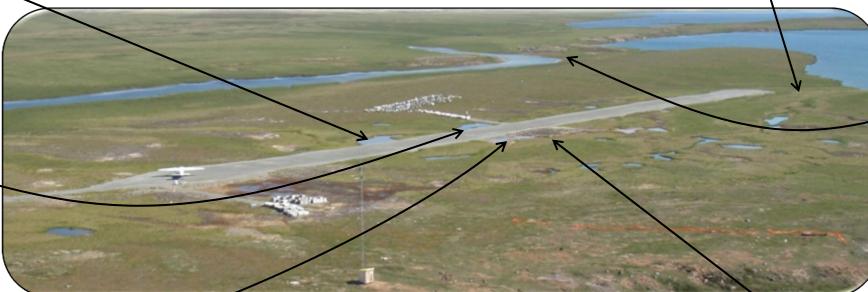
Looking north at bridge and walkway to boat dock on Stickleback Lake.



Permafrost degradation pond along east shoulder of airstrip.



Permafrost degradation pond along west shoulder of airstrip.



Large permafrost degradation and vegetation dieback area along west shoulder of airstrip



Close-up of vegetation dieback.

22



Close-up of permafrost vegetation and vegetation dieback.



SRK Consulting
Engineers and Scientists
VANCOUVER

Job No: 1CH008.032

Filename: Figure 22_BostonAirstrip_20110216.pptx

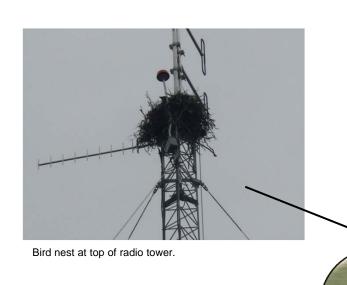


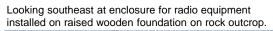
HOPE BAY MINING LTD.

2010 Geotechnical Inspection

Airstrip

Date: Approved: Figure: February 2011 EMR







Looking northeast at enclosure for radio equipment installed on raised wooden foundation on rock outcrop.







Looking north across the vent raise.



Looking south across the vent raise.



Looking southeast across the vent raise.



Looking northeast across the vent raise.



Job No: 1CH008.032

Filename: Figure 23_ RadioTower_Vent Area _ 20110216.pptx



2010 Geotechnical Inspection

Radio Tower and Vent Raise Area

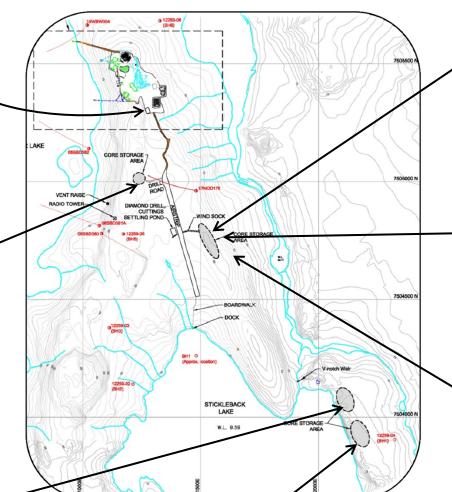
HOPE BAY MINING LTD.

February 2011

Approved: Figure: 23



Looking north towards core box storage area on south end of camp pad.



Looking south across the core storage area east of the airstrip.



Close-up of the core storage area east of the



Looking north towards core storage area. Note extensive vegetation dieback zone in foreground.



Oblique aerial view of the northern section of the core storage area located on the eastern shore of Stickleback Lake.



Oblique aerial view of the southern section of the core storage area on the eastern shore of Stickleback Lake.



Looking west across the core storage area east of the airstrip.



Filename: Figure 24_CoreStorage_20110216.pptx

1CH008.032

Job No:



Core Storage Areas

2010 Geotechnical Inspection

HOPE BAY MINING LTD.

Figure: 24

Diffuser for treated sewage effluent outflow.



Looking north across the treated sewage treatment outflow diffuser and associated discharge area.

Looking north along all weather access road to old STP.



Upper end of the leveling foundation for the new Boston Sewage Treatment Plant.





Lower end of the leveling foundation for the new Boston Sewage Treatment Plant.



Thermal pad and raised foundation for components of the new Boston Sewage Treatment Plant.



Close-up of raised foundation footings used on the new Boston Sewage Treatment Plant.





Looking south along the boardwalk leading up to the old STP extension.



Looking southwest toward the new extension to the existing STP.



Excess potable water outflow.



Job No: 1CH008.032

Filename: Figure 26_Existing-NewSTP_20110216.pptx



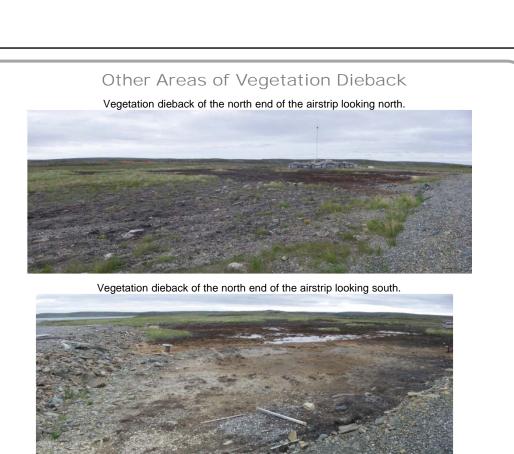
HOPE BAY MINING LTD.

2010 Geotechnical Inspection

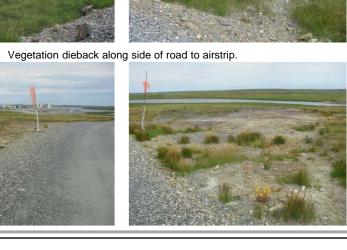
Existing and New STP

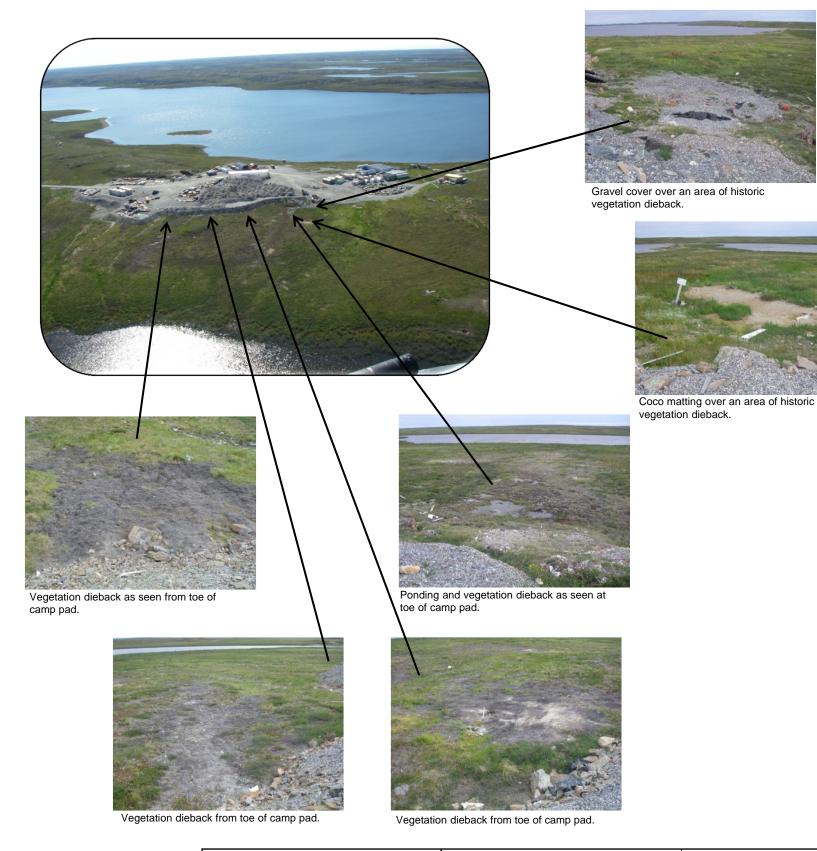
Date: February 2011 proved: Fig EMR

Figure: 25











NEWMONT.

NORTH AMERICA

2010 Geotechnical Inspection

Job No: 1CH008.032

Filename: Figure 26_Vegetation_20110216.pptx

HOPE BAY MINING LTD.

Vegetation Dieback Areas

Date: Approved: Figure: 26

Appendix A Primary Tank Farm Settlement Data

Boston Primary Fuel Tank Farm Settlement Monitoring Tank #1

Date	Tank	Horizontal Angle		Vertical Angle Slo		Slope	HI	Northing	Easting	Elevation	S	ce from F urvey [m			
	Mark	Deg	Min	Sec	Deg	Min	Sec	Dist.	[m]	[m]	[m]	[m]	N	E	EI
22-Apr-08	1A	176	41	38	95	24	55	7.658	1.593	5325.879	1305.901	80.674			
8-Aug-08	1A	176	36	14	94	58	28	7.651	1.519	5325.889	1305.894	80.660	0.009	-0.008	-0.015
18-Oct-08	1A	176	38	26	96	3	2	7.675	1.674	5325.890	1305.905	80.669	0.001	0.011	0.009
25-Jul-09	1A	176	34	52	95	52	11	7.671	1.633	5325.896	1305.899	80.653	0.006	-0.005	-0.016
19-Sep-09	1A	176	35	8	95	53	35	7.676	1.635	5325.898	1305.904	80.651	0.002	0.004	-0.002
2-Aug-10	1A	176	34	14	94	58	19	7.666	1.506	5325.900	1305.904	80.646	0.003	0.000	-0.005
22-Apr-08	1B	58	18	6	94	2	11	9.526	1.632	5326.428	1308.581	80.989			
8-Aug-08	1B	58	19	39	92	54	1	9.527	1.436	5326.439	1308.574	80.982	0.011	-0.007	-0.008
18-Oct-08	1B	58	19	8	93	54	32	9.530	1.610	5326.434	1308.579	80.988	-0.005	0.005	0.006
25-Jul-09	1B	58	20	36	94	0	48	9.538	1.610	5326.441	1308.576	80.970	0.007	-0.003	-0.018
19-Sep-09	1B	58	20	27	94	6	27	9.541	1.626	5326.442	1308.574	80.971	0.001	-0.002	0.000
2-Aug-10	1B	58	20	28	93	19	3	9.533	1.484	5326.442	1308.574	80.960	0.000	0.000	-0.010
22-Apr-08	1F	304	22	12	91	9	4	24.193	1.635	5328.263	1306.711	80.992			
8-Aug-08	1F	304	22	16	91	4	38	24.184	1.575	5328.271	1306.709	80.963	0.008	-0.002	-0.029
18-Oct-08	1F	304	22	16	91	11	6	24.189	1.637	5328.267	1306.710	80.980	-0.004	0.001	0.016
25-Jul-09	1F	304	22	13	91	0	29	24.178	1.530	5328.276	1306.708	80.948	0.009	-0.002	-0.032
19-Sep-09	1F	304	22	18	91	15	12	24.182	1.632	5328.274	1306.708	80.946	-0.002	0.000	-0.002
2-Aug-10	1F	304	21	53	91	2	35	24.176	1.535	5328.279	1306.710	80.938	0.005	0.002	-0.008

	22-Apr-08	0.0	0.0	0.0
	8-Aug-08	9.5	-5.7	-17.0
TANK AVERAGES BY DATE (mm)	18-Oct-08	-2.8	5.6	10.7
	25-Jul-09	7.6	-3.3	-22.1
	19-Sep-09	0.2	0.8	-1.1
	2-Aug-10	2.6	0.7	-7.9
OVERALL PERIOD AVE	3.4	-0.4	-7.5	

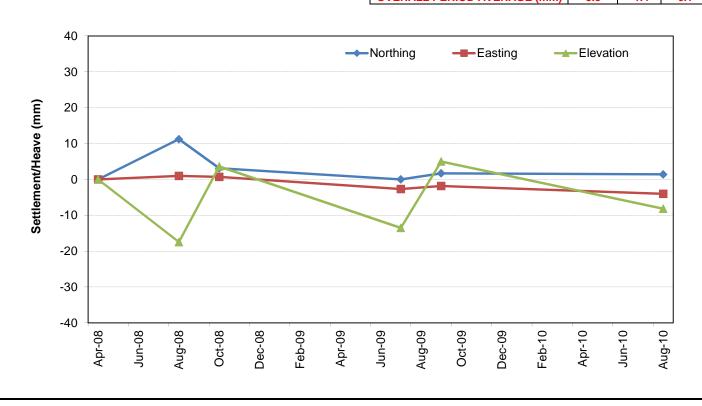


Boston Primary Fuel Tank Farm Settlement Monitoring

Tank	#2
-------------	----

Date	Tank	Horizo	ntal /	Anala	Vort	ical A	alna	Slope	HI	Northing	Easting	Elevation	Difference	ce from F	revious
Date	I allk	1101120	Jiilai 7	riigie	Vert	icai A	iigie	Slope	'''	Northing	Lasting	Lievation	Survey [m]		
	Mark	Deg	Min	Sec	Deg	Min	Sec	Dist.	[m]	[m]	[m]	[m]	N	E	EI
22-Apr-08	2A	188	32	48	91	42	56	17.357	1.593	5327.678	1315.749	80.877			
8-Aug-08	2A	188	30	39	91	31	5	17.357	1.519	5327.689	1315.747	80.863	0.011	-0.002	-0.014
18-Oct-08	2A	188	30	44	92	1	58	17.369	1.674	5327.691	1315.754	80.862	0.002	0.007	-0.001
25-Jul-09	2A	188	30	41	91	55	2	17.365	1.633	5327.690	1315.752	80.856	-0.001	-0.003	-0.006
19-Sep-09	2A	188	30	32	91	55	46	17.369	1.635	5327.692	1315.755	80.854	0.002	0.003	-0.002
2-Aug-10	2A	188	29	57	91	32	0	17.365	1.506	5327.695	1315.754	80.845	0.003	-0.001	-0.009
22-Apr-08	2C	66	46	17	93	28	22	8.891	1.669	5326.866	1318.217	81.190			
8-Aug-08	2C	66	49	58	92	18	25	8.890	1.471	5326.878	1318.219	81.173	0.012	0.002	-0.017
18-Oct-08	2C	66	51	15	93	13	45	8.903	1.625	5326.885	1318.217	81.183	0.007	-0.002	0.010
25-Jul-09	2C	66	51	14	93	4	54	8.903	1.592	5326.886	1318.216	81.173	0.001	-0.001	-0.010
19-Sep-09	2C	66	51	2	93	15	9	8.907	1.622	5326.887	1318.214	81.177	0.002	-0.002	0.003
2-Aug-10	2C	66	50	58	92	42	58	8.906	1.532	5326.889	1318.212	81.170	0.002	-0.002	-0.007
22-Apr-08	2D	284	9	33	90	41	36	22.748	1.669	5329.353	1318.048	81.114			
8-Aug-08	2D	284	9	30	90	25	53	22.736	1.544	5329.363	1318.052	81.093	0.010	0.003	-0.021
18-Oct-08	2D	284	9	59	90	37	33	22.737	1.623	5329.364	1318.048	81.095	0.001	-0.003	0.002
25-Jul-09	2D	284	10	37	90	30	59	22.738	1.555	5329.364	1318.044	81.070	0.000	-0.004	-0.025
19-Sep-09	2D	284	11	40	90	24	42	22.738	1.527	5329.365	1318.037	81.084	0.002	-0.007	0.014
2-Aug-10	2D	284	12	51	90	23	29	22.741	1.510	5329.364	1318.029	81.075	-0.001	-0.008	-0.009

	22-Apr-08	0	0	0
	8-Aug-08	11.2	1.0	-17.5
TANK AVERAGES BY	18-Oct-08	3.1	0.7	3.6
DATE (mm)	25-Jul-09	0.0	-2.7	-13.5
	19-Sep-09	1.7	-1.8	5.0
	2-Aug-10	1.4	-4.0	-8.2
OVERALL PERIOD AVE	3.5	-1.4	-6.1	



-40

Aug-08

Oct-08

Dec-08

Boston Primary Fuel Tank Farm Settlement Monitoring **Boston Primary Fuel Tank Farm Settlement Monitoring** Tank #3 Difference from Previous **Vertical Angle Horizontal Angle** н Northing Elevation Date Tank Slope Easting Survey [m] Dist. Mark Deg Min Sec Deg Min Sec [m] N ΕI [m] [m] [m] Ε 22-Apr-08 38 5331.618 1306.850 ЗА 155 31 38 91 35 12.238 1.593 81.057 8-Aug-08 ЗА 155 29 54 91 20 3 12.240 1.519 5331.624 1306.847 81.038 0.006 -0.003 -0.019 18-Oct-08 ЗА 155 31 55 91 58 52 12.245 1.674 5331.621 1306.853 81.055 -0.004 0.006 0.017 25-Jul-09 ЗА 155 31 45 91 51 50 12.248 1.633 5331.624 1306.855 81.039 0.003 0.002 -0.016 19-Sep-09 12.252 5331.627 81.038 -0.001 ЗА 155 32 4 91 52 38 1.635 1306.858 0.002 0.003 2-Aug-10 155 32 17 91 17 55 12.249 1.506 5331.627 1306.859 0.001 -0.005 ЗА 81.032 0.000 22-Apr-08 3B 80 36 8 92 41 45 12.708 1.632 5331.612 1309.744 81.062 8-Aug-08 3B 80 36 38 91 53 10 12.706 1.436 5331.618 1309.743 81.046 0.005 -0.001 -0.016 18-Oct-08 3B 80 35 55 92 35 15 12.708 1.610 5331.613 1309.743 81.064 -0.005 0.000 0.018 25-Jul-09 3B 80 37 13 92 40 40 12.710 1.610 5331.616 1309.747 81.044 0.003 0.004 -0.020 3B 92 19-Sep-09 80 36 53 44 55 1309.744 81.044 -0.002 0.000 12.713 1.626 5331.618 0.001 3B 36 92 9 22 -0.003 -0.010 2-Aug-10 80 42 12.704 1.484 5331.614 1309.745 81.034 0.001 22-Apr-08 3F 297 17 27 91 16 38 17.426 1.635 5335.467 1307.263 81.090 8-Aug-08 3F 297 16 91 23 17.423 1.575 5335.470 1307.265 81.056 0.003 0.002 -0.033 52 11 18-Oct-08 3F 297 17 24 91 18 7 17.430 1.637 5335.464 1307.265 81.084 -0.007 0.000 0.028 25-Jul-09 3F -0.029 297 16 48 91 2 50 17.425 1.530 5335.468 1307.267 81.055 0.004 0.002 19-Sep-09 91 -0.001 3F 297 57 23 10 17.427 1.632 5335.468 1307.266 81.053 0.000 -0.001 16 3F 2-Aug-10 297 16 23 91 5 19 17.424 1.535 5335.470 1307.268 81.047 0.002 0.002 -0.00622-Apr-08 0 Ω 0 -0.6 -22.8 8-Aug-08 5.1 TANK AVERAGES BY 18-Oct-08 1.9 21.0 -5.1 DATE (mm) 25-Jul-09 3.7 2.4 -21.9 19-Sep-09 1.2 0.1 -0.6 2-Aug-10 -0.5 1.4 -7.3 **OVERALL PERIOD AVERAGE (mm)** 0.9 1.0 40 Northing Easting Elevation 30 Settlement/Heave (mm) 20 10 0 -10 -20

Aug-10

Feb-10

Feb-09

90-unf

Oct-09

Dec-09

Aug-09

-30

-40

Boston Primary Fuel Tank Farm Settlement Monitoring **Boston Primary Fuel Tank Farm Settlement Monitoring** Tank #4 Difference from Previous **Vertical Angle Horizontal Angle** н Northing Elevation Date Tank Slope Easting Survey [m] Mark Deg Min Sec Deg Min Sec Dist. [m] N ΕI [m] [m] [m] Ε 22-Apr-08 49 45 46 12.465 5331.166 81.128 4C 79 37 92 1.669 1318.159 8-Aug-08 4C 79 50 23 91 56 16 12.462 1.471 5331.171 1318.159 81.110 0.005 0.000 -0.019 18-Oct-08 4C 79 51 33 92 32 3 12.471 1.625 5331.177 1318.161 81.134 0.005 0.002 0.024 25-Jul-09 4C 79 51 5 92 28 57 12.473 1.592 5331.178 1318.158 81.112 0.001 -0.003 -0.02219-Sep-09 4C 79 5331.181 1318.156 81.115 0.003 51 1 92 36 19 12.478 1.622 0.003 -0.002 2-Aug-10 4C 79 50 58 92 5 5331.181 81.113 0.000 -0.002 12 12.474 1.532 1318.156 0.000 35 90 25 22-Apr-08 4D 290 20 57 17.796 1.669 5334.739 1317.563 81.092 8-Aug-08 4D 290 20 54 90 36 59 17.789 1.544 5334.744 1317.564 81.073 0.006 0.001 -0.019 18-Oct-08 -0.002 0.016 4D 290 20 51 90 49 8 17.792 1.623 5334.742 1317.563 81.089 -0.001 25-Jul-09 4D 290 21 32 90 42 58 17.791 1.555 5334.744 1317.560 81.053 0.002 -0.003 -0.036 4D 290 22 35 22 19-Sep-09 47 90 5334.742 81.064 -0.002 -0.008 0.011 17.795 1.527 1317.552 2-Aug-10 4D 23 90 32 36 -0.005 -0.003 290 44 17.796 1.510 5334.743 1317.547 81.061 0.001 22-Apr-08 4E 298 41 4 91 11 45 18.548 1.670 5334.220 1314.710 81.128 8-Aug-08 4E 298 40 52 91 18.537 1.583 5334.230 1314.708 81.096 0.010 -0.001 -0.032 1 34 18-Oct-08 4E 298 40 53 91 9 14 18.539 1.650 5334.229 1314.709 81.122 -0.001 0.000 0.026 25-Jul-09 298 -0.025 4E 40 41 91 0 18.532 1.576 5334.235 1314.708 81.096 0.006 0.000 14 19-Sep-09 298 0.000 4F 40 23 91 6 42 18.528 1.611 5334.240 1314.709 81.097 0.005 0.000 39 2-Aug-10 4E 298 54 90 58 23 18.523 1.563 5334.245 1314.710 81.093 0.005 0.001 -0.00322-Apr-08 0 Ω 0 -0.2 -23.2 8-Aug-08 6.9 TANK AVERAGES BY 18-Oct-08 21.9 0.7 0.5 DATE (mm) 25-Jul-09 3.1 -2.1 -27.8 19-Sep-09 2.1 -3.1 4.9 2-Aug-10 1.7 -1.2 -2.6 **OVERALL PERIOD AVERAGE (mm)** -5.4 40 Northing Easting Elevation 30 Settlement/Heave (mm) 20 10 0 -10

Feb-09

Oct-08

Aug-09

Oct-09

Dec-09

-40

Aug-08

Oct-08

Boston Primary Fuel Tank Farm Settlement Monitoring **Boston Primary Fuel Tank Farm Settlement Monitoring** Tank #5 Difference from Previous **Vertical Angle Horizontal Angle** н Northing Elevation Date Tank Slope Easting Survey [m] Mark Deg Min Sec Deg Min Sec Dist. [m] N ΕI [m] [m] [m] Ε 22-Apr-08 38 5337.355 80.896 5A 146 6 15 91 18 17.511 1.593 1307.654 8-Aug-08 5A 146 5 19 91 29 20 17.506 1.519 5337.354 1307.648 80.868 -0.001 -0.006 -0.02818-Oct-08 5A 146 7 20 91 55 18 17.515 1.674 5337.353 1307.660 80.891 0.000 0.011 0.023 25-Jul-09 5A 146 6 28 91 53 1 17.513 1.633 5337.354 1307.655 80.861 0.001 -0.005 -0.02919-Sep-09 5337.357 1307.659 -0.003 5A 146 6 54 91 53 58 17.518 1.635 80.858 0.003 0.004 2-Aug-10 146 43 91 29 39 1.506 1307.659 0.001 -0.001 -0.005 5A 6 17.515 5337.358 80.853 53 22-Apr-08 5B 92 56 58 91 35 17.712 1.632 5337.490 1310.713 81.075 8-Aug-08 5B 92 56 21 91 20 1 17.706 1.436 5337.487 1310.710 81.052 -0.002 -0.003 -0.023 18-Oct-08 5B 92 56 43 91 50 16 17.704 1.610 5337.482 1310.714 81.070 -0.005 0.004 0.018 25-Jul-09 5B 92 56 27 91 55 26 17.709 1.610 5337.486 1310.711 81.043 0.004 -0.003 -0.027 29 19-Sep-09 5B 92 56 12 91 58 1310.709 81.044 -0.002 0.000 17.712 1.626 5337.488 0.002 5B 46 51 -0.003 -0.001 -0.010 2-Aug-10 92 55 91 32 17.705 1.484 5337.484 1310.708 81.034 22-Apr-08 5F 286 10 48 91 45 54 12.624 1.635 5341.035 1307.826 81.089 8-Aug-08 5F 286 10 38 10 12.624 1.575 5341.034 1307.826 81.058 -0.001 0.000 -0.032 54 91 18-Oct-08 5F 286 10 54 91 45 51 12.631 1.637 5341.029 1307.830 81.091 -0.005 0.003 0.034 25-Jul-09 286 -0.044 5F 91 28 48 12.624 1.530 5341.033 1307.826 81.047 0.004 -0.003 11 1 19-Sep-09 5F 286 17 57 -0.002 91 12.628 1.632 5341.032 1307.826 81.045 -0.001 0.000 11 1 5F 5 2-Aug-10 286 10 55 91 32 12.624 1.535 5341.033 1307.827 81.040 0.002 0.001 -0.00522-Apr-08 0 Ω 0 8-Aug-08 -2.8 -27.6 -1.3 TANK AVERAGES BY -3.7 18-Oct-08 24.8 6.1 DATE (mm) 25-Jul-09 2.8 -3.4 -33.4 19-Sep-09 1.3 0.6 -1.5 2-Aug-10 -0.2 -0.4 -6.7 **OVERALL PERIOD AVERAGE (mm)** 0.0 -8.9 40 Northing Easting Elevation 30 Settlement/Heave (mm) 20 10 0 -10 -20

Aug-10

Jun-10

-eb-10

Dec-09

Feb-09

Dec-08

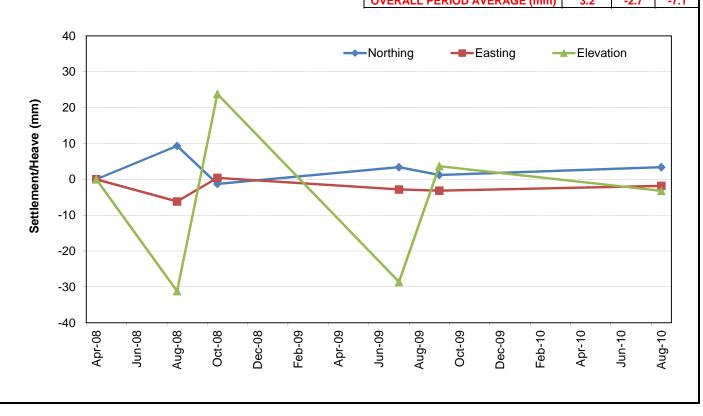
90-unf

4ng-09

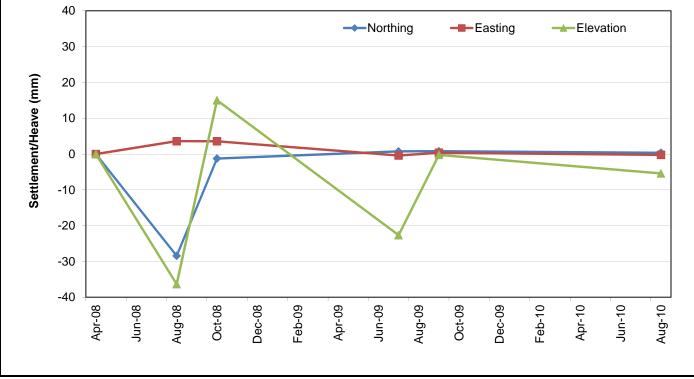
Oct-09

Boston Primary Fuel Tank Farm Settlement Monitoring Tank #6 Difference from Previous **Vertical Angle Horizontal Angle** н Northing Elevation Date Tank Slope Easting Survey [m] Mark Deg Min Sec Deg Min Sec Dist. [m] N ΕI [m] [m] [m] Ε 22-Apr-08 47 5337.092 80.991 6C 86 44 44 92 19 18.155 1.669 1317.422 8-Aug-08 6C 86 44 29 91 47 9 18.157 1.471 5337.099 1317.418 80.965 0.007 -0.004 -0.02618-Oct-08 6C 86 45 2 92 11 48 18.167 1.625 5337.105 1317.418 80.989 0.006 0.001 0.024 25-Jul-09 6C 86 44 30 92 9 45 18.167 1.592 5337.105 1317.416 80.966 -0.001 -0.003 -0.02219-Sep-09 6C 5337.107 1317.413 0.003 86 44 18 92 14 48 18.171 1.622 80.970 0.002 -0.002 2-Aug-10 6C 17 91 58 1.532 5337.108 1317.413 0.001 -0.001 -0.002 86 44 6 18.169 80.968 21 22-Apr-08 6D 301 11 91 39 4 12.434 1.669 5340.813 1317.436 81.031 8-Aug-08 6D 301 23 36 91 11 17 12.430 1.544 5340.819 1317.429 81.006 0.006 -0.007 -0.024 18-Oct-08 7 -0.003 6D 301 23 91 27 28 12.434 1.623 5340.816 1317.430 81.027 0.000 0.020 25-Jul-09 6D 301 24 12 91 18 28 12.434 1.555 5340.818 1317.426 80.991 0.001 -0.004 -0.035 301 12.438 19-Sep-09 6D 26 5 91 8 24 5340.817 81.000 0.000 -0.008 0.008 1.527 1317.417 20-Aug-10 8 52 12.440 0.000 -0.004 6D 301 27 91 4 1.510 5340.818 1317.413 80.995 -0.00422-Apr-08 6E 294 8 42 92 4 22 12.560 1.670 5340.311 1314.183 81.061 8-Aug-08 6E 294 91 52 33 12.542 1.583 5340.325 1314.175 81.017 0.015 -0.008 -0.043 9 24 18-Oct-08 6E 294 9 53 92 3 19 12.550 1.650 5340.318 1314.176 81.045 -0.007 0.000 0.027 25-Jul-09 294 -0.028 6E 35 91 50 52 12.539 1.576 5340.328 1314.174 81.017 0.009 -0.002 9 19-Sep-09 294 6E 9 13 92 0 36 12.539 1.611 5340.329 1314.174 81.016 0.002 0.001 0.000 0.009 2-Aug-10 6E 294 8 34 91 48 31 12.529 1.563 5340.338 1314.174 81.013 -0.001 -0.004

	22-Apr-08	0	0	0
	8-Aug-08	9.3	-6.2	-31.2
TANK AVERAGES BY	18-Oct-08	-1.3	0.4	23.8
DATE (mm)	25-Jul-09	3.4	-2.8	-28.6
	19-Sep-09	1.2	-3.2	3.7
	2-Aug-10	3.4	-1.8	-3.2
OVERALL DEDIOD AVE	2.2	27	7.1	



Boston Primary Fuel Tank Farm Settlement Monitoring **Boston Primary Fuel Tank Farm Settlement Monitoring** Tank #7 Difference from Previous **Vertical Angle Horizontal Angle** н Northing Elevation Date Tank Slope Easting Survey [m] Deg Sec Deg Dist. Mark Min Min Sec [m] N ΕI [m] [m] [m] Ε 22-Apr-08 1307.814 80.875 7A 139 42 34 91 19 5 22.702 1.593 5343.001 8-Aug-08 7A 139 41 54 91 13 37 22.699 1.519 5343.000 1307.809 80.837 0.000 -0.005 -0.038 18-Oct-08 7A 139 42 48 91 35 4 22.706 1.674 5343.001 1307.816 80.850 0.001 0.007 0.013 45 -0.019 25-Jul-09 7A 139 42 40 91 31 22.705 1.633 5343.001 1307.815 80.831 0.000 -0.001 19-Sep-09 2 5343.003 1307.818 -0.002 7A 139 43 91 32 18 22.708 1.635 80.829 0.002 0.003 2-Aug-10 91 10 1.506 1307.818 0.000 -0.003 7A 139 42 56 13 22.706 5343.004 80.827 0.001 22-Apr-08 7B 97 41 28 91 36 36 23.321 1.632 5343.343 1310.862 81.005 8-Aug-08 7B 97 41 3 91 12 7 23.230 1.436 5343.258 1310.879 80.977 -0.085 0.017 -0.028 18-Oct-08 0.011 7B 97 41 12 91 36 11 23.232 1.610 5343.256 1310.881 80.988 -0.002 0.001 25-Jul-09 7B 97 41 14 91 39 3 23.232 1.610 5343.256 1310.881 80.969 0.000 0.000 -0.019 23 41 23.234 19-Sep-09 7B 97 41 3 91 1310.879 80.969 -0.002 0.000 1.626 5343.257 0.001 2-Aug-10 7B 40 48 21 28 23.229 -0.002 -0.007 97 91 1.484 5343.255 1310.878 80.962 -0.001 22-Apr-08 7F 267 27 43 92 53 46 8.278 1.635 5346.505 1307.626 81.060 8-Aug-08 7F 267 27 92 46 47 8.276 1.575 5346.505 1307.624 81.017 0.000 -0.001 -0.043 54 18-Oct-08 7F 267 28 14 93 3 56 8.282 1.637 5346.502 1307.627 81.037 -0.003 0.002 0.020 25-Jul-09 7F -0.030 267 27 32 92 31 52 8.276 1.530 5346.505 1307.626 81.008 0.003 -0.001 19-Sep-09 7F 57 8.281 0.001 267 27 93 13 50 1.632 5346.504 1307.626 81.008 -0.001 -0.001 7F 2-Aug-10 267 27 12 92 36 15 8.276 1.535 5346.506 1307.626 81.002 0.002 0.001 -0.00622-Apr-08 0 Ω 0 3.6 -36.3 8-Aug-08 -28.4 TANK AVERAGES BY 18-Oct-08 15.0 -1.3 3.6 DATE (mm) 25-Jul-09 0.7 -0.4 -22.7 19-Sep-09 8.0 0.4 -0.2 2-Aug-10 0.4 -0.2 -5.4 **OVERALL PERIOD AVERAGE (mm)** 1.4 -9.9 40 Northing Easting ---Elevation 30 20 10 0



Boston Primary Fuel Tank Farm Settlement Monitoring Tank #8 Difference from Previous **Vertical Angle** Northing **Horizontal Angle** н Elevation Date Tank Slope Easting Survey [m] Sec Deg Dist. Mark Deg Min Min Sec [m] N ΕI [m] [m] [m] Ε 22-Apr-08 1317.450 80.956 8C 91 52 15 91 53 25 23.449 1.669 5342.700 8-Aug-08 8C 91 52 27 91 27 51 23.453 1.471 5342.709 1317.449 80.932 0.009 -0.001 -0.024 18-Oct-08 8C 91 52 47 91 44 54 23.460 1.625 5342.713 1317.450 80.969 0.004 0.001 0.038 25-Jul-09 8C 91 52 11 91 44 54 23.460 1.592 5342.712 1317.446 80.936 -0.001 -0.004 -0.033 19-Sep-09 8C 2 5342.715 1317.444 0.002 91 52 1 91 49 23.464 1.622 80.938 0.003 -0.002 2-Aug-10 8C 91 51 51 91 1.532 5342.715 1317.443 -0.001 -0.001 36 4 23.462 80.936 0.000 27 22-Apr-08 8D 318 8 92 56 10 8.342 1.669 5345.860 1317.826 80.962 8-Aug-08 8D 318 11 46 92 12 54 8.340 1.544 5345.864 1317.819 80.942 0.004 -0.007 -0.020 18-Oct-08 8D 318 11 50 92 33 48 8.341 1.623 5345.865 1317.820 80.970 0.001 0.001 0.028 25-Jul-09 8D 318 12 39 92 22 34 8.342 1.555 5345.865 1317.817 80.929 0.000 -0.003 -0.041 8 19 19-Sep-09 8D 318 14 50 92 8.347 80.936 0.000 -0.008 0.006 1.527 5345.865 1317.808 92 2 57 8.350 -0.004 2-Aug-10 8D 318 15 55 1.510 5345.865 1317.804 80.931 0.000 -0.00422-Apr-08 8E 282 47 41 93 37 20 7.635 1.670 5345.604 1313.962 81.033 8-Aug-08 8E 282 46 58 93 16 40 7.615 1.583 5345.619 1313.954 80.993 0.016 -0.007 -0.040 18-Oct-08 8E 282 47 20 93 29 56 7.621 1.650 5345.615 1313.956 81.030 -0.004 0.001 0.037 25-Jul-09 282 50 -0.036 8E 46 37 93 12 7.612 1.576 5345.622 1313.954 80.994 0.007 -0.002 19-Sep-09 282 1.611 -0.001 8F 46 93 29 15 7.613 5345.623 1313.954 80.993 0.001 0.000 11 2-Aug-10 8E 282 44 37 93 10 6 7.603 1.563 5345.632 1313.953 80.988 0.008 -0.001 -0.00522-Apr-08 0 Ω 0 -28.0 8-Aug-08 9.7 -5.3 TANK AVERAGES BY 34.4 18-Oct-08 0.3 1.1 DATE (mm) 25-Jul-09 1.9 -3.0 -36.5 19-Sep-09 1.3 -3.3 2.2 2-Aug-10 2.8 -2.1 -3.6

