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April 18, 2014

Phyllis Beaulieu
Manager of Licensing
Nunavut Water Board
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Re: 2BB-BOS1217 – 2013 Annual Geotechnical Inspection Report

Dear Ms. Beaulieu,

Please find enclosed with this letter TMAC Resources Inc.'s ("TMAC") 2013 Annual Geotechnical Inspection Reports for water licence 2BB-BOS1217.

The Geotechnical Inspection Report is being submitted as per Part D Item 17 of water licence 2BB-BOS1217. As per Part D Item 17, this cover letter outlines TMAC's implementation plan addressing each of the report's recommendations (see attached table).

Should you have any questions or concerns regarding this submission, please do not hesitate to contact me at lea-marie.bowes-lyon@tmacresources.com.

Sincerely,

Léa-Marie Bowes-Lyon
Tenure and Permitting Manager
Hope Bay Project

Inspection Item	2013 Recommendations	Actions
Thermistors	<ul style="list-style-type: none"> The functionality of the three intact thermistors, installed by Golder, should be confirmed. If these strings are operational, the severed string (drill hole 12259-03) should be spliced and tested as well. Any strings that are found to be functional should be included in the formal thermistor monitoring program for the site Formal monitoring of the on-site thermistor strings should continue. This program should consist of an annual reading, if resources are available. Any data collected should be reported as part of subsequent annual geotechnical inspections 	<ul style="list-style-type: none"> To be evaluated during 2014 field season and repairs conducted where possible. Thermistor monitoring to be conducted once a season if the above recommendation is successfully completed.
Primary Tank Farm Settlement Monitoring	<ul style="list-style-type: none"> Annual monitoring (in either July or August) of tank settlement should recommence. This data should be reviewed and reported on as part of the annual geotechnical inspection and, should there be any signs of undue movement, appropriate mitigation plans should be put in motion The foundation settlement risk should be recognized in the spill response plan for the tank farm 	<ul style="list-style-type: none"> Survey will be conducted annually when fuel is stored in tanks. When the Spill Contingence Plan is next revised, the foundation settlement risk will be recognized and included in the plan.
Primary Tank Farm	<ul style="list-style-type: none"> The appearance of surficial slip surfaces and tension cracks on the containment berms should be monitored. Remedial measures should be implemented if the tension cracks become larger. Should excessive deformation of these berms occur (the probability of which is likely low), the tank integrity is not at risk. It is simply the effectiveness of the secondary containment that will be compromised 	<ul style="list-style-type: none"> Containment berms will be monitored.
Power Plant Fuel Containment	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required.
Central Pad Fuel Containment	<ul style="list-style-type: none"> No action required. Should this fuel transfer station be used, the exposed liner should be covered to prevent exposure and/or operational damage 	<ul style="list-style-type: none"> No action required.
Jet Fuel and Lubricant Containment	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required.
Solid Waste Disposal Site (including Burn Pit)	<ul style="list-style-type: none"> Remove the two large pieces of black liner material from the tundra 	<ul style="list-style-type: none"> Material was removed following the inspection in September 2013.

Inspection Item	2013 Recommendations	Actions
Ore Stockpiles	<ul style="list-style-type: none"> The procedures, protocols and monitoring plan stipulated in the 2009 water and ore/waste rock management plan for the Boston site (SRK 2009d) should be implemented A comprehensive review of the annual seep survey data since 2008 should be done to confirm if any trends are present that contradict the 2009 management plan 	<ul style="list-style-type: none"> To be implemented in 2014. Report has been prepared.
Containment Pond	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required.
Soil Containment Berm (Landfarm)	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required.
Drill Cuttings and Settling Pond	<ul style="list-style-type: none"> Remediation efforts to continue to backfill this depression in the tundra with drill cuttings should continue. Ideally this should be done from the upstream side working downstream to gradually remove any ponding water When there is active placement of drill cuttings into the ponded water, best management practices must be put in place to prevent release of silt-laden water Water quality sampling should be carried out to confirm that the drill cuttings are not saline 	<ul style="list-style-type: none"> No active drilling to occur in 2014 so this task cannot be completed until drilling resumes. No active drilling to occur in 2014 so this task cannot be completed until drilling resumes Sampling will be carried out at least once a season.
Portal	<ul style="list-style-type: none"> SRK recommends that TMAC replace the weathered warning notices at the portal entrance advising of the dangers associated with unauthorized access to the area The rock spalling on the exposed section of the portal roof is likely a fall hazard. Persons entering the area should wear appropriate personal protective equipment; however, a site specific hazard assessment should be completed to make people aware of the dangers. Should there be a need for any individual to enter the area for reasons other than a brief inspection, consideration should be given to installing roof support, such as a small diameter wire mesh (50 mm mesh) to mitigate the fall hazard 	<ul style="list-style-type: none"> Warning notices at portal will be replaced. While the site remains in care and maintenance, the recommended repair work cannot be undertaken. Although staff do not generally enter the portal roof area, appropriate personal protective equipment will be worn and proper controls will be put in place in the case where the area needs to be accessed.
Vent Raise	<ul style="list-style-type: none"> The tarps are significantly weathered and their attachment points are starting to come apart. The tarps should be replaced Sign posts warning visitors of potential dangers associated with accessing the area do not exist. It is recommended that signs be erected 	<ul style="list-style-type: none"> Tarps will be replaced in 2014. Signs will be erected in 2014.
Road to Dock	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required.

Inspection Item	2013 Recommendations	Actions
Camp Complex Foundation Pad	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required.
Road to Airstrip	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required.
Airstrip	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required.
Drill Road	<ul style="list-style-type: none"> Monitor the pipe culvert for progressive permafrost degradation 	<ul style="list-style-type: none"> Pipe culvert will be monitored.
Core Storage Road	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required.
Wooden Walkway to Boat Dock	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required.
Radio Tower and Shack	<ul style="list-style-type: none"> Remove the tower from the tundra 	<ul style="list-style-type: none"> Due to the site being in care and maintenance, the tower cannot be removed at this time.
Water Intake Pump Shack	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required.
Original STP Foundation Pad	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required.
New STP Foundation Pad	<ul style="list-style-type: none"> The area where the ore pad was backhauled, and where minor damage to the tundra occurred, must be monitored to ensure no ponding of water, which would lead to increased vegetation die back and subsequent permafrost damage 	<ul style="list-style-type: none"> Area will be monitored for vegetation die back and permafrost damage.
Core Storage Area(s)	<ul style="list-style-type: none"> Monitor the areas where the core boxes have been removed from the tundra, and where minor damage has occurred, to ensure there is no ponding of water, which would lead to increased vegetation die back and subsequent permafrost degradation 	<ul style="list-style-type: none"> Area will be monitored for vegetation die back and permafrost damage.
Grey Water Discharge	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required.
Historic Drill Sites	<ul style="list-style-type: none"> HBML initiated remediation measures to address some of the erosion gully's formed by drilling fluid using cocoa matting and re-vegetation. This program appears to be successful at controlling erosion and although vegetation re-growth appears slow, it is likely to occur. TMAC should consult the services of an expert knowledgeable with tundra vegetation to implement appropriate remediation strategies An action plan is needed to remediate the drill sites where significant permafrost degradation and vegetation die back has resulted in permanent ponds of standing water. This standing water is causing further 	<ul style="list-style-type: none"> An expert in tundra vegetation has been consulted and appropriate remediation strategies will be implemented where possible. TMAC is aware of this issue but limited action can be undertaken while the Boston site remains in care and maintenance.

Inspection Item	2013 Recommendations	Actions
	permafrost degradation, which in turn increases the pond's size	
Orbit 25 Drill Site	<ul style="list-style-type: none"> Continue developing and subsequently implement an appropriate remediation plan for this site 	<ul style="list-style-type: none"> This work is on-going.
Vegetation Die Back Zone	<ul style="list-style-type: none"> Follow recommendations of sections 3.5.3 (Historic Drill Sites) and 3.5.4 (Orbit 25 Drill Site) 	<ul style="list-style-type: none"> See actions for 3.5.3 and 3.5.4.
V-Notch Weir	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required.



2013 Annual Geotechnical Inspection Boston Advanced Exploration Project Hope Bay, Nunavut

Prepared for

TMAC Resources Inc.



Prepared by



SRK Consulting (Canada) Inc.
1CT022.000
March 2014

2013 Annual Geotechnical Inspection Boston Advanced Exploration Project Hope Bay, Nunavut

March 2014

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Executive Summary

The Boston Advanced Exploration Project (Boston Camp) is a wholly owned exploration camp of TMAC Resources Inc. (TMAC). The camp is located about 170 km southwest of Cambridge Bay within the western Kitikmeot Region, Nunavut (with general coordinates of latitude 67°39'N and longitude 106°22'W). Boston Camp was used on a seasonal basis to carry out prospecting and exploration, various forms of exploration drilling, core splitting and logging up until 2011. In addition, the site has historically been subjected to bulk underground sampling and testing. The camp was temporarily closed between mid-2009 and mid-2010, pending improvements to the camp sewage treatment plant (STP). In 2012, the camp was closed as the Hope Bay Project was shut down and placed under Care & Maintenance. In March 2013, the Hope Bay Project was purchased by TMAC Resources and the Boston Camp remained closed while exploration activities were focused around the Doris North area.

Any site operations are currently conducted under Nunavut Water Board (NWB) Licence 2BB-BOS1217, dated August 2, 2012, which entitles TMAC to use water and dispose of waste associated with their operations. TMAC contracted SRK Consulting (Canada) Inc. (SRK) to conduct the annual geotechnical site inspection of Boston Camp in accordance with stipulated License conditions. This investigation was carried out from August 20th to 23rd, 2013.

Table A below provides a summary of the inspection components and the primary recommendations stemming from the inspection. These recommendations are compared with those listed in the 2012 annual geotechnical report (SRK 2013). There are no issues that require urgent and immediate action.

Table A: Summary of Inspection Items

Inspection Item	2012 Recommendations	2013 Recommendations
Thermistors	<ul style="list-style-type: none">• Locate appropriate readout device for older thermistors and confirm functionality of strings• Consider splicing broken string• Confirm status of string in 08SBD381A• Cease quarterly monitoring, but monitor once per year in July or August	<ul style="list-style-type: none">• The functionality of the three intact thermistors, installed by Golder, should be confirmed. If these strings are operational, the severed string (drill hole 12259-03) should be spliced and tested as well. Any strings that are found to be functional should be included in the formal thermistor monitoring program for the site• Formal monitoring of the on-site thermistor strings should continue. This program should consist of an annual reading, if resources are available. Any data collected should be reported as part of subsequent annual geotechnical inspections

Inspection Item	2012 Recommendations	2013 Recommendations
Primary Tank Farm Settlement Monitoring	<ul style="list-style-type: none"> Cease quarterly monitoring, but monitor once per year in July or August Recognize foundation settlement risk in spill response plan 	<ul style="list-style-type: none"> Annual monitoring (in either July or August) of tank settlement should recommence. This data should be reviewed and reported on as part of the annual geotechnical inspection and, should there be any signs of undue movement, appropriate mitigation plans should be put in motion The foundation settlement risk should be recognized in the spill response plan for the tank farm
Primary Tank Farm	<ul style="list-style-type: none"> Monitor the surficial slip surfaces on the tank farm berms Continue settlement monitoring as described above 	<ul style="list-style-type: none"> The appearance of surficial slip surfaces and tension cracks on the containment berms should be monitored. Remedial measures should be implemented if the tension cracks become larger. Should excessive deformation of these berms occur (the probability of which is likely low), the tank integrity is not at risk. It is simply the effectiveness of the secondary containment that will be compromised
Power Plant Fuel Containment	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Central Pad Fuel Containment	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required. Should this fuel transfer station be used, the exposed liner should be covered to prevent exposure and/or operational damage
Jet Fuel and Lubricant Containment	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Solid Waste Disposal Site (including Burn Pit)	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> Remove the two large pieces of black liner material from the tundra
Ore Stockpiles	<ul style="list-style-type: none"> Implement the 2009 water and ore/ waste rock management plan developed for the site 	<ul style="list-style-type: none"> The procedures, protocols and monitoring plan stipulated in the 2009 water and ore/ waste rock management plan for the Boston site (SRK 2009d) should be implemented A comprehensive review of the annual seep survey data since 2008 should be done to confirm if any trends are present that contradict the 2009 management plan
Containment Pond	<ul style="list-style-type: none"> Construct suitable barrier around the pond to prevent inadvertent human and/ or animal access 	<ul style="list-style-type: none"> No action required
Soil Containment Berm (Landfarm)	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required

Inspection Item	2012 Recommendations	2013 Recommendations
Drill Cuttings and Settling Pond	<ul style="list-style-type: none"> Continue practice of infilling depression with drill cuttings starting from the upstream end Implement best management practices to ensure silt containment 	<ul style="list-style-type: none"> Remediation efforts to continue to backfill this depression in the tundra with drill cuttings should continue. Ideally this should be done from the upstream side working downstream to gradually remove any ponding water When there is active placement of drill cuttings into the ponded water, best management practices must be put in place to prevent release of silt-laden water Water quality sampling should be carried out to confirm that the drill cuttings are not saline
Portal	<ul style="list-style-type: none"> Replace the faded notices at the portal entrance advising of the dangers associated with unauthorized access to the area Develop site specific hazard assessment for people entering the portal area to address the rockfall hazard Consider installing a small diameter wire mesh over the exposed section of the portal roof to address the rockfall hazard 	<ul style="list-style-type: none"> SRK recommends that TMAC replace the weathered warning notices at the portal entrance advising of the dangers associated with unauthorized access to the area The rock spalling on the exposed section of the portal roof is likely a fall hazard. Persons entering the area should wear appropriate personal protective equipment; however, a site specific hazard assessment should be completed to make people aware of the dangers. Should there be a need for any individual to enter the area for reasons other than a brief inspection, consideration should be given to installing roof support, such as a small diameter wire mesh (50 mm mesh) to mitigate the fall hazard
Vent Raise	<ul style="list-style-type: none"> Replace weathered protective tarps covering the shelter erected over the vent raise Install notices at the vent raise advising of the dangers associated with unauthorized access to the area 	<ul style="list-style-type: none"> The tarps are significantly weathered and their attachment points are starting to come apart. The tarps should be replaced Sign posts warning visitors of potential dangers associated with accessing the area do not exist. It is recommended that signs be erected
Road to Dock	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Camp Complex Foundation Pad	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Road to Airstrip	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Airstrip	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Drill Road	<ul style="list-style-type: none"> Monitor the pipe culvert for progressive permafrost degradation 	<ul style="list-style-type: none"> Monitor the pipe culvert for progressive permafrost degradation
Core Storage Road	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Wooden Walkway to Boat Dock	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Radio Tower and Shack	<ul style="list-style-type: none"> Remove dismantled tower from tundra 	<ul style="list-style-type: none"> Remove the tower from the tundra

Inspection Item	2012 Recommendations	2013 Recommendations
Water Intake Pump Shack	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Original STP Foundation Pad	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
New STP Foundation Pad	<ul style="list-style-type: none"> Monitor the areas where tundra vegetation damage has occurred Develop long-term re-vegetation plan; involve a tundra vegetation expert 	<ul style="list-style-type: none"> The area where the ore pad was backhauled, and where minor damage to the tundra occurred, must be monitored to ensure no ponding of water, which would lead to increased vegetation die back and subsequent permafrost damage
Core Storage Area(s)	<ul style="list-style-type: none"> Monitor the areas where tundra vegetation damage has occurred Develop long-term re-vegetation plan; involve a tundra vegetation expert 	<ul style="list-style-type: none"> Monitor the areas where the core boxes have been removed from the tundra, and where minor damage has occurred, to ensure there is no ponding of water, which would lead to increased vegetation die back and subsequent permafrost degradation
Grey Water Discharge	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Historic Drill Sites	<ul style="list-style-type: none"> Develop remediation strategy to prevent further permafrost degradation 	<ul style="list-style-type: none"> HBML initiated remediation measures to address some of the erosion gully's formed by drilling fluid using cocoa matting and re-vegetation. This program appears to be successful at controlling erosion and although vegetation re-growth appears slow, it is likely to occur. TMAC should consult the services of an expert knowledgeable with tundra vegetation to implement appropriate remediation strategies An action plan is needed to remediate the drill sites where significant permafrost degradation and vegetation die back has resulted in permanent ponds of standing water. This standing water is causing further permafrost degradation, which in turn increases the pond's size
Orbit 25 Drill Site	<ul style="list-style-type: none"> Continue developing and subsequently implement an appropriate remediation plan for remediation of this site 	<ul style="list-style-type: none"> Continue developing and subsequently implement an appropriate remediation plan for this site
Vegetation Die Back Zones	<ul style="list-style-type: none"> Initiate study to determine why die back continues; involve a tundra vegetation expert Develop remediation strategy to prevent further die back and permafrost degradation 	<ul style="list-style-type: none"> Follow the recommendations in Sections 3.5.3 and 3.5.4
V-Notch Weir	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required

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Appendices

Appendix A: Boston Primary Fuel Tank Farm Settlement Monitoring

1 Introduction and Scope of Report

1.1 Inspection Requirements

The Boston Advanced Exploration Project (Boston Camp) is an exploration camp of TMAC Resources Inc. (TMAC). The camp is located about 170 km southwest of Cambridge Bay within the western Kitikmeot Region, Nunavut (with general coordinates of latitude 67°39'N and longitude 106°22'W, as shown in Figure 1.

The Boston Camp has been closed and is under Care & Maintenance. Up until February 2012 the Boston Camp was used on a seasonal basis to carry out prospecting and exploration, various forms of exploration drilling, core splitting and logging. In addition, the site has historically been subjected to bulk underground sampling and testing.

Site operations are currently conducted under Nunavut Water Board (NWB) Licence 2BB-BOS1217 (the Licence), dated August 2, 2012, which entitles TMAC (the Licensee) to use water and dispose of waste associated with their operations. Part D, Item 17 of the License (NWB 2007) states the following:

“An inspection of the earthworks, geological regime, and the hydrological regime of the Project is to be carried out annually during the summer by a Geotechnical Engineer. The Geotechnical Engineer’s report shall be submitted to the Board within sixty (60) days of the inspection, with a covering letter from the Licensee outlining an implementation plan to respond to the Engineer’s recommendations.”

Additionally, Part D, Item 10 states:

“The Licensee shall design and berm the Containment Ponds to prevent seepage. A report on seepage shall be included as part of the Geotechnical Engineer’s annual report required by Part D, Item 17.”

In fulfillment of these regulatory requirements, Mr. Chris Hanks, Director for Environment and Social Responsibility (ESR) for Newmont Mining Company (NMC), requested that SRK Consulting (Canada) Inc. (SRK) conduct the 2013 geotechnical site inspection. This report provides a summary of the conditions observed and the resulting mitigation recommendations. Table 1 provides a summary of the inspection components. SRK has carried out six previous formal geotechnical inspections in fulfillment of the Water Licence requirements between 2007 and 2011 (SRK 2008, 2009a, f, 2011a, 2012, and 2013). This report describes the seventh formal annual geotechnical inspection.

Table 1: List of Individual Inspection Items

Facility/Data Type	Inspection Item
Instrumentation/Data	Thermistor data (No data collected in 2013)
	Primary Tank Farm Settlement (No surveys conducted in 2013)
Containment Structures	Primary Tank Farm
	Power Plant Fuel Containment
	Central Pad Fuel Containment
	Jet Fuel and Lubricant Containment
	Solid Waste Disposal Site (including Burn Pit)
	Ore Stockpiles
	Containment Pond
	Soil Containment Berm (Landfarm)
	Drill Cuttings and Settling Pond
Mine Openings	Portal
	Vent Raise
Infrastructure	Road to Dock
	Camp Complex Foundation Pad
	Road to Airstrip
	Airstrip
	Drill Road
	Core Storage Road
	Wooden Walkway to Boat Dock
	Radio Tower and Shack
	Water Intake Pump Shack
	Original STP Foundation Pad
	New STP Foundation Pad
Other Areas	Core Storage Area(s)
	Grey Water Discharge
	Historic Drill Sites
	Orbit 25 Drill Site
	Vegetation Die Back Zones
	V-Notch Weir

1.2 Report Structure

Section 2 of this report provides a brief summary of the site history and physical conditions to provide context for the report content. The inspection conditions are described in Section 3 and an overall summary of recommendations is provided in Section 4. Photos representing the inspection conditions are included as Figures. Although there is no new settlement monitoring or thermal data to report, the complete dataset collected to date are included as Appendix A.

2 Site Conditions

2.1 Site History

A brief summary of the site history is listed in Table 2.

Table 2: Summary of Pertinent Site Ownership History

Period	Comment
1964	Sporadic exploration in the Hope Bay area begins, resulting in several gold and silver showings including Ida Point, Ida Bay and Roberts Lake.
1970	Roberts Bay Mining explores the area for about a decade up to 1980.
1977	Noranda begins exploring for volcanogenic massive sulphide deposits. They leave the belt in 1990. Prior to 1980, Roberts Bay Mining also explored the area.
1987	Abermin Corporation stake claims in the vicinity of Aimaokatalok and Doris Lakes. After completing some exploration they allow their claims to expire.
1988	BHP Minerals Canada Inc. explores the southern portion of Hope Bay Volcanic Belt.
1991	BHP acquires a contiguous block of claims covering about 1,106 km ² from Abermin Corporation
1992	BHP commences exploration drilling at the Boston property.
1993	The first camp is constructed on the northeastern shores of Stickleback Lake by BHP.
1994	The Stickleback Lake camp is dismantled and moved to the current location of Boston Camp at the south end of Aimaokatalok Lake. The camp is expanded to house 35 people.
1996 and 1997	BHP complete 2,300 m of underground development, underground exploration (drilling and sampling) and bulk sampling of the Boston deposit.
1999	BHP sells all its interests in the Hope Bay Belt to Hope Bay Joint Venture (HBJV), a 50:50 joint venture between Hope Bay Gold Corporation Inc. (formerly Cambiex Exploration Inc.), and Miramar Hope Bay Limited (MHBL), a wholly owned subsidiary of Miramar Mining Corporation (MMC).
2002	Hope Bay Gold Corporation Inc. formally merges with MMC, and the Hope Bay site is operated under MHBL.
2008	Hope Bay Mining Limited (HBML), a wholly owned subsidiary of Newmont Mining Corporation (NMC) buys out all interests in the Hope Bay Belt from MMC. HBML assumes responsibility of the camp and Water Licence for Boston.
2009 to 2010	The camp is temporarily closed pending upgrades to the STP.
2011	The camp re-opens as a seasonal exploration camp.
2012	HBML decides to suspend operations at Hope Bay, closing the camp in February and placing it under Care & Maintenance.
2013	In March TMAC acquires the Hope Bay Project. The Boston Camp remains under Care & Maintenance.

2.2 Site Infrastructure

The Boston Camp is situated on a ridge and is comprised of a peninsula extending northwards into Aimaokatalok Lake, as illustrated on Figure 2. The main camp footprint spans about 325 m from north to south, and 150 m east to west. The bulk of the camp facilities are located on a crushed rock pad, ranging in thickness from 0.6 m to 3 m. The pad was designed to slope generally north at a gradient of about 1%.

The camp consists of a series of joined trailers to provide accommodations and office space for about 50 people. One trailer houses the water treatment plant and another, off the main pad, the original S-40 ROTORDISK® Sewage Treatment Plant (STP). In 2010, a new SaniBrane® STP was been constructed, and replaced the original STP. There are six tents that act as additional office space and core logging shacks. A “Weatherhaven” type building, that was used to contain the bulk sampling crushing plant, is now used as a workshop and as a general equipment storage shed. The last remaining buildings consist of a maintenance shop and the power generator shed. Generator fuel (diesel) is supplied from two aboveground storage tanks, adjacent to the power house. Eight additional bulk fuel tanks are housed in an engineered containment facility.

The original surveyed as-built site plan is presented in Figure 2, while current conditions of the main camp complex is presented in Figures 3 and 4. In addition to the main camp complex, these figures illustrate the relative locations of all the main infrastructure components, containment structures and mine openings.

2.3 Climate

Site specific climate data at Boston Camp is limited to a few years of data collected by BHP in the late 1990s. Comparison of this data, with regional weather stations operated by Environment Canada, suggests that the mean annual site temperature is about -13.5°C. The extrapolated mean annual precipitation is about 208 mm, with 108 mm of that falling as rain and the remainder as snow. The area is classified as arctic desert (EBA 1997).

2.4 Regional Geomorphology

During the Quaternary period, the region was subjected to multiple glaciations. The northwestern sector of the vast Laurentide Ice Sheet covered the area during each glaciation, and the present day landscape provides clear evidence of the most recent (Late Wisconsin) glaciation. Striations, orientation of eskers, grooves and drumlins indicate that the predominant glacial ice movement was north-northwest (EBA 1996).

The ice disappeared about 8,800 years ago leaving a blanket of basal till. The sea level was about 200 m higher than present immediately following de-glaciation. At that time, the project area was submerged and the edge of the ice sheet abutted the open sea. Melt water streams from the ice carried fine grained sediments towards the sea, resulting in the accumulation of marine sediments on top of the till, with the greatest accumulation in deeper water zones, which now form the valley bottoms (EBA 1996).

Isostatic rebound after de-glaciation resulted in emergent landforms, and during this process all parts of the land were washed by waves. The easily erodible marine sediments, till and glacio-fluvial sands and gravels were subsequently reworked by waves, currents and sea ice. This has resulted in the present day outcrops where thin soil veneers were washed off the uplands and deposited in the valley bottoms. Since emergence, the natural effects of weathering, frost action and permafrost have transformed the landscape to its present day shape (EBA 1996).

2.5 Permafrost and Geotechnical Conditions

Surficial geotechnical investigations at the Boston project area are limited to a series of seven drill holes and a subsequent terrain analysis carried out by EBA Engineering Consultants Ltd. (EBA) in 1996 (EBA 1996, 1997). There is also a series of thermistors that have been installed at the site including three shallow strings in 1996 (EBA 1996), one deep string in 1997 (EBA 1997; Golder 2000a, b), and three deep strings in 2008 (SRK 2009e). A Westbay well was installed in 2010 (SRK 2011b), which allows recording of down hole water temperature during pumping. The location of all surficial geology drill holes and thermistor string locations are presented in Figure 2, and summarized in Table 3. Figures 6 through 13 summarize all available thermistor string data.

Table 3: Summary of Permafrost Drillholes and Thermistor Installations

Drill Hole ID	UTM Coordinates		Surface Elevation (m)	Completion Depth (m)	Thermistor Installed (Serial #)	Source
	Northing	Easting				
12259-01 (BH1)	7,504,261*	441,482*	68.6*	10.9 (below lake)	No	EBA (1996, 1997)
12259-02 (BH2)	7,504,141	441,213	71.7	4.1	No	
12259-03 (BH3)	7,504,380	441,113	77.6	16.1	Yes (#1049)	
12259-04 (BH4)	7,503,905*	442,323*	73.9	13.9	No	
12259-05 (BH5)	7,504,778	441,172	80.8	15.6	Yes (#1050)	
12259-06 (BH6)	7,505,683	441,327	69.7	15.8	Yes (#1051)	
12259-07 (BH7)	7,506,153*	441,830*	Unknown	Unknown	No	
97NOD176	7,504,962	441,481	78.3	367 @ -60° (298 true)	Yes	Golder (2000a, 2000b)
08SBD380	7,504,780	441,080	77.3	402 @ -60° (334 true)	Yes	SRK (2009e)
08SBD381A	7,504,814	441,070	69.6	401 @ -55° (298 true)	Yes	
08SBD382	7,505,141	441,026	72.8	404 @ -60° (323 true)	Yes	
10WBW004	7,505,665	441,018	Unknown	470 @ -55° (250 true)	No (Westbay)	SRK (2011b)

Note:

* Approximate information as interpolated from source drawings by SRK. Exact information is not available. Locations not marked with asterisk are surveyed coordinates.

The available information confirms that the Boston Camp is located well within the region of cold, continuous permafrost. Permafrost temperatures are below about -8°C and the active layer is generally less than 1 m thick, with the depth of zero annual amplitude about 10 m. Based on data from the deep thermistor installed in 1997, the permafrost depth is estimated to be about 520 m (Golder 2000a).

Laboratory testing (moisture contents, Atterberg Limits, grain size distribution and pore water salinity) on intact samples collected during the drilling campaign in 1996 confirms that overburden soils are comprised mainly of marine silt and morainal till ranging in thickness from 1.5 to 8 m. The silt contains up to 50% (by volume of soil) ground ice, while the till contains low to moderate ice contents (5 to 25%) (EBA 1997).

3 Inspection Conditions

Mr. Maritz Rykaart, PhD, PEng, a Principal Consultant with SRK, conducted the geotechnical inspection during the week of August 20th to 23rd, 2013. The detailed site inspection was carried out on foot, after conducting an aerial survey using a low altitude helicopter flyover. The site was accessed via helicopter from the Doris North Camp. Ms. Léa-Marie Bowes-Lyon, TMAC's Tenure and Permitting Manager was on site, accompanied SRK during the inspection, and was also available for questioning.

Weather conditions during the inspection were cool, overcast with light wind, and no precipitation. Photos detailing the inspection conditions are included in Figures 14 through 24.

3.1 Instrumentation/ Data

3.1.1 Thermistors

A summary of the available site thermistors are discussed in Section 2.5 and all available data are presented graphically in Figures 6 through 13. It is not known if any other data from the 1996 and 1997 installations has been recorded since their installation and reporting in 1997 (EBA 1997). Golder Associates Ltd. (Golder) (Golder 2000a, b) documents the findings of a site inspection, including revisiting some of the thermistors; however, no additional data was added. With assistance from HBML's surveyors, the historic thermistors were located as part of the 2009 geotechnical inspection, to determine their status. One string was severed completely (drill hole 12259-03), most likely by an animal. The section of cable to which the readout connector is attached, is still at the site, and it should be possible to re-attach the cable through splicing. The remaining three appear to be intact although they are generally in poor condition, having fallen over from their support struts. Figure 5 illustrates their state during the 2011 annual inspection as the thermistor strings were not visited during the 2012 or 2013 inspections. During the 2011 annual inspection, a readout device compatible with the military connectors of these older strings was not available but has since been located. The functionality of the three thermistor strings should be tested. If the three in-tact strings are functional, the fourth string should be spliced and tested as well. Installation of these thermistor strings represents a considerable investment, and therefore re-instating these old strings to allow ongoing data collection would be valuable.

In 2008, SRK installed three thermistor strings (SRK 2009e) as well as a Westbay Well, in 2010 (SRK 2011a) (Figure 2). Data collected from the three strings and the Westbay Well are presented in Figures 10 through 13. No new data was collected from this instrumentation in 2013.

Recommendations

- The functionality of the three intact thermistors, installed by Golder, should be confirmed. If these strings are operational, the severed string (drill hole 12259-03) should be spliced and tested as well. Any strings that are found to be functional should be included in the formal thermistor monitoring program for the site.
- Formal monitoring of the on-site thermistor strings should continue. This program should consist of an annual reading, if resources are available. Any data collected should be reported as part of subsequent annual geotechnical inspections.

3.1.2 Primary Tank Farm Settlement Monitoring

The 2007 annual geotechnical report recommended that a series of settlement beacons be installed on the Primary Tank Farm containment berm to allow quarterly settlement surveys to provide early warning signs of tank settlement as a result of foundation settlement due to permafrost degradation. HBML opted not to install the recommended beacons, but rather initiated a survey program based on three control points on each of the eight tanks in the containment area. This was an appropriate monitoring program, in the opinion of SRK. The control points were established by the site surveyor, Mr. Jay Hallman, on April 21, 2008. The control point co-ordinates and elevations are listed in Table 4.

Table 4: Summary of Survey Control Points Established for the Primary Tank Farm

Tank	Control Point	Northing (m)*	Easting (m)*	Elevation (m)
1	A	5,325.879	1,305.901	80.674
	B	5,326.428	1,308.581	80.989
	C	5,328.263	1,306.711	80.992
2	A	5,327.678	1,315.749	80.877
	B	5,326.866	1,318.217	81.190
	C	5,329.353	1,318.048	81.114
3	A	5,331.618	1,306.850	81.057
	B	5,331.612	1,309.744	81.062
	C	5,335.467	1,307.263	81.090
4	A	5,331.166	1,318.159	81.128
	B	5,334.739	1,317.563	81.092
	C	5,334.220	1,314.710	81.128
5	A	5,337.355	1,307.654	80.896
	B	5,337.490	1,310.713	81.075
	C	5,341.035	1,307.826	81.089
6	A	5,337.092	1,317.422	80.991
	B	5,340.813	1,317.436	81.031
	C	5,340.311	1,314.183	81.061
7	A	5,343.001	1,307.814	80.875
	B	5,343.343	1,310.862	81.005
	C	5,346.505	1,307.626	81.060
8	A	5,342.700	1,317.450	80.956
	B	5,345.860	1,317.826	80.962
	C	5,345.604	1,313.962	81.033

Note:

* This is a local grid for settlement surveying only.

Two subsequent settlement surveys were carried out in 2008 (August 7 and October 17), two in 2009 (July 25 and September 19), and one each in 2010 (August 2) and 2011 (July 3). No settlement surveys were conducted in 2012 or in 2013. These surveys were completed by HBML survey staff using a TOTAL Station and prisms. The survey accuracy is not stated; however, it should be within ± 10 mm. The complete results are presented in Appendix A and the overall summary data is presented in Table 5.

A review of the data as part of the 2011 inspection suggested a slow but consistent trend of the tanks settling; however, the settlement was very small and since there was no apparent trend of movement in the horizontal plane and there was no indication that differential settlement (that could cause the tanks to topple) was taking place. Visual inspection, of the fuel tanks, during the 2013 site visit confirmed the 2011 observations are probably still valid.

Settlement could occur as a result of permafrost thaw due to the foundation conditions under the fuel tanks. This situation should continue to be monitored and an acknowledgement of the settlement risk should remain.

Table 5: Summary of Overall Settlement Data for the Primary Tank Farm (April 2008 to July 2011)

Tank	Average Survey Differences (mm)		
	Northing ¹	Easting ¹	Elevation ²
#1	3.1	0.5	-5.3
#2	2.6	-0.4	-5.8
#3	0.0	2.7	-2.1
#4	3.1	-1.1	-5.0
#5	-1.2	1.8	-5.0
#6	3.5	-1.9	-6.1
#7	-4.4	2.7	-5.8
#8	3.9	-2.4	-5.6

Notes:

1. A negative value implies tank has moved to the south (Northing) or the west (Easting).
2. A negative value implies tank has moved down.

Recommendations

- Annual monitoring (in either July or August) of tank settlement should recommence. This data should be reviewed and reported on as part of the annual geotechnical inspection and, should there be any signs of undue movement, appropriate mitigation plans should be put in motion.
- The foundation settlement risk should be recognized in the spill response plan for the tank farm.

3.2 Containment Structures

3.2.1 Primary Tank Farm

The Primary Tank Farm, housing eight large fuel tanks is located in an engineered secondary containment facility constructed in 2001 (Figure 14). SRK understands that there is no formal as-built documentation for the facility. The facility was designed by EBA and subsequently constructed by MHBL with engineering supervision by EBA.

It is understood that secondary containment is provided by a PVC liner (type unspecified) placed on a prepared rockfill pad with rockfill containment berms providing the necessary containment capacity. The liner has a top cover of gravel (crushed ore stockpile material) as a protection layer. The eight tanks are placed directly onto the protection layer and are interconnected with permanent steel piping. The entire facility is constructed directly on permafrost overburden soils, as described in Section 2.5

Visual inspection of the secondary containment facility showed past evidence of surficial slip surfaces on the containment side slopes. In 2008, a few small tension cracks were observed along the berm crest. These were not noticed during the 2009 inspection, but were again observed as part of the 2010 and 2011 inspections. During the 2013 inspection, the tension cracks showed evidence of healing over. The slip surfaces could have been an early indication of settlement, or may simply be relaxation due to the over steepened nature of the gravel berm. The liner is not exposed anywhere, and the containment berms for both the main containment facility and the fuel transfer areas are intact. There were no visible signs of fuel spills outside of the respective containment areas. HBML had rigorous protocols in place for fuel transfer, and provided those continue to be followed, the facility design appears adequate to provide environmental protection. During the inspection it was noted that there was no ponded water in the containment area. The facility is equipped with a sump, and the practice of keeping the containment area free of ponded water is appropriate and should be maintained.

Fuel transfer from these main tanks into equipment, fuel drums and Tidy Tanks is done in a contained fuel transfer area, using an electric pump located on top northwest corner of the secondary containment berm adjacent to the access ramp. This fuel transfer area has been shut down under Care & Maintenance.

A Tidy Tank is located at the top of the access ramp. It appears this may still be in use as the fuel transfer pumps have been shut down. This temporary refueling station should be dismantled once all site activities have been completed. Should any fuel be spilled it will not be contained by the bounded area but run down the access ramp onto the camp pad.

The small double-wall fuel tank located at the base of the access ramp sits within a bunded area. The liner is exposed and torn along the south berm. Any exposed liner material should be covered to protect the liner from puncture or exposure damage. This double-wall fuel tank was used to re-fuel light vehicles. Since the Boston Camp is now under Care & Maintenance this fuel tank and secondary containment requires no special attention.

Recommendations

- The appearance of surficial slip surfaces and tension cracks on the containment berms should be monitored. Remedial measures should be implemented if the tension cracks become larger. Should excessive deformation of these berms occur (the probability of which is likely low), the tank integrity is not at risk. It is simply the effectiveness of the secondary containment that will be compromised.

3.2.2 Power Plant Fuel Containment

Two small double-wall fuel tanks servicing the Power Plant are located in a secondary containment facility (rockfill berm) immediately west of the Maintenance Shop (Figure 15). Construction details for this secondary containment are not available; however, repairs to this containment system were completed in 2008, including installation of a liner (SRK 2009a). The liner has been exposed along the southwest berm; however, there are no concerns with this facility.

Recommendations

- No action required.

3.2.3 Central Pad Fuel Containment

The small double-walled fuel tank was installed in 2009 located approximately in the center of the camp pad, immediately east of the geology offices. This fuel tank was installed in a purpose built secondary containment facility using a liner (type unspecified) and the stockpiled crushed ore. The facility was founded directly on the camp pad. Construction details (design or as-built drawings) of this facility are not available. Based on the 2013 visual inspection the liner has been exposed along north, west sides and southeast corner of the containment facility.

Recommendations

- No action required. Should this fuel transfer station be used, the exposed liner should be covered to prevent exposure and/or operational damage.

3.2.4 Jet Fuel and Lubricant Containment

Jet fuel was stored in drums, which were grouped together on wooden pallets, stacked two high, in an area of the rockfill pad north northwest of the primary fuel tank farm. Two portable pollution control berms were used to provide secondary containment. The remaining jet fuel has been relocated to the two sea cans located west of this area. The two portable pollution control berms have been removed and a few remaining empty drums are now being stored at this location (Figure 16).

Recommendations

- No action required.

3.2.5 Solid Waste Disposal Site (Including Burn Pit)

Combustible domestic waste was incinerated on site. Other non-hazardous and hazardous waste was stockpiled, packaged and seasonally removed from site to Yellowknife or Hay River as backhaul opportunities arose. Substantial site cleaned up has been conducted and the backlog of material that still has to be hauled away has been significantly reduced since the 2008 annual geotechnical inspection was completed. The waste material that remains on site is either located in the Bone Yard next to the Landfarm or bagged and stored next to the Ore Stockpiles.

At one time, all wood waste was burned in a Burn Pit (a converted containment pond) located immediately south of the active Containment Pond (Figure 17); however, this practice has been discontinued and all non-combustible materials has been removed from the Burn Pit. Up to 2010, the Burn Pit itself was used to contain unburned wood waste and ash, but it has been completely cleaned in 2011 and remains so in 2013.

To the south of the Burn Pit are two large pieces of black liner material laying on the tundra. These should be picked up to prevent vegetation die-back and permafrost degradation.

Recommendations

- Remove the two large pieces of black liner material from the tundra.

3.2.6 Ore Stockpiles

A large number of crushed Ore Stockpiles are located on the northeastern portion of the camp complex foundation pad (Figure 18). This ore comes from the 27,000 ton bulk sampling program carried out between 1996 and 1997. These stockpiles are individual un-compacted end-dump piles. Surface water drainage from this part of the foundation pile is not specifically separated from the rest of the foundation fill pad, and is not contained, but allowed to flow directly onto the tundra.

The 2007 inspection report recommended that HBML compile a detailed database of all the seep sampling tests carried out over the life of the facility and have that data reviewed by an appropriately qualified professional with the specific objective of determining whether there is any poor quality seepage emanating from the exposed ore stockpiles. HBML contracted a geochemical specialist within SRK to complete an inspection and sampling program to assess the geochemical performance of historic waste rock and ore at Boston. The objectives of this work were twofold: (1) to fulfill the conditions of Water License No. 2BB-BOS0712 Part E, Item 8 and, (2) to assess the geochemical performance of the weathered materials as a part of the geochemical characterization currently in progress to support future permitting activities.

The program included sampling of waste rock and ore from the Ore Stockpiles, roads and airstrip, as well as a seep survey around the perimeter of the Camp Complex Foundation Pad. This work was done in July 2008. Testing of the waste rock included field contact tests, acid-base accounting, metal analyses and leach extraction tests. There is also historical seepage available for this area that was analyzed as part of this program. The results of this study were presented in a technical report (SRK 2009b) which was submitted to the Nunavut Water Board in 2009.

SRK also completed a water and ore/waste rock management plan for the Boston site, based on the results of the geochemical assessment (SRK 2009d). This plan was also submitted to the Nunavut Water Board in 2009 and stipulates appropriate management protocols for this material. Annual seep surveys have continued to be collected, an updated comprehensive review of all seep survey data should be undertaken to confirm if there are any trends that contradict this ore/waste rock management plan.

Recommendations

- The procedures, protocols and monitoring plan stipulated in the 2009 water and ore/ waste rock management plan for the Boston site (SRK 2009d) should be implemented.
- A comprehensive review of the annual seep survey data since 2008 should be completed to confirm if any trends are present that contradict the 2009 management plan.

3.2.7 Containment Pond

One lined Containment Pond (Figure 17) has been constructed along the eastern perimeter of the camp foundation pad (immediately north of the Burn Pit). As-built records for the construction of this pond are not available. It is understood that this pond was used to contain wash water during the screening and crushing of ore as part of the bulk sampling program.

The pond was in poor shape in 2007; however, substantial repairs were carried out on the liner in 2008 (SRK 2009a). The condition of the pond during the 2010 inspection showed signs of deterioration, most notably due to the liner no longer being supported at the crest by sand bags, probably as a result of strong winds. This situation has worsened based on the 2011 inspection and continues to do so based on the 2013 inspection. As in previous years the pond was shown to contain various amounts of gravel (crushed ore) and wood debris which could compromise the liner integrity.

Up until 2010, the Containment Pond was used as an emergency holding pond for possible fuel spills, disposal of water from fuel containment berms, or when the sewage treatment plant experienced upset conditions. SRK was of the opinion that, if this pond is to be used for anything where there would be solids collected in the pond, its design would make it extremely difficult to remove these solids to retain pond capacity due to its depth and the fact that the liner is not protected. Furthermore, since the pond does not have a designed overflow facility (i.e., spillway), it would experience uncontrolled overflow when its capacity was exceeded. TMAC confirmed that an overflow was not required as the management practice was to pump out snowmelt and rainwater as required, after testing for contaminants.

The Containment Pond has no instrumentation of any nature and, as such, nothing can be said about its historic performance. A reconnaissance survey of the pond did identify a clear zone of water seeping from the downstream toe of the pond embankment. Although it could not be definitively confirmed that this seepage was emanating from the pond, there were no other likely sources. During the 2011 inspection, the pond was half full, which provided an opportunity to check for leaks but none were immediately apparent. During the 2012 inspection, the pond was near empty and no leaks were apparent. During the 2013 inspection, the pond did contain some water and there was a zone of water seeping from the downstream toe of the pond embankment.

Regular water samples are collected from this location and a roll of coconut matting has been placed across the flow path in attempts to reduce erosion.

Should the project move out of Care & Maintenance the following recommendations should be implemented:

- Repairs to the liner in the Containment Pond must be carried out. This includes inspecting and repairing any tears as well as re-anchoring the liner to the crest. At the same time a permanent emergency spillway must be constructed.
- Water quality sampling should be undertaken to confirm whether the seepage downstream of the Containment Pond is in fact coming from the Containment Pond. If the flow is confirmed as seepage, an appropriate mitigation plan must be implemented to have the liner repaired.
- The debris in the Containment Pond should be cleared out as it poses a potential puncture risk to the liner.
- A management plan must be implemented to ensure debris can be removed without damaging the liner.
- If the Containment Pond is to be used to retain water for any length of time, a suitable leak detection monitoring system should be implemented. As a minimum, a protocol involving frequent visual inspections would have to be put in place for the Containment Pond. Excessive and prolonged leaking will lead to permafrost degradation, which in turn will result in differential settlement that may cause the liner in the Containment Pond to fail.
- The Containment Pond should have a suitable barricade around it to prevent human and animal access. Due to the current design, it would be extremely difficult to get out of the pond unassisted if a human or animal were to inadvertently enter or fall in.

Under a Care & Maintenance, these recommendations are no longer applicable.

Recommendations

- No action required.

3.2.8 Soil Containment Berm (Landfarm)

As a result of a historic fuel spill, MHL constructed a lined soil containment facility (Figure 19) within which all excavated contaminated soils have been stored (EBA 2004). SRK reviewed the as-built records for this facility (EBA 2004) and, supported by visual inspection, confirms that it consists of a bermed and lined area in which contaminated soil has been placed in a single lift of about 1 m thick.

From discussions with HML site staff, in 2007, and a review of the as-built report, it appears that the soil containment berm was designed to be used as an active hydrocarbon landfarm area. A land farming protocol was not provided in the as-built report; however, site staff confirmed that

since initial placement of the contaminated soils into the containment area, there has been no work carried out in the form of tilling or any other means of soil mixing. HBML did routinely conduct soil sampling within the confines of this facility, the results of which are reported as per the Licence conditions. Based on a review of the formal operational procedure of HBML land farming practices (MHBL 2007), and comparison with on-site sampling practices, SRK doubts whether the soil sampling results reported by HBML would be representative. The primary reason, for coming to this conclusion, is that the soil within the facility is about 1 m thick, and has never been tilled or reworked in any way, which has been confirmed by HBML staff. Furthermore, the soil sampling to date only effectively covers the upper 0.1 m of the 1 m thick soil profile.

HBML did commission a study, in 2009, to test the soils contained in the landfarm in accordance with appropriate protocols, and develop an appropriate remediation strategy for these materials. The current plan is that these hydrocarbon contaminated materials will be backhauled for off-site disposal.

The containment facility itself however appears to be intact; although it is filled to capacity and would not be able to contain more contaminated soil until some of it has been adequately treated and/or relocated.

Recommendations

- No action required.

3.2.9 Drill Cuttings and Settling Pond

Some drill cuttings have historically been disposed of in a drill cutting disposal area immediately west of the airstrip (Figure 22). It is unknown if this area was intentionally designed for the disposal of drill cuttings. If so there are no as-built records, nor could the timeframe for how long this practice has been in operation be determined. Visual inspection suggests that the drill cutting disposal area is located at a historic drill hole. Poor control of the drilling fluid resulted in permafrost degradation and the subsequent annual thaw created by a pool of standing water resulted in the pond increasing in size. At some stage, the pond started to overflow and silt-laden water started to flow overland towards Stickleback Lake. At that time, drill cuttings were placed in the pond in an attempt to stop further degradation. Geotextile was also installed to control silt flowing from the pond.

To the best of SRK's knowledge this pond was used prior to 2007; however it saw no active use between 2008 and 2011. In 2012 drill cuttings were placed in a rectangular area immediately adjacent to the airstrip which resulted in a significant portion of the ponded area being remediated. Ponded water is however still present along all edges of the remediated area. Ongoing backfilling efforts should focus on depositing drill cuttings along the upstream edge and working downstream.

As long as ponded water persists permafrost degradation will not stop, and there will remain a risk of silt laden water flowing from the pond.

Recommendations

- Remediation efforts to continue to backfill this depression in the tundra with drill cuttings should continue. Ideally this should be done from the upstream side working downstream to gradually remove any ponding water.
- When there is active placement of drill cuttings into the ponded water, best management practices must be put in place to prevent release of silt-laden water.
- Water quality sampling should be carried out to confirm that the drill cuttings are not saline.

3.3 Mine Openings

3.3.1 Portal

A bulk sampling program was completed by BHP in 1996 and 1997, at which time 27,000 tonnes of ore and 106,000 tonnes of waste rock were extracted. The ore was crushed on site, and stockpiled on a rockfill pad constructed from the waste rock. The waste rock was also used for the construction of other surface infrastructure such as the airstrip. The bulk sampling extraction was via 2,300 m of underground development (completed by Procon Mining and Tunnelling Ltd.) using a ramp that extends from ground surface at approximately 4,035 m elevation to approximately 3,850 m elevation (local mine grid). The 185 m deep ramp dimensions are approximately 5 m wide by 3.6 m high. The orientation of the ramp is generally north to south. Five cross-cuts were established, three into the B2 Zone and the remaining two into the B3 Zone.

The portal, which is located about 25 m east of the maintenance shop as illustrated in Figure 20, was collared in altered volcanic rock, all within permafrost. This was confirmed through installation of four underground thermistors (Golder 2000a, b). During extraction of the bulk sample, the portal was not heated but operated at an ambient temperature of about -10°C. The portal was operated under dry conditions with no groundwater inflow. After completion of the bulk sample collection, the portal was abandoned and sealed off with a locked gate.

The decline was reported to be dry and geotechnically sound during a site inspection by Golder. in April 2000 (Golder 2000b). According to site personnel the last operational entrance of the portal was in 2001. An attempt to enter in 2004 was aborted, reportedly due to the presence of a frost plug, likely created due to pooled water (from rainfall and snowmelt) at the portal entrance. There are also unconfirmed reports that water has run down the ramp some distance and formed an ice dam.

During the 2013 site inspection, the bulk of the portal access was flooded. It would appear as if the condition of the portal remains unchanged from the last inspection in 2012 where it was found that the portal seal, to prevent unauthorized access, was intact and the signpost that identifies the area as potentially hazardous and warning persons against entering the area without permission were badly weathered and barely legible.

The visible exposed portion of the portal roof shows signs of minor rock spalling; however, the roof appears to be essentially structurally intact. There continues to be evidence of small fragments (less than 10 cm diameter) having broken off. The most likely cause of spalling is freeze-thaw action. The roof is armoured with 10 cm wide steel banding and rock bolts.

Recommendations

- SRK recommends that TMAC replace the weathered warning notices at the portal entrance advising of the dangers associated with unauthorized access to the area.
- The rock spalling on the exposed section of the portal roof is likely a fall hazard. Persons entering the area should wear appropriate personal protective equipment; however, a site specific hazard assessment should be completed to make people aware of the dangers. Should there be a need for any individual to enter the area for reasons other than a brief inspection, consideration should be given to installing roof support, such as a small diameter wire mesh (50 mm mesh) to mitigate the fall hazard.

3.3.2 Vent Raise

There is a single vent raise located about 100 m southwest of the portal entrance. Mechanical and electrical support equipment is installed on an elevated wooden platform about 0.6 m off the tundra. The vent area and wooden platform base are sealed off with tarps and the mechanical and electrical equipment is locked in a steel shed. Overall the facility looks weathered; but there does not appear to be permafrost degradation. Site staff could not confirm when the facility was last accessed or inspected in detail.

Recommendations

- The tarps are significantly weathered and their attachment points are starting to come apart. The tarps should be replaced.
- Sign posts warning visitors of potential dangers associated with accessing the area do not exist. It is recommended that signs be erected.

3.4 Infrastructure

3.4.1 Road to Dock

The single lane road to the dock consists of 0.3 to 0.6 m thick rockfill placed directly onto the tundra (Figure 21). This single lane road also is the start of the Winter Road to Roberts Bay. Since the road runs down-gradient towards Aimaokatalok Lake, small contour berms have been constructed, redirecting surface runoff away from the roadway. Minor signs of surface water erosion are evident along the road, but this damage would be considered quite normal for a road of this nature. Likewise, minor undulations in the road suggest there may be isolated small pockets where permafrost degradation has occurred, and the active layer has consolidated. There is no thermal instrumentation or geologic data to support this observation. Considering the amount of time the road has been in operation, this deformation is likely historic; however, the undulating road could be a safety concern. Appropriate speed control should be implemented for the road.

Site staff confirmed that repairs have been conducted to the road surface if and when there were any signs of surface erosion or other significant undulations. Based on descriptions from site staff, the predominant material used for maintenance purposes is crushed ore. Maintenance, however, has never been substantial.

Recommendations

- No action required.

3.4.2 Camp Complex Foundation Pad

The Camp Complex Foundation Pad is composed of crushed rock (Figure 21), which underlies most of the site infrastructure, varies in thickness from 0.6 to 3 m according to previous records. Initially the pad was constructed to ensure north to south drainage with the pad sloping about 1% towards the north. The foundation pad was designed to prevent thaw settlement and permafrost degradation within the operating footprint of the advanced exploration camp.

There is no instrumentation installed in the Camp Complex Foundation Pad to confirm the thermal regime within the original ground. Visual inspection suggests that localized settlement has occurred, as there are local low spots and evidence of significant ponded water on the surface of the Camp Complex Foundation Pad. There is no longer a constant grade to conduct drainage off the pad.

Differential settlement appears to be within areas where the Camp Complex Foundation Pad rock fill is the thinnest, although there are no as-built records to corroborate this observation. The accommodation complex does not appear to be impacted structurally by this differential settlement, probably since these structures can be levelled by simply adding more blocking as required. It is not known how much levelling of the camp has occurred over the years. The only significant consequence of the differential settlement is the localized ponding of water. This ponding is likely an inconvenience in day-to-day camp life, but more importantly, it acts as a new heat source which further increases the active layer depth leading to more differential settlement.

There is one large erosion gully located southwest of the Camp Complex Foundation Pad (Figure 21). This gully has been repaired by infilling with fine crush material, from the Ore Stockpiles. Whilst this appears to have been successful in preventing further erosion and permafrost degradation, this material may contribute towards poor quality leachate. This should be evaluated as part of the approved Water and Ore/Waste Rock Management Plan (SRK 2009d). Other than this gully, there are no visual signs of concentrated flows from this pad, and there is no evidence of any erosion gullies along the edges of the Camp Complex Foundation Pad.

There was a fuel spill at one time immediately south of the camp complex. The hydrocarbon contaminated soils were excavated and placed into the landfarm (Section 3.2.8). Currently this area is poorly drained but at the time of inspection, contained no standing water.

During the 2013 inspection, several zones of water seeping from the downstream toe of the Camp Complex Foundation Pad were observed by the ore stockpiles. A review of previous year inspection photos indicates these zones are not new.

Recommendations

- No action required.

3.4.3 Road to Airstrip

The single lane roadway to the airstrip is constructed from crushed rock ranging in thickness from 0.3 to 0.6 m (Figure 22). There are local depressions along the road that are more pronounced than the immediately adjacent topography, suggesting that some permafrost degradation has occurred resulting in differential settlement. Site staff confirmed that on a few occasions minor infilling of low spots has been carried out; however, there does not appear to be a formal record of any such remediation works.

Visual inspection did not identify any signs of surface water erosion, and although there are no culverts through the road, there are no signs that the road is restricting the flow of surface water.

Recommendations

- No action required.

3.4.4 Airstrip

The airstrip (Figure 22) was constructed in the summer of 1997 by Procon Mining & Tunnelling Ltd. under contract to BHP. Boston development waste rock was used to construct the airstrip (BHP 1997).

The north-south all-weather airstrip is a rockfill structure similar to the roads and Camp Complex Foundation Pad. It appears to be generally thicker than the road, and although there is no as-built information available, visual inspection suggests that its thickness ranges between 0.6 and 1.2 m.

Historically, significant settlement along the airstrip alignment has occurred every year, and as a result frequent infilling and levelling had to be carried out over the years to ensure safe aircraft operation. When in operation, the airstrip has been inspected annually by the aircraft charter company for operational suitability and, if requested, maintenance is carried out as needed. The most recent levelling and maintenance activities were carried out in August 2007 by Nuna Logistics (Nuna), under the direction of SNC-Lavalin Engineers and Contractors (SLEC). Material from the crushed Ore Stockpiles was used as infill material for the repairs, and it has been confirmed that this material was used for repairs in previous years as well.

Although there is no thermal monitoring instrumentation under the airstrip, the settlement is most likely as a result of thaw settlement in the underlying permafrost.

There are no signs of surface erosion on the airstrip. The airstrip does not have any culverts to allow water flow; however, visual inspection did not identify any pre-construction flow paths that may have been obstructed by the airstrip. There is a significant number of standing ponds of water immediately adjacent to the airstrip. These ponds are permafrost degradation zones resulting from drillholes. More details about these ponds are discussed in Section 3.5.3; however, the presence of these ponds threatens the integrity of the airstrip.

There are small tension cracks along the crest of the airstrip shoulder, generally in areas where large ponds are situated. These cracks do not suggest any immediate risk.

Recommendations

- No action required.

3.4.5 Drill Road

This road leads off from the north end of the airstrip to an old drill staging area (Figure 22). It is of the same design as the other roads at this site. There are no additional issues or concerns relating to this road other than those raised previously for other roads.

Core boxes, from the old core storage areas which were located on the tundra, have been relocated and placed along at the end of the Drill Road and the staging area.

Recommendations

- No action required.

3.4.6 Core Storage Road

The Core Storage Road (Figure 22) leads off midway from the airstrip eastwards towards a rock outcrop area where core boxes were stored on the tundra. This road, which receives relatively little traffic, is of similar design to the other roads at this site. There is a 200 mm steel pipe culvert at the junction to the airstrip, apparently allowing ponded water from the large permafrost degradation area to the north to drain south towards Stickleback Lake. The pipe culvert appears to have settled to a point where its invert level is below that of the area to be drained. Subsequently the culvert no longer functions and ponded water at either end of the pipe is contributing to additional permafrost degradation.

Just like the Drill Road, core boxes, that were stored on the tundra, have been relocated and placed along the road alignment.

Recommendations

- Consideration should be given to removing the culvert and implementing appropriate remedial measures to the areas of permafrost degradation. This should not be done without developing a comprehensive permafrost degradation mitigation plan for the site, as there are many ponded areas that may have to be interconnected to resolve the problem in the long term (see also Section 3.5.3).

3.4.7 Wooden Walkway to Boat Dock

A wooden walkway leading from the southern end of the airstrip to a boat dock in Stickleback Lake (Figure 22) had been constructed as a floating walkway directly on the tundra. The walkway had settled into the tundra hummocks and although there is no lasting permafrost damage at this time, vegetation die back has occurred, which may result in the start of an erosion gully leading to permafrost degradation.

In 2012, the boat dock and walkway had been completely removed. During the 2013 inspection there was little evidence the wooden walkway to the boat dock existed.

Recommendations

- No action required.

3.4.8 Radio Tower and Shack

The original Radio Tower was installed southeast of the vent raise in 2009 (Figures 4 and 20). The Radio Tower was designed and installed by SLEC and was supported by a concrete foundation embedded into bedrock with three wire anchors also embedded into bedrock. The Radio Tower equipment was installed in an un-insulated wooden shack immediately adjacent to the Radio Tower. The shack is on a timber foundation of levelling blocks directly on an outcrop area.

In 2011, a new Radio Tower location was permitted further to the south but construction was never completed. In 2012, inspection the original Radio Tower had been disconnected from the wooden shack and was lying on the tundra. During the 2013 inspection no changes to the dismantled Radio Tower and shack were observed.

Recommendations

- Remove the original Radio Tower from the tundra.

3.4.9 Water Intake Pump Shack

Potable water for the Boston Camp is supplied from Aimaokatalok Lake. A wooden pump shack houses the primary pump elements (Figure 4). This wooden shack is located immediately outside the ordinary high water mark on Aimaokatalok Lake, and is placed directly onto the tundra. There are no signs of permafrost damage at this time; however, vegetation die back likely has occurred immediately beneath the shack.

Recommendations

- No action required.

3.4.10 Original STP Foundation Pad

The original S-40 ROTORDISK® Full Steel Packaged STP is constructed on a small levelling pad of crushed ore, some distance west of the camp pad (Figure 25). The pad is generally very thin, (less than 0.5 m thick) and therefore not sufficiently thick to act as a true thermal pad. There are however no signs of permafrost damage at this time.

Recommendations

- No action required.

3.4.11 New STP Foundation Pad

In 2010, the new SaniBrane® STP was constructed northwest of the camp, and north of the original S-40 ROTORDISK® Full Steel Packaged STP (Figure 25). Originally the new STP was to be constructed on a levelled thermal pad constructed from crushed ore; however, in accordance with the approved Water and Ore/Waste Rock Management Plan (SRK 2009d), HBML changed the design. The thermal pads were however already constructed before the decision to change the foundations from thermal pads to timber blocking was made and therefore the ore had to be backhauled. One of the two constructed thermal pads was not removed. Where the thermal pad has been removed some minor damage to the tundra vegetation occurred, which could result in ongoing permafrost degradation if not monitored and repaired if and when it permafrost degradation becomes evident.

The new STP foundation consists of levelling timbers and platforms to allow circulation of cold air, which in turn will ensure integrity of the permafrost.

Recommendations

- The area where the ore pad was backhauled, and where minor damage to the tundra occurred, must be monitored to ensure no ponding of water, which would lead to increased vegetation die back and subsequent permafrost damage.

3.5 Other Areas

3.5.1 Core Storage Area(s)

Core boxes are being stored at the following locations, as illustrated in Figure 23:

- East of the airstrip, along the Core Storage Road. These core boxes were scattered around sections of exposed bedrock and occasionally directly on the tundra; however, due to the location, the permafrost overburden at these locations is likely shallow. A visual inspection, of the tundra, yields no concerns with respect to permafrost degradation with little vegetation die back. During the 2013 inspection the long term barrel tests were still located on the tundra southeast of the Core Store Road.
- West of the airstrip, at the end of the Drill Road and on the staging area. The surrounding tundra has extensive permafrost and vegetation die back damage, but this is not from storage of the core boxes (Section 3.5.4).
- On the Camp Complex Foundation Pad at various locations. There are no concerns about any of these areas.
- The core boxes stored at the two locations immediately east of Stickleback Lake have been relocated. Visual inspection yielded no concerns with respect to permafrost degradation, but vegetation die back has occurred immediately beneath the boxes.

Recommendations

- Monitor the areas where the core boxes have been removed from the tundra, and where minor damage has occurred, to ensure there is no ponding of water, which would lead to increased vegetation die back and subsequent permafrost degradation.

3.5.2 Grey Water Discharge

Grey water from the original S-40 ROTORDISK® Full Steel Packaged STP and the new SaniBrane® STP, installed in 2010, is discharged at a location immediately north of the Camp Complex Foundation Pad (Figure 24). This water ultimately flows overland towards the east arm of Aimaokatalok Lake. During the 2007 inspection it was noted that a large clearing devoid of any vegetation had developed where the water is discharged, and although there was no standing water at the time of the inspection, it was evident that at times significant ponding of water did exist. A well-developed overland channel had also formed where these ponds overflowed onto the tundra, and since the vegetation in this area no longer exists, there were signs of overland erosion.

The 2008 inspection revealed that HBML had constructed a permanent drop box for the grey water discharge. Water overflowed from this box onto an area covered with cocoa fibre matting that had been placed in the area where vegetation die back was observed in 2007. This practice has continued to date. A new management plan for the disposal of grey water was developed in 2009 for the new SaniBrane® STP (SRK 2009c).

Recommendations

- No action required.

3.5.3 Historic Drill Sites

The bulk of exploration drilling is carried out with diamond core drills, using mud and brine as drilling fluid. Much of this drilling fluid is recycled; however, there are instances where a significant amount of this fluid ends up being discharged at the drill site (or at least this has historically been the case). Along the north and eastern perimeter of the site, there are a number of locations where drilling fluid was allowed to discharge directly onto the tundra. At these locations vegetation die back has occurred, and over time has resulted in minor erosion damage. Examples of this design are illustrated in Figure 22.

A number of historic drill sites are visible from the airstrip (some of which are immediately adjacent to the airstrip). In these areas the drilling fluid has resulted in permafrost degradation and vegetation die back. This causes surface water to pond and since the natural drainage in this area is poor, the ponded water remains in place causing more permafrost degradation and vegetation die back. This process of increased permafrost degradation and vegetation die back continues to get progressively worse over time.

Historically, water has been pumped out of any large ponds caused by permafrost degradation and vegetation die back, whenever practical. This practice was not conducted during the bird nesting season as the water is discharged onto the tundra.

Recommendations

- HBML initiated remediation measures to address some of the erosion gully's formed by drilling fluid using cocoa matting and re-vegetation. This program appears to be successful at controlling erosion and although vegetation re-growth appears slow, it is likely to occur. TMAC should consult the services of an expert knowledgeable with tundra vegetation to implement appropriate remediation strategies.
- An action plan is needed to remediate the drill sites where significant permafrost degradation and vegetation die back has resulted in permanent ponds of standing water. This standing water is causing further permafrost degradation, which in turn increases the pond's size.

3.5.4 Orbit 25 Drill Site

An incident at an exploration drill hole located due east of the airstrip in 2011 resulted in release of a significant amount of drilling fluid which subsequently resulted in a substantial salt-burn killing the tundra vegetation (Figure 22). In addition, immediately beneath the drill permafrost

degradation occurred leaving an exposed depression with no drainage. The permanent ponding of surface water will exacerbate permafrost degradation at this location.

Following the spill HBML installed cocoa matting over the damaged tundra and consulted appropriate experts to develop a suitable remediation plan for this area.

During the 2013 inspection the area of vegetation die back has increased and has reached the east arm of Aimaokatalok Lake.

Recommendations

- Continue developing and subsequently implement an appropriate remediation plan for this site.

3.5.5 Vegetation Die Back Zones

In addition to the localized areas of vegetation die back described in Sections 3.5.2, 3.5.3, and 3.5.4, there are two large areas of vegetation die back on the property, the origin of which is not clear (Figure 22). The first is an area south of the Core Storage Road and east of the Airstrip. In this area, the vegetation has died but the underlying soils have not yet been exposed. The second area is between the Drill Road and the Airstrip. At this location the vegetation has died back and the overburden soils have been exposed and are very soft and wet.

Recommendations

- Follow the recommendations in Sections 3.5.3 and 3.5.4.

3.5.6 V-Notch Weir

A V-notch weir was installed at the outlet from Stickleback Lake in the early 1990's as part of baseline data gathering studies (Figure 23). The installation was done with the least amount of invasive techniques, by wedging in the measurement weir using tote bags filled with drill cuttings. In accordance with the Water Licence, this weir was removed during the summer of 2012. A detailed inspection of the conditions at this weir was not completed during either the 2011 or 2012 inspections; however, the 2012 flyover inspection confirmed that it had been removed and attempts made to return the stream bed profile to natural conditions. No change in ground conditions were observed in the 2013 flyover inspection.

Recommendations

- No action required.

4 Summary of Recommendations

This report provides a performance assessment of the numerous foundation pads and infrastructure at the Boston Advanced Exploration Camp. The findings are based on a site visit and walkover survey on between August 20th to 23rd, 2013 and subsequent consultation with site staff and contractors. This is the seventh formal annual geotechnical inspection undertaken at the site, and continues to show many improvements over the findings observed in previous years. HBML had completed a significant clean-up of the site which specifically targeted many of the remaining issues identified during previous geotechnical inspections prior to being taken over by TMAC.

Overall there are no immediate or significant areas of concern at the Boston Advanced Exploration Camp from a geotechnical point of view. There are also no issues that require urgent and immediate action, but there are elements that should be monitored. Table 6 below provides a summary of recommendations resulting from the geotechnical inspection completed in 2013, complete with observations listed in the 2012 annual geotechnical report (SRK 2013).

Table 6: Summary of Inspection Items and Associated Recommendations

Inspection Item	2012 Recommendations	2013 Recommendations
Thermistors	<ul style="list-style-type: none"> • Locate appropriate readout device for older thermistors and confirm functionality of strings • Consider splicing broken string • Confirm status of string in 08SBD381A • Cease quarterly monitoring, but monitor once per year in July or August 	<ul style="list-style-type: none"> • The functionality of the three intact thermistors, installed by Golder, should be confirmed. If these strings are operational, the severed string (drill hole 12259-03) should be spliced and tested as well. Any strings that are found to be functional should be included in the formal thermistor monitoring program for the site • Formal monitoring of the on-site thermistor strings should continue. This program should consist of an annual reading, if resources are available. Any data collected should be reported as part of subsequent annual geotechnical inspections
Primary Tank Farm Settlement Monitoring	<ul style="list-style-type: none"> • Cease quarterly monitoring, but monitor once per year in July or August • Recognize foundation settlement risk in spill response plan 	<ul style="list-style-type: none"> • Annual monitoring (in either July or August) of tank settlement should recommence. This data should be reviewed and reported on as part of the annual geotechnical inspection and, should there be any signs of undue movement, appropriate mitigation plans should be put in motion • The foundation settlement risk should be recognized in the spill response plan for the tank farm

Inspection Item	2012 Recommendations	2013 Recommendations
Primary Tank Farm	<ul style="list-style-type: none"> Monitor the surficial slip surfaces on the tank farm berms Continue settlement monitoring as described above 	<ul style="list-style-type: none"> The appearance of surficial slip surfaces and tension cracks on the containment berms should be monitored. Remedial measures should be implemented if the tension cracks become larger. Should excessive deformation of these berms occur (the probability of which is likely low), the tank integrity is not at risk. It is simply the effectiveness of the secondary containment that will be compromised
Power Plant Fuel Containment	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Central Pad Fuel Containment	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required. Should this fuel transfer station be used, the exposed liner should be covered to prevent exposure and/or operational damage
Jet Fuel and Lubricant Containment	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Solid Waste Disposal Site (including Burn Pit)	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> Remove the two large pieces of black liner material from the tundra
Ore Stockpiles	<ul style="list-style-type: none"> Implement the 2009 water and ore/ waste rock management plan developed for the site 	<ul style="list-style-type: none"> The procedures, protocols and monitoring plan stipulated in the 2009 water and ore/ waste rock management plan for the Boston site (SRK 2009d) should be implemented A comprehensive review of the annual seep survey data since 2008 should be done to confirm if any trends are present that contradict the 2009 management plan
Containment Pond	<ul style="list-style-type: none"> Construct suitable barrier around the pond to prevent inadvertent human and/ or animal access 	<ul style="list-style-type: none"> No action required
Soil Containment Berm (Landfarm)	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Drill Cuttings and Settling Pond	<ul style="list-style-type: none"> Continue practice of infilling depression with drill cuttings starting from the upstream end Implement best management practices to ensure silt containment 	<ul style="list-style-type: none"> Remediation efforts to continue to backfill this depression in the tundra with drill cuttings should continue. Ideally this should be done from the upstream side working downstream to gradually remove any ponding water When there is active placement of drill cuttings into the ponded water, best management practices must be put in place to prevent release of silt-laden water Water quality sampling should be carried out to confirm that the drill cuttings are not saline

Inspection Item	2012 Recommendations	2013 Recommendations
Portal	<ul style="list-style-type: none"> Replace the faded notices at the portal entrance advising of the dangers associated with unauthorized access to the area Develop site specific hazard assessment for people entering the portal area to address the rockfall hazard Consider installing a small diameter wire mesh over the exposed section of the portal roof to address the rockfall hazard 	<ul style="list-style-type: none"> SRK recommends that TMAC replace the weathered warning notices at the portal entrance advising of the dangers associated with unauthorized access to the area The rock spalling on the exposed section of the portal roof is likely a fall hazard. Persons entering the area should wear appropriate personal protective equipment; however, a site specific hazard assessment should be completed to make people aware of the dangers. Should there be a need for any individual to enter the area for reasons other than a brief inspection, consideration should be given to installing roof support, such as a small diameter wire mesh (50 mm mesh) to mitigate the fall hazard
Vent Raise	<ul style="list-style-type: none"> Replace weathered protective tarps covering the shelter erected over the vent raise Install notices at the vent raise advising of the dangers associated with unauthorized access to the area 	<ul style="list-style-type: none"> The tarps are significantly weathered and their attachment points are starting to come apart. The tarps should be replaced Sign posts warning visitors of potential dangers associated with accessing the area do not exist. It is recommended that signs be erected
Road to Dock	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Camp Complex Foundation Pad	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Road to Airstrip	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Airstrip	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Drill Road	<ul style="list-style-type: none"> Monitor the pipe culvert for progressive permafrost degradation 	<ul style="list-style-type: none"> Monitor the pipe culvert for progressive permafrost degradation
Core Storage Road	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Wooden Walkway to Boat Dock	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Radio Tower and Shack	<ul style="list-style-type: none"> Remove dismantled tower from tundra 	<ul style="list-style-type: none"> Remove the tower from the tundra
Water Intake Pump Shack	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Original STP Foundation Pad	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
New STP Foundation Pad	<ul style="list-style-type: none"> Monitor the areas where tundra vegetation damage has occurred Develop long-term re-vegetation plan; involve a tundra vegetation expert 	<ul style="list-style-type: none"> The area where the ore pad was backhauled, and where minor damage to the tundra occurred, must be monitored to ensure no ponding of water, which would lead to increased vegetation die back and subsequent permafrost damage

Inspection Item	2012 Recommendations	2013 Recommendations
Core Storage Area(s)	<ul style="list-style-type: none"> Monitor the areas where tundra vegetation damage has occurred Develop long-term re-vegetation plan; involve a tundra vegetation expert 	<ul style="list-style-type: none"> Monitor the areas where the core boxes have been removed from the tundra, and where minor damage has occurred, to ensure there is no ponding of water, which would lead to increased vegetation die back and subsequent permafrost degradation
Grey Water Discharge	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required
Historic Drill Sites	<ul style="list-style-type: none"> Develop remediation strategy to prevent further permafrost degradation 	<ul style="list-style-type: none"> HBML initiated remediation measures to address some of the erosion gulley's formed by drilling fluid using cocoa matting and re-vegetation. This program appears to be successful at controlling erosion and although vegetation re-growth appears slow, it is likely to occur. TMAC should consult the services of an expert knowledgeable with tundra vegetation to implement appropriate remediation strategies An action plan is needed to remediate the drill sites where significant permafrost degradation and vegetation die back has resulted in permanent ponds of standing water. This standing water is causing further permafrost degradation, which in turn increases the pond's size
Orbit 25 Drill Site	<ul style="list-style-type: none"> Continue developing and subsequently implement an appropriate remediation plan for remediation of this site 	<ul style="list-style-type: none"> Continue developing and subsequently implement an appropriate remediation plan for this site
Vegetation Die Back Zones	<ul style="list-style-type: none"> Initiate study to determine why die back continues; involve a tundra vegetation expert Develop remediation strategy to prevent further die back and permafrost degradation 	<ul style="list-style-type: none"> Follow the recommendations in Sections 3.5.3 and 3.5.4
V-Notch Weir	<ul style="list-style-type: none"> No action required 	<ul style="list-style-type: none"> No action required

This report, **“2013 Annual Geotechnical Inspection, Boston Advanced Exploration Project, Hope Bay, Nunavut”**, was prepared by

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All data used as source material plus the text, tables, figures, and attachments of this document have been reviewed and prepared in accordance with generally accepted professional engineering and environmental practices.

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“This report and the opinions and conclusions contained herein (“Report”) contains the expression of the professional opinion of SRK Consulting (Canada) Inc. (“SRK”) as to the matters set out herein, subject to the terms and conditions of the agreement dated [HBML.BOC-CM.PSA.003, September 30, 2008] (the “Agreement”) between Consultant and Hope Bay Mining Ltd., as assigned to TMAC Resources Inc. (“TMAC”), the methodology, procedures and sampling techniques used, SRK’s assumptions, and the circumstances and constraints under which Services under the Agreement were performed by SRK. This Report is written solely for the purpose stated in the Agreement, and for the sole and exclusive benefit of TMAC, whose remedies are limited to those set out in the Agreement. This Report is meant to be read as a whole, and sections or parts thereof should thus not be read or relied upon out of context. In addition, this report is based in part on information not within the control of SRK. Accordingly, use of such report shall be at the user’s sole risk. Such use by users other than TMAC and its corporate affiliates shall constitute a release and agreement to defend and indemnify SRK from and against any liability (including but not limited to liability for special, indirect or consequential damages) in connection with such use. Such release from and indemnification against liability shall apply in contract, tort (including negligence of SRK whether active, passive, joint or concurrent), strict liability, or other theory of legal liability; provided, however, such release, limitation and indemnity provisions shall be effective to, and only to, the maximum extent, scope or amount allowable by law.” .

5 References

- BHP Minerals Canada Ltd. 1997. *1997 Report on the Construction of the Boston Camp Airstrip. Internal Report*, December 17.
- EBA Engineering Consultants Ltd. 1996. *Boston Gold Project, Surficial Geology and Permafrost Features*. Report prepared for Rescan Environmental Services Ltd., Report No. 0101-96-12259. December.
- EBA Engineering Consultants Ltd. 1997. *Boston Gold Project, Tailings Disposal Evaluation - DRAFT*. Report prepared for BHP World Minerals, Report No. 0101-96-12259.006. December.
- EBA Engineering Consultants Ltd. 2004. *Hydrocarbon Spill Assessment and Remediation, Boston Camp, Nunavut*. Report Submitted to Miramar Mining Corporation. Project Number 1740065. February.
- Golder Associates Ltd. 2000a. *Data Review – Hope Bay Project*. Letter Report to Miramar Mining Corporation, ref. No. 002-1446. May 24.
- Golder Associates Ltd. 2000b. *Site Visit – Hope Bay Project*. Letter Report to Miramar Mining Corporation, ref. No. 002-1446. May 24. Miramar Hope Bay Limited. 2007a. *Landfarm Management Plan, Doris North Project, Nunavut*. April.
- Miramar Hope Bay Limited. 2007. *Landfarm Operations & Maintenance Manual for Boston Camp Landfarm Treatment Area & Windy Lake Camp Landfarm Treatment Area*. October.
- Nunavut Water Board. 2007. *Licence Number 2BB-BOS0712*. Water Licence issued to Miramar Hope Bay Limited. July 6.
- SRK Consulting (Canada) Inc. 2008. *2007 Annual Geotechnical Inspection, Boston Advanced Exploration Project, Hope Bay, Nunavut*. Report prepared for Miramar Hope Bay Limited, Report No. 1CM014.013, February.
- SRK Consulting (Canada) Inc. 2009a. *2008 Annual Geotechnical Inspection, Boston Advanced Exploration Project, Hope Bay, Nunavut*. Report prepared for Hope Bay Mining Limited, Report No. 1CH008.006, March.
- SRK Consulting (Canada) Inc. 2009b. *Geochemical Characterization of Historic Waste Rock and Ore Stockpiles at the Boston Deposit, Hope Bay Project, Nunavut*. Report prepared for Hope Bay Mining Limited, Report No. 1CH008.005.1700, April.
- SRK Consulting (Canada) Inc. 2009c. *Boston Advanced Exploration Project: Operation and Maintenance Manual for the Waste Water Treatment Facility, Hope Bay, Nunavut, Canada*. Report prepared for Hope Bay Mining Limited, Report No. 1CH008.008.200, April.

SRK Consulting (Canada) Inc. 2009d. *Water and Ore/Waste Rock Management Plan for the Boston Site, Hope Bay Project, Nunavut*. Report prepared for Hope Bay Mining Limited, Report No. 1CH008.022, July.

SRK Consulting (Canada) Inc. 2009e. *Hope Bay Gold Project: Stage 2 Overburden Characterization Report, Hope Bay, Nunavut, Canada*. Report prepared for Hope Bay Mining Limited, Report No. 1CH008.002, September.

SRK Consulting (Canada) Inc. 2009f. *2009 Annual Geotechnical Inspection, Boston Advanced Exploration Project, Hope Bay, Nunavut*. Report prepared for Hope Bay Mining Limited, Report No. 1CH008.021, November.

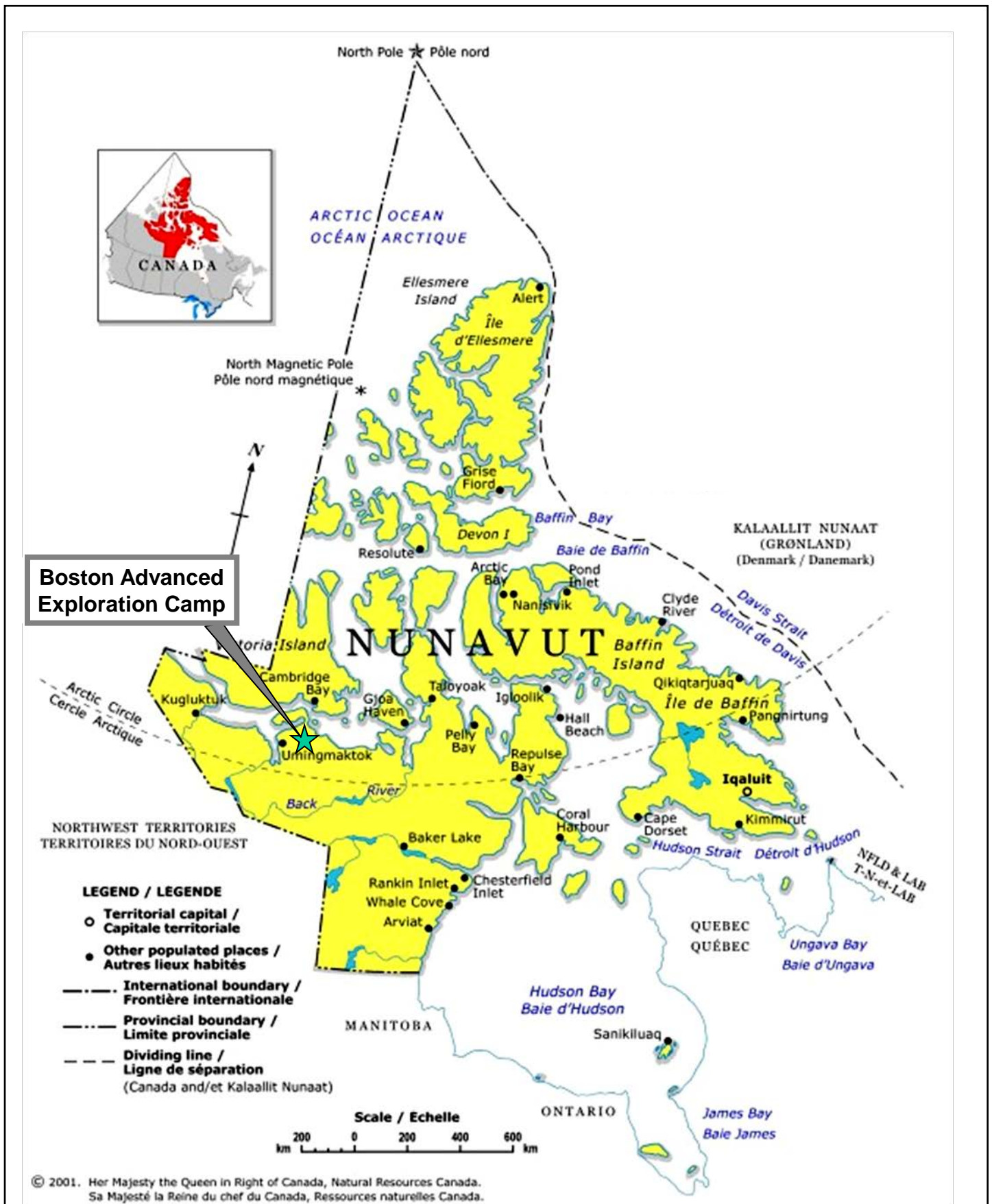
SRK Consulting (Canada) Inc. 2011a. *2010 Annual Geotechnical Inspection, Boston Advanced Exploration Project, Hope Bay, Nunavut*. Report prepared for Hope Bay Mining Limited, Report No. 1CH008.033, February.

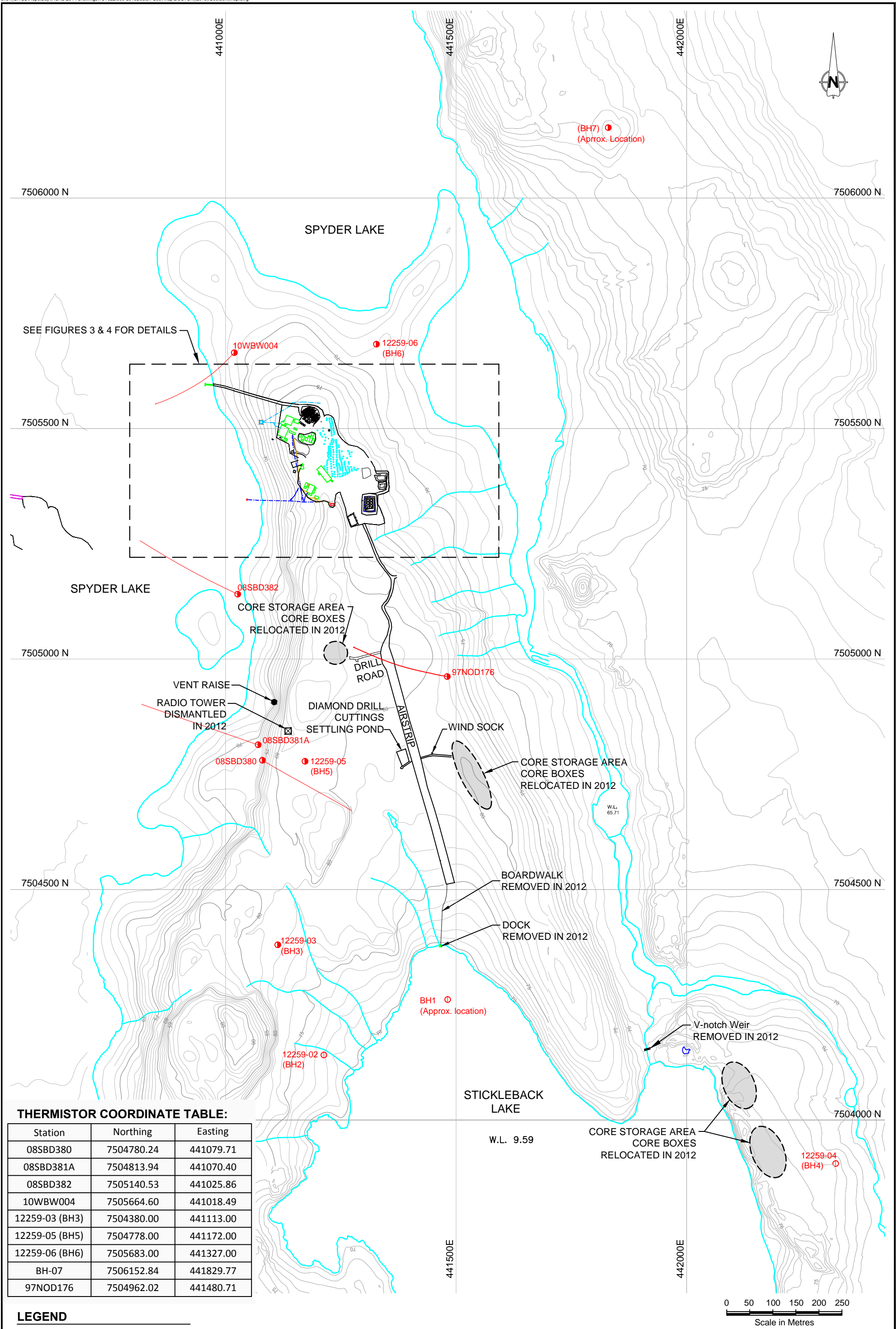
SRK Consulting (Canada) Inc. 2011b. *Hope Bay 2010 Westbay Program Data Report – Final Draft*. Report prepared for Hope Bay Mining limited, Report No. 1CH008.013, February.

SRK Consulting (Canada) Inc. 2012. *2011 Annual Geotechnical Inspection, Boston Advanced Exploration Project, Hope Bay, Nunavut*. Report prepared for Hope Bay Mining Limited, Report No. 1CH008.046, March.

SRK Consulting (Canada) Inc. 2013. *2012 Annual Geotechnical Inspection, Boston Advanced Exploration Project, Hope Bay, Nunavut*. Report prepared for Hope Bay Mining Limited, Report No. 1CH008.066, January.

Figures





THERMISTOR COORDINATE TABLE:

Station	Northing	Easting
08SBD380	7504780.24	441079.71
08SBD381A	7504813.94	441070.40
08SBD382	7505140.53	441025.86
10WBW004	7505664.60	441018.49
12259-03 (BH3)	7504380.00	441113.00
12259-05 (BH5)	7504778.00	441172.00
12259-06 (BH6)	7505683.00	441327.00
BH-07	7506152.84	441829.77
97NOD176	7504962.02	441480.71

LEGEND

- 12259-03

(BH1)

08SBD380
- Thermistor Installed

Thermistor Not Installed

Angled Holes



SRK JOB NO.: 1CT022.000
FILE NAME: BOSTON_2013_Geotech_Insp.dwg

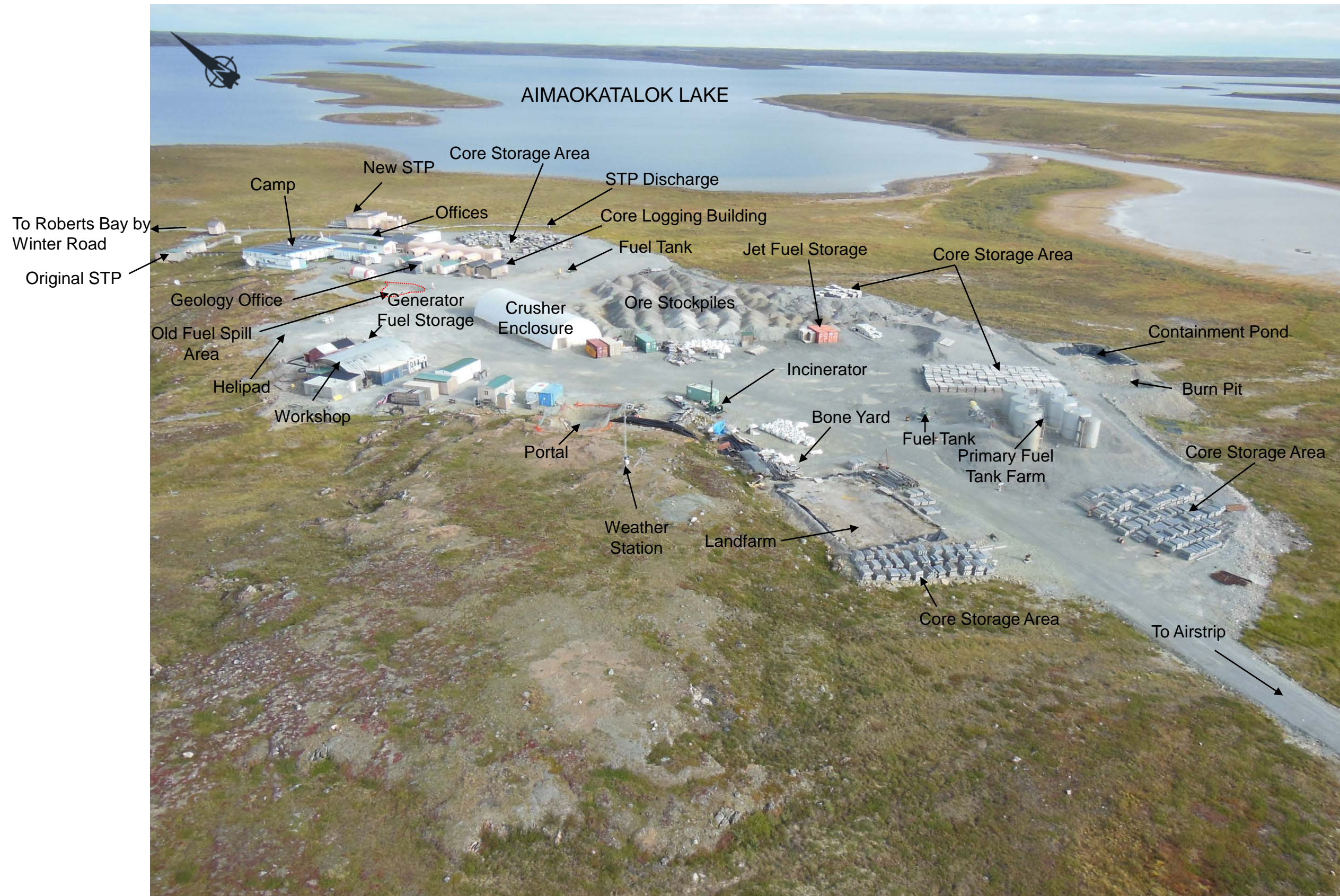


HOPE BAY MINING LTD.

2013 Geotechnical Inspection

Overall Site Layout

DATE: March 2014	APPROVED: EMR	FIGURE: 2
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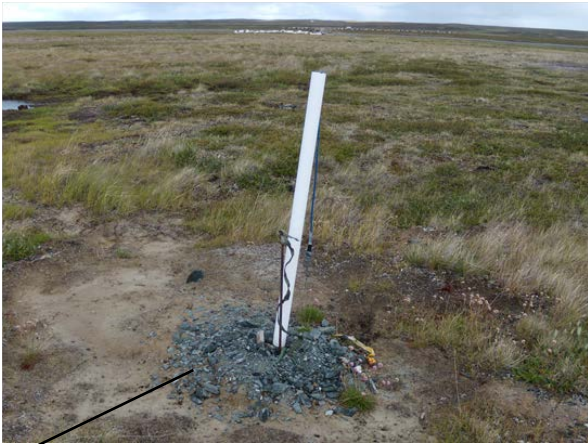
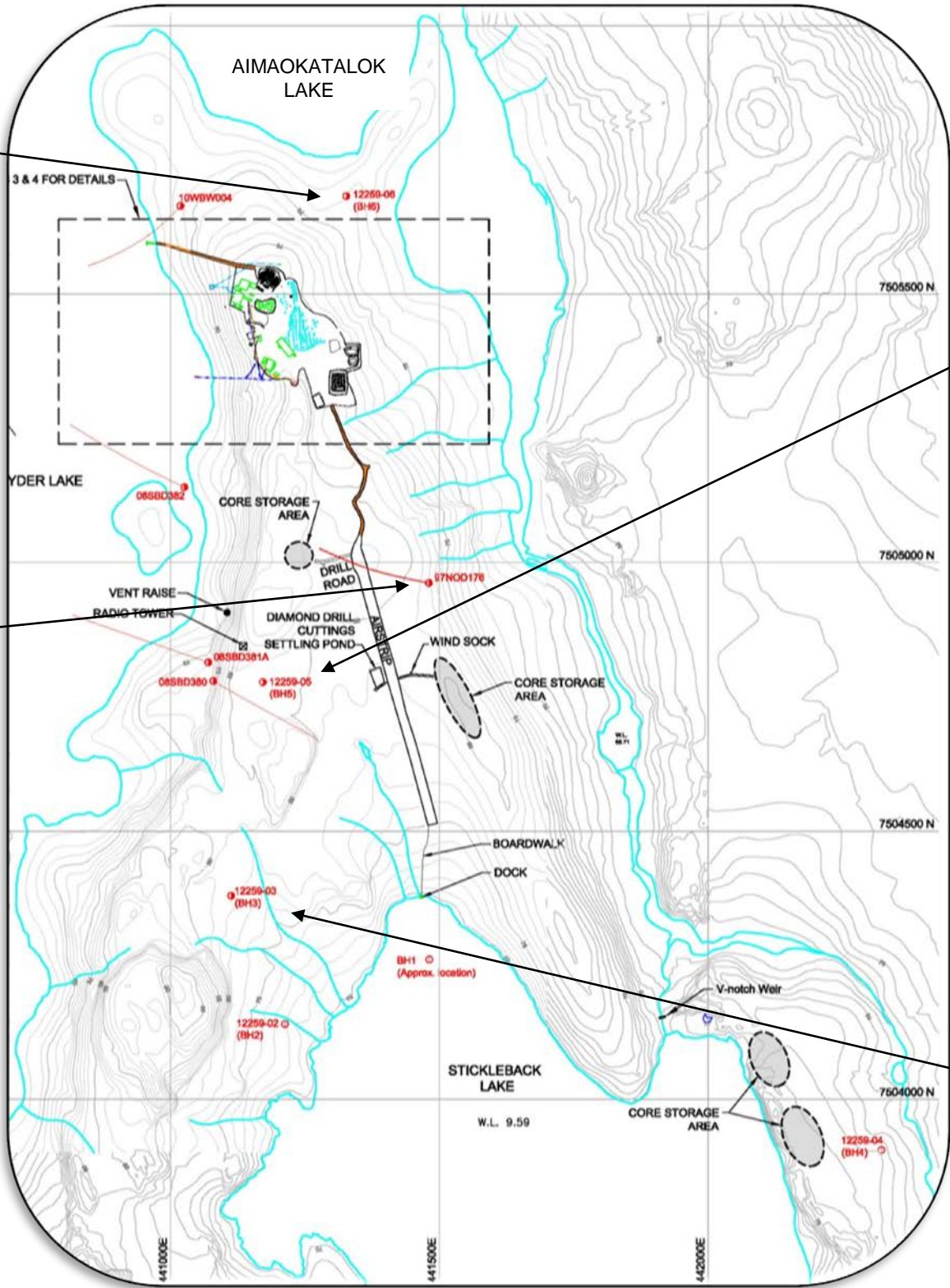
Drill hole 12259-06 (BH6) with thermistor string #1051.



Drill hole 97NOD176 with thermistor string.



Close-up of the readout box and terminal connector for the thermistor string on drill hole 97NOD176.



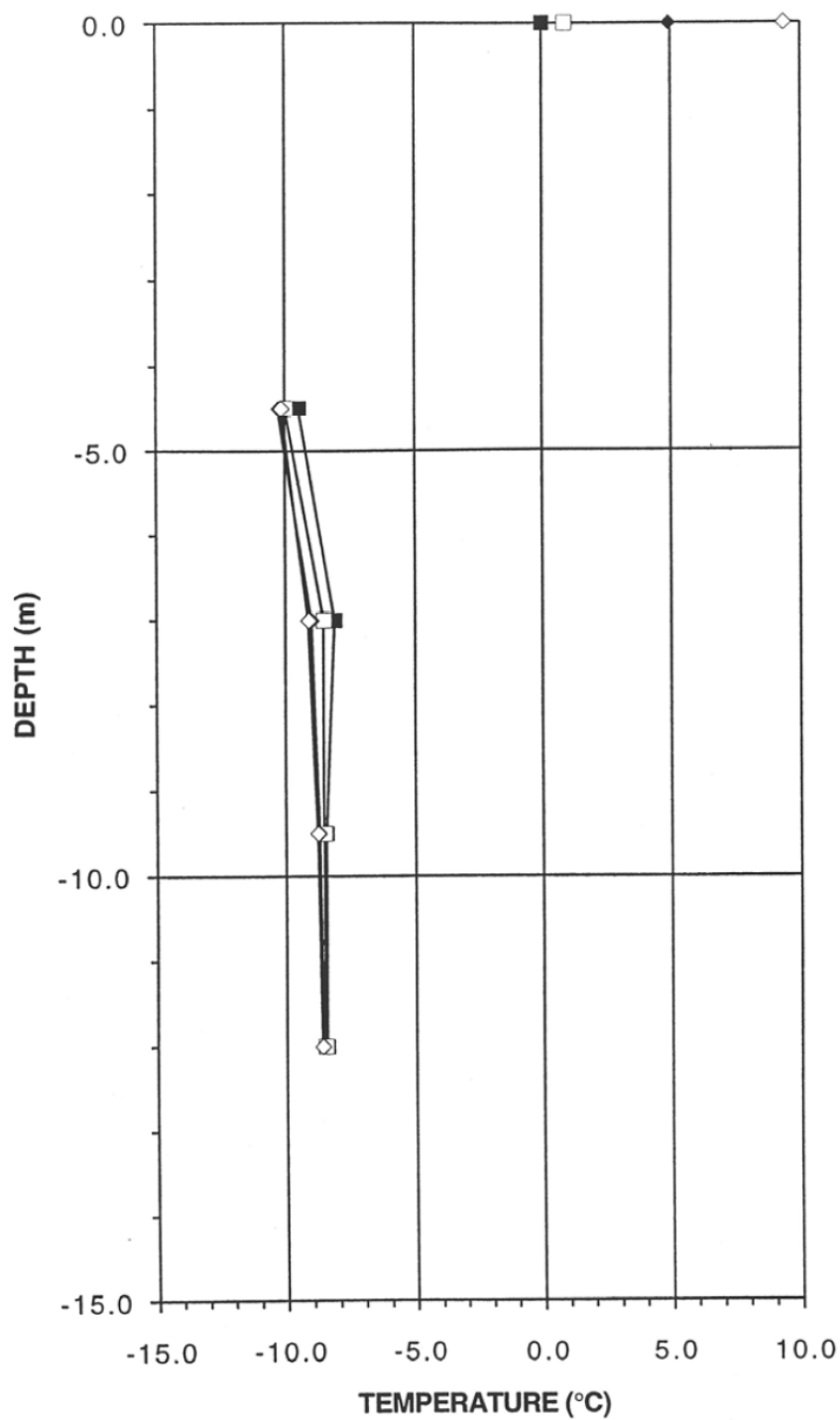
Drill hole 12259-05 (BH5) with thermistor string #1050.



Close-up of the severed cable on drill hole 12259-03 (BH3) with thermistor string #1049.



Drill hole 12259-03 (BH3) with thermistor string #1049. The cable has been severed.



Source: Boston Gold Project – Surficial Geology and Permafrost Features,
EBA Engineering 1996



2013 Geotechnical Inspection

Ground Temperature Profile EBA Drillhole 12259-03

Job No: 1CT022.000

Filename: Figure 6-9_EBA graphs_20140328.pptx

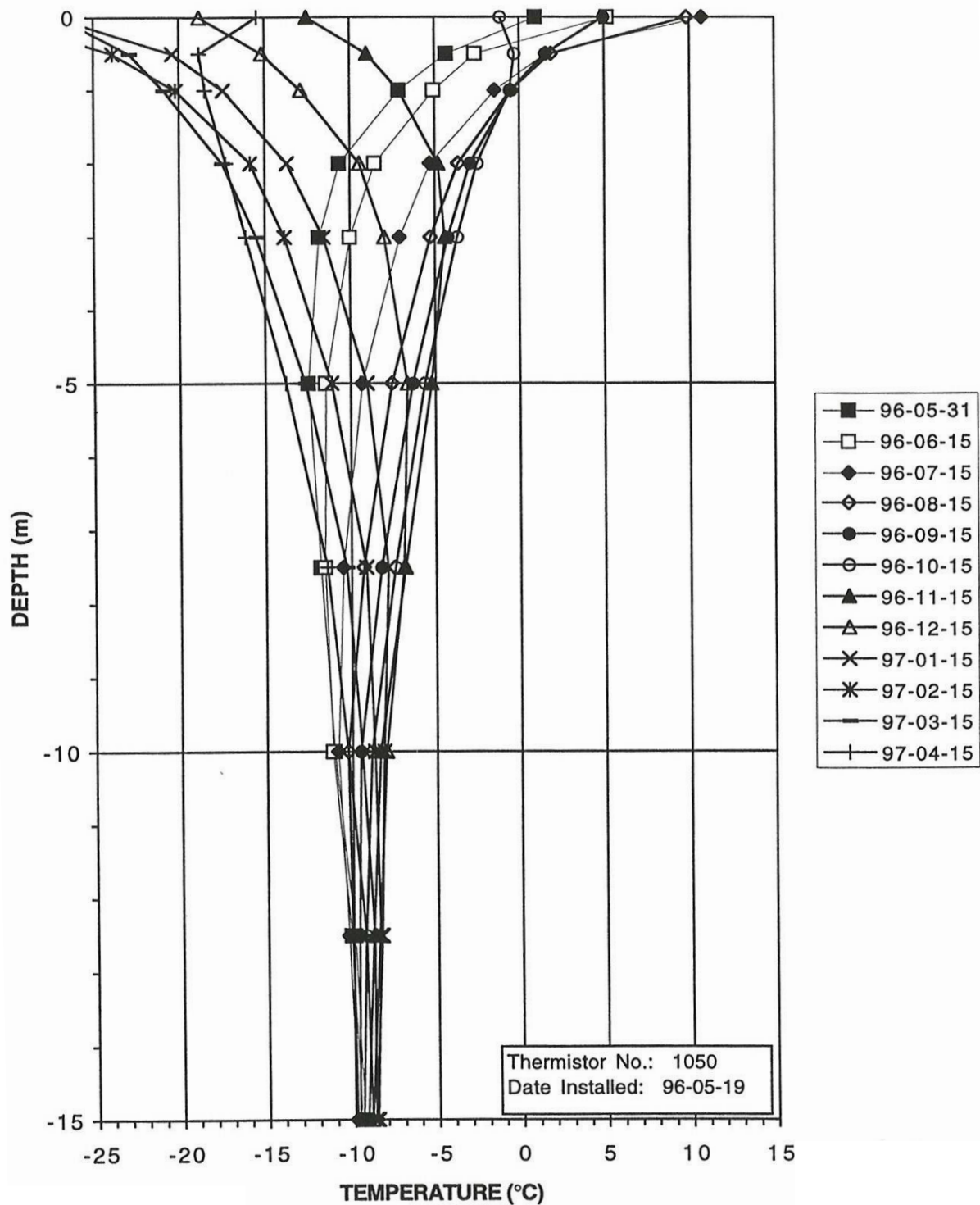
HOPE BAY MINING LTD.

Date:
March 2014

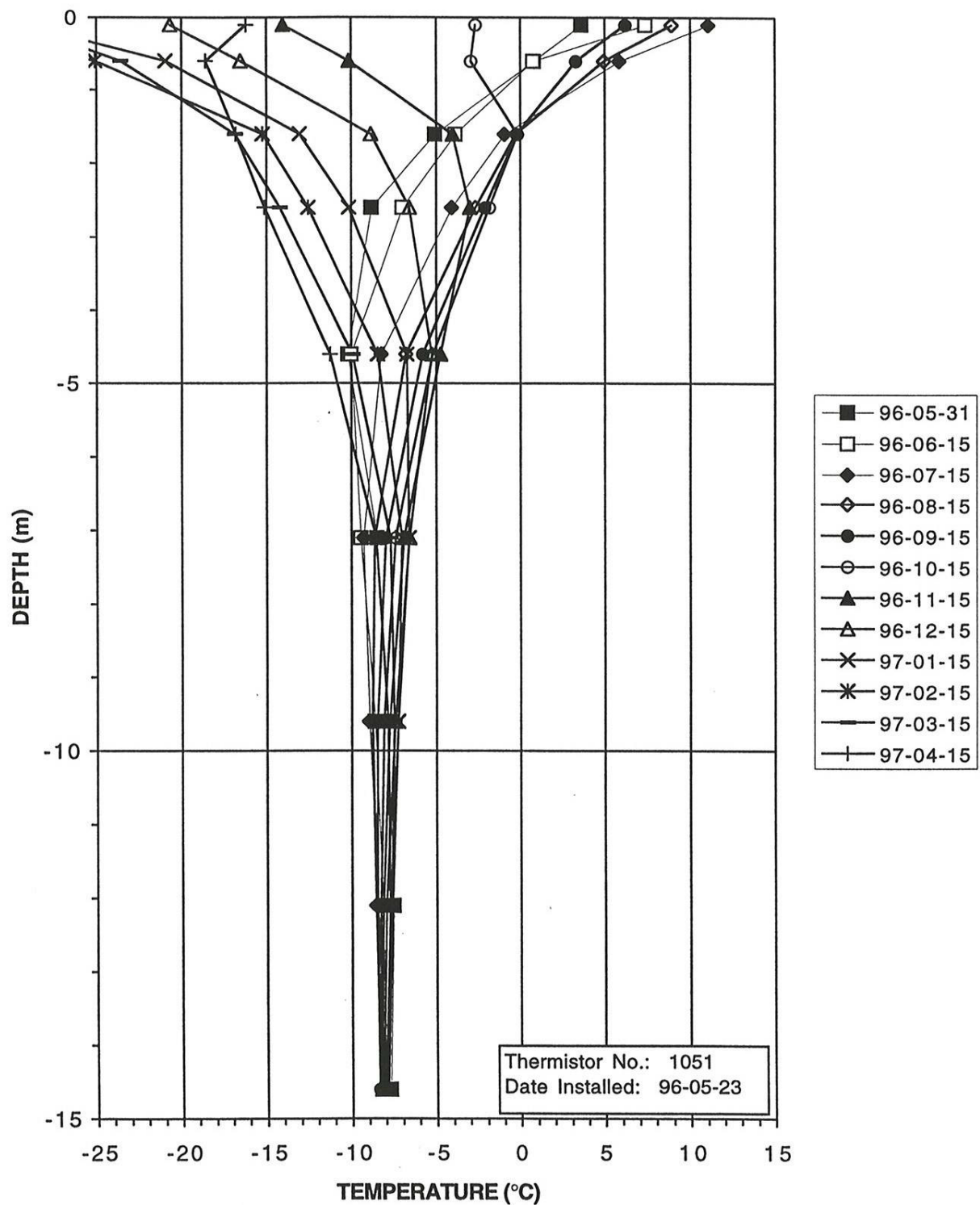
Approved:
LW

Figure:

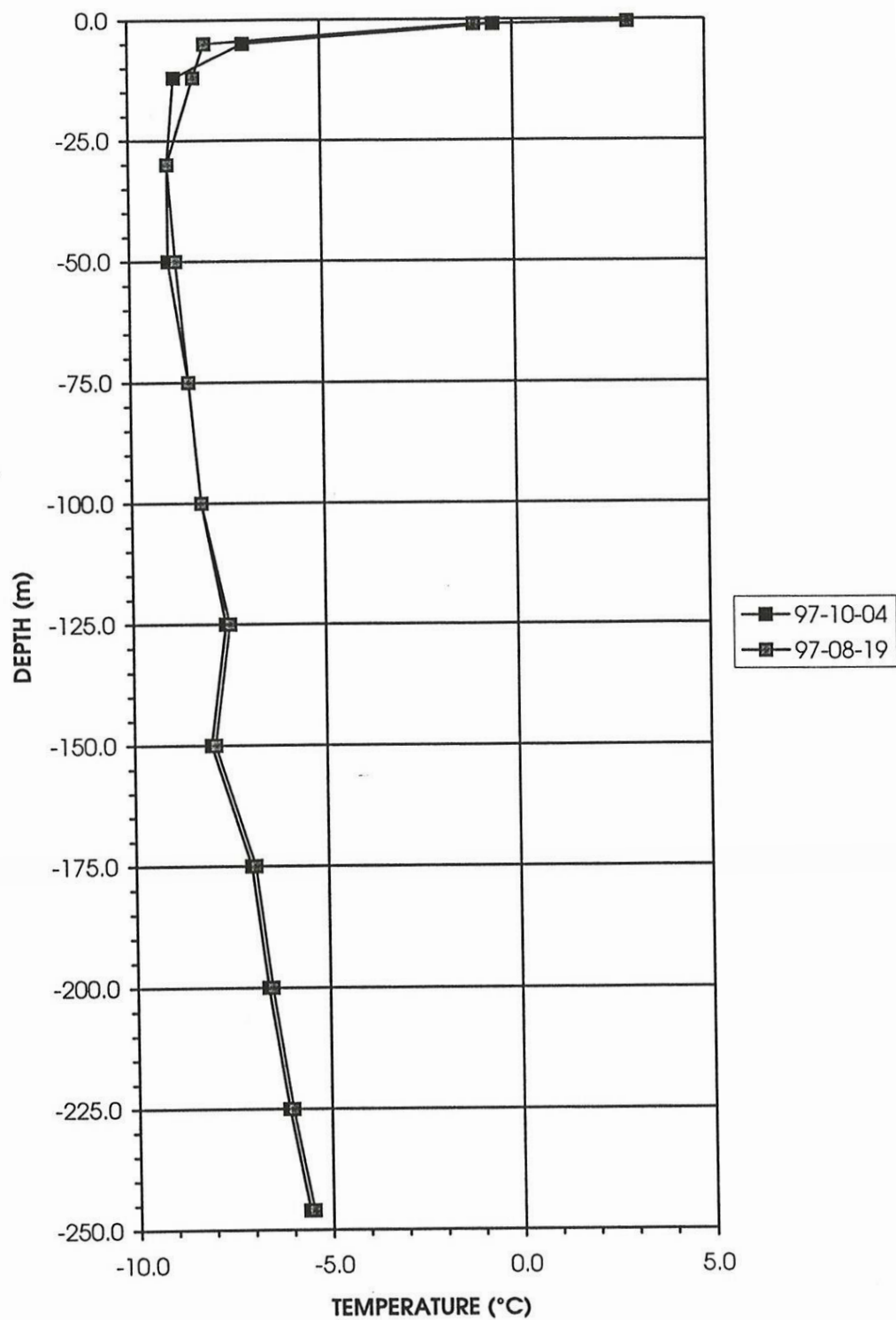
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Source: Boston Technical Reports – Environmental General,
Tailings Disposal Evaluation-Draft, EBA Engineering 1997



Source: Boston Technical Reports – Environmental General,
Tailings Disposal Evaluation-Draft, EBA Engineering 1997



Source: Boston Technical Reports – Environmental General,
Tailings Disposal Evaluation-Draft, EBA Engineering 1997



2013 Geotechnical Inspection

Ground Temperature Profile EBA Deep Drillhole (97NOD176)

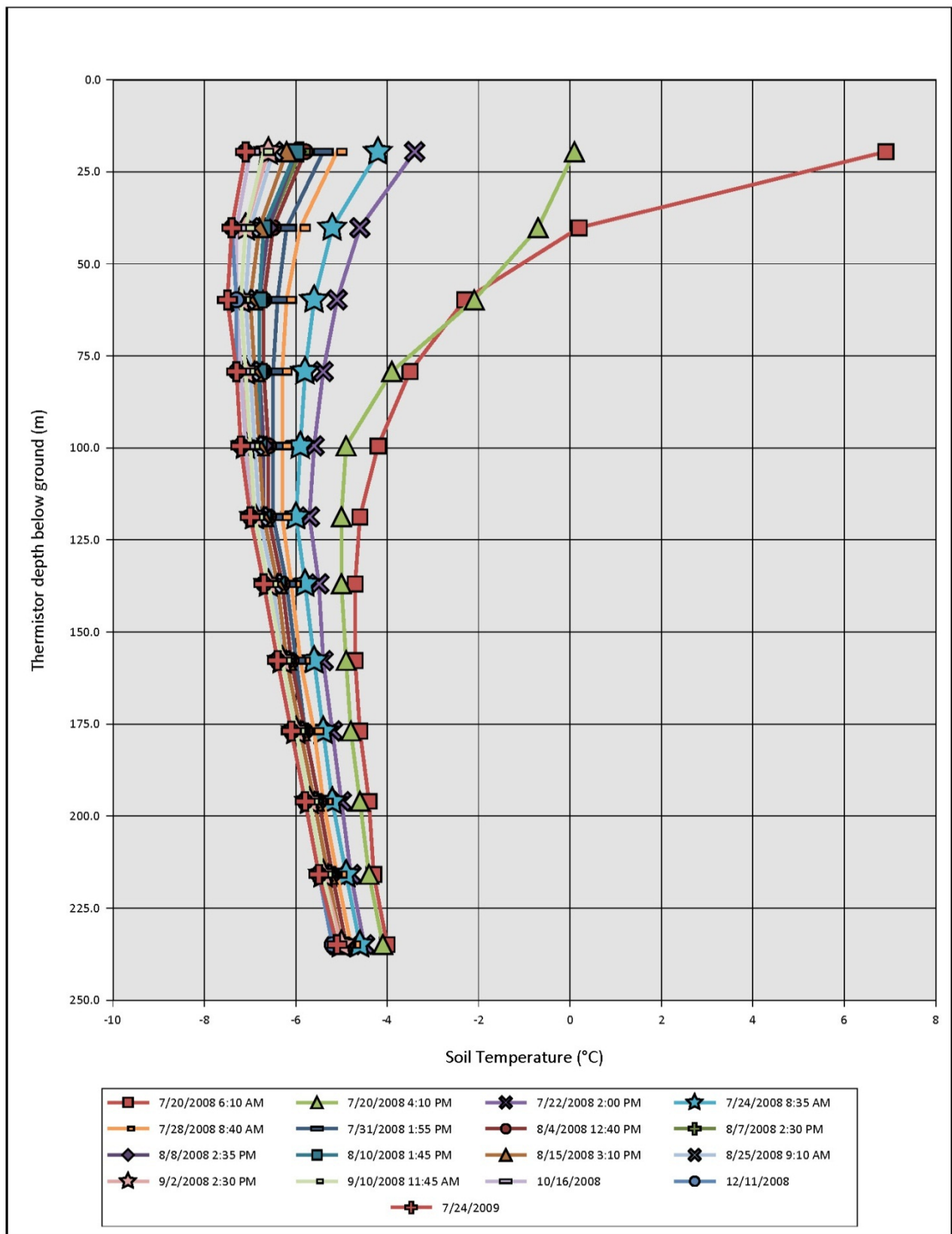
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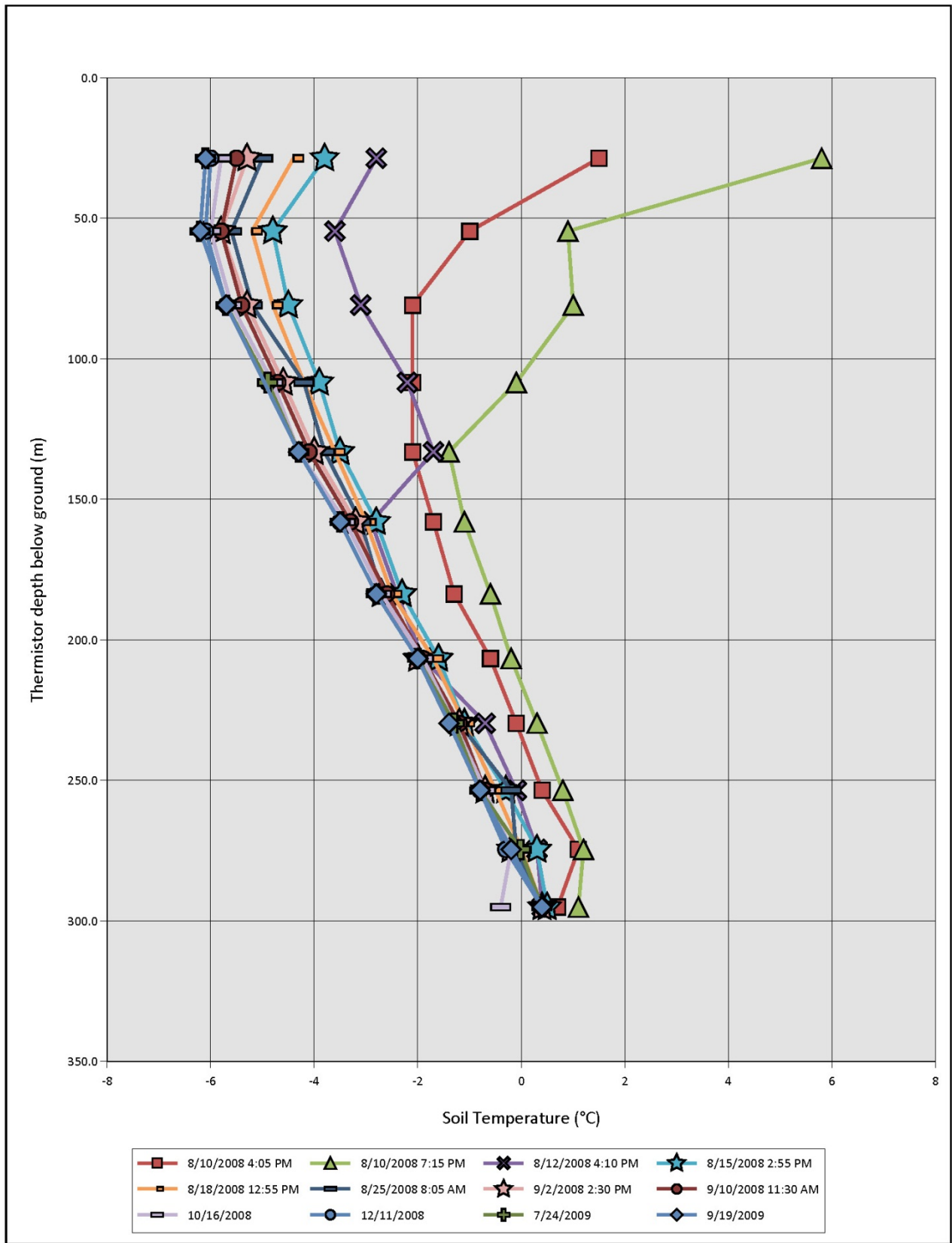
HOPE BAY MINING LTD.

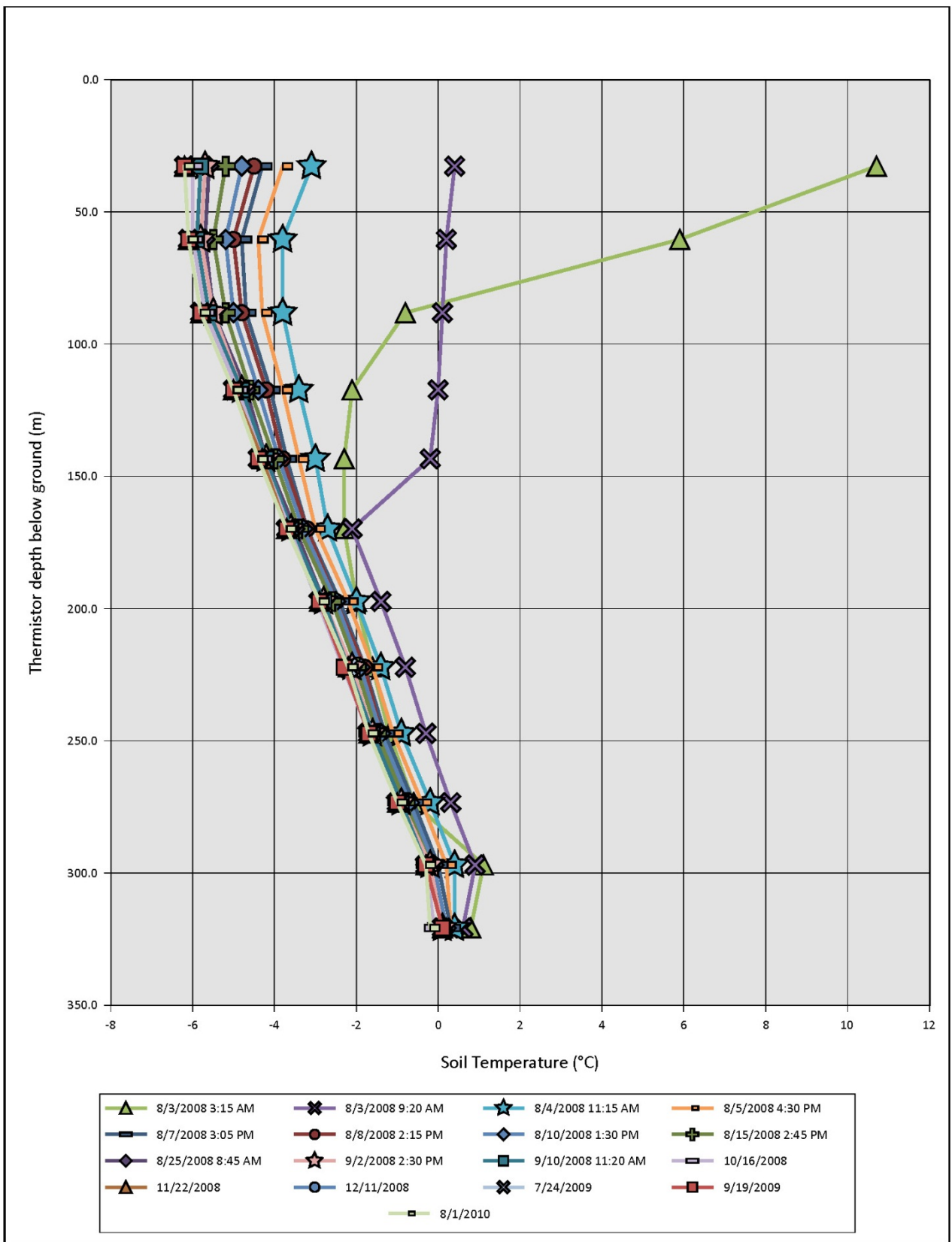
Date:
March 2014

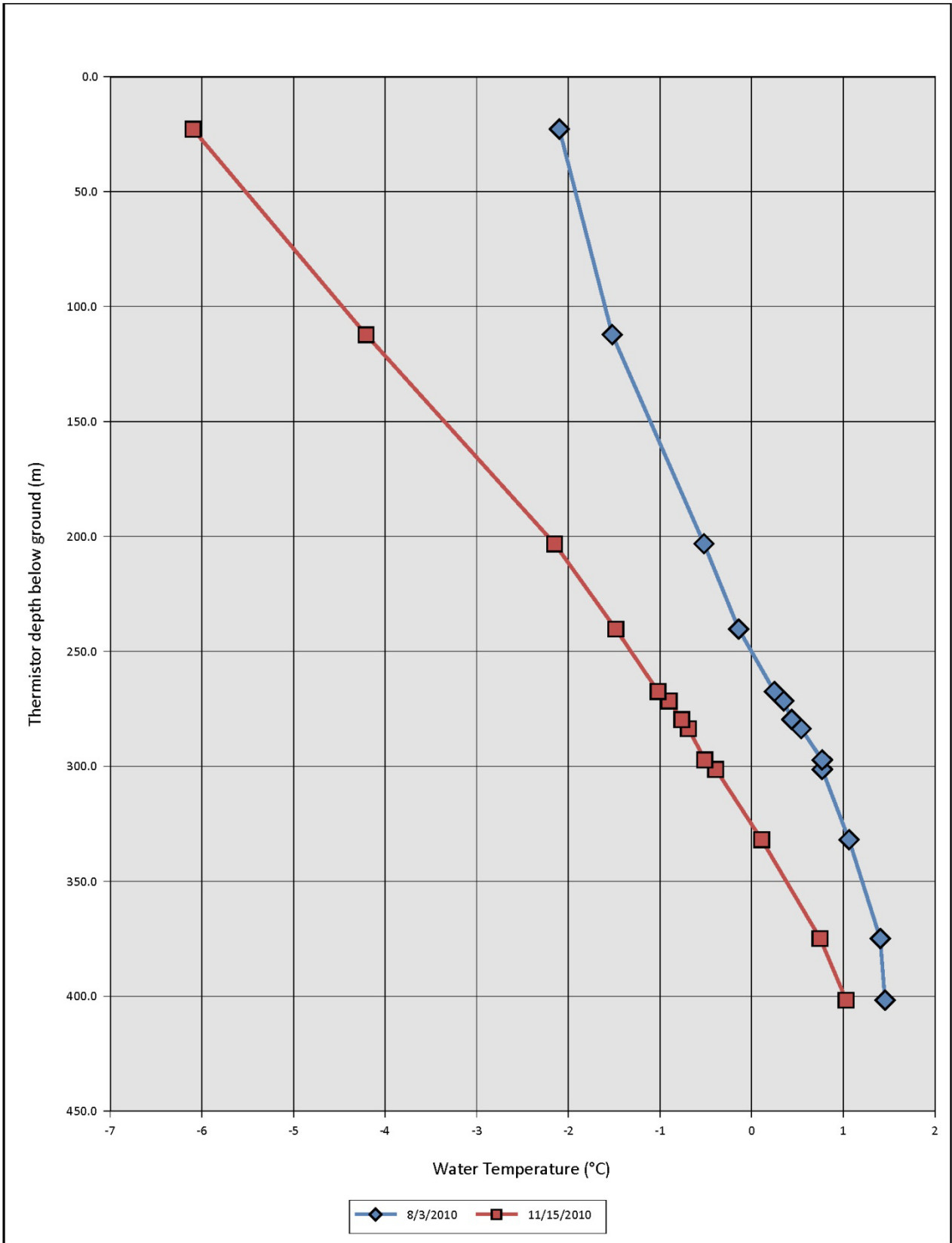
Approved:
LW

Figure:











Vehicle fueling station – looking north from across ramp



Condition of sump in north west corner of the Primary Tank Farm



A depression at the north end of the Primary Tank Farm



Vehicle fueling station and spill kit – looking southeast from north end of facility



Vehicle fueling station and access ramp – looking north from south end of Primary Tank Farm



North side of Primary Tank Farm - looking west towards the incinerator



East side of Primary Tank Farm – looking north



Generator fuel storage



Old fuel spill area



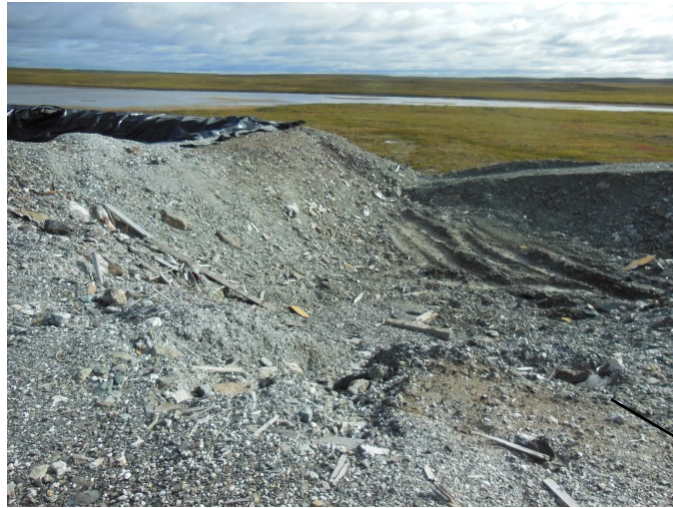
Mid pad fuel transfer station



Jet fuel stored in two sea cans



Empty fuel drums stored in the Jet Fuel and Lubricant Storage Area



Burn Pit – Looking northwest



Containment Pond - looking northwest



Containment Pond – looking southeast



Pieces of liner laying on the tundra to the south of the Burn Pit



Containment Pond – looking south



Seepage and vegetation die back along the toe of the Burn Pit

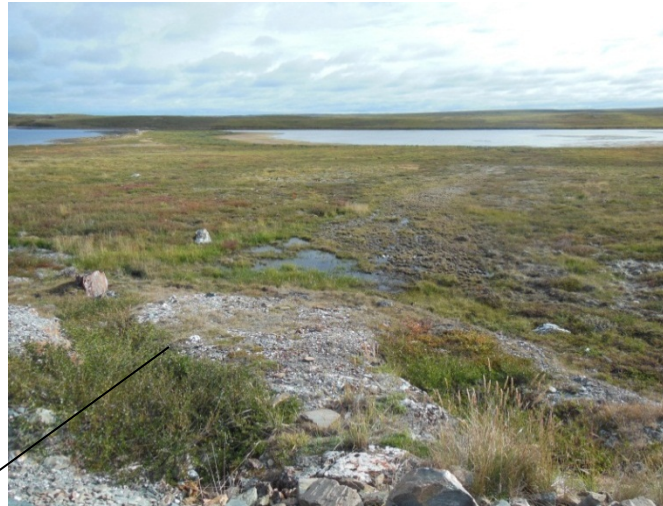


Looking southwest across the Burn Pit towards the Primary Tank Farm



Seepage and vegetation die back along the toe of the Containment Pond

		2013 Geotechnical Inspection	
		Containment Pond and Burn Pit	
Job No: 1CT022.000	HOPE BAY PROJECT	Date: March 2014	Approved: LW
Filename: Boston Geotech_Figures_1CT022.000_Rev04.pptx		Figure: 17	



Seepage and vegetation die back at the toe of the rock fill pad at north end of the Ore Stockpiles



Seepage and vegetation die back at the toe of the rock fill pad at north end of the Ore Stockpiles



Seepage and vegetation die back at the toe of the rock fill pad by the Ore Stockpiles



End of the rock fill pad beside the Ore Stockpiles – looking north



Seepage and vegetation die back at the south end of the Ore Stockpiles



Seepage and vegetation die back at the toe of the rock fill pad by the Ore Stockpiles



Job No: 1CT022.000
Filename: Boston Geotech_Figures_1CT022.000_Rev04.pptx



HOPE BAY PROJECT

2013 Geotechnical Inspection

Ore Stockpiles

Date: March 2014	Approved: LW	Figure: 18
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Aerial view overlooking the Bone Yard and Landfarm and the Incinerator - looking north



Aerial view looking down on the Landfarm, Core Box Storage, Bone Yard and Primary Tank Farm at the south end of the camp pad



Aerial view looking down on the landfarm, core box storage area and the bone yard – looking south

 Job No: 1CT022.000 Filename: Boston Geotech_Figures_1CT022.000_Rev04.pptx	 HOPE BAY PROJECT	2013 Geotechnical Inspection		
		Landfarm and Bone Yard		
		Date: March 2014	Approved: LW	Figure: 19



Aerial view of the Portal with the adjacent Incinerator, Weather Station, and Bone Yard – looking northeast



Condition of the reinforcement over the Portal entrance



Portal entrance – looking southeast





Abandoned fresh water intake pipe line and backfilled erosion gully

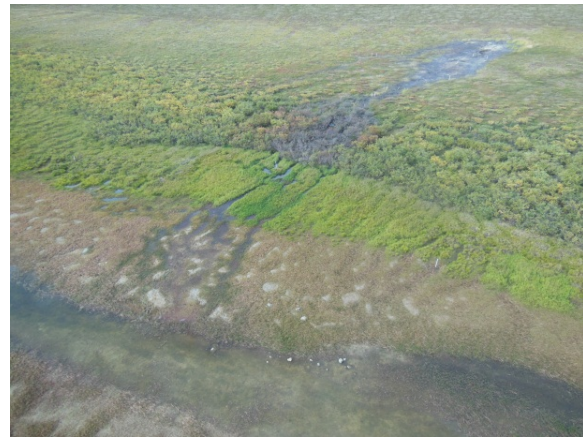


Looking northwest over Aimaokatalok Lake along the winter road access



North end of camp complex – looking south





Orbit 25 Drill Site salt-burn



Vegetation die back within the Orbit 25 Drill Site salt-burn



Permafrost degradation and ponded water along edge of the Airstrip



Aerial view of core box clean-up along Core Storage Road. Barrel tests have not been disturbed



South end of airstrip with the board walk removed



Tundra damage along east side of airstrip – looking northwest towards core boxes stored along Drill Road



Aerial view of core box clean-up along Drill Road



Drill cutting disposal area along the west side of the airstrip – looking southwest



Job No: 1CT022.000
Filename: Boston Geotech_Figures_1CT022.000_Rev04.pptx



HOPE BAY PROJECT

2013 Geotechnical Inspection

Airstrip and Vegetation Die Back Areas (including Orbit 25 Drill Site)

Date: March 2014	Approved: LW	Figure: 22
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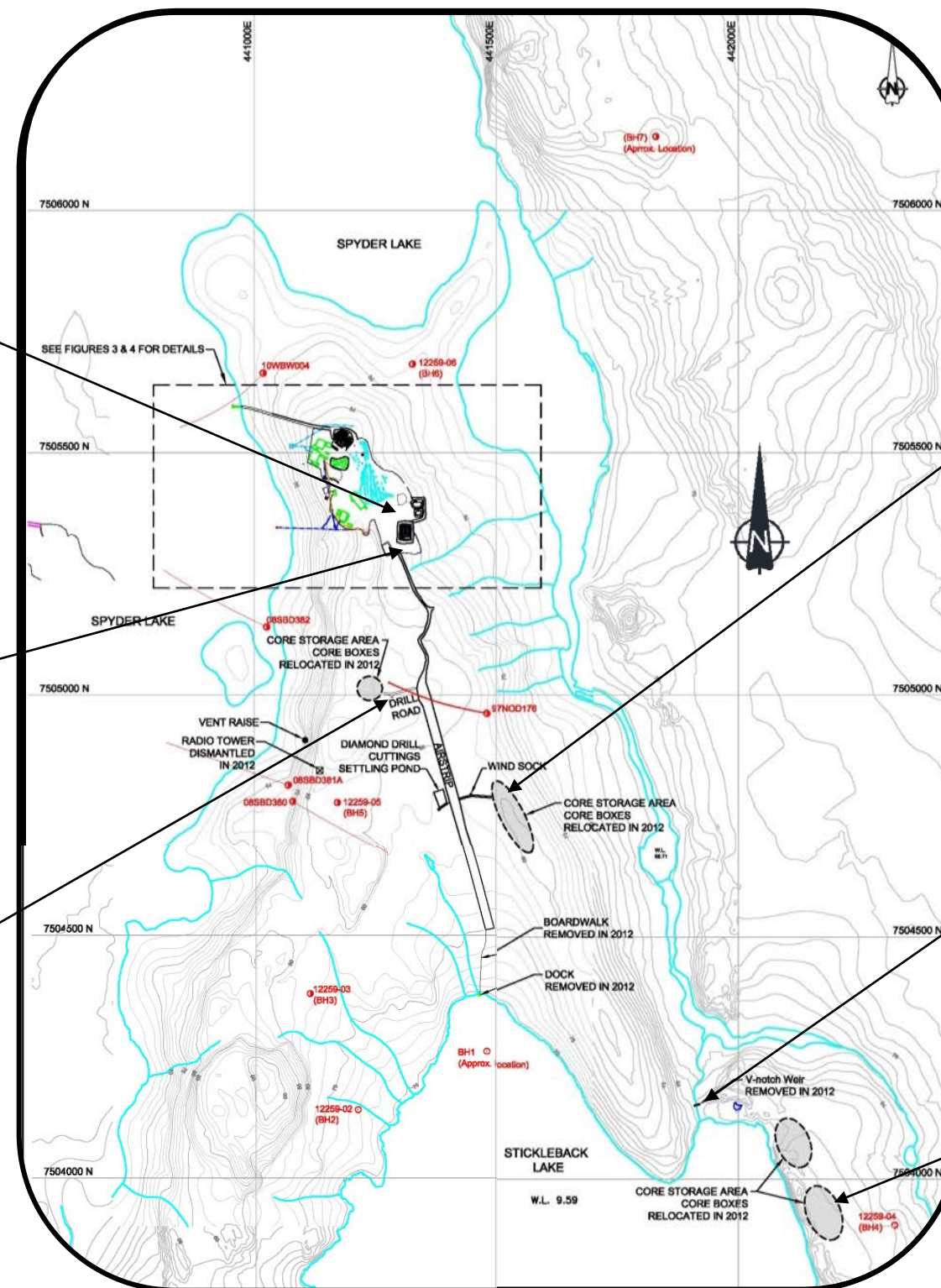
Relocated core boxes by Primary Tank Farm



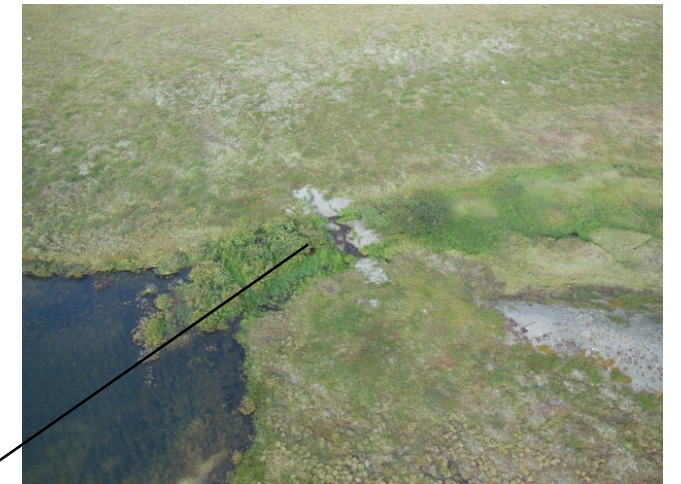
Core boxes stored at the south end of the Camp Complex Foundation Pad



Core boxes relocated onto the Drill Road.



Only the barrel tests remain at the core storage area by the Core Storage Road



V-notch weir removed in 2012



Core storage area at the original camp location



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HOPE BAY PROJECT

2013 Geotechnical Inspection

Core Storage Areas

Date: March 2014	Approved: LW	Figure: 23
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STP discharge location



East and south sides of the old STP



East side of the new STP



North and west sides of the old STP



West side of the new STP



North side of the remaining thermal Pad for new STP



South side of the remaining thermal Pad for new STP



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HOPE BAY PROJECT

2013 Geotechnical Inspection

Existing and New Sewage Treatment Plants

Date: March 2014	Approved: LW	Figure: 24
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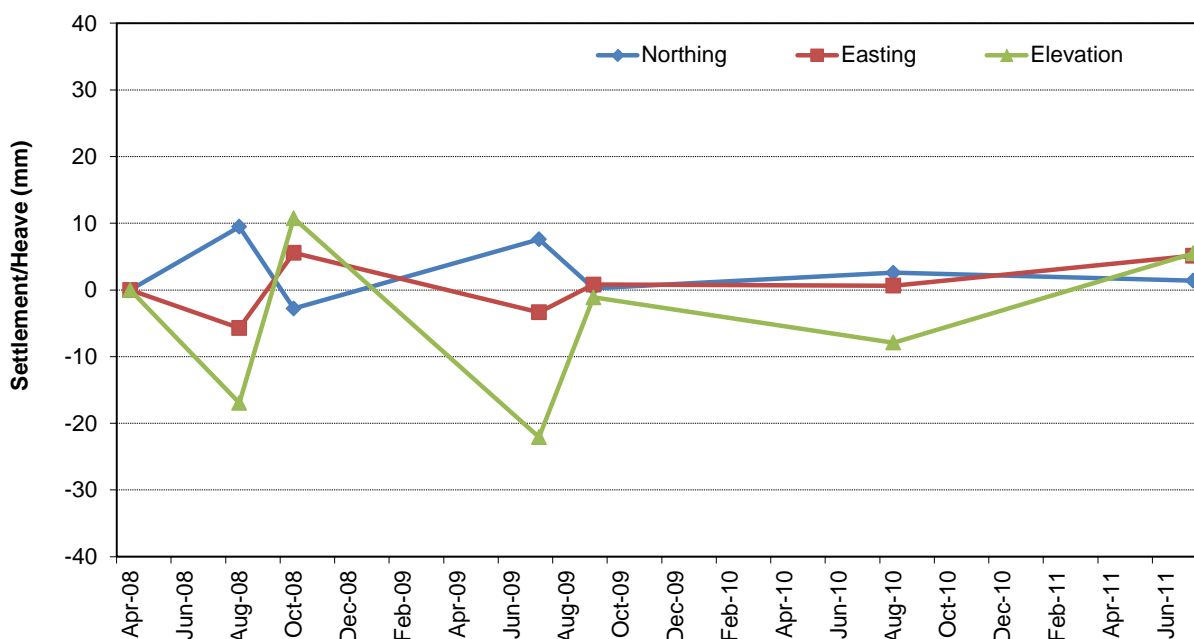
Appendix A: Boston Primary Fuel Tank Farm Settlement Monitoring

Boston Primary Fuel Tank Farm Settlement Monitoring

Tank #1

Date	Tank Mark	Horizontal Angle			Vertical Angle			Slope Dist.	HI [m]	Northing [m]	Easting [m]	Elevation [m]	Difference from Previous Survey [m]		
		Deg	Min	Sec	Deg	Min	Sec						N	E	EI
22-Apr-08	1A	176	41	38	95	24	55	7.658	1.593	5325.879	1305.901	80.674			
8-Aug-08	1A	176	36	14	94	58	28	7.651	1.519	5325.889	1305.894	80.660	0.009	-0.008	-0.015
18-Oct-08	1A	176	38	26	96	3	2	7.675	1.674	5325.890	1305.905	80.669	0.001	0.011	0.009
25-Jul-09	1A	176	34	52	95	52	11	7.671	1.633	5325.896	1305.899	80.653	0.006	-0.005	-0.016
19-Sep-09	1A	176	35	8	95	53	35	7.676	1.635	5325.898	1305.904	80.651	0.002	0.004	-0.002
2-Aug-10	1A	176	34	14	94	58	19	7.666	1.506	5325.900	1305.904	80.646	0.003	0.000	-0.005
03-Jul-11	1A	176	40	40	94	12	40	7.672	1.416	5325.895	1305.923	80.657	-0.005	0.020	0.011
22-Apr-08	1B	58	18	6	94	2	11	9.526	1.632	5326.428	1308.581	80.989			
8-Aug-08	1B	58	19	39	92	54	1	9.527	1.436	5326.439	1308.574	80.982	0.011	-0.007	-0.008
18-Oct-08	1B	58	19	8	93	54	32	9.530	1.610	5326.434	1308.579	80.988	-0.005	0.005	0.006
25-Jul-09	1B	58	20	36	94	0	48	9.538	1.610	5326.441	1308.576	80.970	0.007	-0.003	-0.018
19-Sep-09	1B	58	20	27	94	6	27	9.541	1.626	5326.442	1308.574	80.971	0.001	-0.002	0.000
2-Aug-10	1B	58	20	28	93	19	3	9.533	1.484	5326.442	1308.574	80.960	0.000	0.000	-0.010
03-Jul-11	1B	58	20	53	92	29	57	9.529	1.350	5326.445	1308.572	80.962	0.003	-0.002	0.002
22-Apr-08	1F	304	22	12	91	9	4	24.193	1.635	5328.263	1306.711	80.992			
8-Aug-08	1F	304	22	16	91	4	38	24.184	1.575	5328.271	1306.709	80.963	0.008	-0.002	-0.029
18-Oct-08	1F	304	22	16	91	11	6	24.189	1.637	5328.267	1306.710	80.980	-0.004	0.001	0.016
25-Jul-09	1F	304	22	13	91	0	29	24.178	1.530	5328.276	1306.708	80.948	0.009	-0.002	-0.032
19-Sep-09	1F	304	22	18	91	15	12	24.182	1.632	5328.274	1306.708	80.946	-0.002	0.000	-0.002
2-Aug-10	1F	304	21	53	91	2	35	24.176	1.535	5328.279	1306.710	80.938	0.005	0.002	-0.008
03-Jul-11	1F	304	22	2	91	0	43	24.169	1.525	5328.285	1306.707	80.941	0.006	-0.003	0.003

TANK AVERAGES BY DATE (mm)	22-Apr-08	0.0	0.0	0.0
	8-Aug-08	9.5	-5.7	-17.0
	18-Oct-08	-2.8	5.6	10.7
	25-Jul-09	7.6	-3.3	-22.1
	19-Sep-09	0.2	0.8	-1.1
	2-Aug-10	2.6	0.7	-7.9
	3-Jul-11	1.4	5.1	5.5
OVERALL PERIOD AVERAGE (mm)		3.1	0.5	-5.3

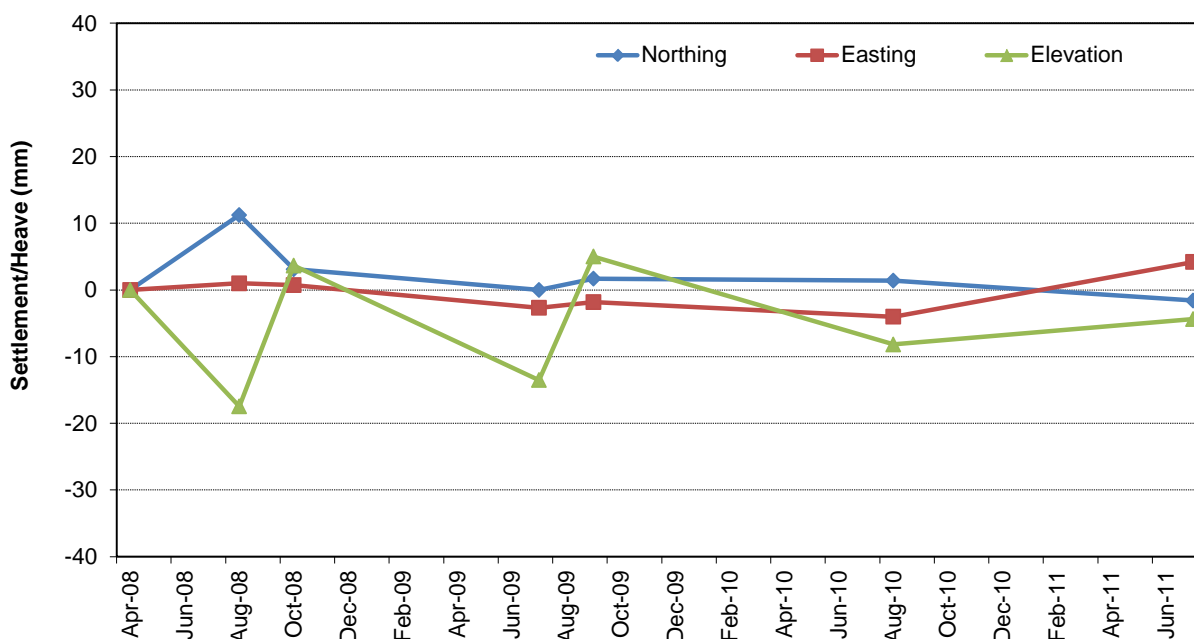


Boston Primary Fuel Tank Farm Settlement Monitoring

Tank #2

Date	Tank Mark	Horizontal Angle			Vertical Angle			Slope Dist.	HI [m]	Northing [m]	Easting [m]	Elevation [m]	Difference from Previous Survey [m]		
		Deg	Min	Sec	Deg	Min	Sec						N	E	EI
22-Apr-08	2A	188	32	48	91	42	56	17.357	1.593	5327.678	1315.749	80.877			
8-Aug-08	2A	188	30	39	91	31	5	17.357	1.519	5327.689	1315.747	80.863	0.011	-0.002	-0.014
18-Oct-08	2A	188	30	44	92	1	58	17.369	1.674	5327.691	1315.754	80.862	0.002	0.007	-0.001
25-Jul-09	2A	188	30	41	91	55	2	17.365	1.633	5327.690	1315.752	80.856	-0.001	-0.003	-0.006
19-Sep-09	2A	188	30	32	91	55	46	17.369	1.635	5327.692	1315.755	80.854	0.002	0.003	-0.002
2-Aug-10	2A	188	29	57	91	32	0	17.365	1.506	5327.695	1315.754	80.845	0.003	-0.001	-0.009
03-Jul-11	2A	188	33	14	91	12	31	17.379	1.416	5327.684	1315.775	80.853	-0.010	0.021	0.008
22-Apr-08	2C	66	46	17	93	28	22	8.891	1.669	5326.866	1318.217	81.190			
8-Aug-08	2C	66	49	58	92	18	25	8.890	1.471	5326.878	1318.219	81.173	0.012	0.002	-0.017
18-Oct-08	2C	66	51	15	93	13	45	8.903	1.625	5326.885	1318.217	81.183	0.007	-0.002	0.010
25-Jul-09	2C	66	51	14	93	4	54	8.903	1.592	5326.886	1318.216	81.173	0.001	-0.001	-0.010
19-Sep-09	2C	66	51	2	93	15	9	8.907	1.622	5326.887	1318.214	81.177	0.002	-0.002	0.003
2-Aug-10	2C	66	50	58	92	42	58	8.906	1.532	5326.889	1318.212	81.170	0.002	-0.002	-0.007
03-Jul-11	2C	66	50	6	91	50	37	8.905	1.380	5326.891	1318.207	81.154	0.002	-0.005	-0.016
22-Apr-08	2D	284	9	33	90	41	36	22.748	1.669	5329.353	1318.048	81.114			
8-Aug-08	2D	284	9	30	90	25	53	22.736	1.544	5329.363	1318.052	81.093	0.010	0.003	-0.021
18-Oct-08	2D	284	9	59	90	37	33	22.737	1.623	5329.364	1318.048	81.095	0.001	-0.003	0.002
25-Jul-09	2D	284	10	37	90	30	59	22.738	1.555	5329.364	1318.044	81.070	0.000	-0.004	-0.025
19-Sep-09	2D	284	11	40	90	24	42	22.738	1.527	5329.365	1318.037	81.084	0.002	-0.007	0.014
2-Aug-10	2D	284	12	51	90	23	29	22.741	1.510	5329.364	1318.029	81.075	-0.001	-0.008	-0.009
03-Jul-11	2D	284	13	33	90	1	32	22.738	1.360	5329.368	1318.025	81.070	0.004	-0.004	-0.005

TANK AVERAGES BY DATE (mm)	22-Apr-08	0.0	0.0	0.0
	8-Aug-08	11.2	1.0	-17.5
	18-Oct-08	3.1	0.7	3.6
	25-Jul-09	0.0	-2.7	-13.5
	19-Sep-09	1.7	-1.8	5.0
	2-Aug-10	1.4	-4.0	-8.2
	3-Jul-11	-1.6	4.2	-4.4
OVERALL PERIOD AVERAGE (mm)		2.6	-0.4	-5.8

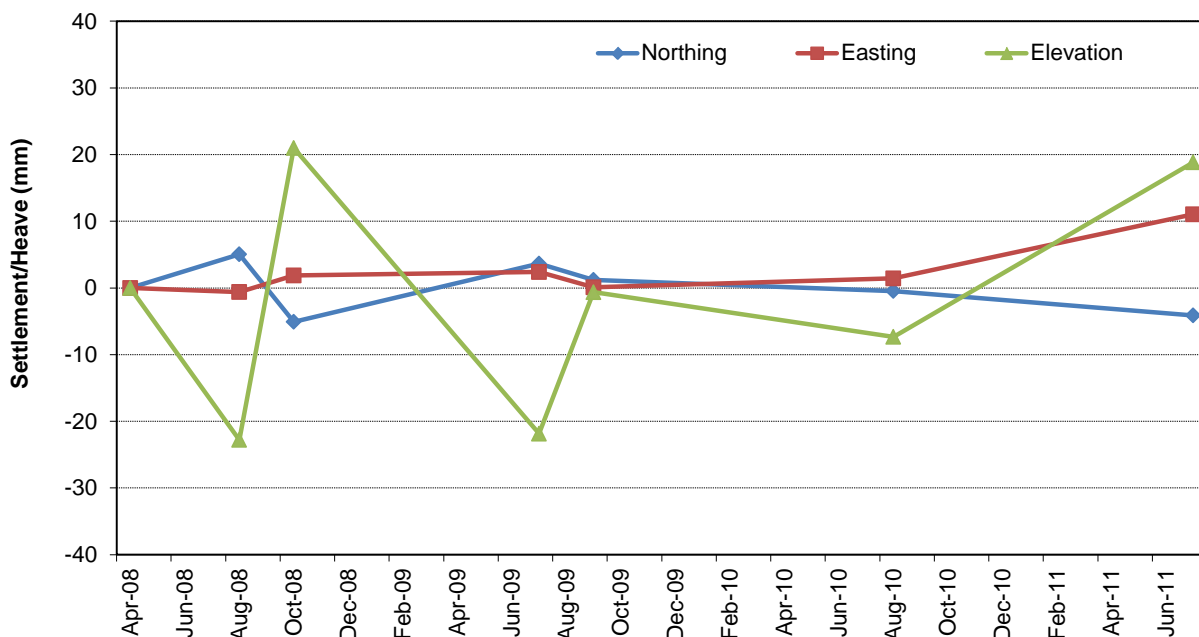


Boston Primary Fuel Tank Farm Settlement Monitoring

Tank #3

Date	Tank Mark	Horizontal Angle			Vertical Angle			Slope Dist.	HI [m]	Northing [m]	Easting [m]	Elevation [m]	Difference from Previous Survey [m]		
		Deg	Min	Sec	Deg	Min	Sec						N	E	EI
22-Apr-08	3A	155	31	38	91	35	38	12.238	1.593	5331.618	1306.850	81.057			
8-Aug-08	3A	155	29	54	91	20	3	12.240	1.519	5331.624	1306.847	81.038	0.006	-0.003	-0.019
18-Oct-08	3A	155	31	55	91	58	52	12.245	1.674	5331.621	1306.853	81.055	-0.004	0.006	0.017
25-Jul-09	3A	155	31	45	91	51	50	12.248	1.633	5331.624	1306.855	81.039	0.003	0.002	-0.016
19-Sep-09	3A	155	32	4	91	52	38	12.252	1.635	5331.627	1306.858	81.038	0.002	0.003	-0.001
2-Aug-10	3A	155	32	17	91	17	55	12.249	1.506	5331.627	1306.859	81.032	0.000	0.001	-0.005
03-Jul-11	3A	155	40	17	90	46	7	12.254	1.416	5331.615	1306.886	81.056	-0.012	0.027	0.023
22-Apr-08	3B	80	36	8	92	41	45	12.708	1.632	5331.612	1309.744	81.062			
8-Aug-08	3B	80	36	38	91	53	10	12.706	1.436	5331.618	1309.743	81.046	0.005	-0.001	-0.016
18-Oct-08	3B	80	35	55	92	35	15	12.708	1.610	5331.613	1309.743	81.064	-0.005	0.000	0.018
25-Jul-09	3B	80	37	13	92	40	40	12.710	1.610	5331.616	1309.747	81.044	0.003	0.004	-0.020
19-Sep-09	3B	80	36	53	92	44	55	12.713	1.626	5331.618	1309.744	81.044	0.001	-0.002	0.000
2-Aug-10	3B	80	36	42	92	9	22	12.704	1.484	5331.614	1309.745	81.034	-0.003	0.001	-0.010
03-Jul-11	3B	80	37	15	91	30	35	12.693	1.350	5331.610	1309.750	81.044	-0.005	0.005	0.010
22-Apr-08	3F	297	17	27	91	16	38	17.426	1.635	5335.467	1307.263	81.090			
8-Aug-08	3F	297	16	52	91	11	23	17.423	1.575	5335.470	1307.265	81.056	0.003	0.002	-0.033
18-Oct-08	3F	297	17	24	91	18	7	17.430	1.637	5335.464	1307.265	81.084	-0.007	0.000	0.028
25-Jul-09	3F	297	16	48	91	2	50	17.425	1.530	5335.468	1307.267	81.055	0.004	0.002	-0.029
19-Sep-09	3F	297	16	57	91	23	10	17.427	1.632	5335.468	1307.266	81.053	0.000	-0.001	-0.001
2-Aug-10	3F	297	16	23	91	5	19	17.424	1.535	5335.470	1307.268	81.047	0.002	0.002	-0.006
03-Jul-11	3F	297	15	52	90	58	40	17.420	1.525	5335.474	1307.269	81.071	0.004	0.001	0.024

TANK AVERAGES BY DATE (mm)	22-Apr-08	0.0	0.0	0.0
	8-Aug-08	5.1	-0.6	-22.8
	18-Oct-08	-5.1	1.9	21.0
	25-Jul-09	3.7	2.4	-21.9
	19-Sep-09	1.2	0.1	-0.6
	2-Aug-10	-0.5	1.4	-7.3
OVERALL PERIOD AVERAGE (mm)		0.0	2.7	-2.1

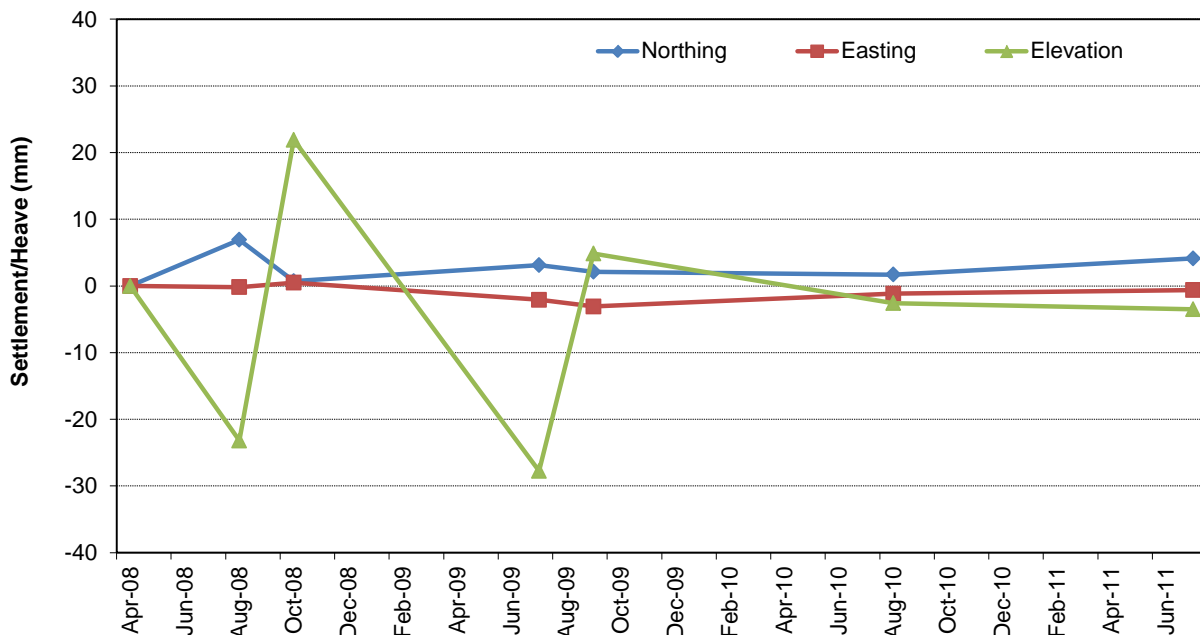


Boston Primary Fuel Tank Farm Settlement Monitoring

Tank #4

Date	Tank Mark	Horizontal Angle			Vertical Angle			Slope Dist.	HI [m]	Northing [m]	Easting [m]	Elevation [m]	Difference from Previous Survey [m]		
		Deg	Min	Sec	Deg	Min	Sec						N	E	EI
22-Apr-08	4C	79	49	37	92	45	46	12.465	1.669	5331.166	1318.159	81.128			
8-Aug-08	4C	79	50	23	91	56	16	12.462	1.471	5331.171	1318.159	81.110	0.005	0.000	-0.019
18-Oct-08	4C	79	51	33	92	32	3	12.471	1.625	5331.177	1318.161	81.134	0.005	0.002	0.024
25-Jul-09	4C	79	51	5	92	28	57	12.473	1.592	5331.178	1318.158	81.112	0.001	-0.003	-0.022
19-Sep-09	4C	79	51	1	92	36	19	12.478	1.622	5331.181	1318.156	81.115	0.003	-0.002	0.003
2-Aug-10	4C	79	50	58	92	12	5	12.474	1.532	5331.181	1318.156	81.113	0.000	0.000	-0.002
03-Jul-11	4C	79	51	1	91	33	38	12.472	1.380	5331.183	1318.155	81.100	0.002	-0.001	-0.013
22-Apr-08	4D	290	20	35	90	57	25	17.796	1.669	5334.739	1317.563	81.092			
8-Aug-08	4D	290	20	54	90	36	59	17.789	1.544	5334.744	1317.564	81.073	0.006	0.001	-0.019
18-Oct-08	4D	290	20	51	90	49	8	17.792	1.623	5334.742	1317.563	81.089	-0.002	-0.001	0.016
25-Jul-09	4D	290	21	32	90	42	58	17.791	1.555	5334.744	1317.560	81.053	0.002	-0.003	-0.036
19-Sep-09	4D	290	22	47	90	35	22	17.795	1.527	5334.742	1317.552	81.064	-0.002	-0.008	0.011
2-Aug-10	4D	290	23	44	90	32	36	17.796	1.510	5334.743	1317.547	81.061	0.001	-0.005	-0.003
03-Jul-11	4D	290	24	7	90	3	28	17.793	1.360	5334.746	1317.546	81.062	0.003	-0.001	0.001
22-Apr-08	4E	298	41	4	91	11	45	18.548	1.670	5334.220	1314.710	81.128			
8-Aug-08	4E	298	40	52	91	1	34	18.537	1.583	5334.230	1314.708	81.096	0.010	-0.001	-0.032
18-Oct-08	4E	298	40	53	91	9	14	18.539	1.650	5334.229	1314.709	81.122	-0.001	0.000	0.026
25-Jul-09	4E	298	40	41	91	0	14	18.532	1.576	5334.235	1314.708	81.096	0.006	0.000	-0.025
19-Sep-09	4E	298	40	23	91	6	42	18.528	1.611	5334.240	1314.709	81.097	0.005	0.000	0.000
2-Aug-10	4E	298	39	54	90	58	23	18.523	1.563	5334.245	1314.710	81.093	0.005	0.001	-0.003
03-Jul-11	4E	298	39	31	90	45	45	18.515	1.496	5334.252	1314.710	81.095	0.007	0.000	0.001

TANK AVERAGES BY DATE (mm)	22-Apr-08	0.0	0.0	0.0
	8-Aug-08	6.9	-0.2	-23.2
	18-Oct-08	0.7	0.5	21.9
	25-Jul-09	3.1	-2.1	-27.8
	19-Sep-09	2.1	-3.1	4.9
	2-Aug-10	1.7	-1.2	-2.6
	3-Jul-11	4.1	-0.6	-3.5
OVERALL PERIOD AVERAGE (mm)		3.1	-1.1	-5.0

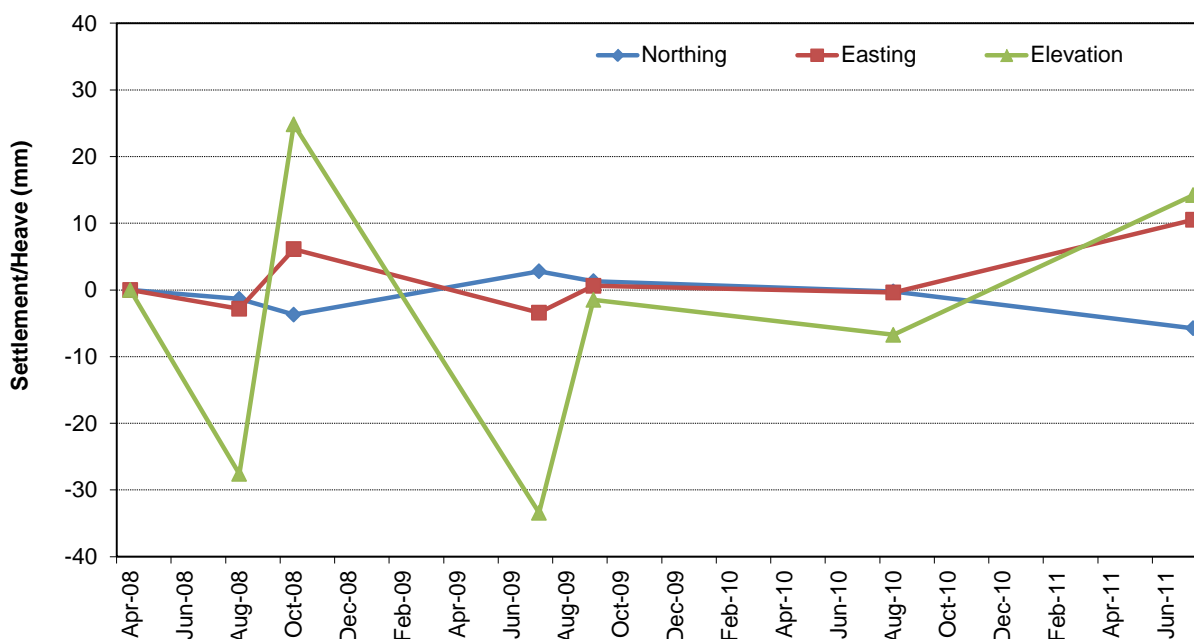


Boston Primary Fuel Tank Farm Settlement Monitoring

Tank #5

Date	Tank Mark	Horizontal Angle			Vertical Angle			Slope Dist.	HI [m]	Northing [m]	Easting [m]	Elevation [m]	Difference from Previous Survey [m]		
		Deg	Min	Sec	Deg	Min	Sec						N	E	EI
22-Apr-08	5A	146	6	15	91	38	18	17.511	1.593	5337.355	1307.654	80.896			
8-Aug-08	5A	146	5	19	91	29	20	17.506	1.519	5337.354	1307.648	80.868	-0.001	-0.006	-0.028
18-Oct-08	5A	146	7	20	91	55	18	17.515	1.674	5337.353	1307.660	80.891	0.000	0.011	0.023
25-Jul-09	5A	146	6	28	91	53	1	17.513	1.633	5337.354	1307.655	80.861	0.001	-0.005	-0.029
19-Sep-09	5A	146	6	54	91	53	58	17.518	1.635	5337.357	1307.659	80.858	0.003	0.004	-0.003
2-Aug-10	5A	146	6	43	91	29	39	17.515	1.506	5337.358	1307.659	80.853	0.001	-0.001	-0.005
03-Jul-11	5A	146	12	6	91	8	9	17.515	1.416	5337.347	1307.684	80.873	-0.011	0.025	0.020
22-Apr-08	5B	92	56	58	91	53	35	17.712	1.632	5337.490	1310.713	81.075			
8-Aug-08	5B	92	56	21	91	20	1	17.706	1.436	5337.487	1310.710	81.052	-0.002	-0.003	-0.023
18-Oct-08	5B	92	56	43	91	50	16	17.704	1.610	5337.482	1310.714	81.070	-0.005	0.004	0.018
25-Jul-09	5B	92	56	27	91	55	26	17.709	1.610	5337.486	1310.711	81.043	0.004	-0.003	-0.027
19-Sep-09	5B	92	56	12	91	58	29	17.712	1.626	5337.488	1310.709	81.044	0.002	-0.002	0.000
2-Aug-10	5B	92	55	46	91	32	51	17.705	1.484	5337.484	1310.708	81.034	-0.003	-0.001	-0.010
03-Jul-11	5B	92	56	9	91	5	10	17.698	1.350	5337.481	1310.711	81.043	-0.003	0.003	0.009
22-Apr-08	5F	286	10	48	91	45	54	12.624	1.635	5341.035	1307.826	81.089			
8-Aug-08	5F	286	10	54	91	38	10	12.624	1.575	5341.034	1307.826	81.058	-0.001	0.000	-0.032
18-Oct-08	5F	286	10	54	91	45	51	12.631	1.637	5341.029	1307.830	81.091	-0.005	0.003	0.034
25-Jul-09	5F	286	11	1	91	28	48	12.624	1.530	5341.033	1307.826	81.047	0.004	-0.003	-0.044
19-Sep-09	5F	286	11	17	91	57	1	12.628	1.632	5341.032	1307.826	81.045	-0.001	0.000	-0.002
2-Aug-10	5F	286	10	55	91	32	5	12.624	1.535	5341.033	1307.827	81.040	0.002	0.001	-0.005
03-Jul-11	5F	286	10	40	91	25	23	12.628	1.525	5341.030	1307.830	81.054	-0.003	0.003	0.014

TANK AVERAGES BY DATE (mm)	22-Apr-08	0.0	0.0	0.0
	8-Aug-08	-1.3	-2.8	-27.6
	18-Oct-08	-3.7	6.1	24.8
	25-Jul-09	2.8	-3.4	-33.4
	19-Sep-09	1.3	0.6	-1.5
	2-Aug-10	-0.2	-0.4	-6.7
OVERALL PERIOD AVERAGE (mm)		-1.2	1.8	-5.0

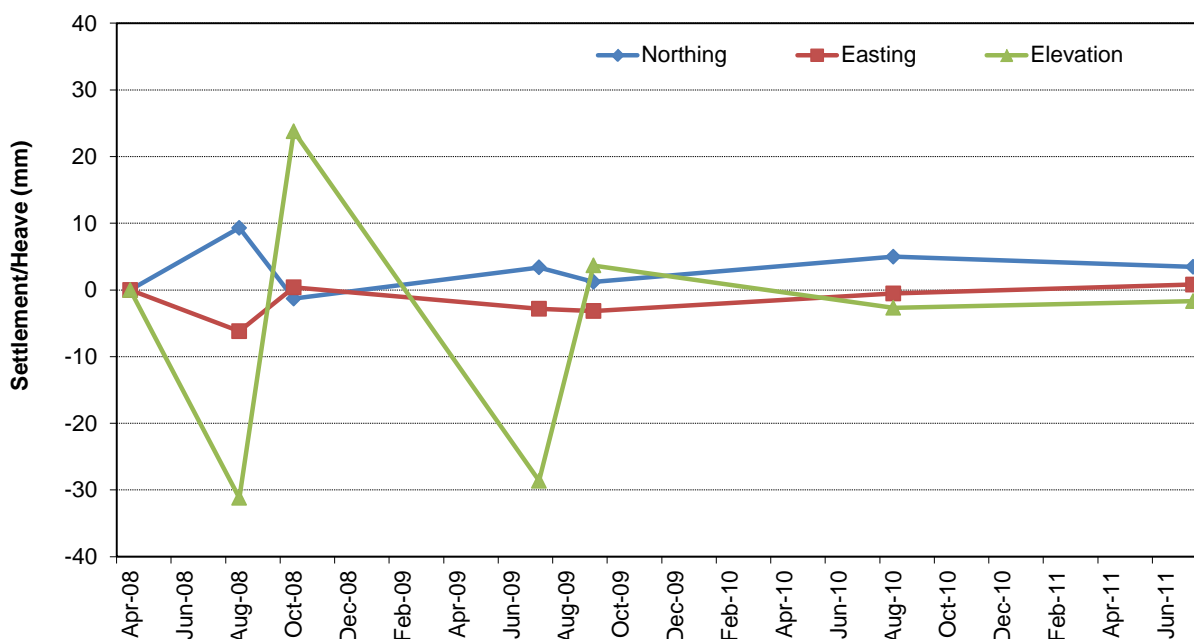


Boston Primary Fuel Tank Farm Settlement Monitoring

Tank #6

Date	Tank Mark	Horizontal Angle			Vertical Angle			Slope Dist.	HI [m]	Northing [m]	Easting [m]	Elevation [m]	Difference from Previous Survey [m]		
		Deg	Min	Sec	Deg	Min	Sec						N	E	EI
22-Apr-08	6C	86	44	44	92	19	47	18.155	1.669	5337.092	1317.422	80.991			
8-Aug-08	6C	86	44	29	91	47	9	18.157	1.471	5337.099	1317.418	80.965	0.007	-0.004	-0.026
18-Oct-08	6C	86	45	2	92	11	48	18.167	1.625	5337.105	1317.418	80.989	0.006	0.001	0.024
25-Jul-09	6C	86	44	30	92	9	45	18.167	1.592	5337.105	1317.416	80.966	-0.001	-0.003	-0.022
19-Sep-09	6C	86	44	18	92	14	48	18.171	1.622	5337.107	1317.413	80.970	0.002	-0.002	0.003
2-Aug-10	6C	86	44	17	91	58	6	18.169	1.532	5337.108	1317.413	80.968	0.001	-0.001	-0.002
03-Jul-11	6C	86	44	26	91	31	27	18.166	1.380	5337.110	1317.413	80.957	0.001	0.000	-0.011
22-Apr-08	6D	301	21	11	91	39	4	12.434	1.669	5340.813	1317.436	81.031			
8-Aug-08	6D	301	23	36	91	11	17	12.430	1.544	5340.819	1317.429	81.006	0.006	-0.007	-0.024
18-Oct-08	6D	301	23	7	91	27	28	12.434	1.623	5340.816	1317.430	81.027	-0.003	0.000	0.020
25-Jul-09	6D	301	24	12	91	18	28	12.434	1.555	5340.818	1317.426	80.991	0.001	-0.004	-0.035
19-Sep-09	6D	301	26	5	91	8	24	12.438	1.527	5340.817	1317.417	81.000	0.000	-0.008	0.008
20-Aug-10	6D	301	27	8	91	4	52	12.440	1.510	5340.818	1317.413	80.995	0.000	-0.004	-0.004
03-Jul-11	6D	301	27	19	90	23	4	12.436	1.360	5340.820	1317.414	80.997	0.002	0.001	0.001
22-Apr-08	6E	294	8	42	92	4	22	12.560	1.670	5340.311	1314.183	81.061			
8-Aug-08	6E	294	9	24	91	52	33	12.542	1.583	5340.325	1314.175	81.017	0.015	-0.008	-0.043
18-Oct-08	6E	294	9	53	92	3	19	12.550	1.650	5340.318	1314.176	81.045	-0.007	0.000	0.027
25-Jul-09	6E	294	9	35	91	50	52	12.539	1.576	5340.328	1314.174	81.017	0.009	-0.002	-0.028
19-Sep-09	6E	294	9	13	92	0	36	12.539	1.611	5340.329	1314.174	81.016	0.002	0.001	0.000
2-Aug-10	6E	294	8	34	91	48	31	12.529	1.563	5340.338	1314.174	81.013	0.009	-0.001	-0.004
03-Jul-11	6E	294	7	33	91	28	51	12.521	1.496	5340.345	1314.176	81.017	0.007	0.002	0.005

TANK AVERAGES BY DATE (mm)	22-Apr-08	0.0	0.0	0.0
	8-Aug-08	9.3	-6.2	-31.2
	18-Oct-08	-1.3	0.4	23.8
	25-Jul-09	3.4	-2.8	-28.6
	19-Sep-09	1.2	-3.2	3.7
	2-Aug-10	5.0	-0.5	-2.7
OVERALL PERIOD AVERAGE (mm)		3.5	-1.9	-6.1

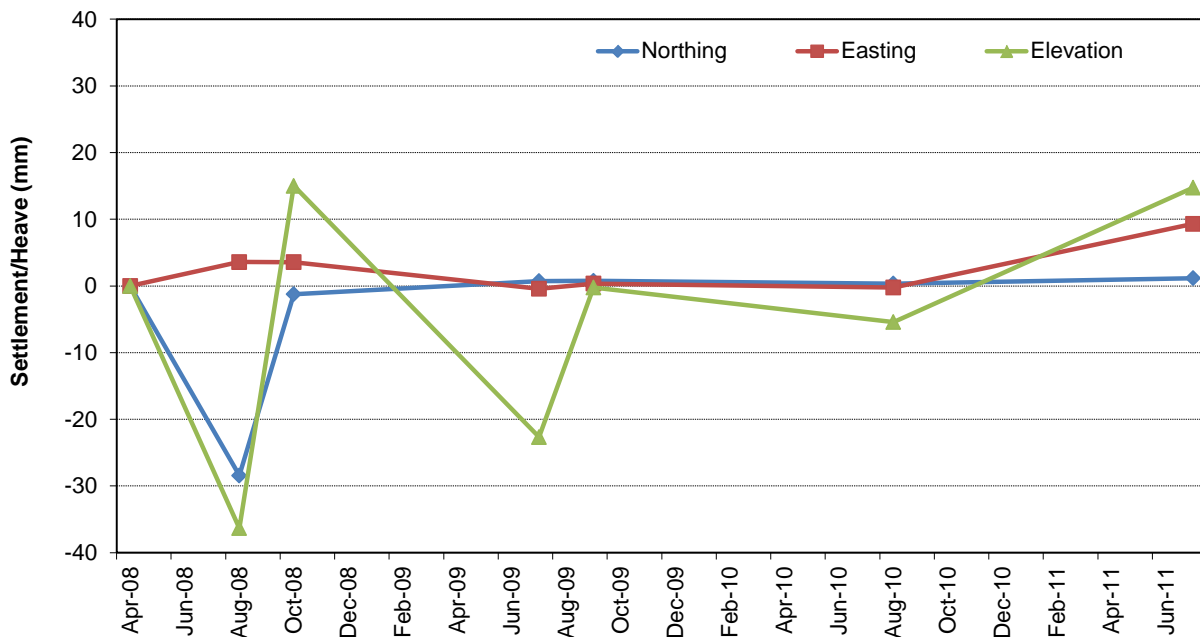


Boston Primary Fuel Tank Farm Settlement Monitoring

Tank #7

Date	Tank Mark	Horizontal Angle			Vertical Angle			Slope Dist.	HI [m]	Northing [m]	Easting [m]	Elevation [m]	Difference from Previous Survey [m]		
		Deg	Min	Sec	Deg	Min	Sec						N	E	EI
22-Apr-08	7A	139	42	34	91	19	5	22.702	1.593	5343.001	1307.814	80.875			
8-Aug-08	7A	139	41	54	91	13	37	22.699	1.519	5343.000	1307.809	80.837	0.000	-0.005	-0.038
18-Oct-08	7A	139	42	48	91	35	4	22.706	1.674	5343.001	1307.816	80.850	0.001	0.007	0.013
25-Jul-09	7A	139	42	40	91	31	45	22.705	1.633	5343.001	1307.815	80.831	0.000	-0.001	-0.019
19-Sep-09	7A	139	43	2	91	32	18	22.708	1.635	5343.003	1307.818	80.829	0.002	0.003	-0.002
2-Aug-10	7A	139	42	56	91	13	10	22.706	1.506	5343.004	1307.818	80.827	0.001	0.000	-0.003
03-Jul-11	7A	139	46	55	90	56	11	22.709	1.416	5342.999	1307.845	80.849	-0.005	0.026	0.022
22-Apr-08	7B	97	41	28	91	36	36	23.321	1.632	5343.343	1310.862	81.005			
8-Aug-08	7B	97	41	3	91	12	7	23.230	1.436	5343.258	1310.879	80.977	-0.085	0.017	-0.028
18-Oct-08	7B	97	41	12	91	36	11	23.232	1.610	5343.256	1310.881	80.988	-0.002	0.001	0.011
25-Jul-09	7B	97	41	14	91	39	3	23.232	1.610	5343.256	1310.881	80.969	0.000	0.000	-0.019
19-Sep-09	7B	97	41	3	91	41	23	23.234	1.626	5343.257	1310.879	80.969	0.001	-0.002	0.000
2-Aug-10	7B	97	40	48	91	21	28	23.229	1.484	5343.255	1310.878	80.962	-0.002	-0.001	-0.007
03-Jul-11	7B	97	41	8	91	0	2	23.228	1.350	5343.258	1310.880	80.972	0.002	0.002	0.011
22-Apr-08	7F	267	27	43	92	53	46	8.278	1.635	5346.505	1307.626	81.060			
8-Aug-08	7F	267	27	54	92	46	47	8.276	1.575	5346.505	1307.624	81.017	0.000	-0.001	-0.043
18-Oct-08	7F	267	28	14	93	3	56	8.282	1.637	5346.502	1307.627	81.037	-0.003	0.002	0.020
25-Jul-09	7F	267	27	32	92	31	52	8.276	1.530	5346.505	1307.626	81.008	0.003	-0.001	-0.030
19-Sep-09	7F	267	27	57	93	13	50	8.281	1.632	5346.504	1307.626	81.008	-0.001	-0.001	0.001
2-Aug-10	7F	267	27	12	92	36	15	8.276	1.535	5346.506	1307.626	81.002	0.002	0.001	-0.006
03-Jul-11	7F	267	25	19	92	27	30	8.271	1.525	5346.512	1307.626	81.013	0.006	0.000	0.011

TANK AVERAGES BY DATE (mm)	22-Apr-08	0.0	0.0	0.0
	8-Aug-08	-28.4	3.6	-36.3
	18-Oct-08	-1.3	3.6	15.0
	25-Jul-09	0.7	-0.4	-22.7
	19-Sep-09	0.8	0.4	-0.2
	2-Aug-10	0.4	-0.2	-5.4
	3-Jul-11	1.2	9.3	14.7
OVERALL PERIOD AVERAGE (mm)		-4.4	2.7	-5.8



Boston Primary Fuel Tank Farm Settlement Monitoring

Tank #8

Date	Tank Mark	Horizontal Angle			Vertical Angle			Slope Dist.	HI [m]	Northing [m]	Easting [m]	Elevation [m]	Difference from Previous Survey [m]		
		Deg	Min	Sec	Deg	Min	Sec						N	E	EI
22-Apr-08	8C	91	52	15	91	53	25	23.449	1.669	5342.700	1317.450	80.956			
8-Aug-08	8C	91	52	27	91	27	51	23.453	1.471	5342.709	1317.449	80.932	0.009	-0.001	-0.024
18-Oct-08	8C	91	52	47	91	44	54	23.460	1.625	5342.713	1317.450	80.969	0.004	0.001	0.038
25-Jul-09	8C	91	52	11	91	44	54	23.460	1.592	5342.712	1317.446	80.936	-0.001	-0.004	-0.033
19-Sep-09	8C	91	52	1	91	49	2	23.464	1.622	5342.715	1317.444	80.938	0.003	-0.002	0.002
2-Aug-10	8C	91	51	51	91	36	4	23.462	1.532	5342.715	1317.443	80.936	0.000	-0.001	-0.001
03-Jul-11	8C	91	51	39	91	15	5	23.465	1.380	5342.721	1317.439	80.928	0.006	-0.003	-0.009
22-Apr-08	8D	318	8	27	92	56	10	8.342	1.669	5345.860	1317.826	80.962			
8-Aug-08	8D	318	11	46	92	12	54	8.340	1.544	5345.864	1317.819	80.942	0.004	-0.007	-0.020
18-Oct-08	8D	318	11	50	92	33	48	8.341	1.623	5345.865	1317.820	80.970	0.001	0.001	0.028
25-Jul-09	8D	318	12	39	92	22	34	8.342	1.555	5345.865	1317.817	80.929	0.000	-0.003	-0.041
19-Sep-09	8D	318	14	50	92	8	19	8.347	1.527	5345.865	1317.808	80.936	0.000	-0.008	0.006
2-Aug-10	8D	318	15	55	92	2	57	8.350	1.510	5345.865	1317.804	80.931	0.000	-0.004	-0.004
03-Jul-11	8D	318	18	11	91	1	8	8.342	1.360	5345.872	1317.804	80.932	0.007	-0.001	0.000
22-Apr-08	8E	282	47	41	93	37	20	7.635	1.670	5345.604	1313.962	81.033			
8-Aug-08	8E	282	46	58	93	16	40	7.615	1.583	5345.619	1313.954	80.993	0.016	-0.007	-0.040
18-Oct-08	8E	282	47	20	93	29	56	7.621	1.650	5345.615	1313.956	81.030	-0.004	0.001	0.037
25-Jul-09	8E	282	46	37	93	12	50	7.612	1.576	5345.622	1313.954	80.994	0.007	-0.002	-0.036
19-Sep-09	8E	282	46	11	93	29	15	7.613	1.611	5345.623	1313.954	80.993	0.001	0.000	-0.001
2-Aug-10	8E	282	44	37	93	10	6	7.603	1.563	5345.632	1313.953	80.988	0.008	-0.001	-0.005
03-Jul-11	8E	282	42	57	92	39	13	7.591	1.496	5345.641	1313.952	80.990	0.009	-0.001	0.002

TANK AVERAGES BY DATE (mm)	22-Apr-08	0.0	0.0	0.0
	8-Aug-08	9.7	-5.3	-28.0
	18-Oct-08	0.3	1.1	34.4
	25-Jul-09	1.9	-3.0	-36.5
	19-Sep-09	1.3	-3.3	2.2
	2-Aug-10	2.8	-2.1	-3.6
OVERALL PERIOD AVERAGE (mm)		3.9	-2.4	-5.6

