

October 24, 2008
3.393 – GO/01

Mr. Stephen Hartman / Mr. Luis Manzo / Mr. Jackson Lindell
Kivalliq Inuit Association
P.O Box 340
Rankin Inlet, N.T.
X0C 0G0

Dear Stephen,

Comaplex is in the process of responding to reviewer's comments on the proposed fuel berm on the Meliadine West project. We have observed your concerns that were forwarded to the NWB regarding possible ARD issues with the waste rock and your request for additional ARD testing and information. This letter is to provide you with the additional information and to provide further details on the construction of the berm, which we hope will alleviate these concerns.

As discussed in your office in the August, Comaplex has completed extensive ARD testing of the waste rock from both the portal area and of rock excavated from the decline and exploration drifts. Most of this data was presented in the January 26, 2006 memo by K. Sexsmith of SRK Consulting (you have this report). In addition to these samples and this report, Comaplex has the results of additional sampling of the till/overburden in the immediate area of the portal (data attached). Furthermore, as part of our advancement of the project towards feasibility, we are in the process of a feasibility level waste rock characterization by Golder (Ottawa), where an additional 80 samples of waste rock have been collected this past month. Results and analysis from these samples will not be available for at least 4-5 months.

Sexsmith Memo:

Please note the density of ARD sampling completed to date as shown in the attached figure 'ARD Samples – Cross Section'. There have been 90 samples taken directly in the area of the decline and below it. In addition to this, six more samples of till and overburden were also taken (not in the Sexsmith memo). These samples are shown on the 'Overburden ARD Sample Locations' map attached. While no samples were taken of the esker/till in the area of the proposed berm, the till can be considered to be identical to the tested areas.

As stated in the Sexsmith memo, AP/NP ratios of 3 or less "are typically used as an indication that samples could have potential for acid generation, while samples with NP/AP ratios of less than 1 are considered likely to be acid generating" (p. 4, section 3, Sexsmith memo). Of the 90 samples taken, plus the additional six overburden samples, 2 samples had NP/AP ratios of <1. Both these samples were of sediments taken in the ore zone, immediately adjacent to the 1000 lode at depth. An additional 4 samples of the sediments and 13 samples of mineralized rock and iron formation had NP/AP ratios of 1-3. None of the 25 samples denoted GT, which were samples of waste rock from geo-technical holes recently drilled specifically for the decline are potentially acid generating. Iron formation and mineralized rock is not going to be used for the berm construction and is presently segregated on the waste pad on neutralizing piles of waste rock behind secondary containment.

As noted in the Sexsmith memo (p. 10, conclusions), "a few samples from the hanging wall of the deposit were classified as acid generating or potentially acid generating. However, they contain significant amounts of neutralizing potential. Provided these isolated intervals of material are well distributed in the waste dump, ARD is unlikely to occur." We concur with her findings that the 4 samples are very isolated in occurrence and will be easily buffered in overwhelmingly neutralizing waste rock and till/overburden (offsets or neutralizes any small pockets of sulphide bearing rock). See the following averages for each rock type:

Sediments (43 samples) NP/AP = 11.8
Mineralized (8 samples) NP/AP = 3.5
Gabbro (4 samples) NP/AP = 44.8
Mafic Volcanics (15 samples) NP/AP = 27.4
Iron Formation (13 samples) NP/AP = 2.2
Overburden (7 samples) NP / AP = 21.5

Berm Construction

As noted above, Comaplex segregated out all iron formation and mineralized rock as it comes out of the decline. None of this material will be used in the berm construction. We have already crushed a pile of the waste rock (seds/gabbros) and crushed a pile of the till/overburden (limited amount of material that was overlying the portal) for the berm construction. The plan is to build the base of the berm with predominantly the overburden/till as it makes an excellent base, but hosts some clay which is too tacky for inside the berm. We then lay down the three layers of liner and geo-textile. The crushed waste rock is then laid on top of the geo-textile to protect it. As such, the waste rock is basically contained within liner. The neutralizing capacity of the till/overburden is very high, so any waste rock that may be used in the base will be further buffered in the process. We believe this plan is environmentally prudent and sound.

As you are aware, we have been patiently waiting for the 30 day review process and have almost run out of time to build the berm this fall. It would be greatly appreciated if you could respond to this letter as quickly as possible.

Yours truly,

A handwritten signature in black ink, appearing to read 'Mark Balog', with a long horizontal line extending to the right.

Mark Balog
Comaplex Minerals Corp.

cc. Phyllis Beaulieu
David Hohnstein

ARD Sampling Results Summary

HOLE ID	From	To	Width	Strat	Litho	ZONE	Sample	Tag	NetNP	NP / AP
GT05-10	6.00	11.00	5.00	K	Kwa-s	SEDS	ARD-GT10-1A	415055	29.1	6.48
GT05-10	11.00	16.00	5.00	K	Ks-wa	SEDS	ARD-GT10-2A	415061	26.6	7.09
GT05-10	16.00	21.00	5.00	K	Kwa	SEDS	ARD-GT10-3A	415067	33.2	6.90
GT05-11	11.00	16.00	5.00	K	Kwa	SEDS	ARD-GT11-1A	415073	39.8	11.60
GT05-11	16.00	21.00	5.00	K	Kwa-qv	SEDS	ARD-GT11-2A	415079	57.7	19.46
GT05-11	21.00	26.00	5.00	K	Kwa-s	SEDS	ARD-GT11-3A	415085	41.3	9.26
GT05-2	10.40	15.40	5.00	K	Kwa-s	SEDS	ARD-GT2-1A	415091	38.9	9.90
GT05-2	15.40	20.40	5.00	K	Kwa-s	SEDS	ARD-GT2-2A	415097	20.5	3.05
GT05-4	13.45	18.45	5.00	K	Kwa'ser	SEDS	ARD-GT4-1A	415401	34.5	6.51
GT05-4	18.45	23.45	5.00	K	Kwa'ser	SEDS	ARD-GT4-2A	415407	39.1	8.82
GT05-4	23.45	28.45	5.00	K	Ks	SEDS	ARD-GT4-3A	415413	33.8	7.76
GT05-5	14.00	19.00	5.00	K	Kwa-s	SEDS	ARD-GT5-1A	415419	54.80	11.96
GT05-5	19.00	24.00	5.00	K	Kwa-s	SEDS	ARD-GT5-2A	415425	47.65	13.71
GT05-5	24.00	29.00	5.00	K	Kwa'ser	SEDS	ARD-GT5-3A	415431	56.18	10.99
GT05-6	6.00	11.00	5.00	K	Kwa	SEDS	ARD-GT6-1A	415437	38.0	8.60
GT05-6	11.00	16.00	5.00	K	Kwa	SEDS	ARD-GT6-2A	415443	46.2	5.00
GT05-6	16.00	21.00	5.00	K	Kwa'ser	SEDS	ARD-GT6-3A	415449	48.1	6.13
GT05-7	4.80	8.10	3.30	K	Ks-wa	SEDS	ARD-GT7-1A	415455	35.1	17.05
GT05-7	8.65	13.35	4.70	K	Ks-wa	SEDS	ARD-GT7-2A	415459	37.2	10.17
GT05-7	13.35	18.35	5.00	K	Kwa'ser	SEDS	ARD-GT7-3A	415464	50.7	7.49
GT05-8	6.10	11.10	5.00	K	Ks	SEDS	ARD-GT8-1A	415470	39.3	9.99
GT05-8	11.10	16.10	5.00	K	Kwa	SEDS	ARD-GT8-2A	415476	42.9	10.81
GT05-8	16.10	21.10	5.00	K	Kwa	SEDS	ARD-GT8-3A	415482	48.2	6.50
GT05-9	13.97	18.97	5.00	K	Kwa-qv	SEDS	ARD-GT9-2A	415494	25.3	5.49
GT05-9	18.97	23.10	4.13	K	Kwa-s	SEDS	ARD-GT9-3A	415500	26.0	6.20
M03-497	29.35	35.55	6.20	K	Ks	SEDS	ARD-M03-497-2A	451379	18.8	1.76
M03-497	35.55	40.55	5.00	K	Kwa	SEDS	ARD-M03-497-3A	451380	88.9	7.77
M03-497	40.55	45.10	4.55	K	Kwa-qv	SEDS	ARD-M03-497-4A	451381	45.9	4.67
M04-518	14.00	15.00	1.00	K	Kwa-s	SEDS	ARD-M04-518-1A	339260	15.18	3.70
M04-518	86.00	87.00	1.00	K	Kwa	SEDS	ARD-M04-518-2A	339264	9.16	1.84
M96-41	300.95	301.20	0.25	K	Kwa-m	SEDS	CR504400		-35.00	0.76
M96-42	231.00	231.98	0.98	K	Kwa-m	SEDS	CR107023		72.30	8.20
M96-43	291.75	292.76	1.01	K	Kwa	SEDS	CR107106		46.30	150.00
M96-52	361.00	362.00	1.00	K	Kwa-m	SEDS	CR300099		43.90	12.60
M97-136	144.00	145.00	1.00	K	Kwa	SEDS	CR805509		38.80	7.60
M97-137	189.46	190.00	0.54	K	Kwa-s	SEDS	CR805652		54.70	22.90
M97-139	57.97	59.08	1.11	K	Kwa-m	SEDS	CR805845		45.10	19.00
M97-140	348.71	349.74	1.03	K	Kwa	SEDS	CR802930		43.90	21.00
M97-91	217.43	218.18	0.75	K	Kwa-qv	SEDS	CR809552		-95.00	0.55
M98-265	88.00	94.00	6.00	K	Kwa	SEDS	ARD-M98-265-1A	451400	44.0	5.27
M98-265	97.00	102.00	5.00	K	Kwa	SEDS	ARD-M98-265-2A	415456	35.2	5.50
M98-265	103.00	108.00	5.00	K	Kwa	SEDS	ARD-M98-265-3A	415462	27.5	6.17
M99-366B	46.32	51.32	5.00	K	Kwa	SEDS	ARD-M99-336B-1A	451382	18.9	2.44
Sediments	Number	43					AVERAGE		35.1	11.8
M96-37	226.00	237.95	11.95	M	QQ	1000	MELMET 2		97.30	3.40
M96-42	265.10	269.23	4.13	M	QQ	1000	MELMET 2		97.30	3.40
M96-64	403.00	407.00	4.00	M	QQ	1000	MELMET 2		97.30	3.40
M97-136	152.20	158.00	5.80	M	QQ	1000	COMP 4		51.00	2.30
M97-137	208.08	218.20	10.12	M	QQ	1000	COMP 5		51.00	2.30
M97-94A	209.00	213.14	4.14	M	QQ	1000	COMP 4		51.00	2.30
M95-27	101.00	141.10	40.10	M	NNj-wa'c	ZONE	MELMET 1		84.30	5.40
M96-39	201.30	240.40	39.10	M	NNj-wa'c	ZONE	MELMET 1		84.30	5.40
Mineralized	Number	8					AVERAGE		76.7	3.5

ARD Sampling Results Summary

HOLE_ID	From	To	Width	Strat	Litho	ZONE	Sample	Tag	NetNP	NP / AP
M99-366B	51.32	56.32	5.00	Mg	Mg'bt	GAB	ARD-M99-336B-2A	451388	82.8	14.24
M99-366B	56.32	61.32	5.00	Mg	Mg'ep	GAB	ARD-M99-336B-3A	451394	53.5	6.19
GT05-2	20.40	25.40	5.00	Mg	Mg	GAB	ARD-GT2-3A	451353	32.6	6.48
GT05-9	8.97	13.97	5.00	Mg	Mg	GAB	ARD-GT9-1A	415488	94.7	152.48
Gabbro		Number	4	AVERAGE					65.9	44.8

M96-43	407.88	408.79	0.91	Mv	MV	MV	CR107210		251.00	22.10
M96-52	381.00	382.00	1.00	Mv	MV	MV	CR504927		216.00	78.20
M96-72	329.17	330.26	1.09	Mv	MV	MV	CR300278		37.00	6.40
M97-136	208.00	209.00	1.00	Mv	MV	MV	CR805601		263.00	23.10
M97-139	139.79	140.79	1.00	Mv	MV	MV	CR806966		261.00	8.40
M97-91	253.42	253.93	0.51	Mv	MV	MV	CR809563		280.00	30.70
M98-196	80.70	85.70	5.00	Mv	Mv	MV	ARD-M98-196-1A	451359	231.9	12.97
M98-196	85.70	90.70	5.00	Mv	Mv	MV	ARD-M98-196-2A	451360	259.8	30.69
M98-197	136.80	141.80	5.00	Mv	Mv	MV	ARD-M98-197-1A	451361	243.7	15.72
M98-197	141.80	146.80	5.00	Mv	Mv	MV	ARD-M98-197-2A	451362	266.6	28.52
M00-471	144.55	151.00	6.45	Mv	Mv'ser'ak	MVak	ARD-M00-471-1A	451365	275.3	23.59
M00-471	151.00	156.00	5.00	Mv	Mv'ser'ak	MVak	ARD-M00-471-2A	451366	235.5	25.31
M00-471	156.00	161.00	5.00	Mv	Mv'ca'c	MVca	ARD-M00-471-3A	451372	224.1	56.17
M00-481	161.52	166.52	5.00	Mv	Mv'ser'ak	MVak	ARD-M00-481-1A	451363	263.1	23.76
M00-481	166.52	171.52	5.00	Mv	Mv'ser'ak	MVak	ARD-M00-481-2A	451364	277.8	25.03
Mafic Volcanics		Number	15	AVERAGE					239.1	27.4

M95-17	87.30	92.00	4.70	N	Nj	1100	MELMET 3		15.10	1.10
M96-37	196.50	203.00	6.50	N	Nj	1100	MELMET 3		15.10	1.10
M96-41	250.00	256.50	6.50	N	Nj	1100	COMP 1		20.33	1.40
M96-43	310.40	315.80	5.40	N	Nj	1100	MELMET 3		15.10	1.10
M96-66	66.30	72.40	6.10	N	Nj	1100	COMP 1		20.33	1.40
M97-136	148.00	152.20	4.20	N	Nj	1100	COMP 2		20.33	1.40
M97-138	142.00	146.00	4.00	N	Nj	1100	COMP 2		20.33	1.40
M97-82	366.82	376.64	9.82	N	Nj	1100	COMP 3		20.33	1.40
M03-497	24.60	27.24	2.64	N	Nimj	IF	ARD-M03-497-1A	451378	42.4	2.25
M96-41	235.00	236.00	1.00	N	Nj	ORE	CR504368		108.00	3.60
M96-72	295.78	296.91	1.13	N	Nj	ORE	CR300264		31.90	5.30
M96-76	248.78	249.93	1.15	N	Nj	ORE	CR301 750		73.10	4.80
M03-497	24.60	27.24	2.64	N	Nimj	IF	ARD-M03-497-1A	451378	42.4	2.25
Iron Formation		Number	13	AVERAGE					34.2	2.2

SampleNum	UTM_N	UTM_E				Description		NetNP	NP/AP
CS500156	6987097	542435	UG	UG	NA	Mud-Boil 1	CS500156	7.2	12.4
CS500184	6989009	540024	UG	UG	NA	Mud-Boil 2	CS500184	10.5	34.8
CS500187	6988742	539467	UG	UG	NA	Mud-Boil 3	CS500187	6.1	19.7
CS500188	6988470	539487	UG	UG	NA	Mud-Boil 4	CS500188	8.3	27.7
CS500189	6988190	539524	UG	UG	NA	Mud-Boil 5	CS500189	5.2	16.8
CS500190	6988264	539991	UG	UG	NA	Mud-Boil 6	CS500190	6.1	19.7
CS500191	6987923	539969	UG	UG	NA	Mud-Boil 7	CS500191	6	19.4
Overburden		Number	7	AVERAGE				7.1	21.5



